Appendix B.12.2

Crawford Overburden Geotechnical Investigation Factual Report Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1

Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1

Prepared for

Canada Nickel Company Inc.



Prepared by

SRK Consulting (Canada) Inc.
CAPR003118
September 2024

Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1

September 2024

Prepared for

Canada Nickel Company Inc.
Suite 1900-130 King St West
Toronto, ON M5X 1E3
Canada

Email.: info@canadanickel.com
Web: www.canadanickel.com

Prepared by

SRK Consulting (Canada) Inc.
320 Granville Street, Suite 2600
Vancouver, BC V6C 1S9
Canada

Tel.: +1 604 681 4196
Web: www.srk.com

Project Number: CAPR003118
File Name:
CRWD_Overburden_Geo_Investigation_Factual_Report_2024_CAPR003118_FINAL_20240906.docx

Suggested Citation:
SRK Consulting (Canada) Inc. 2024. Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 prepared for Canada Nickel Company Inc: Toronto, ON. Project number: CAPR003118. Issued September. 2024.

Copyright © SRK Consulting (Canada) Inc., 2024

srk consulting

Contents

1 Introduction 2
2 Field Program Summary 2
2.1 Test Pit 2
2.2 Borehole Drilling 2
2.3 Cone Penetration Test 3
2.4 Soil Logging and Sampling 4
3 Investigated Locations: Test pit, Boreholes and CPTs 4
4 Monitoring Well Installations 8
5 Closure 9
6 References 10

List of Tables

Table 3.1: Test Pit Locations 5
Table 3.2: Borehole Locations 6
Table 3.3: CPT Locations 8
Table 4.4: Monitoring well installation details 8

List of Figures

Figure 1 Geotechnical site investigation 2024-QI: Crawford Facilities Layout 9
Figure 2 Geotechnical site investigation 2024-QI: Borehole Locations 10
Figure 3 Geotechnical site investigation 2024-QI: Core Penetration Test Locations 11
Figure 4 Geotechnical site investigation 2024-QI: Test Pit locations 12

Appendices

Appendix A: Borehole Logs
Appendix B: Test Pit Log
Appendix C: Core Photologs
Appendix D: CPT Report

1 Introduction

Canada Nickel Company Inc. (CNC) is proposing to develop the Crawford Nickel Project located 40 km north of Timmins, ON. In this occasion, SRK Consulting (Canada) Inc. was retained by CNC to coordinate, conduct, and supervise the geotechnical field investigation program for 2024-QI. The previous editions, in 2021 and 2023, were also conducted and carried out by SRK. The recent geotechnical field investigation was planned to explore locations not fully covered in the past campaigns of 2021-2022 and 2023 (SRK 2023).

This document summarizes the results of the geotechnical site investigation program conducted in and around the Impoundment Facility, East Stockpile, and Tailings Management Facility (TMF); including stratigraphy, groundwater levels, and geotechnical description of each of the major soil units identified. The information documented in this report will be used later in the foundation characterization memorandums and design of the facilities.

2 Field Program Summary

The geotechnical investigation program was carried out from January to March 2024. The program included 30 sonic boreholes, 1 test pit, an extensive field test program, and the installation of 14 monitoring wells. The field tests were conducted and supervised by SRK, and included 186 standard penetration tests (SPT), 55 vane shear tests (VST), 14 cone penetration tests (CPT), 95 pore pressure dissipation tests, and 271 seismic shear tests. The total number of soil samples collected was 367, broken down into 68 Shelby tubes, 14 SPT samples, and 285 grab samples. The layout of the facilities is shown in Figure **1**. The location of the sonic boreholes, CPTs, and test pit are shown separately in Figures 2, 3, and 4, respectively.

2.1 Test Pit

The original program did not include the excavation of a test pit. However, the detection of a bedrock outcrop at the south boundary of the planned TMF during the drilling campaign led to the decision to conduct a test pit to investigate the extension and depth of the rock near the borehole that detected the surface rock. The test pit was conducted and supervised by SRK on March 16th, 2024. It was excavated using a medium excavator from Choice Sonic, SANY SY155U. The excavation was terminated after reaching refusal on the excavator arm. Once the observations and logging of the test pit were completed, it was backfilled with the excavated material and compacted using the excavator bucket.

2.2 Borehole Drilling

The sonic borehole drilling commenced on January 28th, 2024, and ended on March 22nd, of the same year. The boreholes were drilled using the sonic drill track rig, SDC 550-24, from Choice sonic. This rig is equipped with a 25-foot tower and a mechanical arm to handle core and casing barrels. In general, the drilling was carried out using core rods of 1.5 m (5 ft) in length that opened a hole diameter of 0.1 m (4 in). The length of each drill run, which varied between 1.5 m (5 ft) and 3.1 m (10 ft), was determined by the SRK field representative. The boreholes were terminated with a minimum of 3 m of competent bedrock, except for borehole SRK24-LGE-BH-201, which

was terminated after drilling 11 m of weathered bedrock. SPTs were performed every 1.5 m (5 ft) until reaching a depth of 17.7 m (58 ft), at which point SPTs were performed every 3 m (10 ft) until reaching the SPT cutoff stablished at 61 m (200 ft). The SPT were performed in granular soils, including non-plastic silts. In some instances, SPTs were performed in fine grained soils. The drilling was carried out by Choice Sonic and supervised by SRK. The sonic drilling played a key role in determining overburden thickness, bedrock depth, and retrieving high-quality soil samples.

In summary, 30 boreholes were completed. One day was registered as a minor delay because the highway access was closed due to winter conditions. This delay represented 2% of the duration of the site investigation program. The borehole program had a production rate of 11 m/shift (a shift is considered as 12 hours of work).

2.3 Cone Penetration Test

CPTs were performed using the sonic tracked rig from Choice Sonic and the additional portable rig provided by CONETEC. The cone was pushed from the ground surface until tip refusal was reached. The speed of penetration did not to exceed 2 cm/s. The CPT cone equipped with a piezometer load cell and a geophone to enable measurements of dynamic and static pore pressure, and seismic horizontal shear waves. The CPT was key to obtaining continuous soil data based on values of tip resistance, sleeve friction, and pore pressures considered at each data point.

Pore pressure dissipation tests (PPDT), performed by CONETEC and supervised by SRK, were performed around the target depths of 7.5 m, 12.5 m, 17.5 m, and 22.5 m. In fine-grained soils, PPDTs were performed until either 50% of the equilibrium pressure was reached or a cut-off time of 3 hours was achieved, whichever occurred first. In coarse-grained soil, PPDTs were performed until 90% of the equilibrium pressure was reached. The pore pressure data can be interpreted to provide estimates of equilibrium piezometric pressure, phreatic surface, in situ horizontal coefficient of consolidation (c_h) and in situ horizontal coefficient of permeability (k_h). A total of 95 PPDTs were performed.

The cone for the seismic cone penetration test (SCPT) was equipped with a horizontal active geophone located 0.2 m (0.66 ft) above the cone tip. This geophone measures the arrival time of a generated shear wave. The seismic shear wave tests were conducted at various intervals during the SCPT pushing. The SCPTs were used to determine the shear wave velocity profiles over specified intervals with depth. Seismic shear wave tests were carried out every 1 m for the first 10 m, every 2 m from depths of 10-20 m, and every 5 m for depths below 20 m. In some cases, multiple wave traces were recorded at the same depth to improve the quality of the data. A total of 271 seismic shear wave tests were completed. The complete report of the CPT tests is included in Appendix C.

In summary, 14 CPT tests were performed from February 15th, 2024, to March 22nd of the same year.

2.4 Soil Logging and Sampling

Test Pit Logging

A photo was captured from the soil wall inside the test pit, and it was used as a visual soil profile indicator. An additional photo was taken to the soil wall once the test pit excavation was terminated to show the complete test pit soil profile. During the logging exercise, grab samples were collected for laboratory physical testing.

Borehole Logging

The soil retrieve from the core barrel was logged inside a portable climate-controlled trailer. Detailed photographs were taken from each run and later compiled into a photolog (see Appendix B). The soil retrieved at each run was placed inside a 1.5 m (5 ft) long core box. The soil logging was completed per the Unified Soil Classification System (USCS) using ASTM standards (ASTM D2487-17e1, ASTM D2488-17e1).

Soil Sampling

Soil samples were divided into three types: grab, Shelby and SPT. The soil taken directly from the drill run was labeled as grab samples. On average, 4 kg of soil material was taken in each grab sample and placed inside two large Ziploc bags to preserve the natural water content. The Ziploc bags were stored inside 5-gallon plastic pails and properly labeled for later shipment to the designated laboratories.

The samples labeled as Shelby were retrieved directly from the ground using a piston sampler as specified in ASTM (D6519-15) and placed inside a Shelby tube 76.6 cm long and 7.1 cm in diameter. The tube was sealed in-situ by pouring wax on both ends and covered with plastic lids to preserve the natural water content. Once sealed, the Shelby tubes were placed inside a wooden box, as specified in ASTM (D4220/D4220M-14), with thermal insulation to prevent the soil from freezing. At the end of each drilling-shift, soil samples were brought and placed inside a climate-controlled trailer.

3 Investigated Locations: Test pit, Boreholes and CPTs

In summary, 1 test pit, 30 boreholes, and 14 CPTs were completed, and 14 groundwater monitoring wells were installed. Each CPT location was paired with a borehole ID at the same location. An overall view of all the explored locations is displayed in Figure **1**.

Table 3.1 provides the location, total depth, number of grab samples collected, and coordinates of the test pit.

Table 3.1: Test Pit Locations

Location	Test Pit ID	Total Depth (m)	Grab Samples	Easting	Northing	Elevation (masl[1])
Tailings Management Facility	SRK24-TMF-TP-01	4.6	2	474853.0	5401914.0	N/A

Notes:

As-built coordinates were provided by a handheld GPS.

[1]masl: meters above sea level

Table 3.2 and Table 3.3 provides the location, total depth, and coordinates of the boreholes and CPTs, respectively.

Table 3.2: Borehole Locations

Location	Borehole ID	Total Depth (m)	Paired CPT	Grab Samples	SPT	Shelby Samples	VST	Easting	Northing	Collar Elevation (masl[1])
Process Plant	AUS24-PP-BH-12	32.9	AUS24-PP-CPT-12[2]	20	16	1	-	470700.0	5407321.1	275.7
Process Plant	AUS24-PP-BH-14	28.9	AUS24-PP-CPT-14[2]	13	15	-	-	470595.1	5407334.1	276.6
Process Plant	AUS24-PP-BH-16	30.5	AUS24-PP-CPT-16[2]	14	13	1	-	470514.1	5407334.0	277.1
Process Plant	AUS24-PP-BH-10	26.8	AUS24-PP-CPT-10[2]	11	11	3	-	470903.8	5407277.9	271.7
Process Plant	AUS24-PP-BH-11	36.9	AUS24-PP-CPT-11[2]	15	13	3	-	470784.9	5407264.0	273.4
Monitoring Wells	ST24-BH-MW-13AB	80.8	No	12	12	4	-	470682.8	5406375.9	271.0
Monitoring Wells	ST24-BH-MW-12AB	32.6	No	11	8	1	-	471077.2	5405237.1	272.9
Monitoring Wells	ST24-BH-MW-11AB	22.6	No	6	7	1	-	471215.2	5402249.1	284.4
Monitoring Wells	ST24-BH-MW-14AB	42.1	No	11	2	2	-	466776.2	5407468.5	276.4
Impoundment Facility	ST24-BH-MW-04AB	41.1	No	9	1	4	-	470492.2	5411263.1	268.6
Monitoring Wells	ST24-BH-MW-16A	39.6	No	-	-	-	-	475544.0	5408903.1	273.2
East Stockpile	Combined24-BH-05A	71.9	No	11	12	2	2	475899.4	5408923.4	272.1
East Stockpile	SRK24-LGE-BH-205	28.3	SRK24-LGE-CPT-205	4	1	3	-	476457.1	5408412.6	271.8
East Stockpile	SRK24-LGE-BH-203	40.5	SRK24-LGE-CPT-203	5	2	3	4	476448.5	5409211.8	271.3
East Stockpile	SRK24-LGE-BH-202	25.3	SRK24-LGE-CPT-202	5	8	-	1	475366.0	5408591.1	274.1
East Stockpile	SRK24-LGE-BH-201	54.6	SRK24-LGE-CPT-201	6	6	2	2	474825.7	5407392.8	274.2
East Stockpile	SRK24-LGE-BH-204	61.9	SRK24-LGE-CPT-204	8	6	2	3	475667.1	5407347.8	274.2
East Stockpile	Combined24-BH-04A	71.9	No	18	9	4	4	476518.4	5407273.6	272.7

Location	Borehole ID	Total Depth (m)	Paired CPT	Grab Samples	SPT	Shelby Samples	VST	Easting	Northing	Collar Elevation (masl[1])
Tailings Management Facility	ST24-BH-MW-10A	87.6	No	-	-	-	-	476796.2	5407113.5	272.7
Impoundment Facility	SRK24-WRD-BH-201	68.3	SRK24-WRD-CPT-201	18	9	6	6	473338.3	5411099.5	276.8
Impoundment Facility	SRK24-WRD-BH-212	35.7	SRK24-WRD-CPT-212	7	1	3	3	474392.4	5411192.2	273.1
Impoundment Facility	SRK24-WRD-BH-215	68.9	No	13	15	2	1	473009.0	5413538.8	281.1
Tailings Management Facility	ST24-BH-MW-08AB	47.2	ST24-CPT-MW-08AB	13	6	4	4	476469.3	5401996.3	287.2
Impoundment Facility	SRK24-WRD-BH-218	14.6	No	6	-	2	2	473202.7	5414716.5	280.3
Impoundment Facility	SRK24-WRD-BH-207	14.6	SRK24-WRD-CPT-207	4	-	2	2	474234.8	5414555.3	277.3
Tailings Management Facility	SRK24-TMF-BH-207	39.0	SRK24-TMF-CPT-207	9	-	3	7	476820.5	5402796.7	281.2
Impoundment Facility	SRK24-WRD-BH-205	68.6	SRK24-WRD-CPT-205	11	11	2	3	474142.5	5413524.3	276.2
Tailings Management Facility	SRK24-TMF-BH-203	7.9	No	3	-	-	-	475737.7	5401911.4	290.3
Tailings Management Facility	SRK24-TMF-BH-202A	39.0	SRK24-TMF-CPT-202	15	2	4	5	476821.6	5404208.4	275.9
Impoundment Facility	SRK23-WRD-BH-202	23.8	SRK24-WRD-CPT-202	5	-	4	6	474129.8	5412170.4	287.2

Notes:

[1]masl: meters above sea level

[2]CPTs supervised by Ausenco.

Table 3.3: CPT Locations

Location	CPT ID	Total Depth (m)	PPD Test	Seismic Test	Easting	Northing	Collar Elevation (masl[1])
East Stockpile	SRK24-LGE-CPT-205	26.7	5	25	476457.1	5408412.6	271.8
East Stockpile	SRK24-LGE-CPT-203	29.3	5	25	476448.5	5409211.8	271.3
East Stockpile	SRK24-LGE-CPT-202	5.3	3	3	475366.0	5408591.1	274.1
East Stockpile	SRK24-LGE-CPT-201	10.0	7	9	474825.7	5407392.8	274.2
East Stockpile	SRK24-LGE-CPT-204	15.5	4	14	475667.1	5407347.8	274.2
Tailings Management Facility	SRK24-CPT-MW-03AB	2.4	3	1	472166.6	5414672.4	280.5
Impoundment Facility	SRK24-WRD-CPT-201	23.1	11	21	473338.3	5411099.5	276.8
Impoundment Facility	SRK24-WRD-CPT-212	15.0	5	12	474392.4	5411192.2	273.1
Tailings Management Facility	ST24-CPT-MW-08AB	34.5	13	31	476469.3	5401996.3	287.2
Impoundment Facility	SRK24-WRD-CPT-207	6.4	3	4	474234.8	5414555.3	277.3
Tailings Management Facility	SRK24-TMF-CPT-207	24.2	13	22	476820.5	5402796.7	281.2
Impoundment Facility	SRK24-WRD-CPT-205	7.7	6	7	474142.5	5413524.3	276.2
Tailings Management Facility	SRK24-TMF-CPT-202	29.0	12	26	476821.6	5404208.4	275.9
Impoundment Facility	SRK24-WRD-CPT-202	18.9	5	15	474129.8	5412170.4	287.2

Notes:

As-built coordinates were paired with the adjacent borehole coordinates.

[1]masl: meters above sea level

4 Monitoring Well Installations

Standpipe piezometers were installed in 8 locations to monitor groundwater levels in the foundation soil and bedrock. In total, 14 standpipes were installed. Each installation consisted of an open PVC standpipe of 50.8 mm (2 in). The screen length was varied between 1.5 m (5 ft) and 3 m (10 ft). Installation details and screen elevations are shown in the boreholes logs in Appendix A. The depths of the screen, sand, and bentonite chips were determined by the SRK field representative. The PVC standpipe piezometers were protected using a square-shape steel casing that raised approximately 1.0 m above the ground surface.

Table 4.4 presents a summary of the monitoring well locations, borehole IDs, ground elevations, and screen elevations.

Table 4.4: Monitoring well installation details

Borehole ID	Well ID	Ground Elevation (masl[1])	Hole Depth (mbgs[2])	Easting	Northing	Well PVC Stick-up (m)	Top of Screened Interval (mbgs[2])	Bottom of Screened Interval (mbgs[2])
ST24-BH-MW11AB	A	284.4	22.6	471215.2	5402249.1	0.65	20.7	22.2
ST24-BH-MW11AB	B	284.5	15.8	471213.8	5402249.1	0.92	13.4	14.9
ST24-BH-MW12AB	A	272.9	32.6	471077.2	5405237.1	0.83	31.1	32.6
ST24-BH-MW12AB	B	272.9	26.5	471077.9	5405238.7	1.04	25.0	26.5
ST24-BH-MW13AB	A	271.0	80.8	470682.8	5406375.9	0.67	74.4	77.4
ST24-BH-MW13AB	B	270.9	30.8	470684.1	5406376.3	1.02	27.7	30.8
ST24-BH-MW14AB	A	276.4	42.1	466776.2	5407468.5	0.80	40.2	42.1
ST24-BH-MW14AB	B	276.3	28.6	466776.9	5407467.3	1.11	27.1	28.6
ST24-BH-MW04AB	A	268.6	41.1	470492.2	5411263.1	0.78	39.6	41.1
ST24-BH-MW04AB	B	268.5	30.5	470492.3	5411264.2	0.85	28.3	29.9
SRK24-TMF-BH-202A	A	275.9	39.0	476821.6	5404208.4	N/A	27.7	29.3
ST24BH-MW08AB	A	287.3	47.2	476469.4	5401995.0	0.95	45.7	47.2
ST24BH-MW08AB	B	287.2	40.5	476469.3	5401996.3	0.98	39.0	40.5
ST24-BH-MW10A	A	272.7	87.6	476796.2	5407113.5	1.00	85.4	86.9

Notes:

[1]masl: meters above sea level

[2]mbgs: meters below ground surface

5 Closure

As part of the ongoing Crawford Nickel Project, SRK completed an extensive site investigation program for CNC to characterize the overburden materials in and around the planned facilities of the project. The field investigation included sonic boreholes, test pits, piezometer installations, SPTs, CPTs, pore pressure dissipation tests, seismic shear wave tests, and vane shear tests.

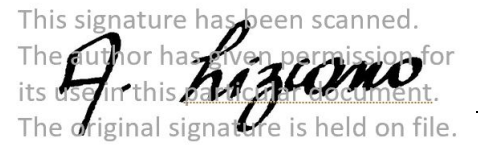
This document summarizes the geotechnical field results of the site investigation. The interpretation of the site investigation results will be included in future subsequent reports and will serve as the main inputs for the geotechnical design of open pit slopes as well as the design of stockpiles and impoundment facilities.

This report, Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1, was prepared by



Andres R. Barrero Bernal, *PhD*
Consultant

and reviewed by



Arcesio Lizcano, *PhD*
Corporate Consultant

All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

Disclaimer—SRK Consulting (Canada) Inc. has prepared this document for Canada Nickel Corporation, our client. Any use or decisions by which a third party makes of this document are the responsibility of such third parties. In no circumstance does SRK accept any consequential liability arising from commercial decisions or actions resulting from the use of this report by a third party.

The opinions expressed in this document have been based on the information available to SRK at the time of preparation. SRK has exercised all due care in reviewing information supplied by others for use on this project. While SRK has compared key supplied data with expected values, the accuracy of the results and conclusions from the review are entirely reliant on the accuracy and completeness of the supplied data. SRK does not accept responsibility for any errors or omissions in the supplied information, except to the extent that SRK was hired to verify the data.

6 References

ASTM D2487-17e1, Standard Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System), ASTM International, West Conshohocken, PA, 2017, www.astm.org

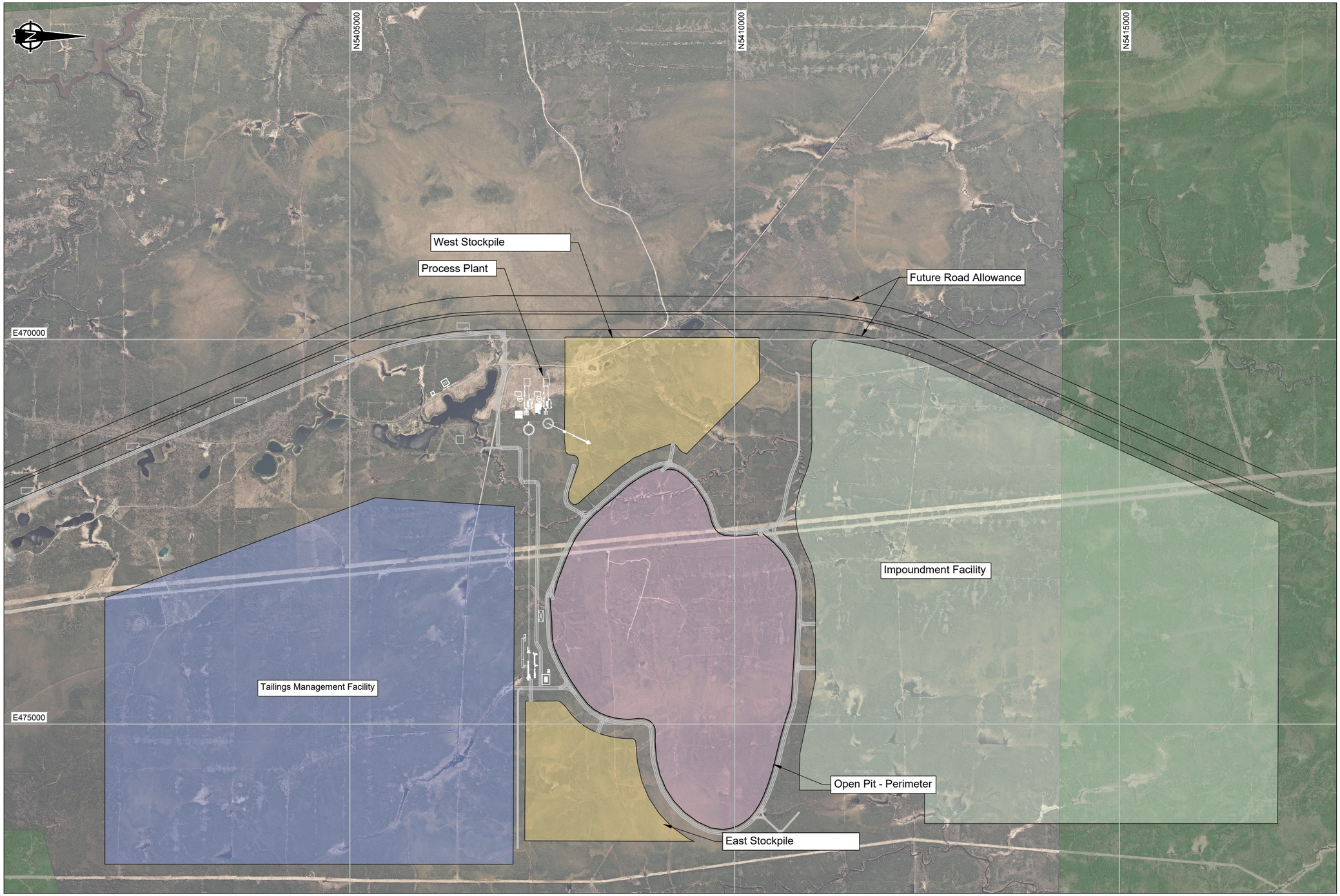
ASTM D2488-17e1, Standard Practice for Description and Identification of Soils (Visual-Manual Procedures), ASTM International, West Conshohocken, PA, 2017, www.astm.org

ASTM D4220/D4220M-14 (2014), Standard Practice for Preserving and Transporting Soil Samples, ASTM International, West Conshohocken, PA, 2014, www.astm.org

ASTM D6519-15 (2015), Standard Practice for Sampling of Soil Using the Hydraulically Operated Stationary Piston Sampler, ASTM International, West Conshohocken, PA, 2015, www.astm.org

SRK Consulting (Canada) Inc., 2023. Crawford Overburden Geotechnical Investigation Factual Report. Technical Report prepared to Canada Nickel Corporation. Project no CAPR000801, 2933pp, March.

Figures



LEGEND

- Open Pit
- Stockpile (East & West)
- Impoundment Facility
- Tailings Management Facility
- Road

NOTES

1. All units are in meters unless otherwise specified.
2. Open Pit - Perimeter, Plant Site Area, Tailings Storage Facility, Low Grade Stockpiles, Waste Rock Stockpiles footprints are based on the latest information available on October 19, 2022, and are subjected to change if necessary.

REFERENCES

NAD83 CSRS UTM Zone 17.
Aerial imagery acquired by Tulloch Mapping Solutions on 2021/05/13 with extended imagery extracted from Global Mapper on 2022/08/24.

0m 500 1000 1500 2000

srk consulting

CANADA NICKEL COMPANY

SRK JOB NO.: CAPR000801

FILE NAME: CAPR000801_Site Investigation.dwg

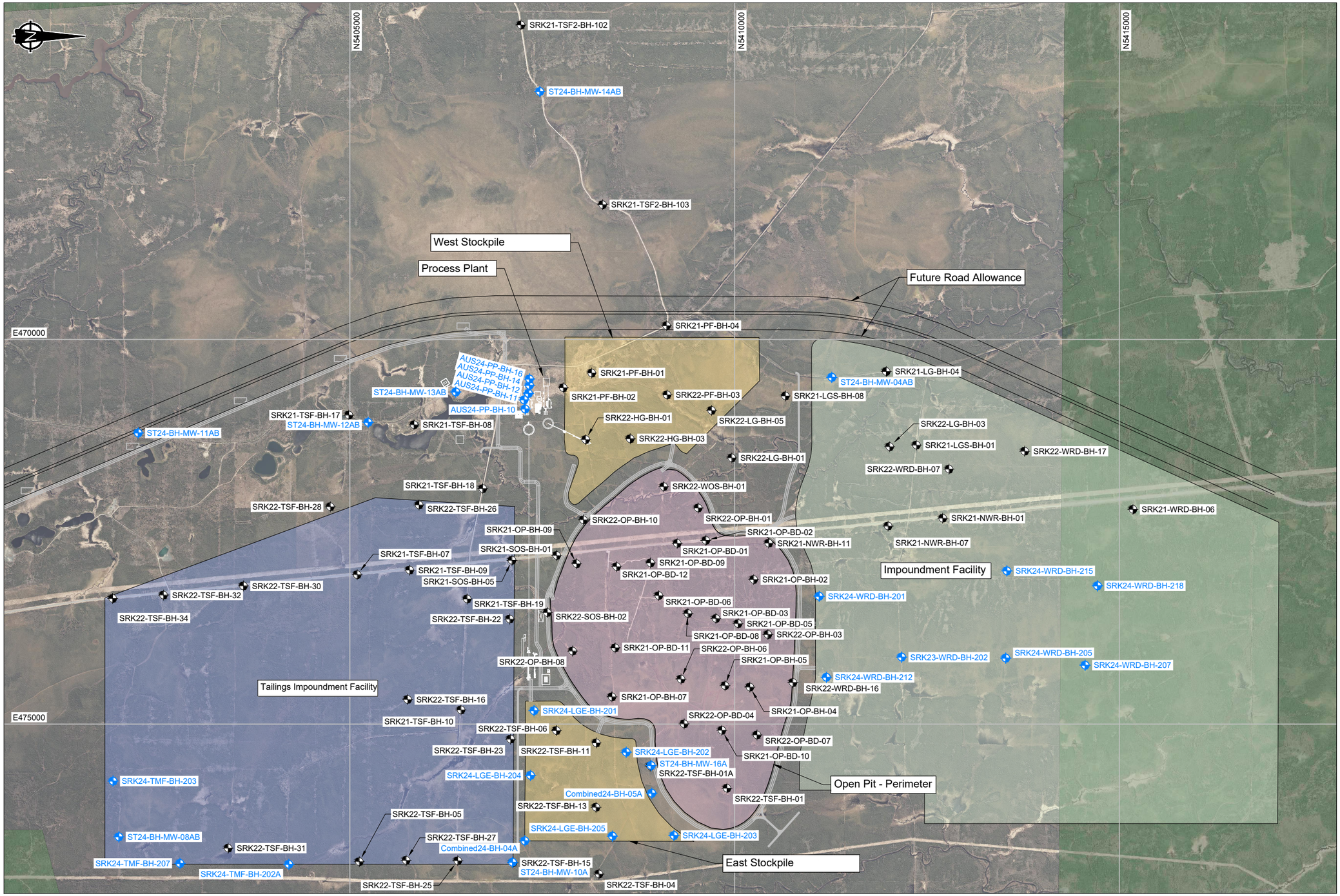
Crawford Ni-Co Project

Geotechnical site investigation 2024-QI

Crawford Facilities Layout

DATE:	APPROVED:	FIGURE:
2024/04/26	-	1

C:\Users\jbokk\SRK Consulting\NA 2CC076.000 CAPR000801 Canada Nickel Crawford FS - 1040_AutoCAD\A CAD_C3D\CAPR000801_Stockpiles\Site Investigation\CAPR000801_Site Investigation.dwg



LEGEND

- Borehole - 2023 & 2024
- Borehole - 2021 & 2022
- Open Pit
- Stockpile (East & West)
- Impoundment Facility
- Tailings Management Facility
- Road

NOTES

1. All units are in meters unless otherwise specified.
2. Open Pit - Perimeter, Plant Site Area, Tailings Storage Facility, Low Grade Stockpiles, Waste Rock Stockpiles footprints are based on the latest information available on October 19, 2022, and are subjected to change if necessary.

REFERENCES

NAD83 CSRS UTM Zone 17.
Aerial imagery acquired by Tulloch Mapping Solutions on 2021/05/13 with extended imagery extracted from Global Mapper on 2022/08/24.

0m 500 1000 1500 2000

C:\Users\jbokk\SRK Consulting\NA 2CO276.000 CAPR000801 Canada Nickel Crawford FS - 1040_AutoCAD\A CAD_C3D\CAPR000801_Stockpiles\Site Investigation\CAPR000801_Site Investigation.dwg

srk consulting

SRK JOB NO.: CAPR000801
FILE NAME: CAPR000801_Site Investigation.dwg

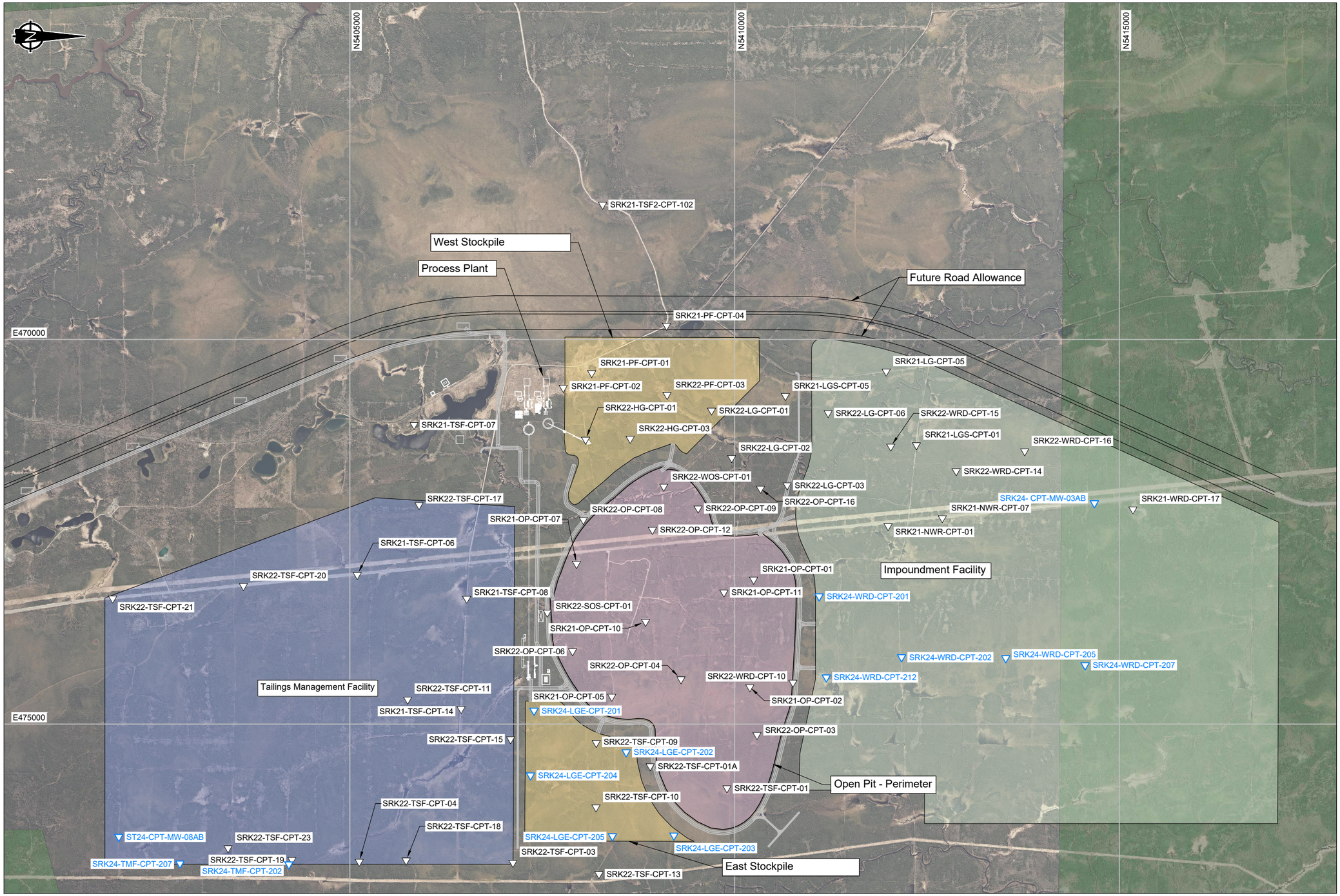
CANADA NICKEL COMPANY

Crawford Ni-Co Project

Geotechnical site investigation 2024-QI

Borehole Locations

DATE: 2024/04/26
APPROVED: -
FIGURE: 2



LEGEND

- Cone Penetration Test - 2024 Cone
- Penetration Test - 2021 & 2022 Open
- Open Pit
- Stockpile (East & West)
- Impoundment Facility
- Tailings Management Facility
- Road

NOTES

1. All units are in meters unless otherwise specified.
2. Open Pit - Perimeter, Plant Site Area, Tailings Storage Facility, Low Grade Stockpiles, Waste Rock Stockpiles footprints are based on the latest information available on October 19, 2022, and are subjected to change if necessary.

REFERENCES

NAD83 CSRS UTM Zone 17.
Aerial imagery acquired by Tulloch Mapping Solutions on 2021/05/13 with extended imagery extracted from Global Mapper on 2022/08/24.

0m 500 1000 1500 2000

srk consulting

CANADA NICKEL COMPANY

SRK JOB NO.: CAPR000801
FILE NAME: CAPR000801_Site Investigation.dwg

Crawford Ni-Co Project

Geotechnical site investigation 2024-QI

Core Penetration Test Locations

DATE: 2024/04/26 | APPROVED: - | FIGURE: 3

C:\Users\bokot\SRK Consulting\NA 2CO376.000 CAPR000801 Canada Nickel Crawford FS - 1040_AutoCAD\CAD_C3D\CAPR000801_Stockpiles\Site Investigation\CAPR000801_Site Investigation.dwg

N5405000
N5410000
N5415000
E470000
E475000

West Stockpile
Process Plant
Future Road Allowance
Impoundment Facility
Tailings Management Facility
Open Pit - Perimeter
East Stockpile

SRK22-BP-TP-14
SRK22-BP-TP-13
SRK22-BP-TP-12
SRK22-BP-TP-11
SRK22-BP-TP-17
SRK22-BP-TP-06
SRK21-OP-TP-04
SRK21-SOS-TP-01
SRK21-TSF-TP-06
SRK21-OP-TP-05
SRK22-TSF-TPT-06
SRK24-TMF-TP-01
SRK22-TSF-TP-04
SRK22-TSF-TP-03
SRK21-TSF-TP-02
SRK22-TSF-TP-05

LEGEND

- Test Pit - 2024
- Test Pit - 2021 & 2022
- Open Pit
- Stockpile (East & West)
- Impoundment Facility
- Tailings Management Facility
- Road

NOTES

1. All units are in meters unless otherwise specified.
2. Open Pit - Perimeter, Plant Site Area, Tailings Storage Facility, Low Grade Stockpiles, Waste Rock Stockpiles footprints are based on the latest information available on October 19, 2022, and are subjected to change if necessary.

REFERENCES

NAD83 CSRS UTM Zone 17.
Aerial imagery acquired by Tulloch Mapping Solutions on 2021/05/13 with extended imagery extracted from Global Mapper on 2022/08/24.

0m 500 1000 1500 2000

C:\Users\jbokk\SRK Consulting\NA 2CC076.000 CAPR000801 Canada Nickel Crawford FS - 1040_AutoCAD\A CAD_C3D\CAPR000801_Stockpiles\Site Investigation\CAPR000801_Site Investigation.dwg

srk consulting

SRK JOB NO.: CAPR000801
FILE NAME: CAPR000801_Site Investigation.dwg

CANADA NICKEL COMPANY

Crawford Ni-Co Project

Geotechnical site investigation 2024-QI

Test Pit Locations

DATE: 2024/04/26
APPROVED: -
FIGURE: 4

Appendix A: Borehole Logs

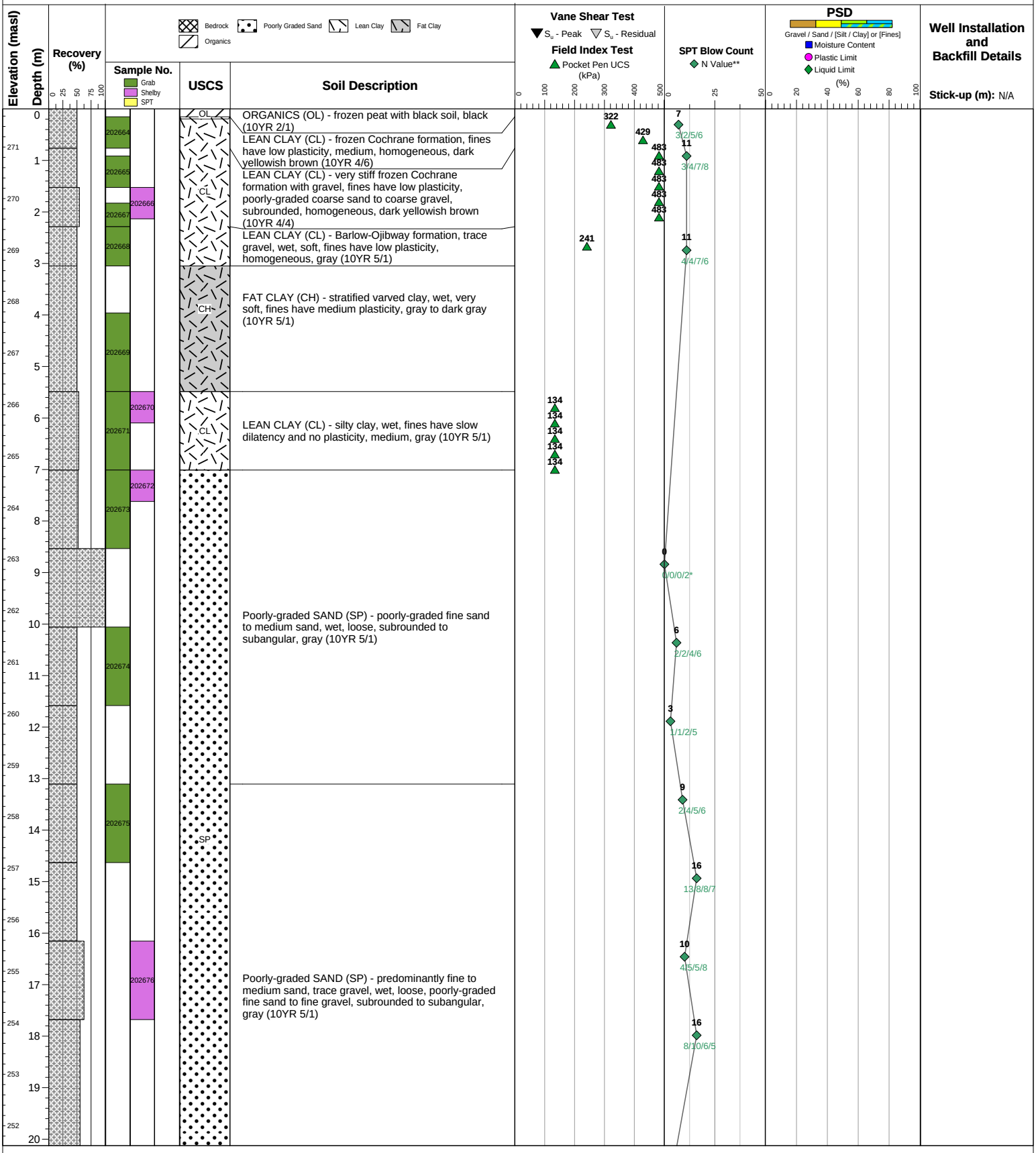
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-10
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 01-Feb-24 **TO:** 02-Feb-24
COORDINATES: 470903.8 E 5407277.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.74
TOTAL DEPTH (m): 26.8
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

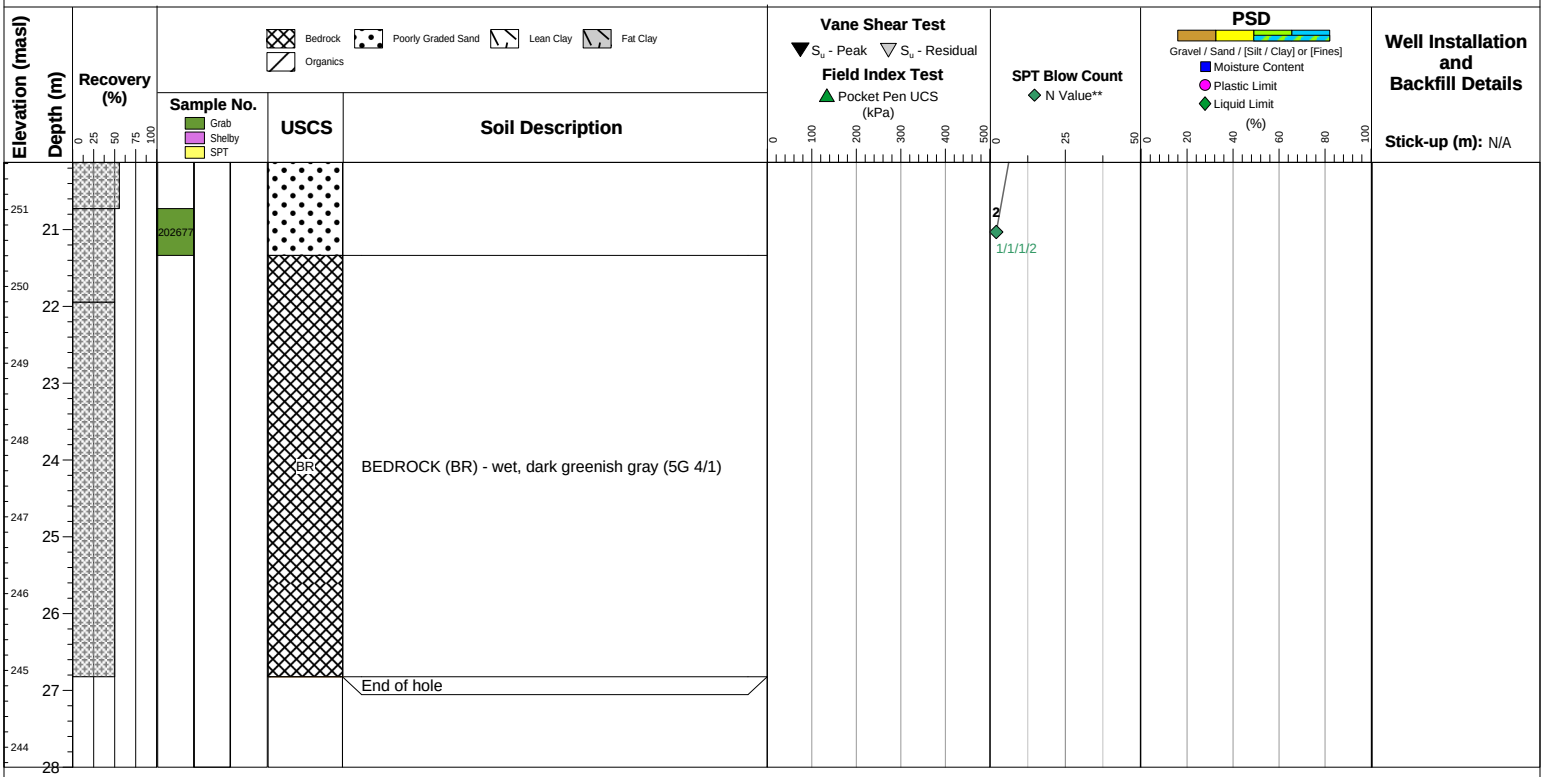
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-10
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 01-Feb-24 **TO:** 02-Feb-24
COORDINATES: 470903.8 E 5407277.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.74
TOTAL DEPTH (m): 26.8
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

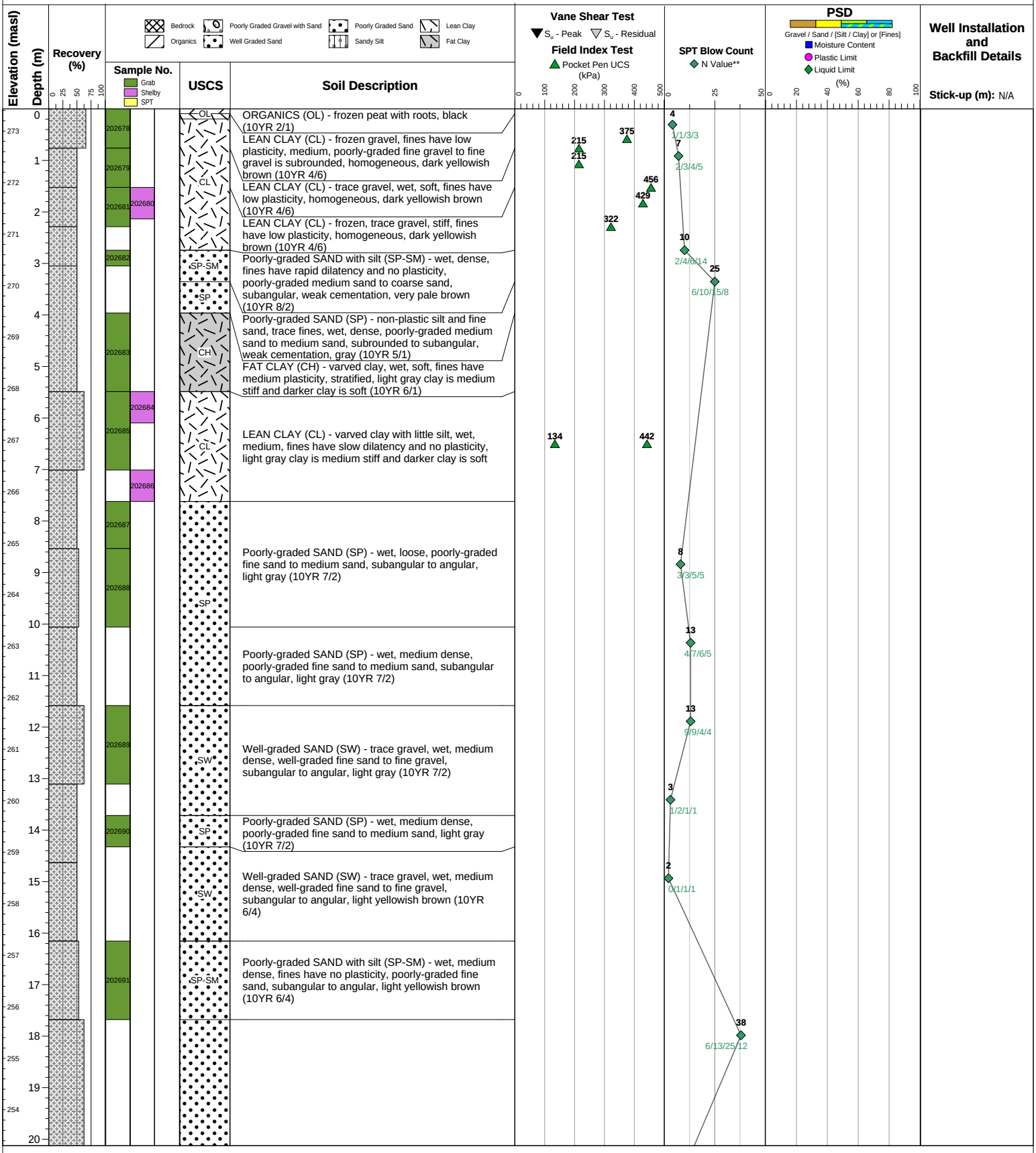
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-11
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 02-Feb-24 **TO:** 03-Feb-24
COORDINATES: 470784.9 E 5407264.0 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 273.43
TOTAL DEPTH (m): 36.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

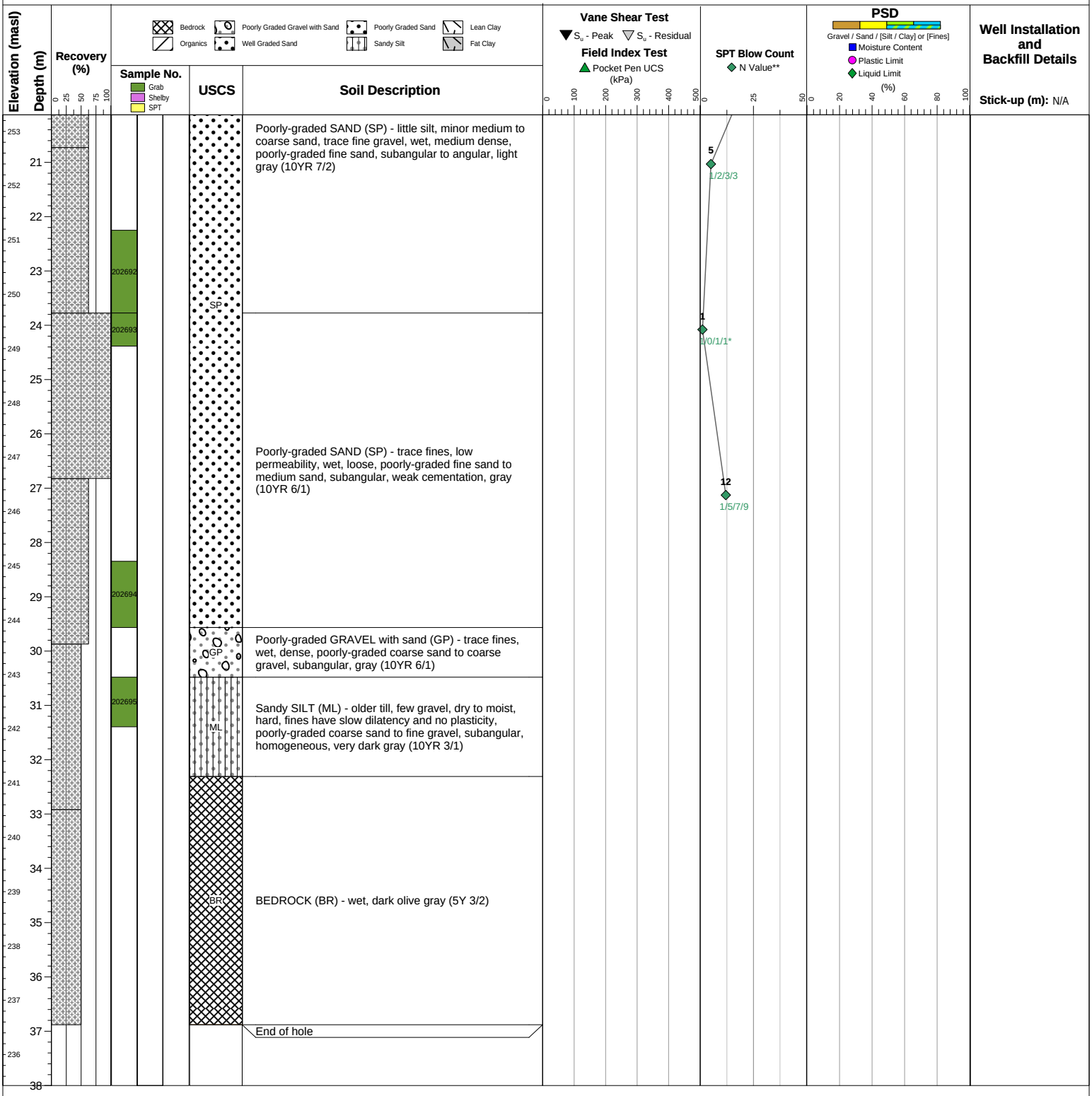
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-11
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 02-Feb-24 **TO:** 03-Feb-24
COORDINATES: 470784.9 E 5407264.0 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 273.43
TOTAL DEPTH (m): 36.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Poorly-graded SAND (SP) - little silt, minor medium to coarse sand, trace fine gravel, wet, medium dense, poorly-graded fine sand, subangular to angular, light gray (10YR 7/2)

Poorly-graded SAND (SP) - trace fines, low permeability, wet, loose, poorly-graded fine sand to medium sand, subangular, weak cementation, gray (10YR 6/1)

Poorly-graded GRAVEL with sand (GP) - trace fines, wet, dense, poorly-graded coarse sand to coarse gravel, subangular, gray (10YR 6/1)

Sandy SILT (ML) - older till, few gravel, dry to moist, hard, fines have slow dilatency and no plasticity, poorly-graded coarse sand to fine gravel, subangular, homogeneous, very dark gray (10YR 3/1)

BEDROCK (BR) - wet, dark olive gray (5Y 3/2)

End of hole

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

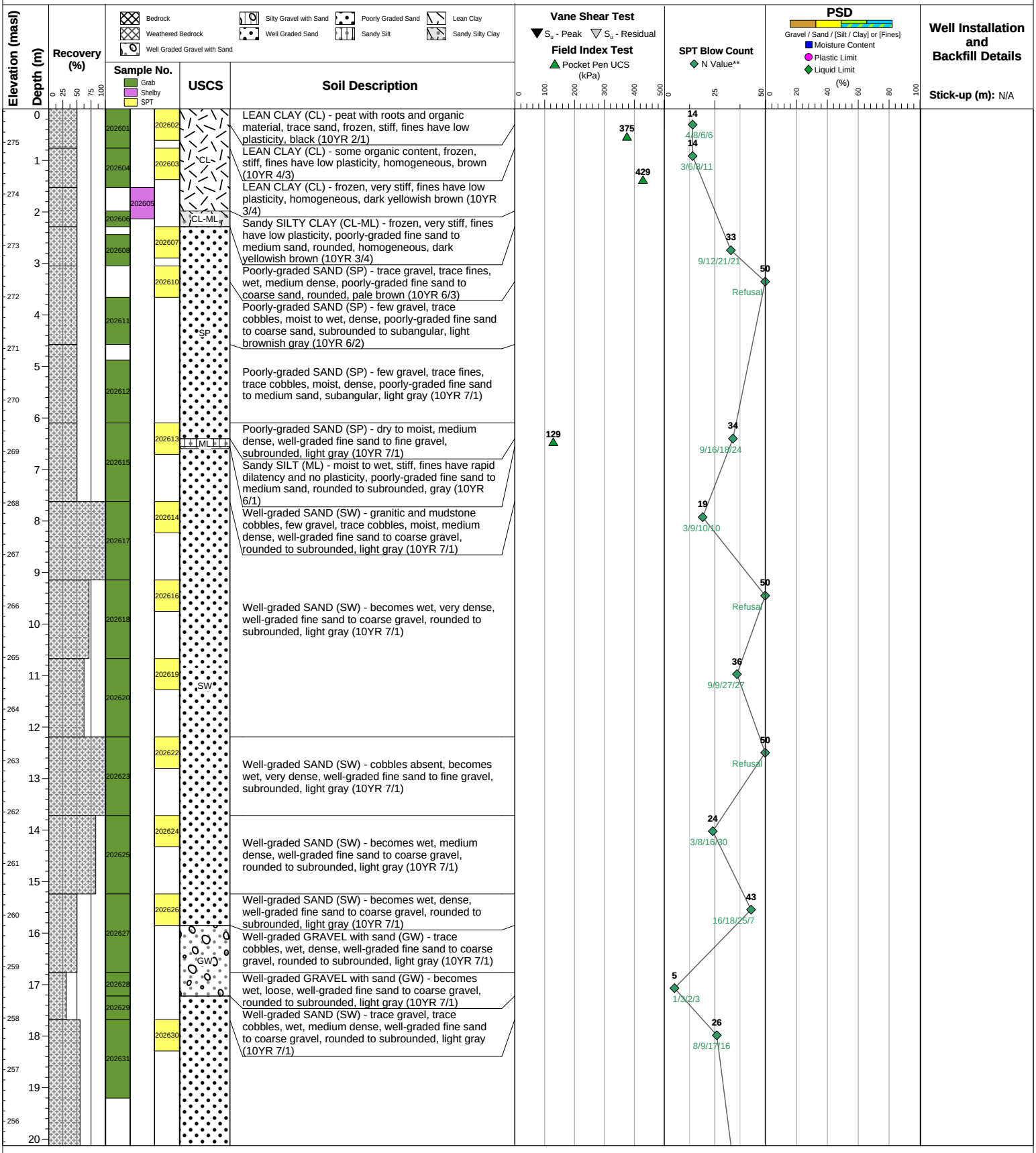
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-12
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 29-Jan-24 **TO:** 30-Jan-24
COORDINATES: 470700.0 E 5407321.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 275.65
TOTAL DEPTH (m): 32.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

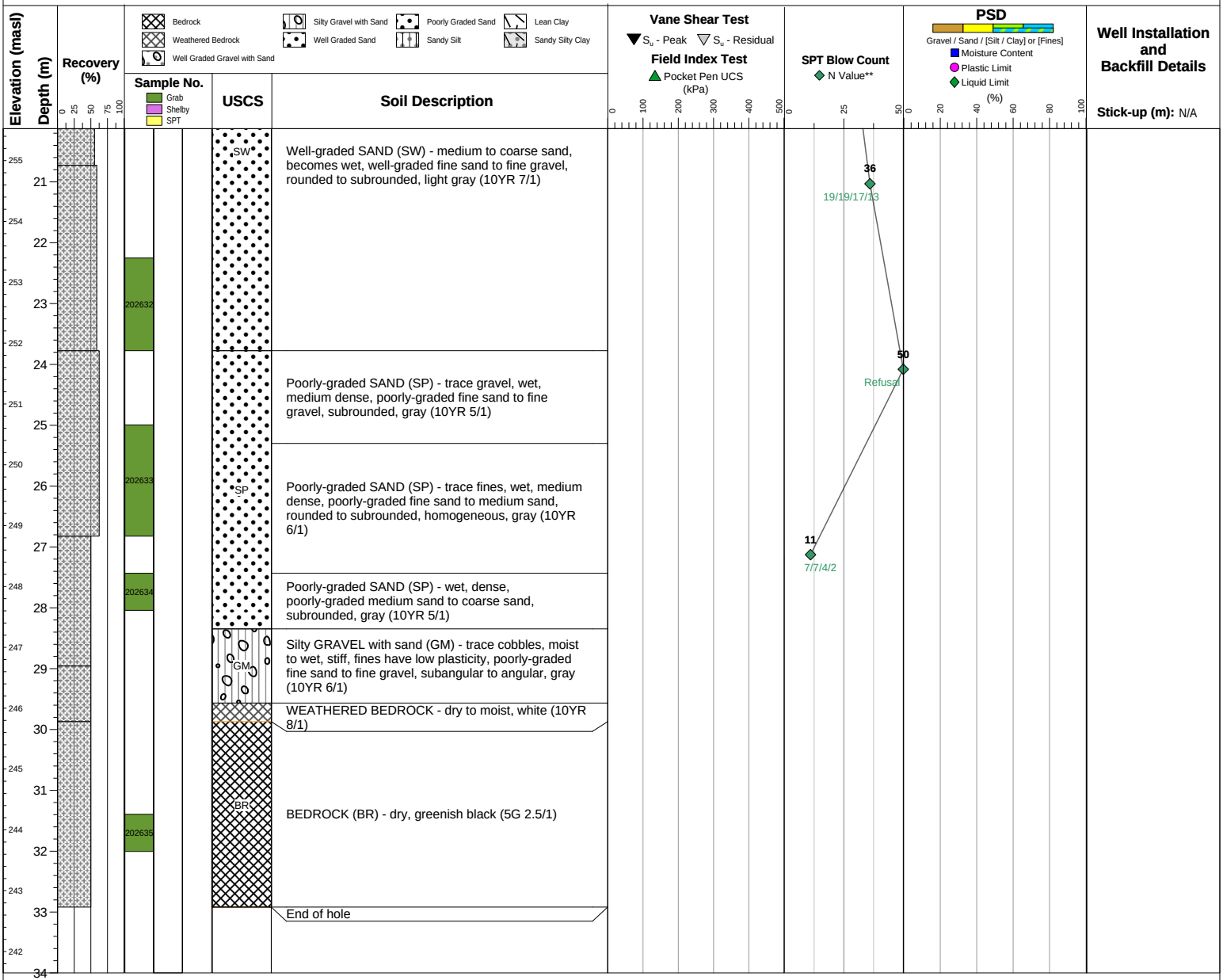
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: AUS24-PP-BH-12
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 29-Jan-24 **TO:** 30-Jan-24
COORDINATES: 470700.0 E 5407321.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 275.65
TOTAL DEPTH (m): 32.9
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

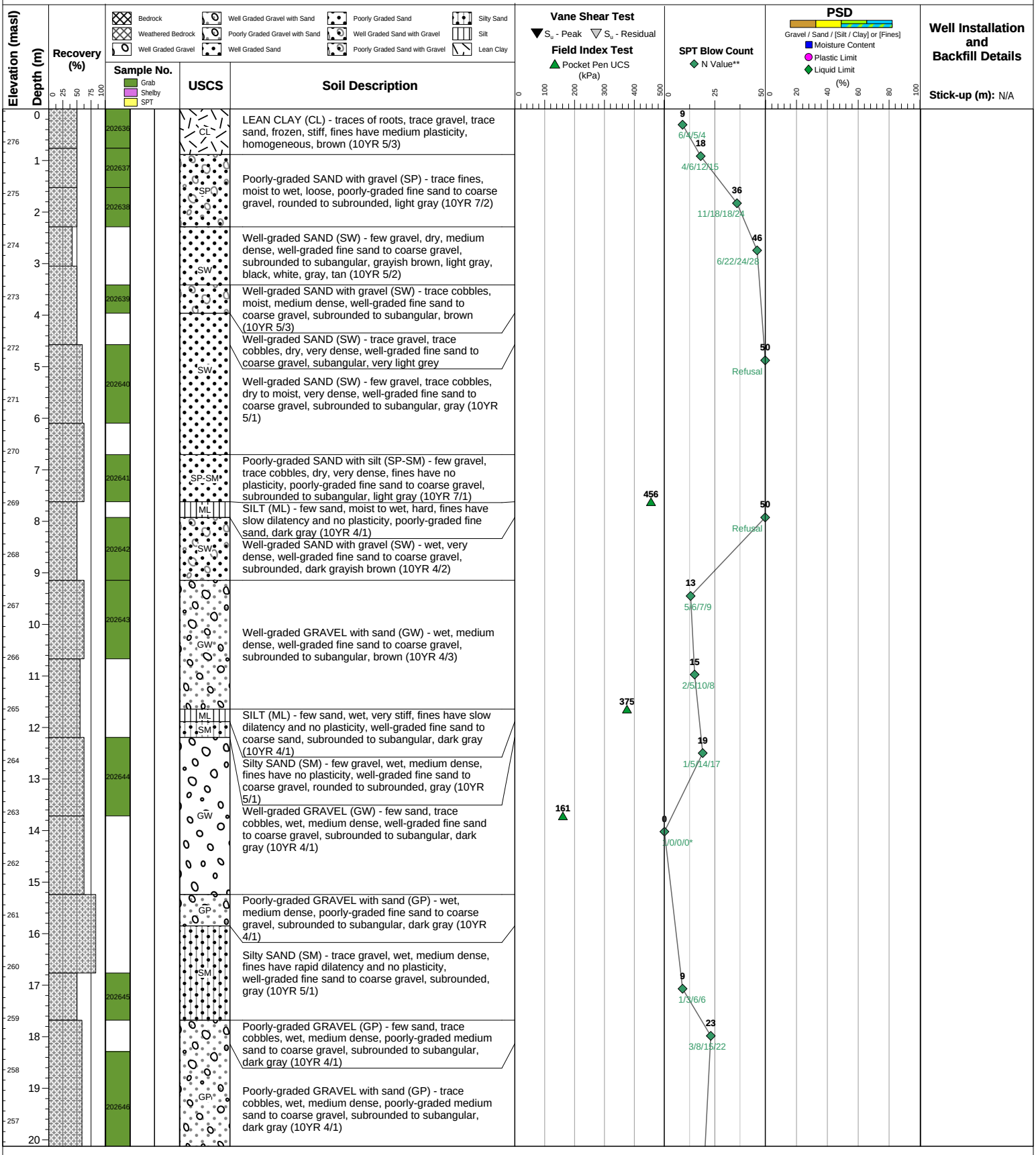
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-14
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 30-Jan-24 **TO:** 31-Jan-24
COORDINATES: 470595.1 E 5407334.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.64
TOTAL DEPTH (m): 28.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

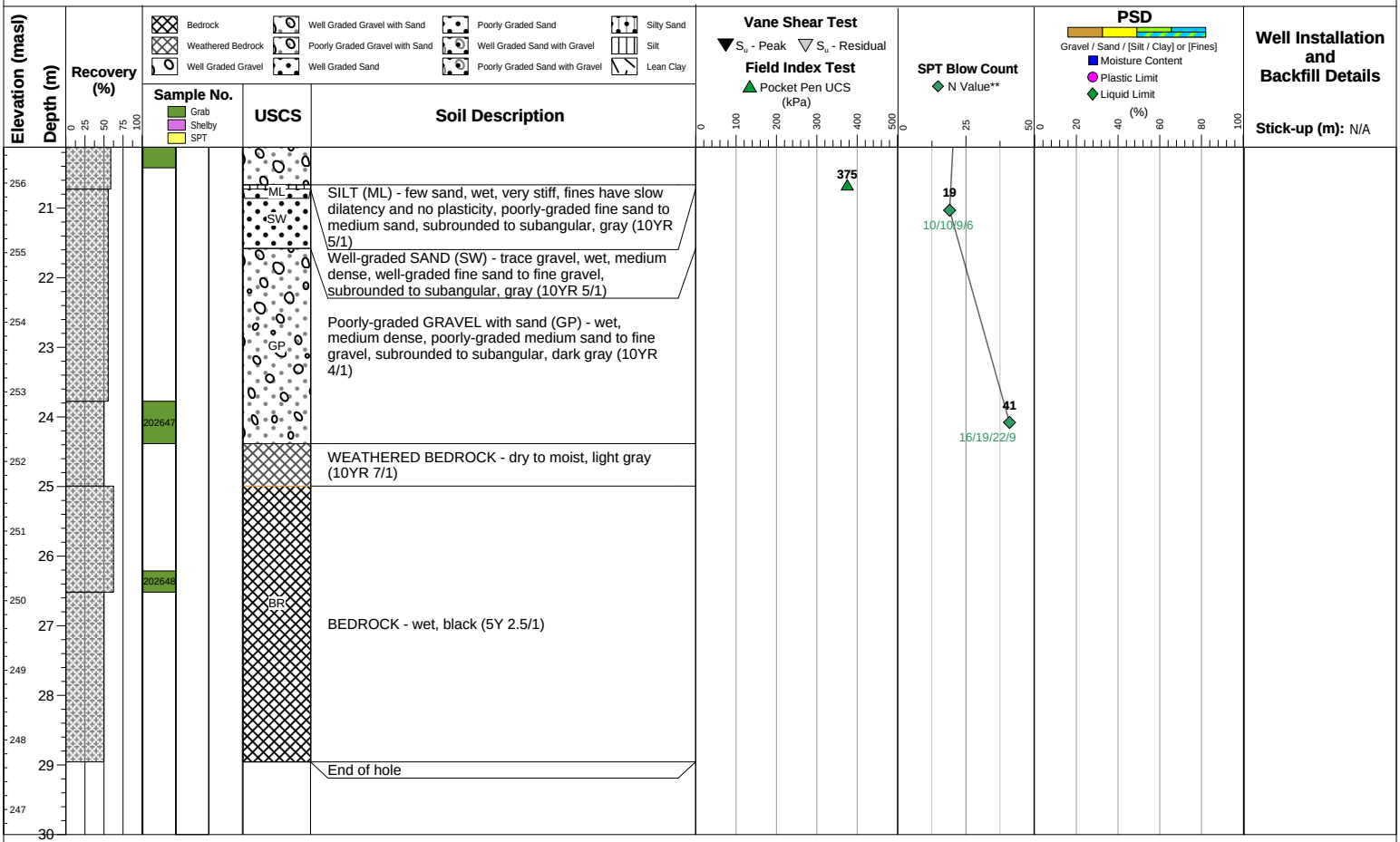
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-14
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 30-Jan-24 **TO:** 31-Jan-24
COORDINATES: 470595.1 E 5407334.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.64
TOTAL DEPTH (m): 28.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

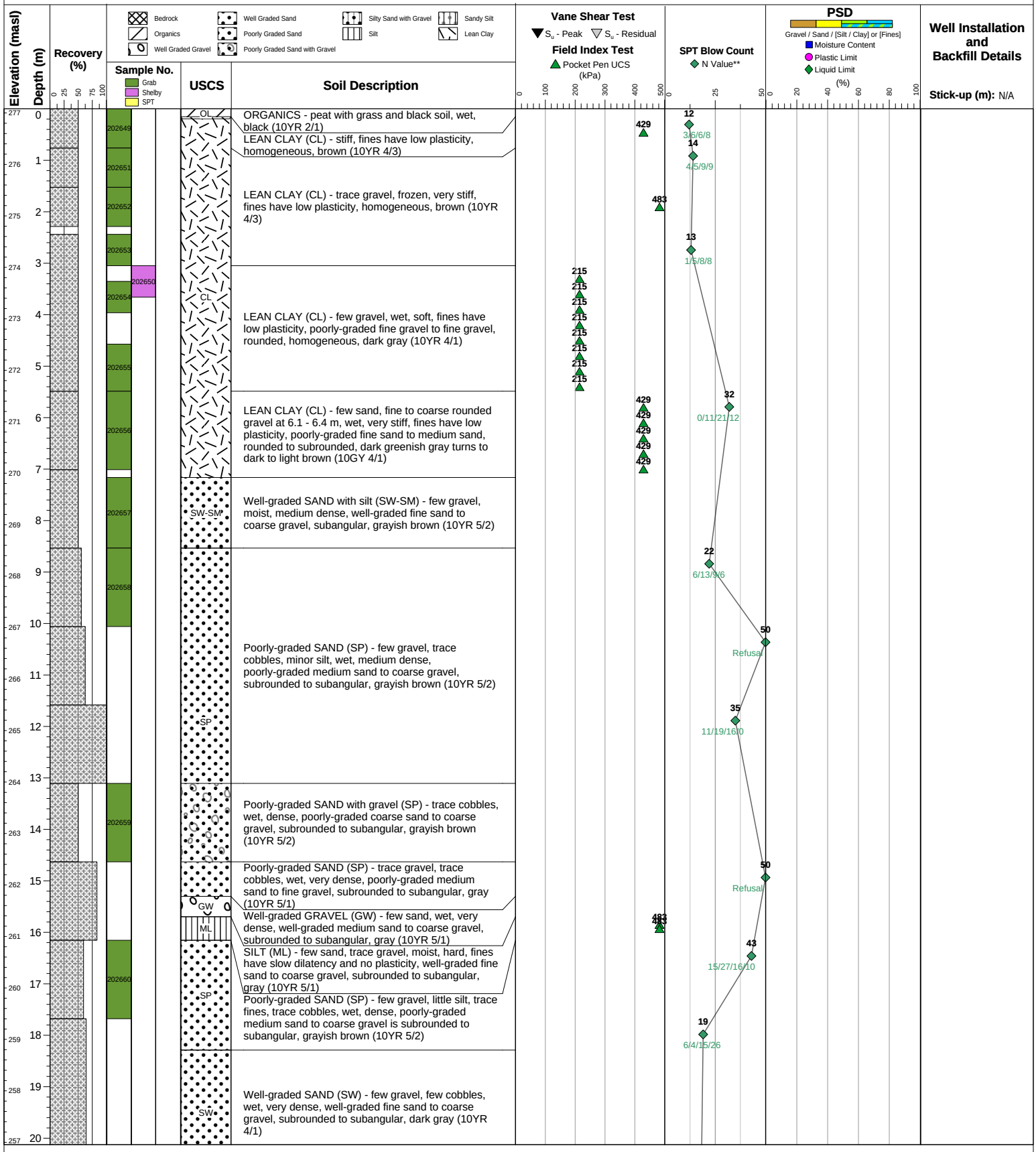
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-16
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 31-Jan-24 **TO:** 01-Feb-24
COORDINATES: 470514.1 E 5407334.0 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 277.08
TOTAL DEPTH (m): 30.5
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

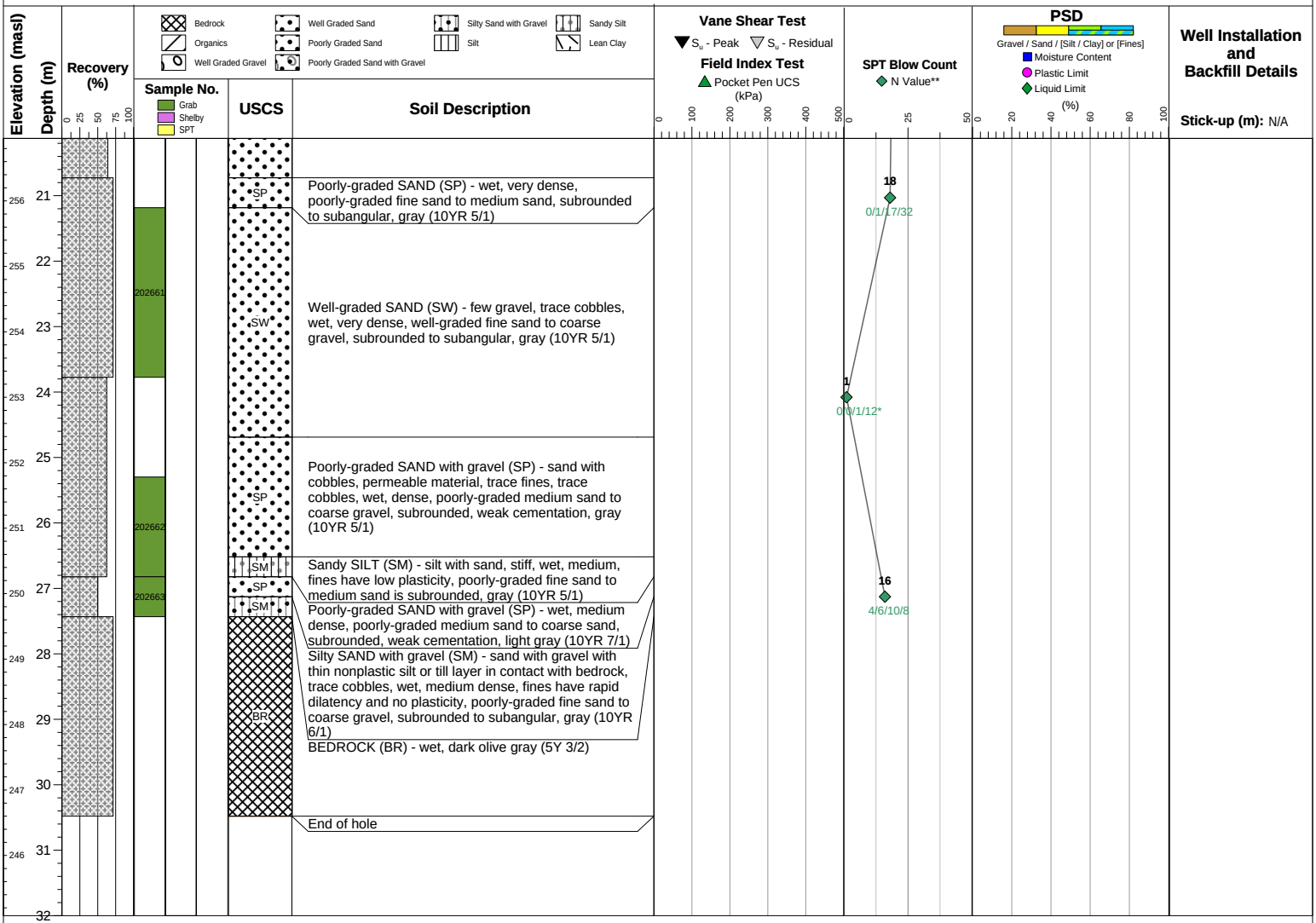
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: AUS24-PP-BH-16
LOCATION: Process Plant
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 31-Jan-24 **TO:** 01-Feb-24
COORDINATES: 470514.1 E 5407334.0 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 277.08
TOTAL DEPTH (m): 30.5
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-04A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Jasur Umarov/Parker Tully

DRILLING DATE: 26-Feb-24 **TO:** 01-Mar-24
COORDINATES: 476518.4 E 5407273.6 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.72
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Weathered Bedrock; Organics; Boulder; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Poorly Graded Sand with Silt; Silt; Sandy Silt; Silt with Gravel; Gravelly Silt; Lean Clay; Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description	Vane Shear Test / Field Index Test (kPa)	SPT Blow Count (N Value**)	PSD (%)	Well Installation and Backfill Details
272.72	0				ICE - snow with some rootlets				Stick-up (m): N/A
272	0.3		202863	OL	ORGANICS (OL) - peat, some rootlets, organic odour, moist to wet, very dark brown (10YR 2/2)				
271	1			CL	LEAN CLAY (CL) - Cochrane formation, laminated sandy interval between 1.7m and 1.8m, angular gravel piece at 2.1m, few sand, moist, soft, fines have medium plasticity, homogeneous, pale brown (10YR 6/3)	107, 161, 80, 134			
270	3			CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist, medium, fines have medium plasticity, homogeneous, gray (10YR 5/1)	107, 54, 27, 27, 27, 27			
268	5		202864	CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist, very soft, fines have high plasticity, homogeneous, gray (10YR 5/1)	0, 0, 0, 11, 0, 11, 11, 0			
265	7		202865	CL-ML	SILTY CLAY (CL-ML) - trace gravel, moist, very soft, fines have high plasticity, homogeneous, gray (10YR 5/1)	0, 0, 11, 0, 11, 54, 27, 11, 0, 11			
263	10		202866						
262	11		202867	CH	FAT CLAY (CH) - Barlow-Ojibway formation, 3cm varved clay, varves are more disturbed by still visible at 16.1m to 17.7 m, moist to wet, very soft, fines have high plasticity, stratified, gray (10YR 5/1)	0, 11, 11, 27, 27, 11, 11, 11, 27, 11, 27, 32, 11, 27, 27, 27			
260	13		202869						
259	14		202868						
258	15		202870						
256	17		202871						
255	18			CL-ML	SILTY CLAY (CL-ML) - Barlow-Ojibway formation, varved clay with higher silt content compared to the layer above, silt stratifications (3-4cm) are thicker than clay laminations (0.2-0.3cm), moist to wet, medium, fines have medium plasticity, laminated, gray (10YR 5/1)	54, 80, 134, 27, 134			
253	20		202872						

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-04A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Jasur Umarov/Parker Tully

DRILLING DATE: 26-Feb-24 **TO:** 01-Mar-24
COORDINATES: 476518.4 E 5407273.6 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.72
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Weathered Bedrock; Organics; Boulder; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Poorly Graded Sand with Silt; Silt; Sandy Silt; Silt with Gravel; Gravelly Silt; Lean Clay; Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
272	0				
252	21			ML	SILT (ML) - likely Matheson till, thin 1mm laminations of clay are present, few sand but higher sand content with depth, moist to wet, very stiff, fines have rapid dilatency and no plasticity, homogeneous, dark grayish brown (10YR 4/2)
251	22				
250	23		202873		
249	24		202874	SM	Silty SAND (SM) - laminations are dark brown, gray, and organic-like, less fines with depth, moist to wet, medium dense, fines have no plasticity, well-graded fine sand to medium sand, laminated, very dark grayish brown (10YR 3/2)
248	25				
247	26		202875	SP-SM	Poorly-graded SAND with silt (SP-SM) - less fines with depth, trace pieces of wood, moist, fines have rapid dilatency and no plasticity, poorly-graded fine sand, homogeneous, gray (10YR 6/1)
246	27			SW-SM	Well-graded SAND with silt (SW-SM) - few gravel, moist, very dense, fines have no plasticity, well-graded fine sand to fine gravel is subrounded to subangular, homogeneous, dark gray (10YR 4/1)
245	28			SP	Poorly-graded SAND (SP) - trace gravel, moist, poorly-graded medium sand to coarse sand is subangular, homogeneous, very dark gray (10YR 3/1)
244	29				
243	30		202876	SW-SM	Well-graded SAND with silt (SW-SM) - higher silt content than the layers above, less fines with depth, trace gravel, moist, fines have no plasticity, well-graded fine sand to coarse sand is subangular, homogeneous, dark gray (10YR 4/1)
242	31			SM	Silty SAND (SM) - likely Matheson till, gravel is sub-angular, few gravel, moist to wet, very stiff, fines have low plasticity, light gray (10YR 7/2)
241	32		202877		
240	33				Sandy SILT (ML) - Matheson till, few gravel is subrounded, angular coarse gravel at 33.7m, trace cobbles, moist, hard, fines have no plasticity, gray (10YR 5/1)
239	34				
238	35			ML	
237	36				SILT with gravel (ML) - older till, gravel is sub-rounded to sub-angular, angular 8cm black cobble at 37.6m, few sand, moist, hard, fines have no plasticity, gray (10YR 6/1)
236	37		202878		
235	38				Sandy SILT (ML) - older till, black hard clay laminations throughout, gravel is sub-angular, few gravel, dry to moist, hard, fines have no plasticity, gray (10YR 6/1)
234	39				
233	40				Silty SAND (SM) - disturbed, non-homogenous,

Vane Shear Test (S_u - Peak, S_u - Residual)
Field Index Test: Pocket Pen UCS (kPa)

Depth (m)	Pocket Pen UCS (kPa)
21	134, 134
22	134, 134, 241
23	134, 161, 188
24	107
31	161, 134
32	134, 134
33	241, 268

SPT Blow Count: N Value**

Depth (m)	N Value**
21	29 (7/14/15)
24	29 (5/12/17)
27	50 (Refusal)
30	39 (14/18/21)
33	45 (14/25/20)
36	50 (Refusal)
39	50 (Refusal)

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-04A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Jasur Umarov/Parker Tully

DRILLING DATE: 26-Feb-24 **TO:** 01-Mar-24
COORDINATES: 476518.4 E 5407273.6 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.72
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Weathered Bedrock; Organics; Boulder; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Poorly Graded Sand with Silt; Silt; Sandy Silt; Silt with Gravel; Gravelly Silt; Lean Clay; Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
272	0				approximately 0.3m thick sandy and silty layers, trace gravel, moist, fines have no plasticity, poorly-graded fine sand to medium sand is subangular, gray (10YR 6/1)
232	41		202879		
231	42				Silty SAND (SM) - trace coarse gravel is angular and black at 42.5m, moist, very dense, fines have no plasticity, poorly-graded fine sand to medium sand is subangular, homogeneous, gray (10YR 5/1)
230	43			SM	
229	44				Silty SAND (SM) - higher silt content with depth, wet, fines have no plasticity, poorly-graded fine sand to medium sand is subangular, homogeneous, gray (10YR 6/1)
228	45				
227	46		202880		Silty SAND (SM) - hard to drill but crumbly recovery, disturbed, well-sorted, primarily sand and silt-sized particles, moist, fines have no plasticity, poorly-graded fine sand is subangular, homogeneous, gray (10YR 6/1)
226	47				
225	48				
224	49			SP-SM	Poorly-graded SAND with silt (SP-SM) - well-sorted, primarily sand and silt-sized particles, moist, dense, fines have no plasticity, poorly-graded fine sand to medium sand is subangular, gray (10YR 6/1)
223	50				
222	51		202881		Silty SAND (SM) - significantly higher silt content than the layer above, moist to wet, fines have no plasticity, gap-graded fine sand is subangular, gray (10YR 6/1)
221	52				Silty SAND (SM) - angular gravel-sized particles at 54.3m, trace gravel, moist, fines have no plasticity, poorly-graded fine sand is subangular, gray (10YR 6/1)
220	53			SM	
219	54		202882		
218	55				Silty SAND (SM) - Matheson till, crushed coarse angular gravel at 55.8m, trace gravel, moist to wet, fines have no plasticity, poorly-graded fine sand is subangular to angular, gray (10YR 6/1)
217	56				
216	57			ML	Gravelly SILT (ML) - older till, crushed cobbles 57.6m to 57.9m, gravel is sub-angular, few sand but more with depth, weathered dark orange gravel sized particles between 58.2m to 58.5m, dry to moist, fines have no plasticity, very dark gray (5Y 3/1)
215	58		202883		
214	59				BOULDER - fine grained, crushed into angular and platey gravel size pieces, <1% pyrate inclusions (medium sand size), wet, black (2.5Y 2.5/1)
213	60				SILT with gravel (ML) - older till, gravel is sub-rounded, drier with depth, cobble (fine grained,

SPT Blow Count: 50 Refusal; 49 13/18/31

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-04A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Jasur Umarov/Parker Tully

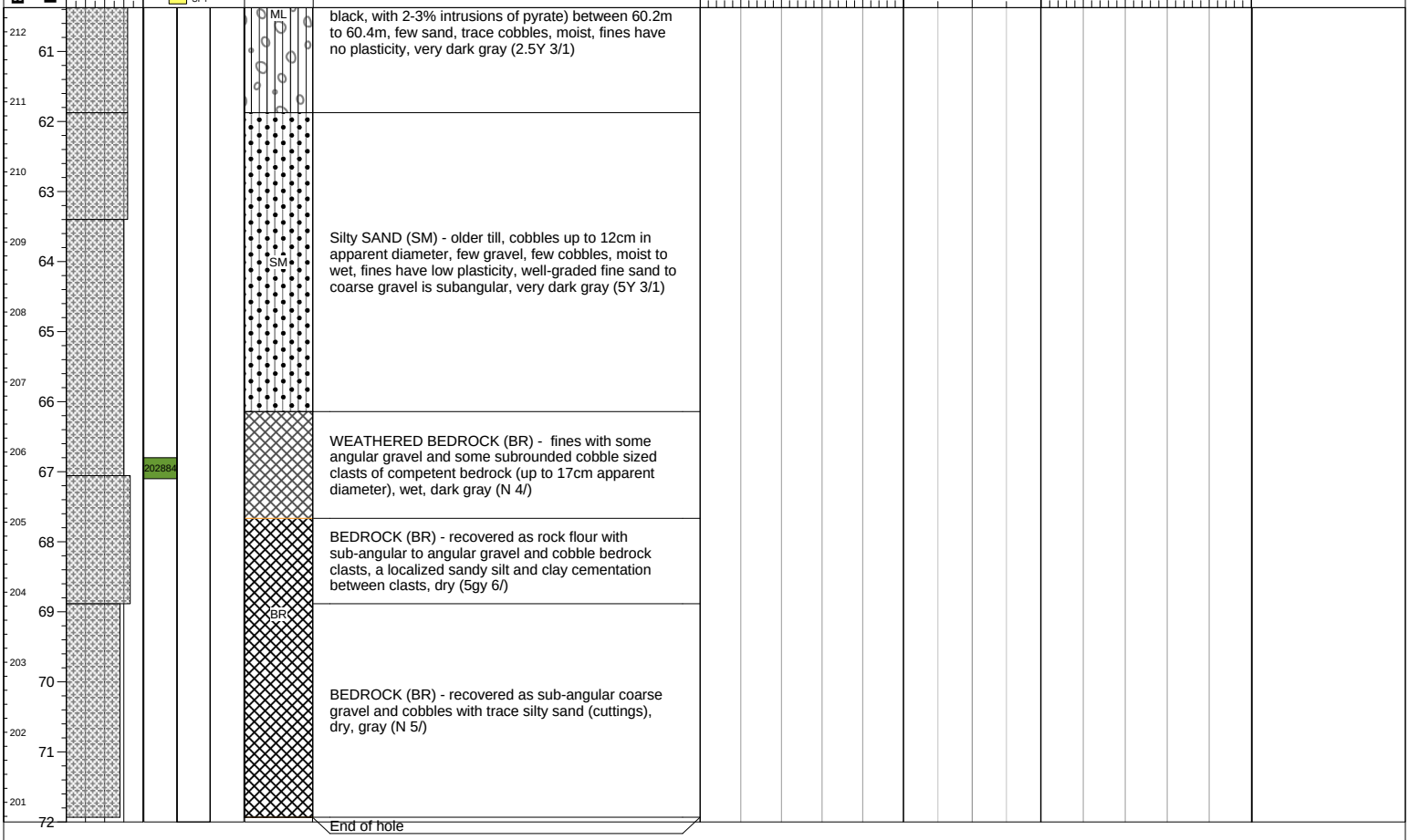
DRILLING DATE: 26-Feb-24 **TO:** 01-Mar-24
COORDINATES: 476518.4 E 5407273.6 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.72
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Weathered Bedrock; Organics; Boulder; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Poorly Graded Sand with Silt; Silt; Sandy Silt; Silt with Gravel; Gravelly Silt; Lean Clay; Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)



Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

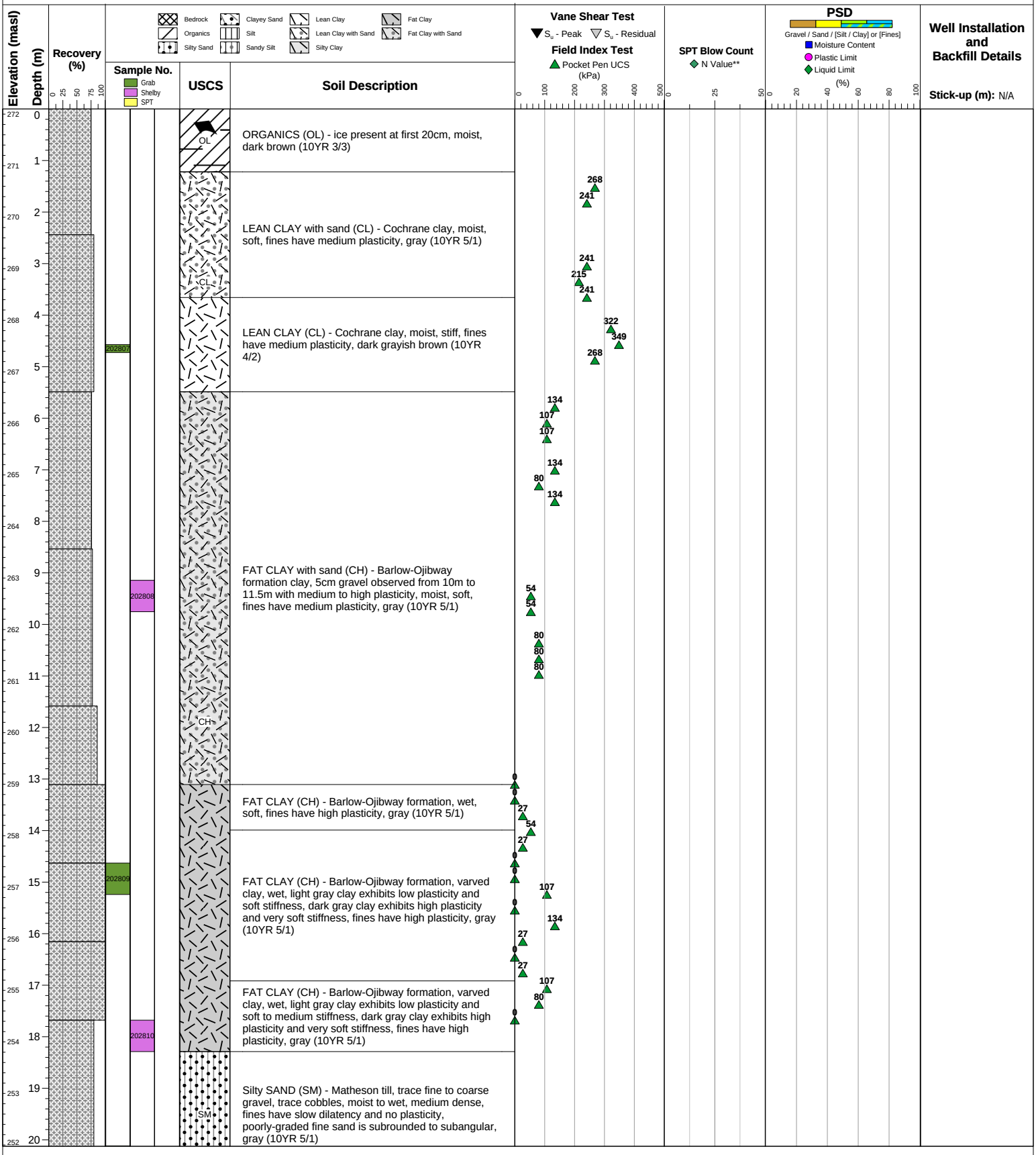
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-05A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 15-Feb-24 **TO:** 17-Feb-24
COORDINATES: 475899.4 E 5408923.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.1
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

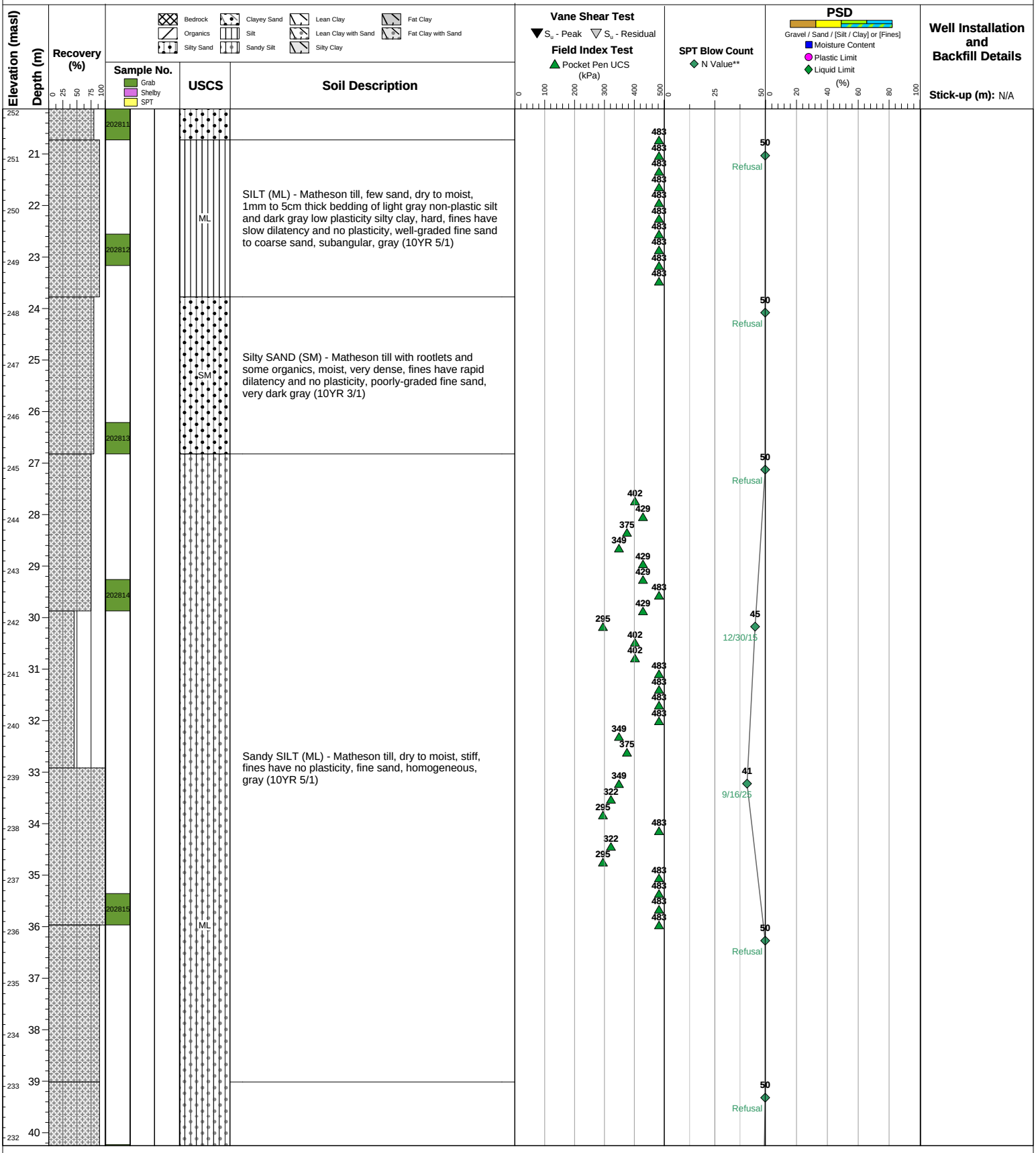
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-05A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 15-Feb-24 **TO:** 17-Feb-24
COORDINATES: 475899.4 E 5408923.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.1
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-05A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 15-Feb-24 **TO:** 17-Feb-24
COORDINATES: 475899.4 E 5408923.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.1
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock, Organics, Silty Sand, Clayey Sand, Silt, Sandy Silt, Lean Clay, Lean Clay with Sand, Silty Clay, Fat Clay, Fat Clay with Sand

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
231	41		202816 (Grab)		Sandy SILT (ML) - Matheson till, moist, stiff, fines have no plasticity, homogeneous, gray (10YR 5/1)
230	42				
229	43				
228	44				Sandy SILT (ML) - Matheson till, wet, soft to medium stiffness, fines have no plasticity, homogeneous, gray (10YR 5/1)
227	45				Sandy SILT (ML) - Matheson till, dry to moist, stiff, fines have no plasticity, homogeneous, gray (10YR 5/1)
226	46		202817 (Grab)	SM	Silty SAND (SM) - Matheson till, few gravel, moist to wet, loose, fines have no plasticity, poorly-graded coarse fraction, homogeneous, gray (10YR 5/1)
225	47				
224	48			ML	Sandy SILT (ML) - Matheson till, moist to wet, medium, fines have no plasticity, homogeneous, gray (10YR 5/1)
				SM	Silty SAND (SM) - Matheson till, moist, medium dense, fines have low plasticity, poorly-graded sand, homogeneous, gray (10YR 5/1)
223	49				
222	50			ML	Sandy SILT (ML) - Matheson till, moist, medium, fines have no plasticity, homogeneous, gray (10YR 5/1)
221	51				
220	52		202818 (Grab)		
219	53				
218	54				SILTY CLAY (CL-ML) - Matheson till, dry to moist, hard, fines have low plasticity, very dark gray (10YR 3/1)
217	55				
216	56			CL-ML	
215	57				
214	58				SILTY CLAY (CL-ML) - Matheson till, dry to moist, hard, fines have no plasticity, light and dark gray (10YR 4/1)
213	59				
212	60		202819 (Grab)		

Vane Shear Test (S_u - Peak, S_u - Residual)
Field Index Test
Pocket Pen UCS (kPa): 322, 322, 322, 268, 483, 483, 483, 483, 483, 483, 483, 483, 483, 483, 483, 483, 483

SPT Blow Count
N Value**: 46, 21/22/24, 50, Refusal, 50, Refusal, 50, Refusal

PSD
Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%)

Well Installation and Backfill Details
Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

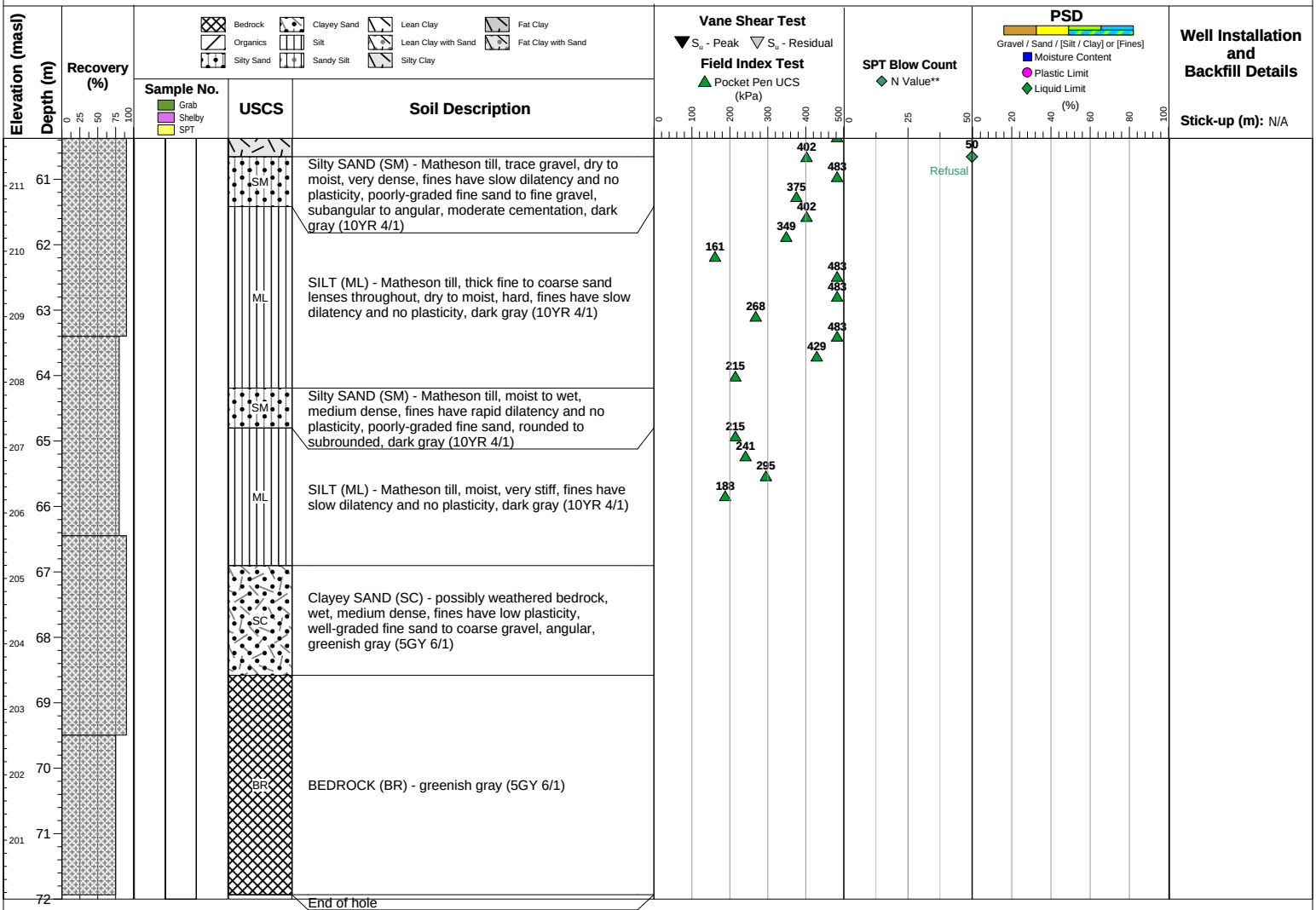
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: Combined24-BH-05A
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 15-Feb-24 **TO:** 17-Feb-24
COORDINATES: 475899.4 E 5408923.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.1
TOTAL DEPTH (m): 71.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

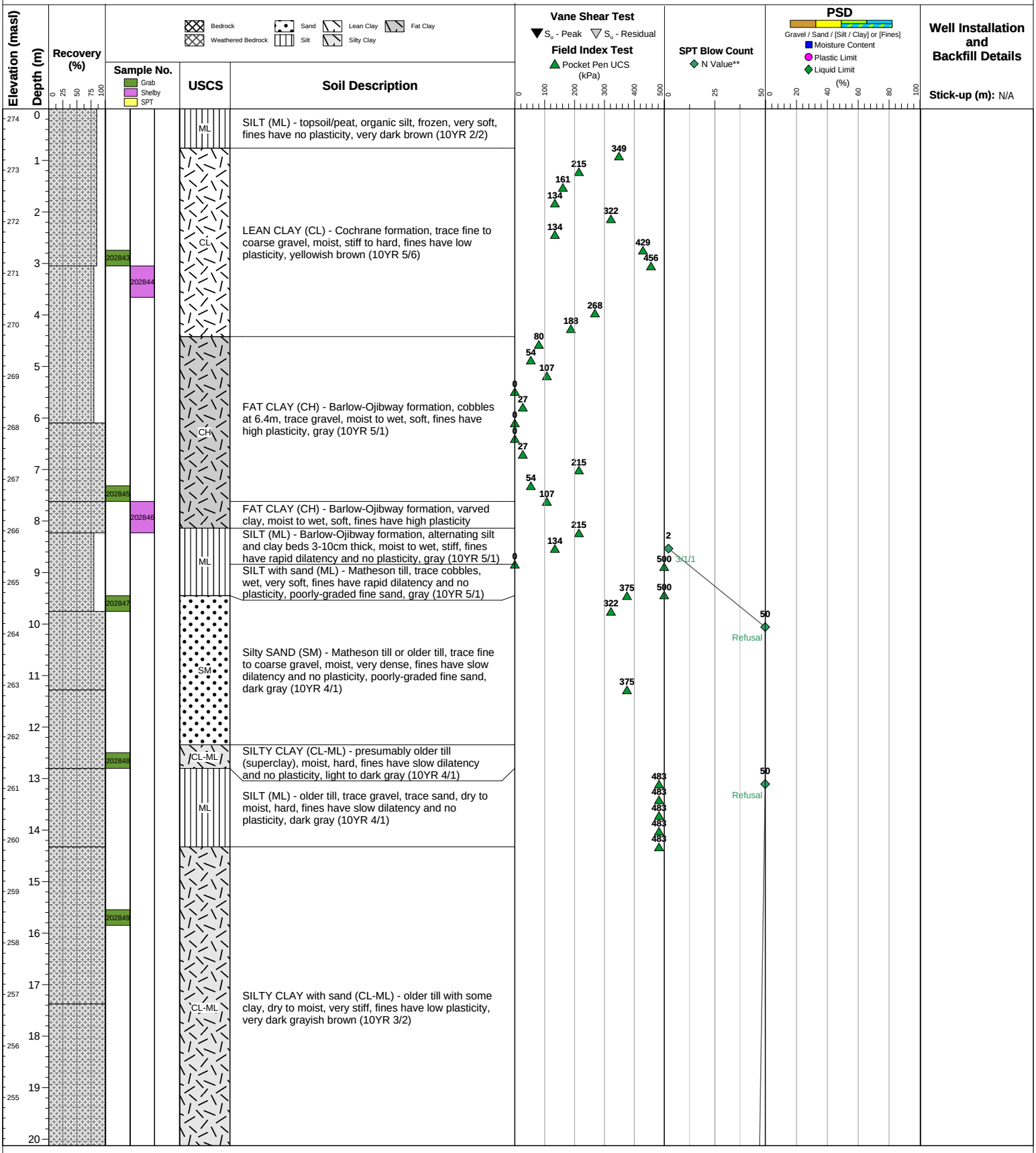
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-201
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 21-Feb-24 **TO:** 23-Feb-24
COORDINATES: 474825.7 E 5407392.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.19
TOTAL DEPTH (m): 54.6
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

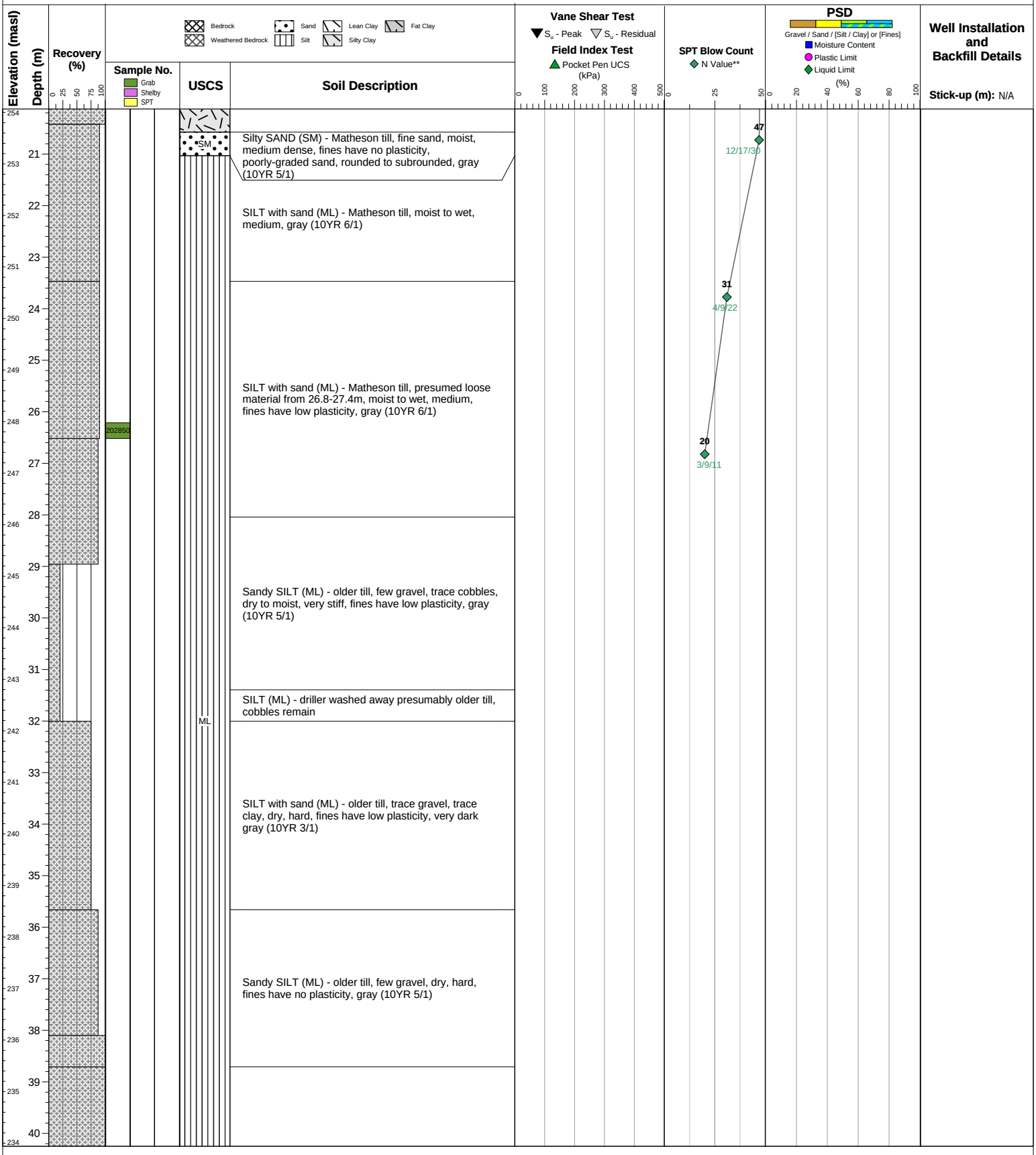
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-201
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 21-Feb-24 **TO:** 23-Feb-24
COORDINATES: 474825.7 E 5407392.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.19
TOTAL DEPTH (m): 54.6
WATER LEVEL (mbgs): N/A



Silty SAND (SM) - Matheson till, fine sand, moist, medium dense, fines have no plasticity, poorly-graded sand, rounded to subrounded, gray (10YR 5/1)

SILT with sand (ML) - Matheson till, moist to wet, medium, gray (10YR 6/1)

SILT with sand (ML) - Matheson till, presumed loose material from 26.8-27.4m, moist to wet, medium, fines have low plasticity, gray (10YR 6/1)

Sandy SILT (ML) - older till, few gravel, trace cobbles, dry to moist, very stiff, fines have low plasticity, gray (10YR 5/1)

SILT (ML) - driller washed away presumably older till, cobbles remain

SILT with sand (ML) - older till, trace gravel, trace clay, dry, hard, fines have low plasticity, very dark gray (10YR 3/1)

Sandy SILT (ML) - older till, few gravel, dry, hard, fines have no plasticity, gray (10YR 5/1)

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-201
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 21-Feb-24 **TO:** 23-Feb-24
COORDINATES: 474825.7 E 5407392.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.19
TOTAL DEPTH (m): 54.6
WATER LEVEL (mbgs): N/A

Elevation (masl) | Depth (m) | Recovery (%) | Sample No. (Grab, Shelby, SPT) | USCS | Soil Description | Vane Shear Test (S_u - Peak, S_u - Residual) / Field Index Test (Pocket Pen UCS (kPa)) | SPT Blow Count (N Value**) | PSD (Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit; (%)) | Well Installation and Backfill Details

Bedrock, Weathered Bedrock, Sand, Silt, Lean Clay, Fat Clay, Silty Clay

Depth (m)	Elevation (masl)	USCS	Soil Description
41	233		SILT (ML) - older till, trace sand, dry, hard, fines have low plasticity, dark gray (10YR 4/1)
43	231		WEATHERED BEDROCK - trace basal till, sandy silt, dry, fissured, medium plasticity, sandy silt with some angular gravel, greenish grayish brown to brown (10YR 5/3)
46	228	BR	WEATHERED BEDROCK - dry, fissured, low plasticity, sandy silt with some angular gravel, light brownish gray (10YR 6/2)
54	220		BEDROCK - reduced to gravelly sandy silt with trace cobble, wet, fissured, low plasticity, subangular to angular coarse, light gray (10YR 7/1)
54.6	219.4		End of hole

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

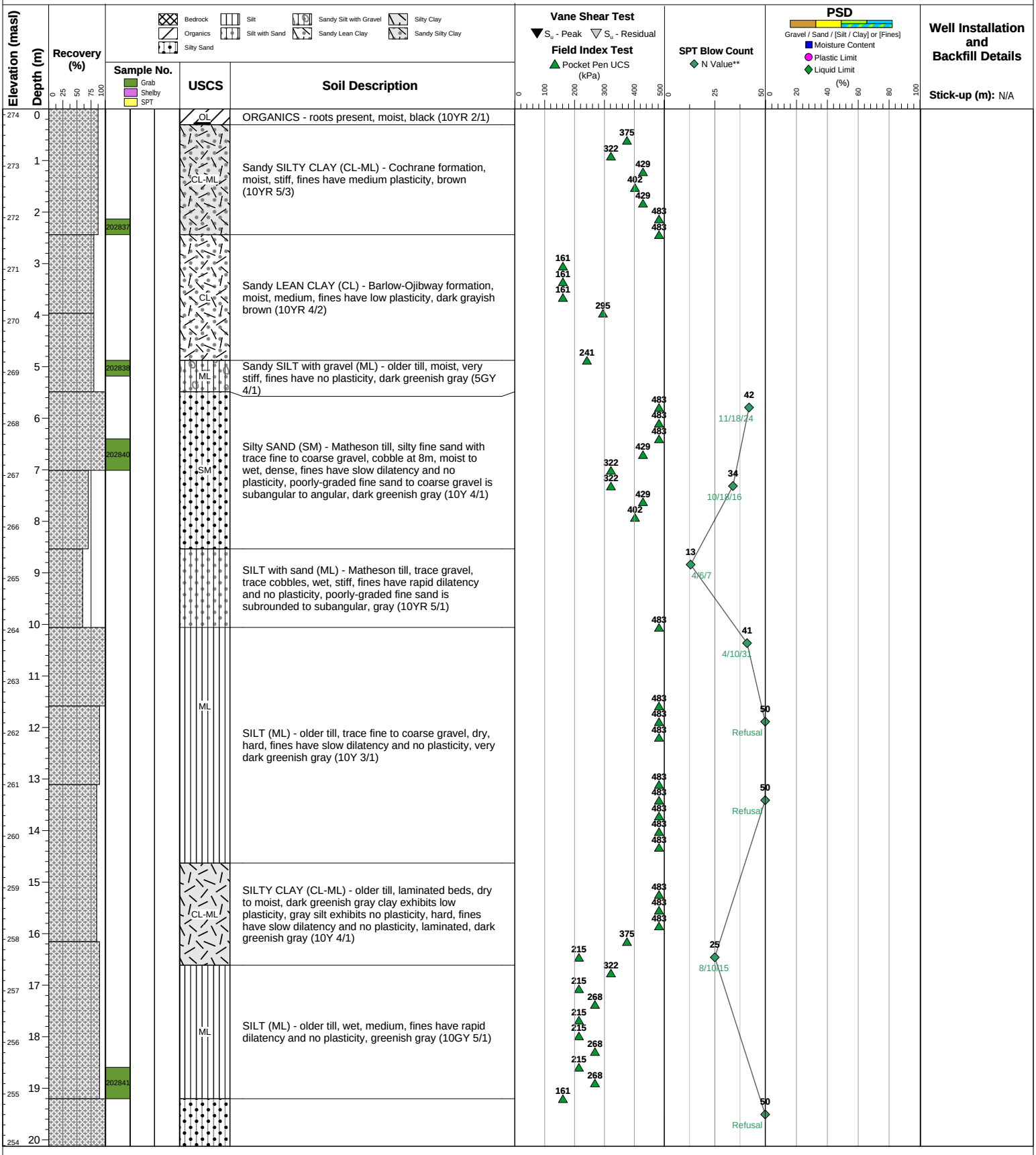
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-202
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 20-Feb-24 **TO:** 21-Feb-24
COORDINATES: 475366.0 E 5408591.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.11
TOTAL DEPTH (m): 25.3
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

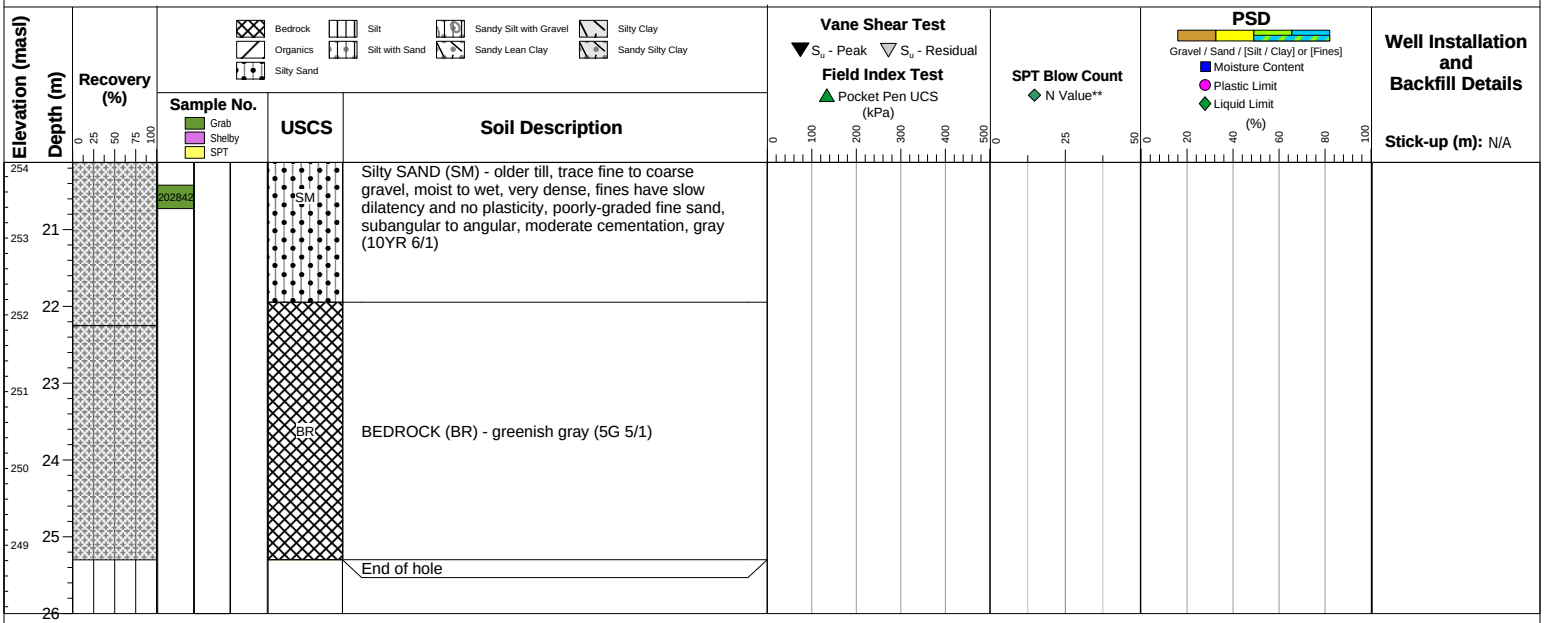
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-202
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 20-Feb-24 **TO:** 21-Feb-24
COORDINATES: 475366.0 E 5408591.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.11
TOTAL DEPTH (m): 25.3
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

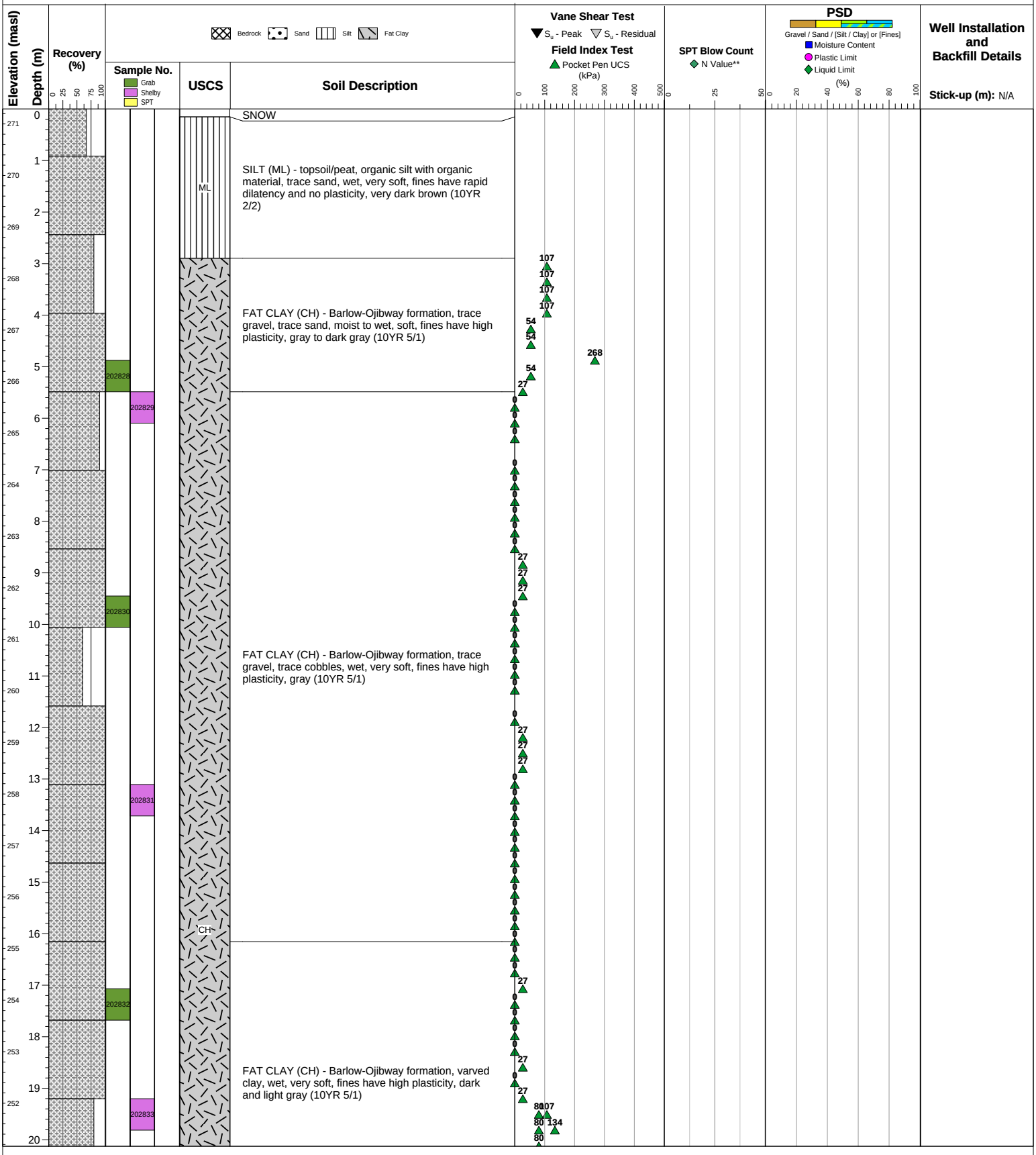
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-203
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 18-Feb-24 **TO:** 19-Feb-24
COORDINATES: 476448.5 E 5409211.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.29
TOTAL DEPTH (m): 40.5
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

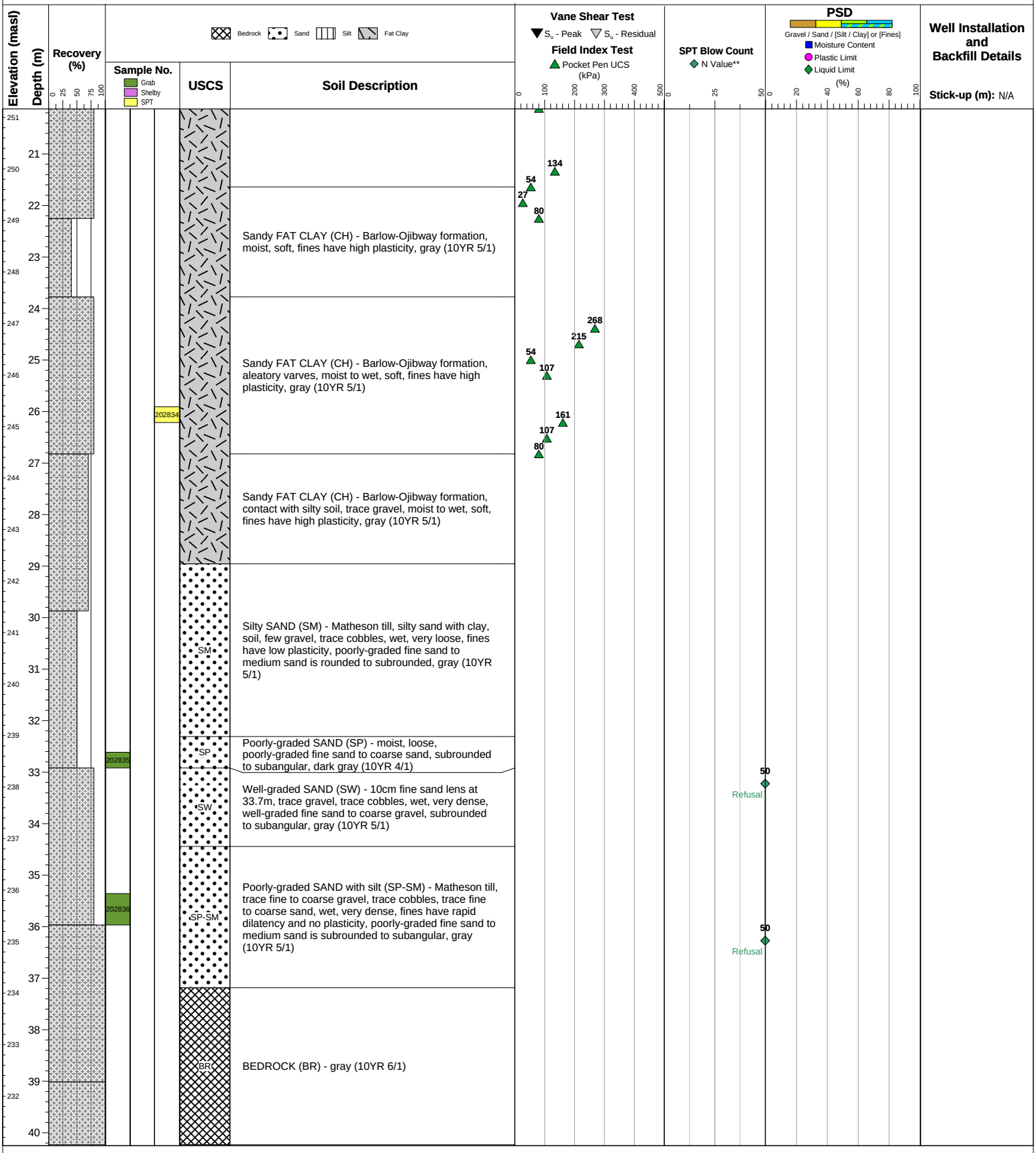
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-203
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 18-Feb-24 **TO:** 19-Feb-24
COORDINATES: 476448.5 E 5409211.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.29
TOTAL DEPTH (m): 40.5
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-203
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 18-Feb-24 **TO:** 19-Feb-24
COORDINATES: 476448.5 E 5409211.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.29
TOTAL DEPTH (m): 40.5
WATER LEVEL (mbgs): N/A

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab / Shelby / SPT)	USCS	Soil Description	Vane Shear Test (S_u - Peak, S_u - Residual) / Field Index Test (Pocket Pen UCS (kPa))	SPT Blow Count (N Value**)	PSD (Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit; (%))	Well Installation and Backfill Details
231	41				End of hole				Stick-up (m): N/A
230	42								

Bedrock, Sand, Silt, Fat Clay

Recovery (%): 0, 25, 50, 75, 100

Vane Shear Test / Field Index Test: 0, 100, 200, 300, 400, 500

SPT Blow Count: 0, 25, 50

PSD (%): 0, 20, 40, 60, 80, 100

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-204
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 23-Feb-24 **TO:** 25-Feb-24
COORDINATES: 475667.1 E 5407347.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.17
TOTAL DEPTH (m): 61.9
WATER LEVEL (mbgs): N/A

Bedrock, Weathered Bedrock, Organics, Boulder, Silty Sand, Silty Sand with Gravel, Silt, Silt with Sand, Sandy Silt, Lean Clay, Lean Clay with Sand, Sandy Lean Clay, Silty Clay, Sandy Silty Clay, Fat Clay

Sample No.: Grab, Shelby, SPT

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details

Stick-up (m): N/A

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
274	0		202852	OL	ORGANICS (OL) - ice/snow presence, moist, brown (10YR 5/3)
273	1				LEAN CLAY with sand (CL) - Cochrane formation, moist, stiff, fines have medium plasticity, brown (10YR 5/3)
272	2				
271	3				LEAN CLAY (CL) - roots present, few sand, moist to wet, soft, fines have low plasticity, brown (10YR 5/3)
270	4			CL	LEAN CLAY (CL) - Cochrane formation, roots present, few sand, moist to wet, soft, fines have low plasticity, gray (10YR 5/1)
269	5				
268	6				
267	7		202853		
266	8				
265	9		202855		
264	10			CH	FAT CLAY (CH) - Barlow-Ojibway formation, varved from 13.1m - 14.6m, trace sand, moist to wet, soft, fines have high plasticity, homogeneous, grayish brown (10YR 5/2)
263	11		202854		
262	12				
261	13		202856		
260	14		202858		
259	15				Sandy LEAN CLAY (CL) - Barlow-Ojibway formation, silt and 2.5cm gravel from 17.1m to 17.7m, presence trace gravel from 17.7m to 19.8m, 7.6cm gravel at 18.9m, moist to wet, very soft, fines have low plasticity, gray (10YR 5/1)
258	16				
257	17			CL	
256	18				
255	19				
	20			ML	SILT (ML) - Matheson till, 7.6cm gravel at 20.1m, dry,

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-204
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 23-Feb-24 **TO:** 25-Feb-24
COORDINATES: 475667.1 E 5407347.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.17
TOTAL DEPTH (m): 61.9
WATER LEVEL (mbgs): N/A

Bedrock, Weathered Bedrock, Organics, Boulder; Silty Sand, Silty Sand with Gravel, Silt, Silt with Sand; Sandy Silt, Lean Clay, Lean Clay with Sand, Sandy Lean Clay; Silty Clay, Sandy Silty Clay, Fat Clay

Sample No.: Grab, Shelby, SPT

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description	Vane Shear Test (kPa)	SPT Blow Count (N Value**)	PSD (%)
254	20				stiff, fines have no plasticity, gray (5Y 5/1) BOULDER - gray (10YR 5/1)			
253	21			ML	SILT (ML) - Matheson till, few gravel, moist, stiff, fines have no plasticity, gray (10YR 5/1)			
252	22							
251	23		202859	CL	LEAN CLAY (CL) - stiff clay from 23.6m to 24.4m, moist, hard, fines have medium plasticity, very dark grayish brown (10YR 3/2)	483, 483, 483		
250	24						50 Refusal	
249	25			CL-ML	SILTY CLAY (CL-ML) - older till, hard fine-grained soil, few sand, dry, hard, fines have medium plasticity, dark gray (10YR 4/1)			
248	26							
247	27				SILT (ML) - older till, few sand, dry, hard, fines have low plasticity, gray (10YR 5/1)		50 Refusal	
246	28							
245	29		202860					
244	30			ML	SILT (ML) - older till, trace fine to coarse sub-rounded gravel at 30.5m, few sand, trace gravel, dry to moist, very stiff, fines have low plasticity, homogeneous, gray (10YR 5/1)		50 Refusal	
243	31							
242	32							
241	33				Sandy SILT (ML) - older till, 10cm sub-angular cobble at 33.5m, angular coarse gravel inclusions appear to be fragments from underlaying bedrock unit, trace gravel, dry to moist, very stiff, fines have low plasticity, poorly-graded fine sand, homogeneous, gray (10YR 5/1)		50 Refusal	
240	34							
239	35		202861					
238	36				Sandy SILT (ML) - old till, stiff to very stiff, trace gravel, dry to moist, very stiff, fines have low plasticity, poorly-graded fine sand is subrounded to subangular, homogeneous, gray (10YR 5/1)	483, 215, 193	50 Refusal	
237	37							
236	38			SM	Silty SAND (SM) - older till, disturbed soil, friable, trace gravel, dry, very dense, fines have medium plasticity, poorly-graded fine sand is subangular to angular, fissured, gray (10YR 5/1)			
235	39						50 Refusal	
234	40				SILT with sand (ML) - older till, trace sub-angular to rounded coarse gravel, friable, 28cm large cobble at			

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-LGE-BH-204
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 23-Feb-24 **TO:** 25-Feb-24
COORDINATES: 475667.1 E 5407347.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.17
TOTAL DEPTH (m): 61.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Weathered Bedrock; Organics; Boulder; Silty Sand; Silty Sand with Gravel; Silt; Silt with Sand; Sandy Silt; Lean Clay; Lean Clay with Sand; Sandy Lean Clay; Silty Clay; Sandy Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
233	41			ML	40.8m, trace gravel, dry, very stiff, fines have medium plasticity, fissured, gray (10YR 5/1)
232	42			ML	SILT with sand (ML) - older till, 18cm pulverized cobble at 43.3m due to drilling, reduced to flour and angular cobble fragments, trace gravel, trace cobbles, dry, hard, fines have medium plasticity, coarse fraction is subangular to angular, fissured, dark gray (10YR 4/1)
231	43			ML	
230	44			CL-ML	SILTY CLAY (CL-ML) - dry, hard, fines have high plasticity, fissured, dark gray (10YR 4/1)
229	45			CL-ML	
228	46			CL-ML	
227	47			CL-ML	
226	48			SM	Silty SAND with gravel (SM) - older till, trace 10cm sub-angular cobble fragments at 48.0m, dry, very stiff, fines have low plasticity, gap-graded fine sand to coarse gravel is subrounded to subangular, fissured, gray (10YR 5/1)
225	49			ML	Sandy SILT (ML) - older till, little cobbles, dry to moist, very stiff, fines have low plasticity, sand is subrounded to subangular, homogeneous, gray (10YR 5/1)
224	50			ML	
223	51			ML	
222	52		202862	SM	Silty SAND (SM) - older till, trace 7.6cm gravel at 53.3m, dry to moist, dense, fines have no plasticity, poorly-graded fine sand, homogeneous, gray (10YR 5/1)
221	53		202862	SM	
220	54		202862	SM	
219	55			SM	
218	56			SM	
217	57			SM	
216	58			CL-ML	Sandy SILTY CLAY (CL-ML) - older till, few gravel, dry to moist, stiff, fines have medium plasticity, fine sand, homogeneous, gray (10YR 5/1)
215	59			BR	WEATHERED BEDROCK (BR) - pulverized rock, degradated to fine sand with gravel, dry, homogeneous, light gray (10YR 7/1)
214	60			BR	

Well Installation and Backfill Details
Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

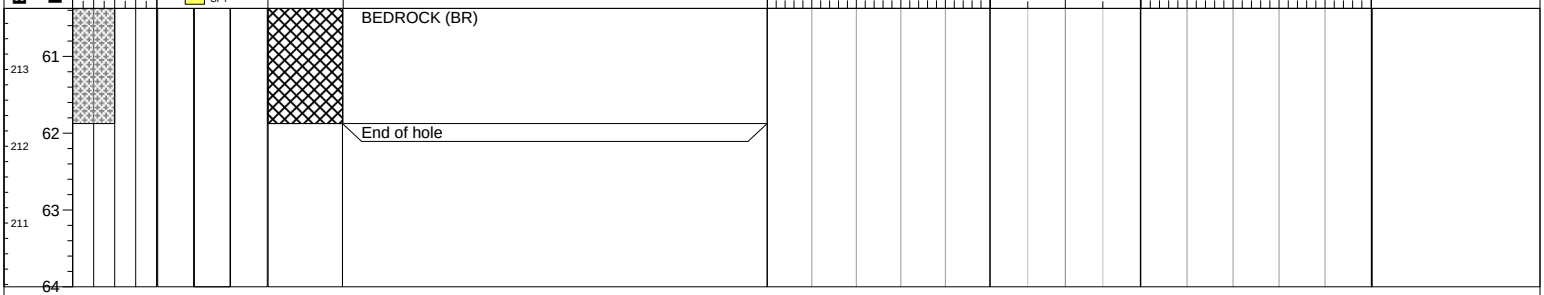
DRILLHOLE ID: SRK24-LGE-BH-204
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Parker Tully

DRILLING DATE: 23-Feb-24 **TO:** 25-Feb-24
COORDINATES: 475667.1 E 5407347.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 274.17
TOTAL DEPTH (m): 61.9
WATER LEVEL (mbgs): N/A

Bedrock; Weathered Bedrock; Organics; Boulder; Silty Sand; Silty Sand with Gravel; Silt; Silt with Sand; Sandy Silt; Lean Clay; Lean Clay with Sand; Sandy Lean Clay; Silty Clay; Sandy Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)



Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-LGE-BH-205
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 17-Feb-24 **TO:** 18-Feb-24
COORDINATES: 476457.1 E 5408412.6 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.76
TOTAL DEPTH (m): 28.3
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock | Sandy Silt | Lean Clay | Fat Clay | Silt

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab / Shelby / SPT)	USCS	Soil Description
271	0			ML	SILT (ML) - topsoil/peat, organic silt with roots and organic matter, few sand, frozen, soft, fines have rapid dilatency and no plasticity, well-graded fine sand to coarse sand, rounded to subrounded, very dark brown (10YR 2/2)
269	2		202820	CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist, medium, fines have high plasticity, gray (10YR 5/1)
268	3				FAT CLAY (CH) - Barlow-Ojibway formation, trace fine to coarse sand, trace fine gravel, moist, medium, fines have high plasticity, gray (10YR 5/1)
267	4		202821		
266	5				FAT CLAY (CH) - Barlow-Ojibway formation, trace fine to coarse sand, trace fine to coarse gravel, wet, very soft, fines have high plasticity, gray (10YR 5/1)
265	6		202822		
264	7				
263	8		202823		
262	9				
261	10				
260	11				
259	12				
258	13				
257	14		202824		
256	15				
255	16		202825		FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, wet, very soft, fines have high plasticity, light and dark gray (10YR 5/1)
254	17				
253	18				
252	19				FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, wet, light gray is soft to medium stiffness with
	20				

Vane Shear Test
S_u - Peak ▽ S_u - Residual

Field Index Test
Pocket Pen UCS (kPa)

SPT Blow Count
N Value**

PSD
Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%)

Well Installation and Backfill Details
Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

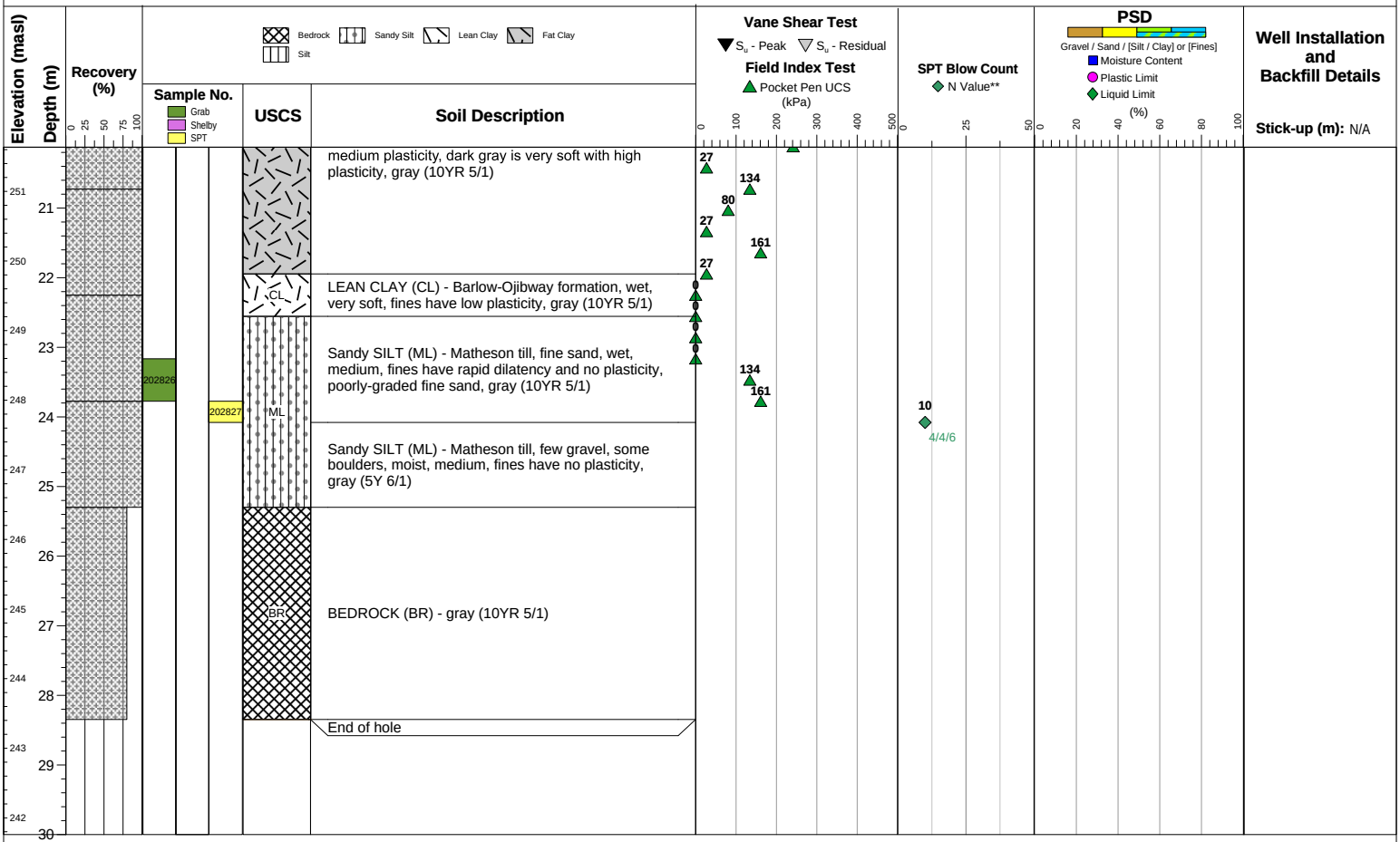
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-LGE-BH-205
LOCATION: East Stockpile
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Erick Lino/Michael Stephens

DRILLING DATE: 17-Feb-24 **TO:** 18-Feb-24
COORDINATES: 476457.1 E 5408412.6 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 271.76
TOTAL DEPTH (m): 28.3
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

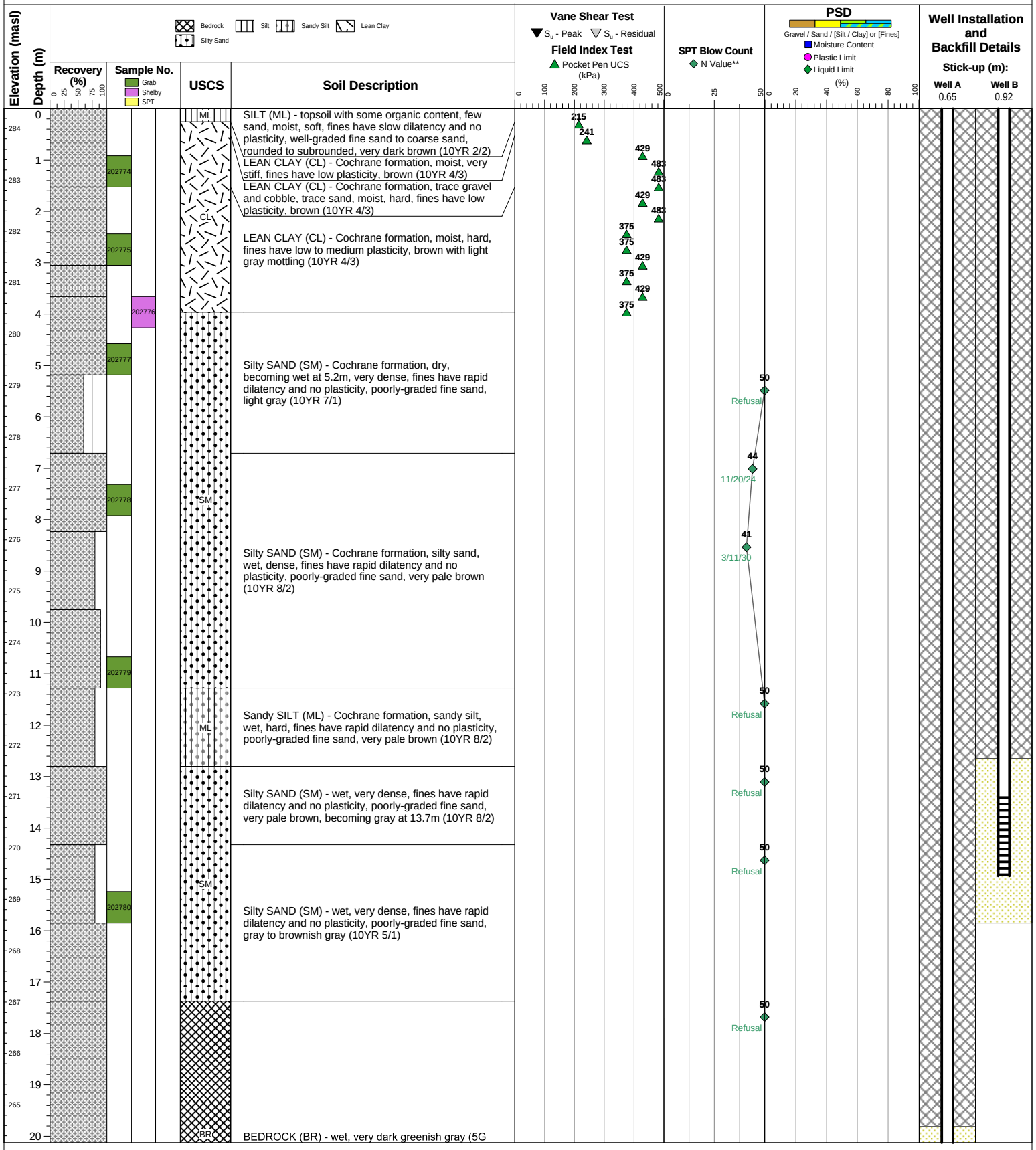
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW11AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 08-Feb-24 **TO:** 09-Feb-24
COORDINATES: 471215.2 E 5402249.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 284.39
TOTAL DEPTH (m): 22.6
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand | Bentonite | PVC | Screen

srk consulting

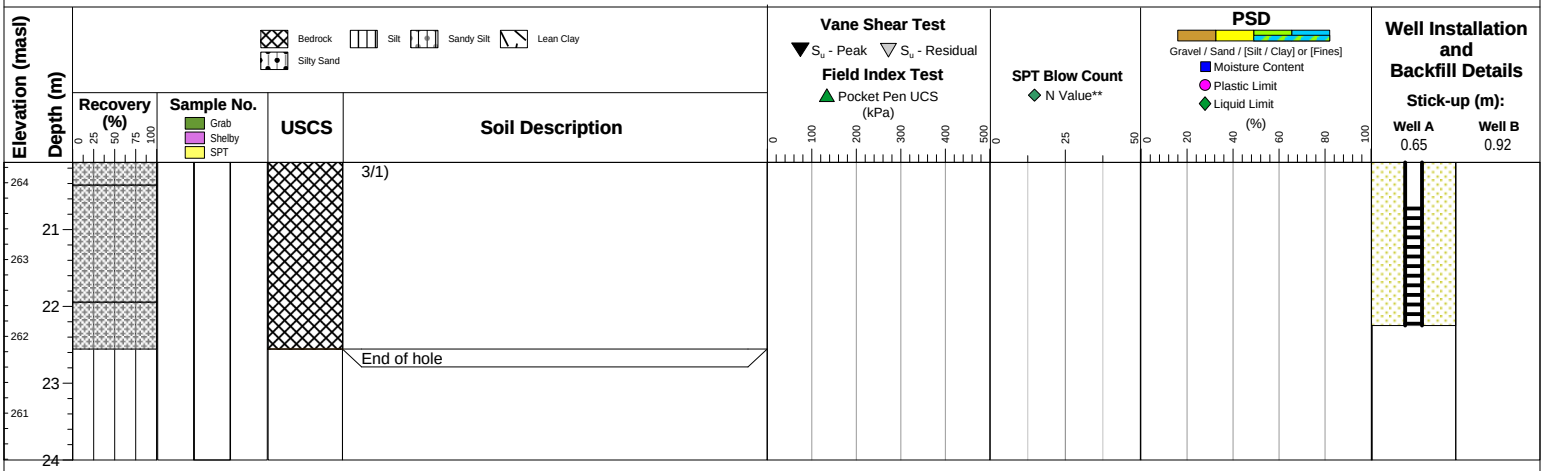
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW11AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 08-Feb-24 **TO:** 09-Feb-24
COORDINATES: 471215.2 E 5402249.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 284.39
TOTAL DEPTH (m): 22.6
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

Sand Bentonite PVC Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW-12AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 06-Feb-24 **TO:** 07-Feb-24
COORDINATES: 471077.2 E 5405237.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.93
TOTAL DEPTH (m): 32.6
WATER LEVEL (mbgs): 4.7

Bedrock; Well Graded Gravel; Poorly Graded Gravel with Sand; Poorly Graded Gravel with Silt and Sand; Well Graded Sand; Well Graded Sand with Gravel; Poorly Graded Sand with Gravel; Silty Sand; Poorly Graded Sand with Silt and Gravel; Clayey Sand; Silt; Sandy Silt; Lean Clay; Fat Clay

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): Well A*** 0.83; Well B 1.04

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
272	0			ML / CH	SILT (ML) - topsoil with some organics, rootlets, moss, and twigs, few sand, frozen, stiff, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
272	1		202762	CH	FAT CLAY (CH) - Cochrane formation, few sand, wet, stiff, fines have high plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
271	2		202763	CL	LEAN CLAY (CL) - Cochrane formation, moist, hard, fines have low plasticity, yellowish brown (10YR 5/4)
270	3			CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist, medium, fines have high plasticity, dark gray (10YR 4/1)
269	4		202764	CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist to wet, soft, fines have high plasticity, dark gray (10YR 4/1)
268	5		202765	CH	FAT CLAY (CH) - Barlow-Ojibway formation, faintly varved, moist to wet, soft, fines have high plasticity, dark gray (10YR 4/1)
267	6			CH	FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, moist to wet, dark gray is soft, light gray is medium stiffness, fines have high plasticity, dark and light gray (10YR 4/1)
266	7		202766	CH	FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, moist to wet, dark gray is soft, light gray is medium stiffness, fines have high plasticity, dark and light gray (10YR 4/1)
265	8			SC	Clayey SAND (SC) - Barlow-Ojibway formation, moist, medium dense, fines have slow dilatency and no plasticity, poorly-graded fine sand to medium sand, dark gray (10YR 4/1)
264	9			CH	FAT CLAY (CH) - Barlow-Ojibway formation, presumably varved, wet, soft, fines have high plasticity, dark gray (10YR 4/1)
263	10			CH	FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, trace fine to medium sand, wet, dark gray is soft, light gray is medium stiffness, fines have high plasticity, dark and light gray (10YR 4/1)
262	11		202767	CH	
261	12			SW	Well-graded SAND with gravel (SW) - Matheson till, wet, medium dense, well-graded fine sand to coarse gravel, rounded to subrounded, dark gray (10YR 4/1)
260	13			GW	Well-graded SAND (SW) - Matheson till, wet, medium dense, well-graded fine sand to coarse sand, subangular to angular, dark gray (10YR 4/1)
259	14		202768	ML / SM	Well-graded GRAVEL (GW) - Matheson till, trace sand, wet, medium dense, well-graded coarse sand to coarse gravel, subrounded to subangular, dark gray (10YR 4/1)
258	15			GP-GM	Sandy SILT (ML) - Matheson till, few gravel, wet, stiff, fines have rapid dilatency and no plasticity, well-graded fine sand to coarse gravel, subrounded, dark gray (10YR 4/1)
257	16		202769	ML	Silty SAND (SM) - Matheson till, wet, medium dense, fines have rapid dilatency and no plasticity, poorly-graded fine sand, dark gray (10YR 4/1)
256	17			SM	Poorly-graded GRAVEL with silt and sand (GP-GM) - trace cobbles, wet, dense, fines have rapid dilatency and no plasticity, poorly-graded fine sand to coarse gravel, subrounded to subangular, gray (10YR 6/1)
255	18		202770	GP-GM	Sandy SILT (ML) - trace gravel, wet, medium, fines have low plasticity, poorly-graded medium sand to coarse sand is subangular, lensed, gray (10YR 6/1)
254	19				Silty SAND (SM) - few gravel, wet, medium dense, fines have slow dilatency and no plasticity, poorly-graded fine sand to fine gravel, subrounded to subangular, weak cementation, light brownish gray (10YR 6/2)
253	20				Poorly-graded GRAVEL with silt and sand (GP-GM) - wet, medium dense, fines have slow dilatency and no plasticity, poorly-graded fine sand to coarse gravel, subangular, weak cementation, gray (10YR 6/1)

SPT N Value**: 8 (4/4/4); 18 (7/9/9); 50 (Refusal); 30 (5/13/17); 21 (16/10/11)

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50
*** Natural sands collapsed from 29.3 - 30.5m in Well A

Well Installation Details
Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW-12AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 06-Feb-24 **TO:** 07-Feb-24
COORDINATES: 471077.2 E 5405237.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.93
TOTAL DEPTH (m): 32.6
WATER LEVEL (mbgs): 4.7

Bedrock; Well Graded Gravel; Poorly Graded Gravel with Sand; Poorly Graded Gravel with Silt and Sand; Well Graded Sand; Well Graded Sand with Gravel; Poorly Graded Sand with Gravel; Silty Sand; Poorly Graded Sand with Silt and Gravel; Clayey Sand; Silt; Sandy Silt; Lean Clay; Fat Clay

Sample No.: Grab, Shelby, SPT

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): Well A*** 0.83; Well B 1.04

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
252–251	21–22		202771	SM	Silty SAND (SM) - wet, medium dense, fines have rapid dilatency and no plasticity, poorly-graded fine sand to coarse sand, subrounded, weak cementation, light brownish gray (10YR 6/2)
250–249	23–24				
248–247	25–26		202772	SP-SM	Poorly-graded SAND with silt and gravel (SP-SM) - wet, medium dense, poorly-graded medium sand to coarse gravel, subangular, weak cementation, very pale brown (10YR 7/3)
246–245	27–28			GP	Poorly-graded GRAVEL with sand (GP) - trace cobbles, wet, medium dense, poorly-graded coarse sand to coarse gravel, subrounded, very dark gray (10YR 3/1)
244–243	29–30		202773	SP	Poorly-graded SAND with gravel (SP) - trace fines, wet, medium dense, poorly-graded fine sand to coarse gravel, subrounded, weak cementation, gray (10YR 5/1)
242–241	31–32			BR	BEDROCK (BR) - dry, gray (10YR 6/1)
240–239	33–34				End of hole

SPT Blow Count: 21 (14/14/7); 7 (2/3/4); 21 (3/13/8)

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50
*** Natural sands collapsed from 29.3 - 30.5m in Well A

Well Installation Details: Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW13AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 03-Feb-24 **TO:** 06-Feb-24
COORDINATES: 470682.8 E 5406375.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 270.98
TOTAL DEPTH (m): 80.8
WATER LEVEL (mbgs): N/A

No Recovery; Bedrock; Well Graded Sand; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Silt; Sandy Silt; Sandy Silt with Gravel; Lean Clay; Fat Clay

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab / Shelby / SPT)	USCS	Soil Description
270	0			ML	SILT (ML) - topsoil, few sand, frozen, medium, fines have low plasticity, poorly-graded fine sand to coarse sand, very dark brown (10YR 2/2)
269	1		202696	CL	LEAN CLAY (CL) - Cochrane formation, little silt, trace sand, moist to wet, very stiff, fines have low plasticity, very dark gray, light yellowish gray at 0.8m, grayish brown at 2.1m (10YR 3/1)
268	2		202697, 202698		
267	3		202699	ML	SILT (ML) - organic with visible rootlets, moist to wet, soft, fines have no plasticity, very dark brown (10YR 2/2)
266	4		202700		
265	5				
264	6		202751	CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist to wet, stiff, fines have high plasticity, dark gray (10YR 4/1)
263	7				
262	8				
261	9				
260	10				
259	11		202752		
258	12				
257	13				
256	14		202753		
255	15				FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, wet, dark gray is soft, light gray is medium stiffness, fines have high plasticity, dark gray (10YR 4/1)
254	16				
253	17				
252	18		202754		
251	19				
	20		202755		

Vane Shear Test (S_u - Peak, S_u - Residual)
Field Index Test — Pocket Pen UCS (kPa)
SPT Blow Count — N Value**
PSD — Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m):
Well A: 0.67
Well B: 1.02

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW13AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 03-Feb-24 **TO:** 06-Feb-24
COORDINATES: 470682.8 E 5406375.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 270.98
TOTAL DEPTH (m): 80.8
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

No Recovery; Bedrock; Well Graded Sand; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Silt; Sandy Silt; Sandy Silt with Gravel; Lean Clay; Fat Clay

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): Well A 0.67; Well B 1.02

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
250	21				Silty SAND (SM) - Matheson till, wet, medium dense, fines have rapid dilatency and no plasticity, poorly-graded fine sand, gray (10YR 5/1)
249	22				
248	23				
247	24				
246	25				
245	26				
244	27		202756	SM	
243	28				
242	29				Silty SAND (SM) - Matheson till, wet, loose, fines have slow dilatency and no plasticity, poorly-graded fine sand to medium sand, rounded, homogeneous, weak cementation, gray (10YR 5/1)
241	30				
240	31				
239	32				
238	33		202757		
237	34				
236	35				
235	36		202758	ML	Sandy SILT (ML) - Matheson till, wet, soft, fines have slow dilatency and no plasticity, poorly-graded fine sand to fine sand, rounded, homogeneous, dark gray (10YR 4/1)
234	37				Silty SAND (SM) - Matheson till, moist to wet, loose, fines have rapid dilatency and no plasticity, gap-graded fine sand to fine sand, rounded, homogeneous, moderate cementation, dark gray (10YR 4/1)
233	38				
232	39		202759		
231	40				

SPT Blow Count (N Value**): 15 (8/8/7); 7 (3/3/4); 34 (4/6/28); 14 (3/6/8); 13 (7/8/5); 34 (2/8/26)

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details: Sand; Bentonite; PVC; Screen

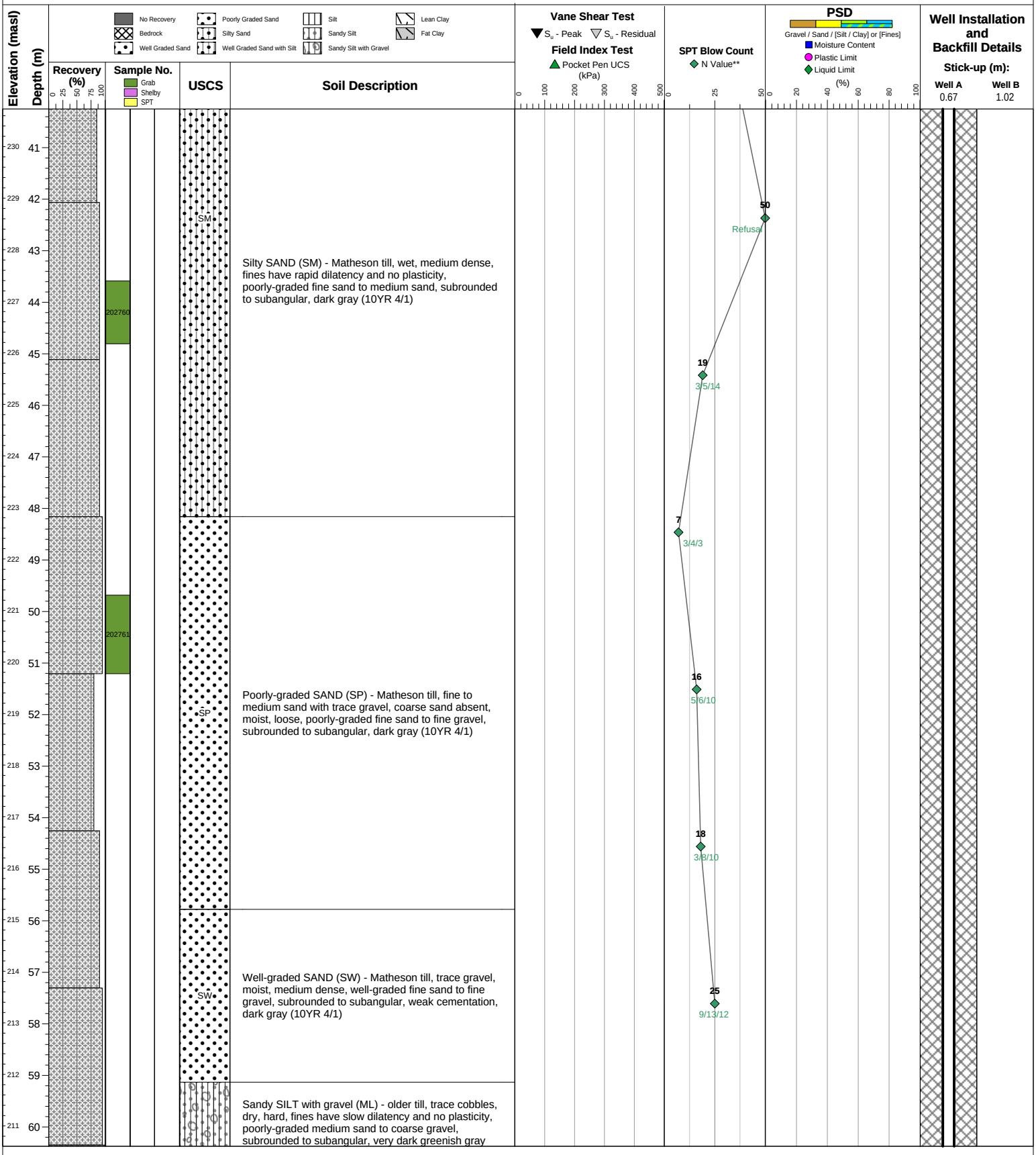
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW13AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 03-Feb-24 **TO:** 06-Feb-24
COORDINATES: 470682.8 E 5406375.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 270.98
TOTAL DEPTH (m): 80.8
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand | Bentonite | PVC | Screen

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW13AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 03-Feb-24 **TO:** 06-Feb-24
COORDINATES: 470682.8 E 5406375.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 270.98
TOTAL DEPTH (m): 80.8
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

No Recovery; Bedrock; Well Graded Sand; Poorly Graded Sand; Silty Sand; Well Graded Sand with Silt; Silt; Sandy Silt; Sandy Silt with Gravel; Lean Clay; Fat Clay

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
					(5G 3/1)
210	61			ML	SILT (ML) - older till, few sand, trace cobbles, dry, hard, fines have low plasticity, poorly-graded fine sand to coarse sand, subangular, yellow (10YR 8/8)
209	62				
208	63				
207	64				
206	65				
205	66				
204	67				
203	68			BR	BEDROCK (BR) - wet, dark olive gray (5Y 3/2)
202	69				NO RECOVERY - no sample retrieved, likely washed away, suspected weathered bedrock
201	70				
200	71				
199	72				
198	73			ML	SILT (ML) - weathered bedrock, trace gravel, trace sand, trace cobbles, moist, hard, fines have slow dilatency and no plasticity, olive gray (5Y 4/2)
				SW-SM	Well-graded SAND with silt (SW-SM) - bedrock, few gravel, trace cobbles, dry, loose, fines have no plasticity, well-graded fine sand to coarse gravel is angular, olive gray (5Y 4/2)
197	74				
196	75				
195	76				
194	77			BR	BEDROCK (BR) - dark olive gray (5Y 3/2)
193	78				
192	79				
191	80				

Well Installation and Backfill Details
Stick-up (m):
Well A: 0.67
Well B: 1.02

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand; Bentonite; PVC; Screen

srk consulting

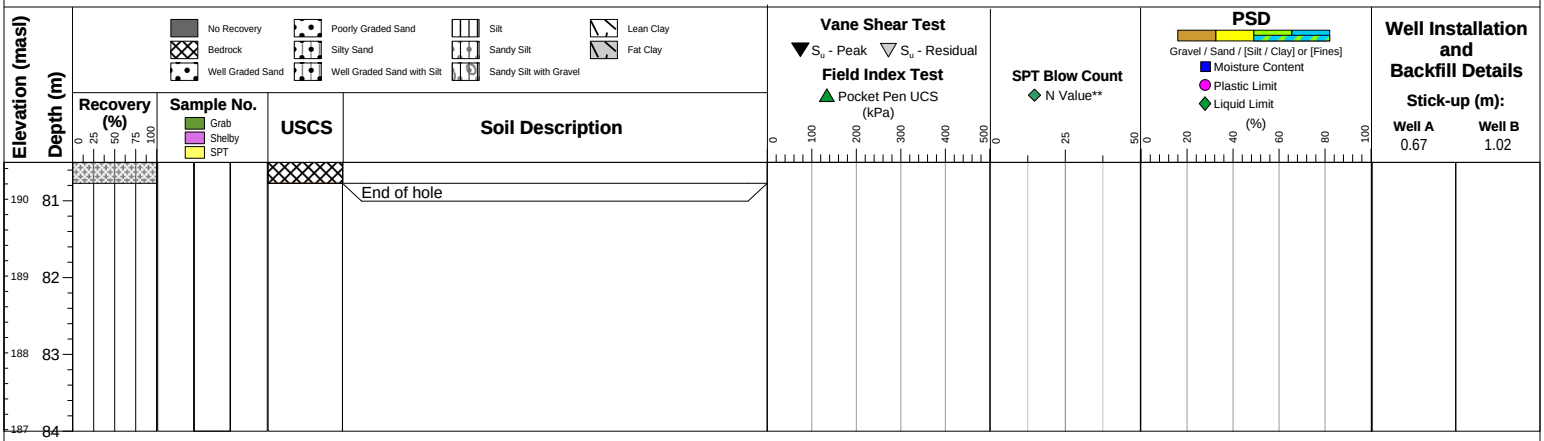
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW13AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 03-Feb-24 **TO:** 06-Feb-24
COORDINATES: 470682.8 E 5406375.9 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 270.98
TOTAL DEPTH (m): 80.8
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

Sand Bentonite PVC Screen

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW14AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 09-Feb-24 **TO:** 11-Feb-24
COORDINATES: 466776.2 E 5407468.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.36
TOTAL DEPTH (m): 42.1
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Well Graded Sand; Poorly Graded Sand; Well Graded Sand with Silt; Silt; Silt with Sand; Sandy Silt with Gravel; Lean Clay; Sandy Lean Clay; Gravelly Lean Clay; Fat Clay; Fat Clay with Sand

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
276	0			ML	SNOW
				SW-SM	SILT (ML) - some organics and rootlets, trace gravel, trace sand, moist, medium, fines have slow dilatency and no plasticity, dark grayish brown (10YR 4/2)
275	1			SP	Well-graded SAND with silt (SW-SM) - trace gravel, dry, loose, fines have rapid dilatency and no plasticity, well-graded fine sand to fine gravel, rounded to subrounded, dark grayish brown (10YR 4/2)
274	2			CL	Poorly-graded SAND (SP) - trace gravel and fine gravel, dry, loose, poorly-graded fine sand to medium sand, rounded to subrounded, very pale brown (10YR 8/2)
273	3		202781	ML	LEAN CLAY (CL) - Cochrane formation, trace gravel and fine gravel, moist, very stiff, fines have low plasticity, brown (10YR 5/3)
				CL	
272	4		202782	SW	SILT (ML) - peat with decomposing wood fragments, moist, soft, fines have rapid dilatency and no plasticity, black (10YR 2/1)
271	5		202783		LEAN CLAY (CL) - Cochrane formation, moist, very stiff, fines have low plasticity, brown (10YR 4/3)
270	6				Sandy LEAN CLAY (CL) - Cochrane formation, moist, medium, fines have low plasticity, poorly-graded fine sand to medium sand, rounded to subrounded, brown (10YR 5/3)
269	7				Well-graded SAND (SW) - Matheson till, dry, loose, well-graded fine sand to fine gravel, subrounded to subangular, light gray (10YR 7/2)
268	8		202784		FAT CLAY (CH) - Barlow-Ojibway formation, trace cobbles, moist to wet, very soft, fines have high plasticity, gray (10YR 5/1)
267	9				
266	10			CH	FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, moist to wet, light gray is very soft, dark gray is medium stiffness, fines have high plasticity, light and dark gray (10YR 5/1)
265	11				
264	12		202785		FAT CLAY (CH) - Barlow-Ojibway formation, possibly varved with no variation in strength, trace cobbles, wet, very soft, fines have high plasticity, gray (10YR 5/1)
263	13				
262	14				FAT CLAY (CH) - Barlow-Ojibway formation, varved with no variation in strength, trace cobbles, wet, very soft, fines have high plasticity, gray (10YR 5/1)
261	15		202786		FAT CLAY with sand (CH) - Barlow-Ojibway formation, clayey silt with some sand and trace fine gravel, wet, very soft, fines have high plasticity, poorly-graded fine sand to fine gravel, gray (10YR 5/1)
260	16				
259	17				
258	18				
257	19				
	20				

Vane Shear Test values: 295, 295, 161, 402, 483, 402
Pocket Pen UCS (kPa) values: 27, 27, 27, 54, 27, 27, 27, 54, 54, 54, 54, 161, 107, 161, 27, 27, 30, 27, 27, 27
SPT N Value**: 9 (4/3/6), 2 (1/1/1)

Well Installation and Backfill Details
Stick-up (m): Well A 0.80; Well B 1.11

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW14AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 09-Feb-24 **TO:** 11-Feb-24
COORDINATES: 466776.2 E 5407468.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.36
TOTAL DEPTH (m): 42.1
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Well Graded Sand; Poorly Graded Sand; Well Graded Sand with Silt; Silt; Silt with Sand; Sandy Silt with Gravel; Lean Clay; Sandy Lean Clay; Gravelly Lean Clay; Fat Clay; Fat Clay with Sand

Recovery (%) | Sample No. (Grab, Shelby, SPT) | USCS | Soil Description

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): Well A 0.80, Well B 1.11

Depth (m)	Elevation (masl)	Sample No.	USCS	Soil Description
0 – 21	256 – 255	202787	ML	Sandy SILT with gravel (ML) - Barlow-Ojibway formation, clayey silt, wet, very soft, fines have low plasticity, poorly-graded fine sand to medium sand, rounded, gray (10YR 6/1)
21 – 22	255 – 254	202788	ML	Sandy SILT with gravel (ML) - Barlow-Ojibway formation, clayey silt, wet, very soft, fines have low plasticity, poorly-graded fine sand to medium sand, rounded, gray (10YR 6/1)
22 – 25	254 – 251	202788	ML	Sandy SILT with gravel (ML) - Barlow-Ojibway formation, clayey silt, wet, very soft, fines have low plasticity, poorly-graded fine sand to medium sand, rounded, gray (10YR 6/1)
25 – 26	251 – 250	202788	ML	Sandy SILT with gravel (ML) - Barlow-Ojibway formation, clayey silt, wet, very soft, fines have low plasticity, poorly-graded fine sand to medium sand, rounded, gray (10YR 6/1)
26 – 26.5	250 – 249.5	202789	CL	Sandy LEAN CLAY (CL) - Barlow-Ojibway formation, few gravel, trace cobbles, moist, stiff, fines have medium plasticity, poorly-graded fine sand to coarse sand, rounded to subrounded, gray (10YR 5/1)
26.5 – 28	249.5 – 248	202789	ML	Sandy SILT with gravel (ML) - presumably Matheson till, trace cobbles, wet, very soft, fines have medium plasticity, poorly-graded fine sand to coarse sand, subrounded, gray (10YR 5/1)
28 – 29	248 – 247	202790	ML	Sandy SILT with gravel (ML) - presumably Matheson till, trace cobbles, wet, very soft, fines have medium plasticity, poorly-graded fine sand to coarse sand, subrounded, gray (10YR 5/1)
29 – 33	247 – 243	202791	ML	Gravelly LEAN CLAY (CL) - presumably older till, few sand, trace cobbles, moist, hard, fines have low plasticity, poorly-graded fine sand to coarse sand, subangular, dark gray (10YR 4/1)
33 – 34	243 – 242	202791	CL	Gravelly LEAN CLAY (CL) - presumably older till, few sand, trace cobbles, moist, hard, fines have low plasticity, poorly-graded fine sand to coarse sand, subangular, dark gray (10YR 4/1)
34 – 35	242 – 241	202792	CL	LEAN CLAY (CL) - Barlow-Ojibway formation, varved clay, moist, very stiff, fines have medium plasticity, stratified, light and dark gray (10YR 6/1)
35 – 36	241 – 240	202792	CL	LEAN CLAY (CL) - Barlow-Ojibway formation, varved clay, moist, very stiff, fines have medium plasticity, stratified, light and dark gray (10YR 6/1)
36 – 37	240 – 239	202792	CL	LEAN CLAY (CL) - Barlow-Ojibway formation, varved clay, moist, very stiff, fines have medium plasticity, stratified, light and dark gray (10YR 6/1)
37 – 38	239 – 238	202793	CL	LEAN CLAY (CL) - few sand, wet, medium, fines have medium plasticity, poorly-graded fine sand to fine sand, rounded, homogeneous, gray (10YR 6/1)
38 – 39	238 – 237	202793	ML	LEAN CLAY (CL) - varved clay, moist to wet, stiff, fines have medium plasticity, stratified, gray (10YR 5/1)
39 – 40	237 – 236		ML	SILT with sand (ML) - older till, trace gravel, few cobbles, dry to moist, hard, fines have low plasticity, poorly-graded fine sand to medium sand, subrounded to subangular, homogeneous, dark gray (10YR 4/1)
40 – 42.1	236 – 234			BEDROCK (BR) - naturally fractured, wet, black

Vane Shear Test values: 0, 0, 0, 0, 0, 0, 0, 0, 21, 21, 27
SPT Blow Count values: 375, 375, 483, 483, 483, 483, 483, 402
PSD: Moisture Content, Plastic Limit, Liquid Limit

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details: Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW14AB
LOCATION: Monitoring Wells
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens

DRILLING DATE: 09-Feb-24 **TO:** 11-Feb-24
COORDINATES: 466776.2 E 5407468.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.36
TOTAL DEPTH (m): 42.1
WATER LEVEL (mbgs): N/A

Bedrock; Well Graded Sand; Poorly Graded Sand; Well Graded Sand with Silt; Silt; Silt with Sand; Sandy Silt with Gravel; Lean Clay; Sandy Lean Clay; Gravelly Lean Clay; Fat Clay; Fat Clay with Sand

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab, Shelby, SPT)	USCS	Soil Description
236	41			BR	(10YR 2/1) BEDROCK (BR) - naturally fractured, wet, very dark greenish gray (10Y 3/1)
235					
234	42				End of hole
233	43				
	44				

Vane Shear Test (S_u - Peak, S_u - Residual)
Field Index Test — Pocket Pen UCS (kPa): 0, 100, 200, 300, 400, 500
SPT Blow Count — N Value**: 0, 25, 50
PSD — Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit; (%): 0, 20, 40, 60, 80, 100

Well Installation and Backfill Details
Stick-up (m):

Well A	Well B
0.80	1.11

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-TMF-BH-202A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 18-Mar-24 **TO:** 19-Mar-24
COORDINATES: 476821.6 E 5404208.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 275.8
TOTAL DEPTH (m): 39.0
WATER LEVEL (mbgs): N/A

Bedrock; Organics; Silty Sand; Silty Sand with Gravel; Silt; Silt with Sand; Sandy Silt; Silt with Gravel; Lean Clay with Gravel; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl) / Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
0				SNOW
1			OL	ORGANICS (OL) - peat, frozen, black (10YR 2/1)
2		275986, 275987	CL	LEAN CLAY with gravel (CL) - Cochrane formation, frozen, medium, fines have low plasticity, poorly-graded fine gravel to fine gravel is subangular, homogeneous, brown (10YR 4/3)
3		275988	CH	FAT CLAY (CH) - Barlow-Ojibway formation, moist, very soft, fines have low plasticity, homogeneous, dark gray (10YR 4/1)
6		275989		FAT CLAY (CH) - Barlow-Ojibway formation, few sand, trace gravel, moist, very soft, fines have medium plasticity, gap-graded fine sand to fine gravel is subrounded to subangular, dark gray (10YR 4/1)
8		275990		FAT CLAY (CH) - Barlow-Ojibway formation, few sand, trace gravel, moist, soft, fines have high plasticity, gap-graded fine sand to coarse sand is subrounded, dark gray (10YR 4/1)
10		275991		FAT CLAY (CH) - Barlow-Ojibway formation, few sand, moist, soft, fines have medium plasticity, gap-graded fine sand to medium sand is subrounded to subangular, dark gray (10YR 4/1)
12		275992		
14		275993		FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, few sand, moist, soft, fines have high plasticity, gap-graded fine sand to fine sand is rounded to subrounded, stratified, dark gray (10YR 4/1)
15		275994		
17		275995		
18		275996		
20				

SPT Blow Count: N Value**

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-TMF-BH-202A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 18-Mar-24 **TO:** 19-Mar-24
COORDINATES: 476821.6 E 5404208.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 275.9
TOTAL DEPTH (m): 39.0
WATER LEVEL (mbgs): N/A

Bedrock; Organics; Silty Sand; Silty Sand with Gravel; Silt; Silt with Sand; Sandy Silt; Silt with Gravel; Lean Clay with Gravel; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Depth (m)	Elevation (masl)	Recovery (%)	Sample No.	USCS	Soil Description
21	255		275997		
22	254			ML	SILT with gravel (ML) - Barlow-Ojibway formation, wet, soft, fines have medium plasticity, poorly-graded coarse gravel to coarse gravel is subangular, homogeneous, gray (10YR 6/1)
23	253				
24	252		275998	SM	Silty SAND with gravel (SM) - Matheson Till, wet, very soft, fines have low plasticity, poorly-graded coarse sand to fine gravel is subrounded, homogeneous, gray (10YR 6/1)
25	251		275999		
26	250			ML	Sandy SILT (ML) - Matheson Till, wet, soft, fines have low plasticity, poorly-graded medium sand to medium sand is rounded, homogeneous, gray (10YR 6/1)
27	249		276000	SM	Silty SAND (SM) - Matheson Till, wet, very loose, fines have slow dilatency and no plasticity, poorly-graded medium sand to coarse sand is rounded, light gray (10YR 7/1)
28	248			ML	Sandy SILT (ML) - Matheson Till, wet, soft, fines have low plasticity, poorly-graded medium sand to coarse sand is rounded, light gray (10YR 7/1)
29	247		275351	SM	Silty SAND (SM) - Matheson Till, few gravel, wet, loose, fines have rapid dilatency and no plasticity, poorly-graded fine sand to coarse sand is rounded, weak cementation, light gray (10YR 7/1)
30	246		275352	SM	Silty SAND with gravel (SM) - Matheson Till, unit with fines/sand mixtures, frozen, very soft, fines have low plasticity, poorly-graded fine sand to coarse sand is subrounded, lensed, light gray (10YR 7/1)
31	245		275353	ML	SILT (ML) - older till, few sand, trace gravel, dry, very stiff, fines have low plasticity, gap-graded fine sand to coarse sand is rounded to subrounded, dark gray (10YR 4/1)
32	244				
33	243				
34	242		275354	SM	Silty SAND with gravel (SM) - older till, trace cobbles, moist, dense, fines have low plasticity, well-graded fine sand to coarse gravel is subrounded, gray (10YR 5/1)
35	241				
36	240			ML	SILT with sand (ML) - older till, silty sand from 36.0m to 36.3m, trace gravel, dry, very stiff, fines have low plasticity, gap-graded fine sand to fine gravel is subrounded, gray (10YR 5/1)
37	239			BR	BEDROCK (BR) - dry, dark gray (10YR 4/1)
38	238				
39	237				End of hole
40	236				

SPT Blow Count: 50 Refusal; 50 Refusal

Well Installation and Backfill Details
Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details: Sand; Bentonite; PVC; Screen

srk consulting

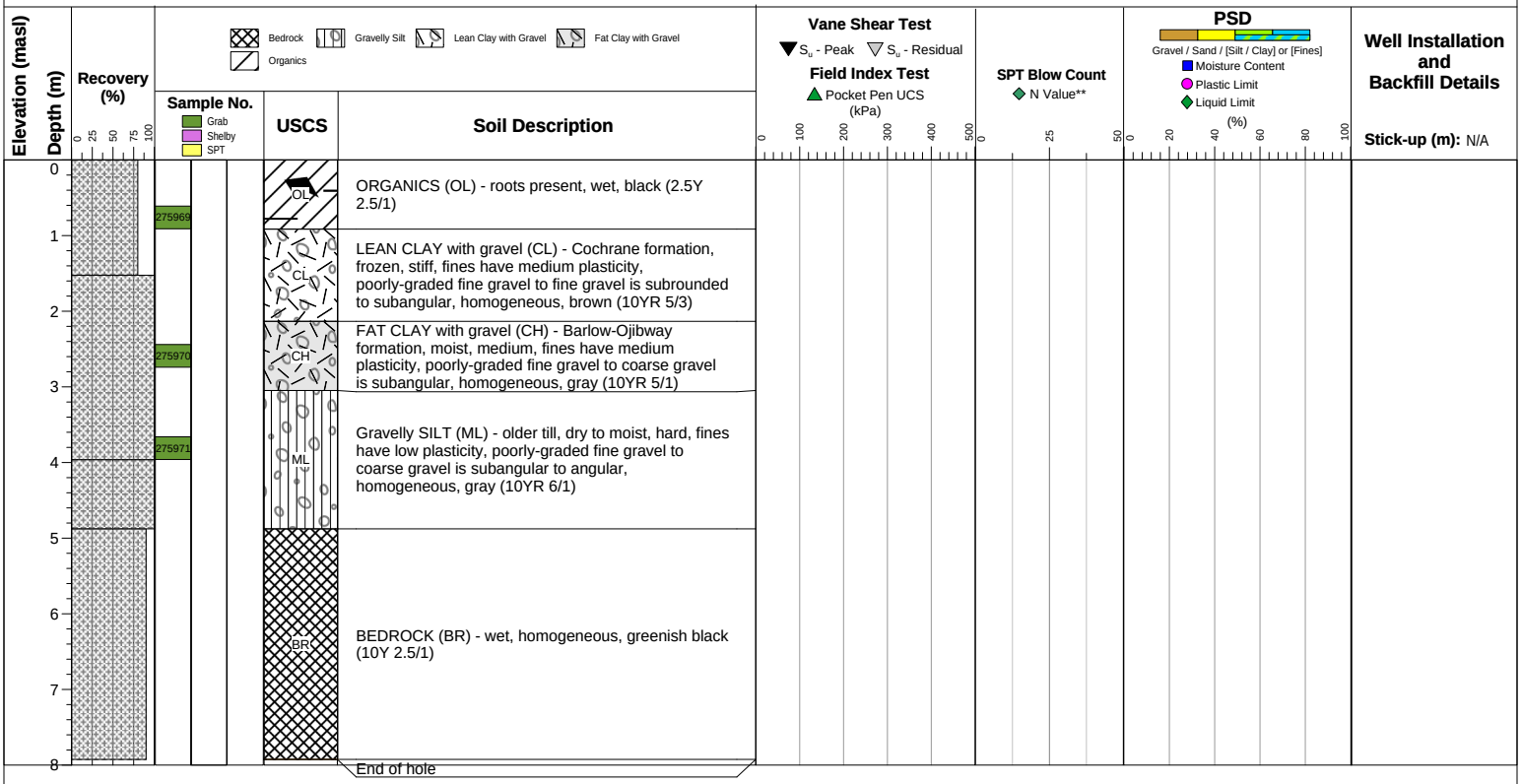
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-TMF-BH-203
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero

DRILLING DATE: 16-Mar-24 **TO:** 16-Mar-24
COORDINATES: 475737.6 E 5401911.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 290.3
TOTAL DEPTH (m): 7.9
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-TMF-BH-207
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 16-Mar-24 **TO:** 17-Mar-24
COORDINATES: 476820.5 E 5402796.7 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 281.2
TOTAL DEPTH (m): 39.0
WATER LEVEL (mbgs): N/A

Bedrock; Organics; Silty Gravel with Sand; Silt with Sand; Lean Clay; Lean Clay with Gravel; Fat Clay

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl) / Depth (m)	Recovery (%)	Sample No. (Grab, Shelby, SPT)	USCS	Soil Description
0 – 1			OL	ORGANICS (OL) - moist, very dark brown (10YR 2/2)
1 – 2			CL	LEAN CLAY (CL) - few sand, moist, medium, fines have medium plasticity, gap-graded fine sand to medium sand is subrounded, dark greenish gray (10Y 4/1)
2 – 3		275974	CL	LEAN CLAY (CL) - Cochrane formation, soft from 1.8m to 2.4 m, few sand, trace gravel, dry to moist, stiff, fines have medium plasticity, gap-graded fine sand to fine gravel is rounded to subrounded, brown (10YR 5/3)
3 – 4		275975	CL	
4 – 5		275976	CH	FAT CLAY (CH) - Barlow-Ojibway formation, very stiff from 3.7m to 4.0m, soft from 8.5m to 9.8m, few sand, trace gravel, dry, medium, fines have high plasticity, gap-graded fine sand to coarse sand is subrounded, dark greenish gray (10Y 4/1)
5 – 6			CH	
6 – 7		275977	CH	
7 – 8			CH	
8 – 9			CH	
9 – 10		275978	CH	
10 – 11			CH	
11 – 12			CH	
12 – 13		275979	CH	
13 – 14		275980	CH	
14 – 15			CH	FAT CLAY (CH) - Barlow-Ojibway formation, trace sand, moist to wet, medium, fines have high plasticity, stratified, dark greenish gray (10Y 4/1)
15 – 16			CH	
16 – 17		275981	CH	
17 – 18			CH	
18 – 19		275982	CH	
19 – 20			CH	

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-TMF-BH-207
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 16-Mar-24 **TO:** 17-Mar-24
COORDINATES: 476820.5 E 5402796.7 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 281.2
TOTAL DEPTH (m): 39.0
WATER LEVEL (mbgs): N/A

Bedrock; Organics; Silty Gravel with Sand; Silt with Sand; Lean Clay; Lean Clay with Gravel; Fat Clay

Elevation (masl) / Depth (m)	Recovery (%)	Sample No. (Grab, Shelby, SPT)	USCS	Soil Description
21		275983	CL	LEAN CLAY with gravel (CL) - Barlow-Ojibway clay, wet, soft, fines have medium plasticity, homogeneous, gray (10YR 6/1)
24		275984	GM	Silty GRAVEL with sand (GM) - older till, 75mm coarse gravel from 34.1m to 34.3m, moist, very stiff, fines have low plasticity, poorly-graded medium sand to fine gravel is subangular, very dark gray (10YR 3/1)
35		275985	ML	SILT with sand (ML) - older till, trace gravel, dry to moist, stiff, fines have low plasticity, poorly-graded fine sand to coarse sand is subrounded, dark greenish gray (10Y 4/1)
37			BR	BEDROCK (BR) - dry, dark greenish gray (10Y 4/1)
39				End of hole

Vane Shear Test
S_u - Peak; S_u - Residual
Field Index Test
Pocket Pen UCS (kPa)
0 100 200 300 400 500

SPT Blow Count
N Value**
0 25 50

PSD
Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%)
0 20 40 60 80 100

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW08AB
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 13-Mar-24 **TO:** 15-Mar-24
COORDINATES: 476469.3 E 5401996.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 287.2
TOTAL DEPTH (m): 47.2
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

No Recovery; Bedrock; Silty Sand; Silty Sand with Gravel; Silt; Silt with Sand; Sandy Silt; Silty Clay; Fat Clay

Recovery (%)

Sample No. (Grab, Shelby, SPT)

Depth (m)	Sample No.
8.5	275952
10.5	275953
12.5	275954
13.5	275955
14.5	275956
15.5	275957
17.0	275958
18.0	275959
19.0	275960

USCS

Soil Description

Material drilled and logged by Stantec

FAT CLAY (CH) - Barlow-Ojibway formation, trace gravel from 7m to 10.7m, 3.5cm varved clay from 16.2m to 20.4m, few sand, moist, very soft, fines have high plasticity, gap-graded fine sand to fine gravel is subrounded, dark greenish gray (10Y 4/1)

CH

Vane Shear Test
S_u - Peak; S_u - Residual

Field Index Test
Pocket Pen UCS (kPa)

SPT Blow Count
N Value**

Depth (m)	N Value**
8.5	3 (1/1/2)
10.5	5 (1/2/3)
12.5	2 (1/1/1)
15.5	2 (1/1/1)
16.5	3 (1/1/2)

PSD
Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%)

Well Installation and Backfill Details
Stick-up (m):
Well A 0.95
Well B 0.98

Notes:
* N-values of 0 are presumably caused by sonic drilling vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand; Bentonite; PVC; Screen

srk consulting

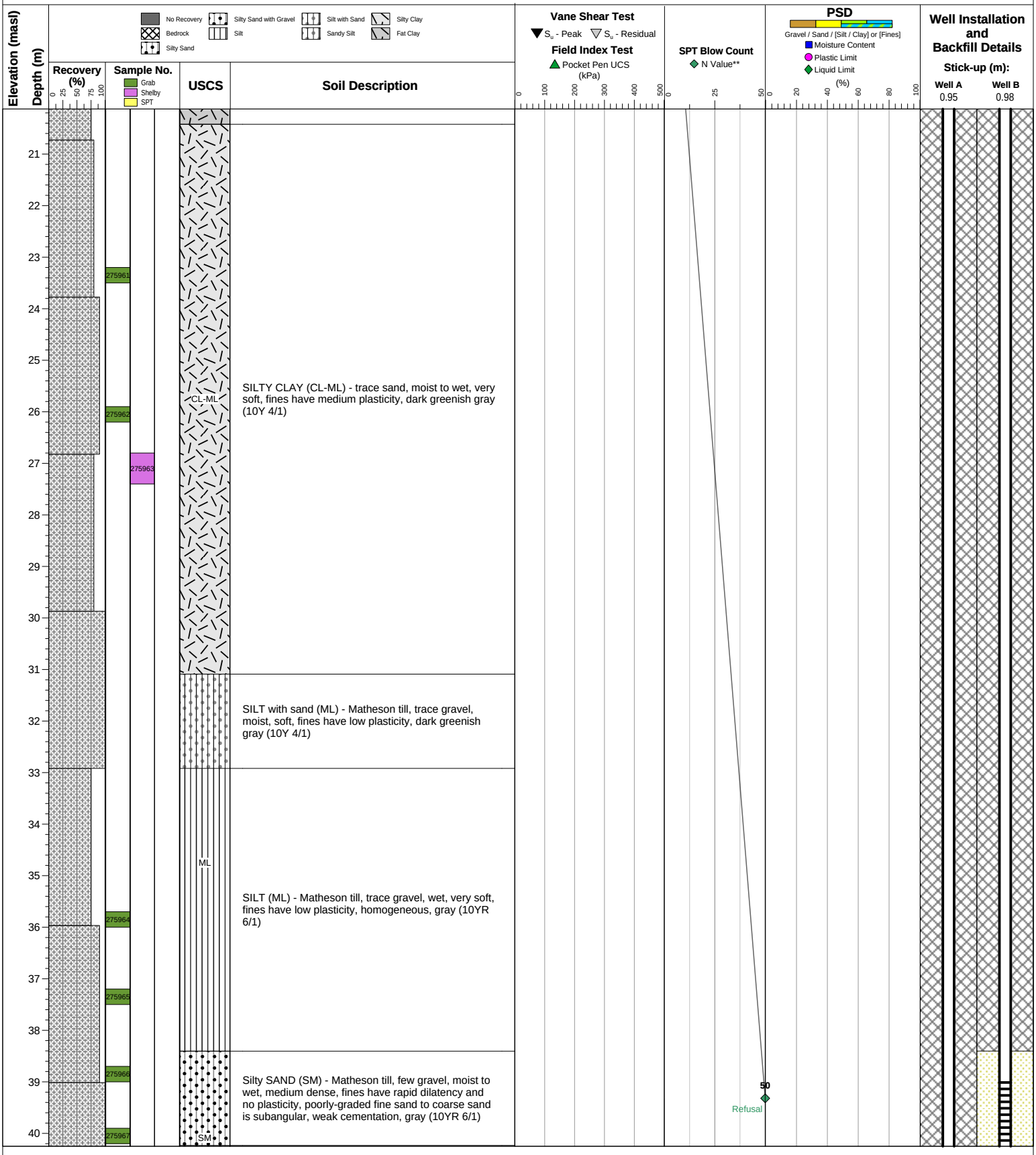
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW08AB
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 13-Mar-24 **TO:** 15-Mar-24
COORDINATES: 476469.3 E 5401996.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 287.2
TOTAL DEPTH (m): 47.2
WATER LEVEL (mbgs): N/A



Notes:
* N-values of 0 are presumably caused by sonic drilling vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand Bentonite PVC Screen

srk consulting

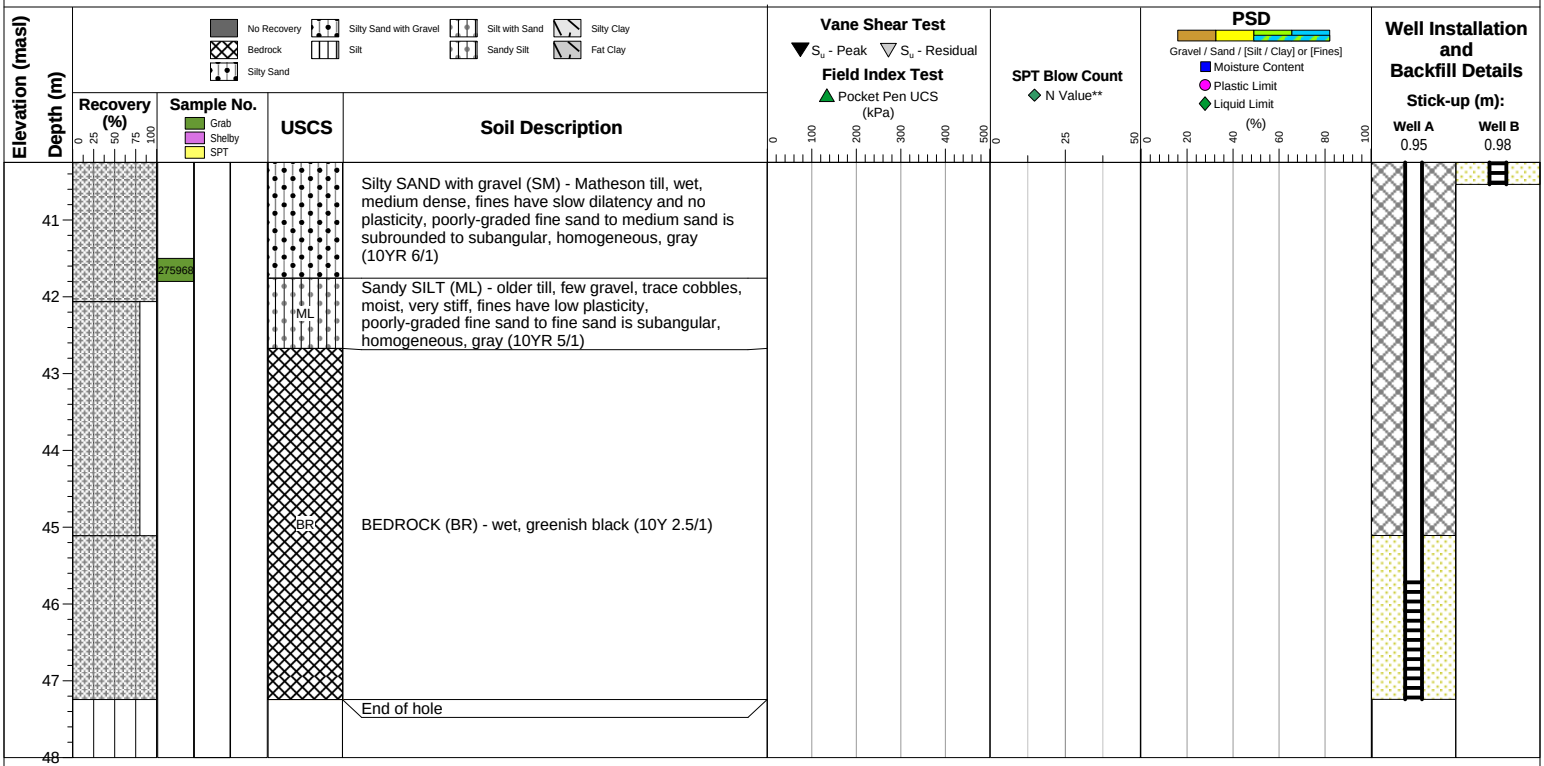
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW08AB
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Clinton Loli

DRILLING DATE: 13-Mar-24 **TO:** 15-Mar-24
COORDINATES: 476469.3 E 5401996.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 287.2
TOTAL DEPTH (m): 47.2
WATER LEVEL (mbgs): N/A



Notes:
* N-values of 0 are presumably caused by sonic drilling vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand | Bentonite | PVC | Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW10A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 02-Mar-24 **TO:** 04-Mar-24
COORDINATES: 476796.2 E 5407113.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.66
TOTAL DEPTH (m): 87.6
WATER LEVEL (mbgs): 5.98

Elevation (masl) / Depth (m)

Recovery (%)

Sample No.: Grab, Shelby, SPT

Drillout, Weathered Bedrock, Silty Sand, Sandy Silt, Bedrock, Well Graded Gravel with Silt and Sand

USCS

Soil Description

Vane Shear Test: S_u - Peak, S_u - Residual

Field Index Test: Pocket Pen UCS (kPa)

SPT Blow Count: N Value**

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details

Stick-up (m): 1.00

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

Sand, Bentonite, PVC, Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW10A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 02-Mar-24 **TO:** 04-Mar-24
COORDINATES: 476796.2 E 5407113.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.66
TOTAL DEPTH (m): 87.6
WATER LEVEL (mbgs): 5.98

Elevation (masl) | Depth (m) | Recovery (%) | Sample No. (Grab, Shelby, SPT) | USCS | Soil Description | Vane Shear Test (S_u - Peak, S_u - Residual) / Field Index Test (Pocket Pen UCS (kPa)) | SPT Blow Count (N Value**) | PSD (Gravel / Sand / [Silt / Clay] or [Fines], Moisture Content, Plastic Limit, Liquid Limit) | Well Installation and Backfill Details

Drillout | Weathered Bedrock | Silty Sand | Sandy Silt | Bedrock | Well Graded Gravel with Silt and Sand

Elevation (masl)	Depth (m)	Soil Description
252	21	
251	22	
250	23	
249	24	
248	25	
247	26	
246	27	NO RECOVERY - soil not logged and samples not taken
245	28	
244	29	
243	30	
242	31	
241	32	
240	33	
239	34	
238	35	
237	36	
236	37	
235	38	
234	39	
233	40	

Stick-up (m): 1.00

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand | Bentonite | PVC | Screen

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW10A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 02-Mar-24 **TO:** 04-Mar-24
COORDINATES: 476796.2 E 5407113.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.66
TOTAL DEPTH (m): 87.6
WATER LEVEL (mbgs): 5.98

Drillout; Bedrock; Weathered Bedrock; Well Graded Gravel with Silt and Sand; Silty Sand; Sandy Silt

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details

Stick-up (m): 1.00

Elevation (masl)	Depth (m)	Recovery (%)	USCS	Soil Description
232	41			
231	42			
230	43			
229	44			
228	45			
227	46			
226	47			
225	48			
224	49			
223	50			
222	51			
221	52			
220	53			
219	54			
218	55		GW-GM	Well-graded GRAVEL with silt and sand (GW-GM) - Matheson till, trace 10cm cobbles, wet, fines have no plasticity, well-graded medium sand to coarse gravel is subrounded to subangular, dark greenish gray (5G 4/1)
217	56		SM	Silty SAND (SM) - Matheson till, few gravel, moist, fines have low plasticity, gap-graded fine sand to coarse gravel is rounded to subrounded, dark greenish gray (5G 4/1)
216	57			Sandy SILT (ML) - older till, cobbles up to 10cm in apparent diameter, some rock flour observed due to pulverizing of cobbles/weathered bedrock clasts, few gravel, trace cobbles, dry, fines have no plasticity, gap-graded fine sand to coarse gravel is subrounded to subangular, fissured, gray (N 5/)
215	58			
214	59			
213	60		ML	Sandy SILT (ML) - older till, sand/silt contents vary

SPT Blow Count: N Value**
483

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details: Sand; Bentonite; PVC; Screen

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW10A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 02-Mar-24 **TO:** 04-Mar-24
COORDINATES: 476796.2 E 5407113.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.66
TOTAL DEPTH (m): 87.6
WATER LEVEL (mbgs): 5.98

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Drillout | Weathered Bedrock | Silty Sand | Sandy Silt
Bedrock | Well Graded Gravel with Silt and Sand

Sample No.: Grab, Shelby, SPT

Elevation (masl)	Depth (m)	Recovery (%)	USCS	Soil Description
212	61			within run, few gravel, trace cobbles, moist, fines have low plasticity, gap-graded fine sand to coarse gravel is subrounded to subangular, dark greenish gray (5G 4/1)
211	62			Sandy SILT (ML) - older till, boulder at 62.3m to 62.9m, recovered as light gray rock flour and sub-angular to sub-rounded gravel and cobbles, over-consolidated, trace gravel, trace cobbles, dry, fines have no plasticity, gap-graded fine sand to coarse gravel is subangular, fissured, dark greenish gray (5G 4/1)
210	63			
209	64		SM	Silty SAND (SM) - older till, sand lense, dry, fines have no plasticity, poorly-graded fine sand, homogeneous, gray (5Y 6/1)
208	65			
207	66			WEATHERED BEDROCK (BR) - becomes yellow (10yr 8/8) at 66.4m, becomes yellowish brown (10yr 6/8) after 68m, friable, more competent (coarser fractured particles) with depth, dry, greenish gray (5GY 6/1)
206	67			
205	68			
204	69			
203	70			WEATHERED BEDROCK (BR) - more competent than the layer above, heavy oxidation (dark brown, dark orange, and dark turquoise) in fractures, crushed into cobble and gravel size pieces, more sand and silt size pieces with depth, moist to wet, yellowish brown (10YR 5/6)
202	71			
201	72			
200	73			
199	74			WEATHERED BEDROCK (BR) - dark brown, dark orange, and turquoise oxidation in fractures, crushed into gravel size particles, pulverised into rock flour at 73.8m to 75.0m, dry, yellow (10YR 8/8)
198	75			
197	76		BR	WEATHERED BEDROCK (BR) - wet due to coring, finer crushed particles likely washed out, dark brown (10yr 2/1) oxidation, natural colour of rock is dark greenish gray (5gy 3/1), moist to wet, yellowish brown (10YR 5/4)
196	77			
195	78			
194	79			WEATHERED BEDROCK (BR) - recovered as a mixture of rock flour, sub-angular gravel and cobble, competent bedrock clasts and some instances of soil-like friable bedrock clasts, dry to moist, olive (5Y 5/6)
193	80			

Vane Shear Test
S_u - Peak ▽ S_u - Residual
Field Index Test
Pocket Pen UCS (kPa)
0 100 200 300 400 500
241

SPT Blow Count
N Value**
0 25 50

PSD
Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%)
0 20 40 60 80 100

Well Installation and Backfill Details
Stick-up (m): 1.00

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand | Bentonite | PVC | Screen

srk consulting

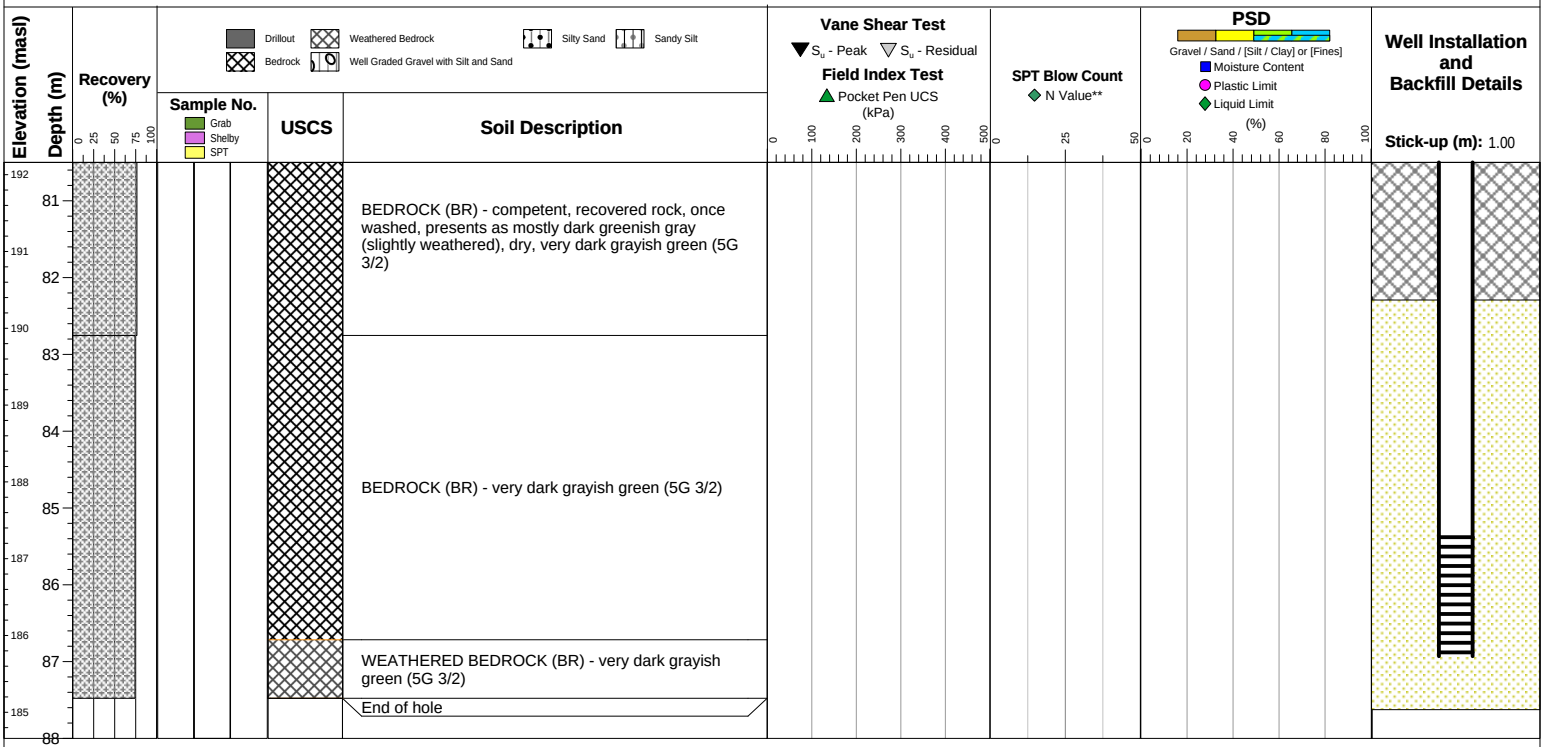
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW10A
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 02-Mar-24 **TO:** 04-Mar-24
COORDINATES: 476796.2 E 5407113.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 272.66
TOTAL DEPTH (m): 87.6
WATER LEVEL (mbgs): 5.98



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

Sand | Bentonite | PVC | Screen

srk consulting

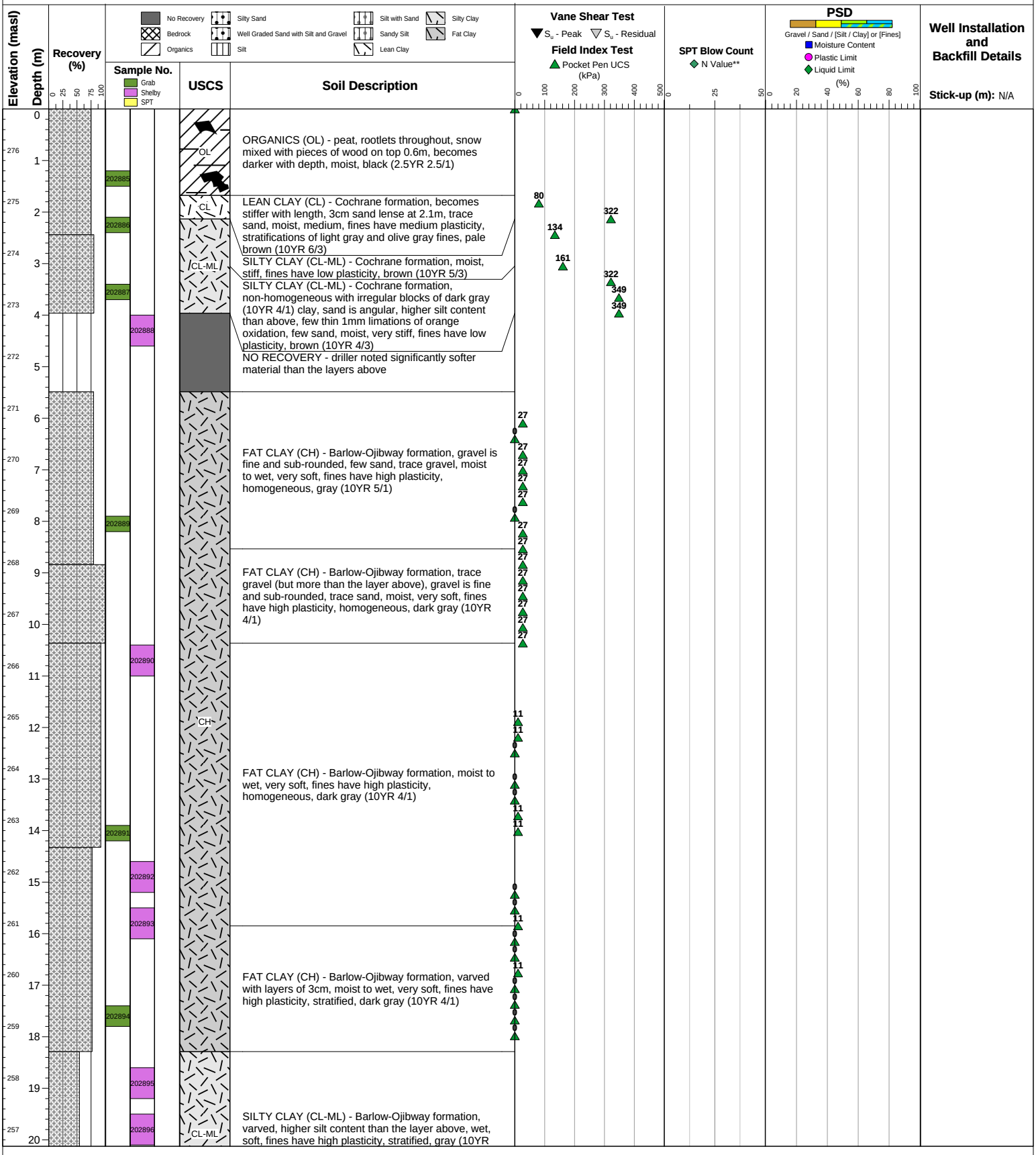
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-201
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 05-Mar-24 **TO:** 08-Mar-24
COORDINATES: 473338.3 E 5411099.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.8
TOTAL DEPTH (m): 68.3
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

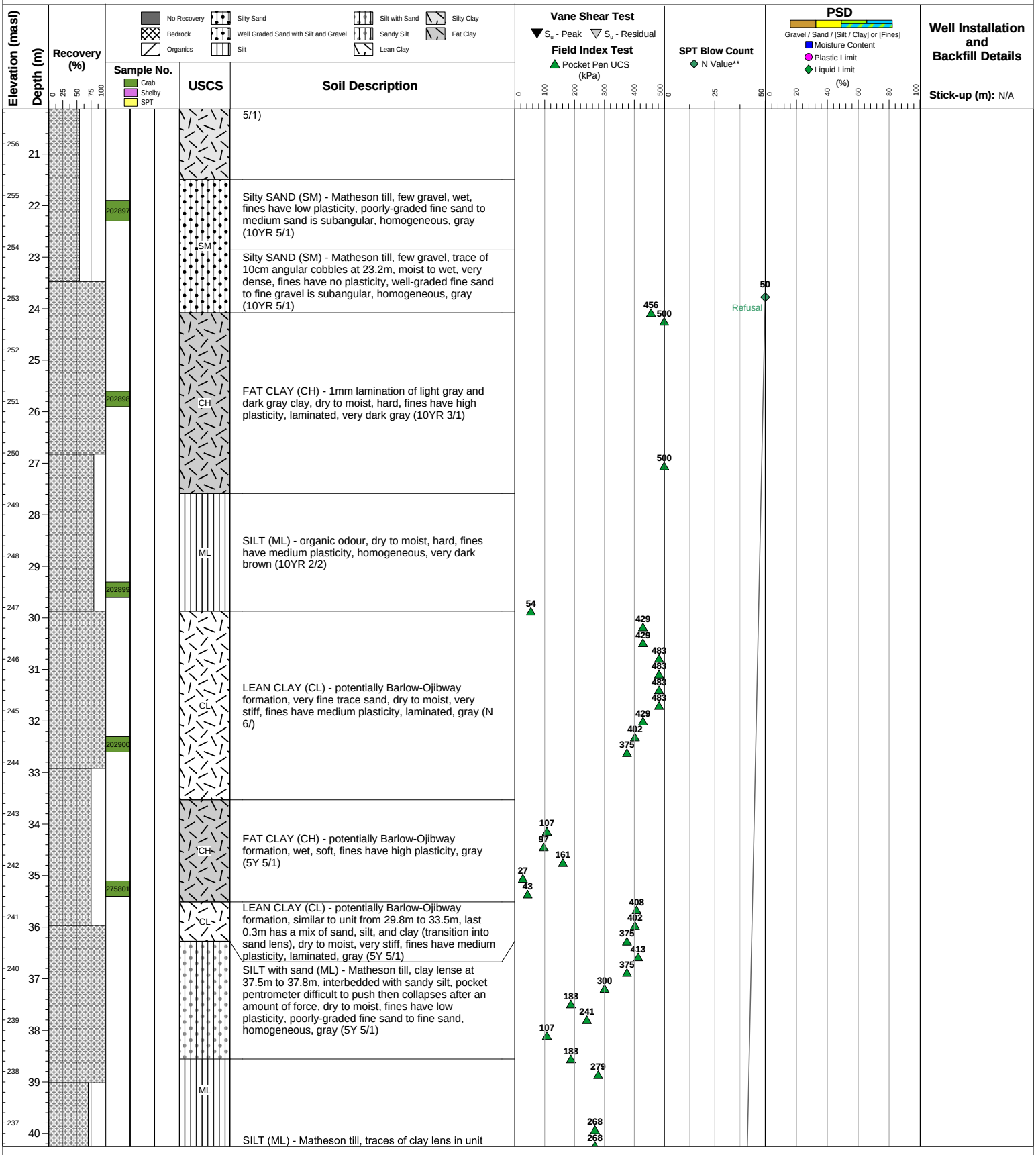
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-201
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 05-Mar-24 **TO:** 08-Mar-24
COORDINATES: 473338.3 E 5411099.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.8
TOTAL DEPTH (m): 68.3
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

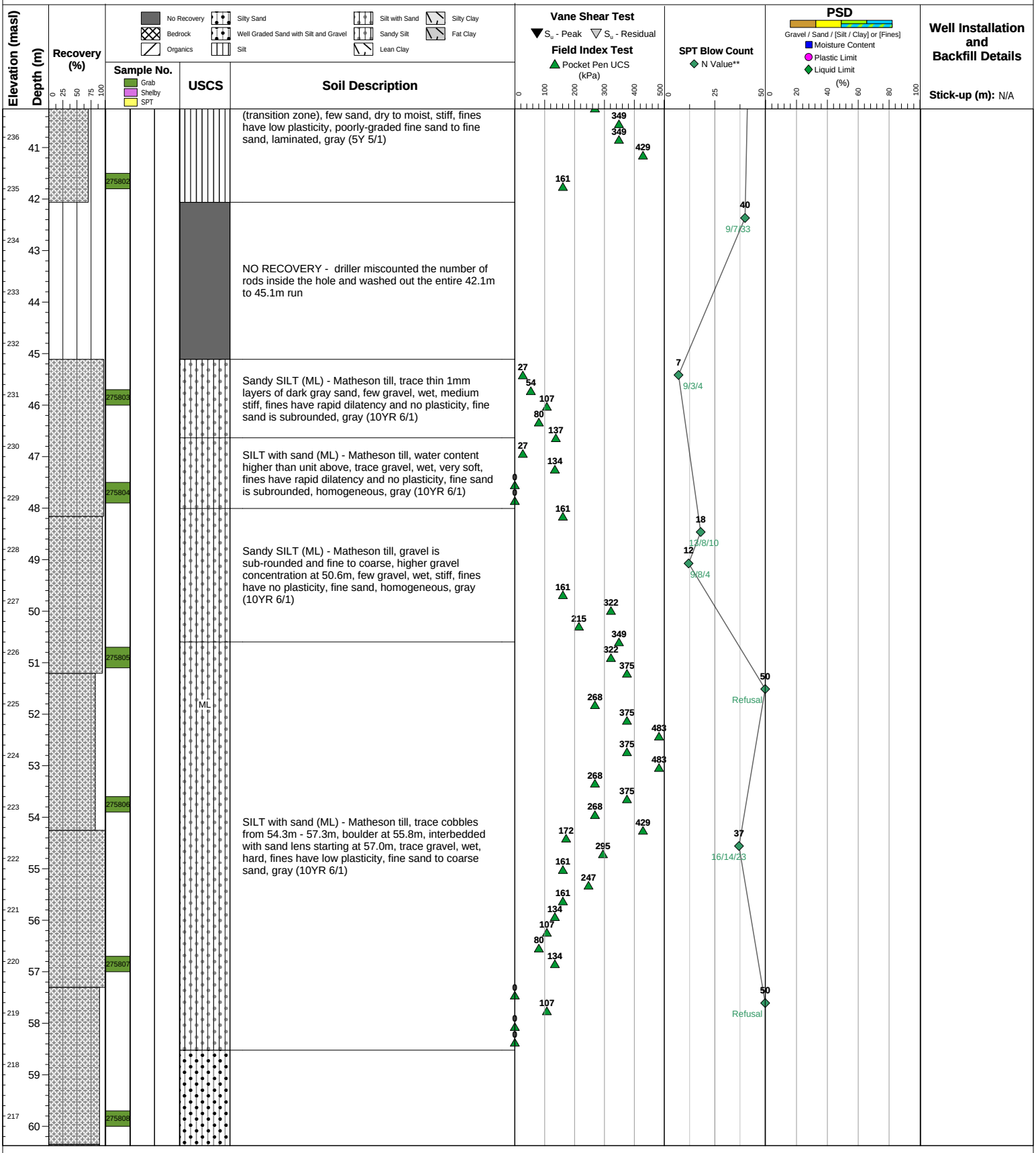
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-201
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 05-Mar-24 **TO:** 08-Mar-24
COORDINATES: 473338.3 E 5411099.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.8
TOTAL DEPTH (m): 68.3
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-201
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Parker Tully/Alice Xu

DRILLING DATE: 05-Mar-24 **TO:** 08-Mar-24
COORDINATES: 473338.3 E 5411099.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.8
TOTAL DEPTH (m): 68.3
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

No Recovery; Bedrock; Organics; Silty Sand; Well Graded Sand with Silt and Gravel; Silt; Silt with Sand; Sandy Silt; Lean Clay; Silty Clay; Fat Clay

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab, Shelby, SPT)	USCS	Soil Description	Vane Shear Test (S_u - Peak, S_u - Residual) / Field Index Test (Pocket Pen UCS (kPa))	SPT Blow Count (N Value**)	PSD (Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%))	Well Installation and Backfill Details
216	61			SM	Silty SAND (SM) - Matheson till, silt lens at 61.7m - 62.0m, trace gravel, trace cobbles, moist to wet, very dense, fines have no plasticity, well-graded fine sand to coarse gravel is subrounded to subangular, gray (10YR 6/1)				
215	62								
214	63			ML	Sandy SILT (ML) - older till, few gravel, trace cobbles, moist to wet, stiff, fines have no plasticity, well-graded fine sand to coarse gravel is subrounded to subangular, gray (10YR 6/1)	80			
213	64			SW-SM	Well-graded SAND with silt and gravel (SW-SM) - trace cobbles, moist, fines have no plasticity, well-graded fine sand to coarse gravel is subrounded to subangular, dark gray (5Y 4/1)				
212	65			ML	Sandy SILT (ML) - older till, potentially encountered bedrock at base, few gravel, trace cobbles, moist, medium, fines have no plasticity, gap-graded fine sand to coarse gravel is subrounded to subangular, gray (N 5/)	241			
211	66								
210	67			BR	BEDROCK (BR) - competent with white 2mm thick quartz veins, wet, very dark grayish green (5G 2.5/2)				
209	68								
208	69								
207	70								
206	71								
205	72						50 Refusal		

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

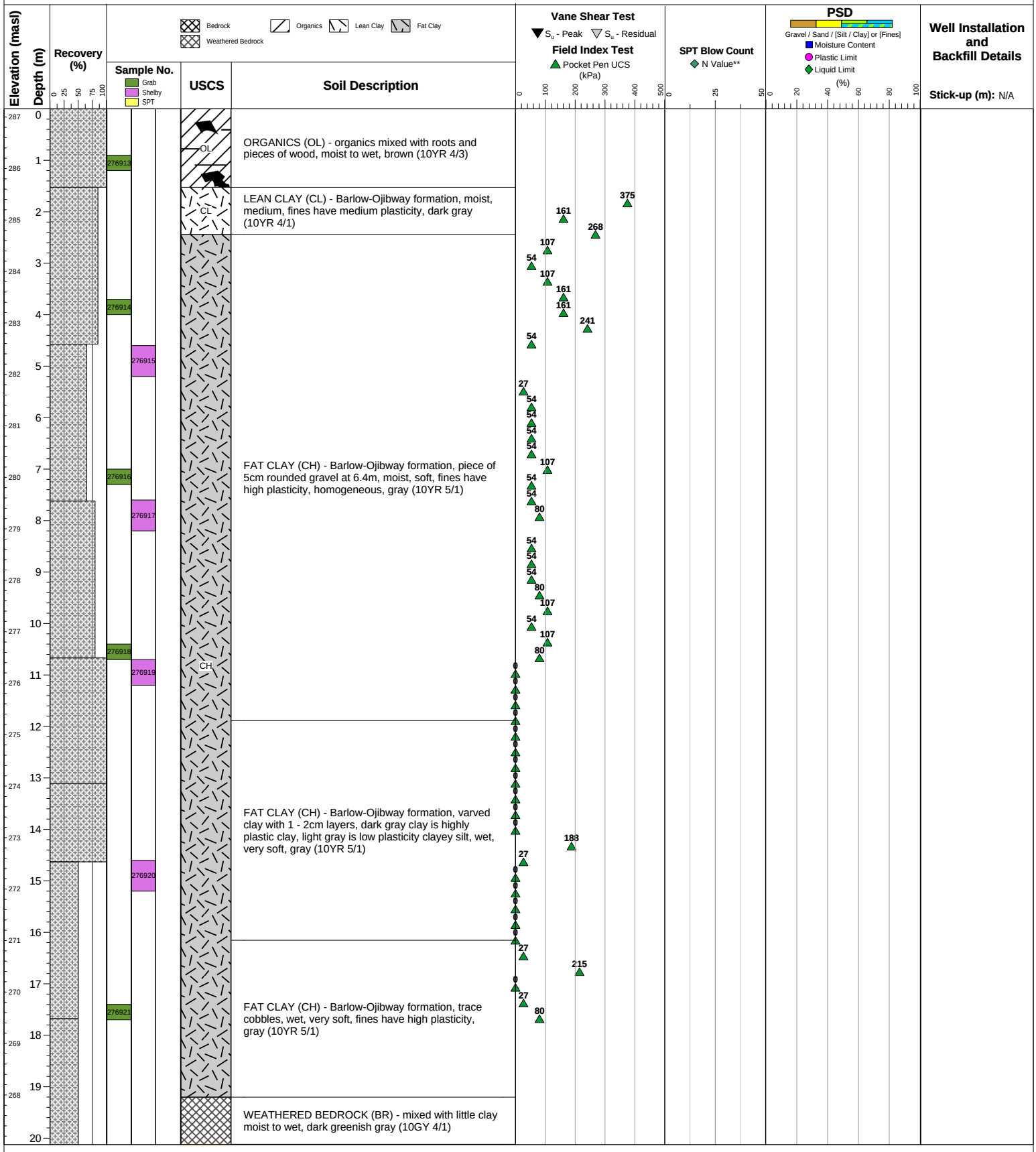
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-202
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Michael Stephens

DRILLING DATE: 20-Mar-24 **TO:** 21-Mar-24
COORDINATES: 474129.8 E 5412170.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 287.16
TOTAL DEPTH (m): 23.8
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

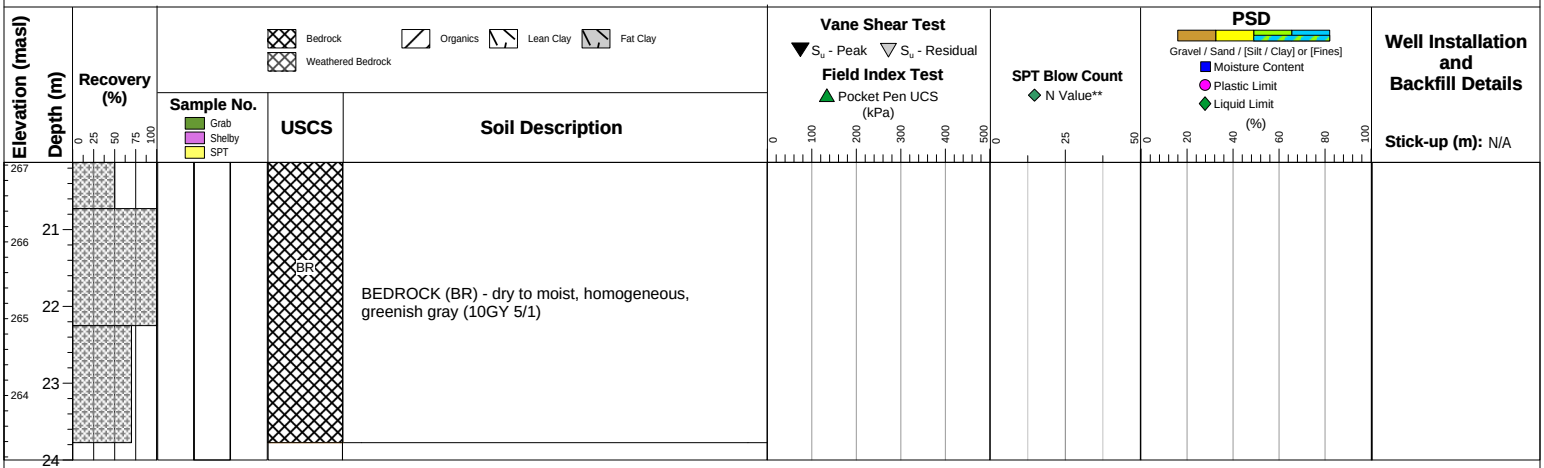
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-202
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Michael Stephens

DRILLING DATE: 20-Mar-24 **TO:** 21-Mar-24
COORDINATES: 474129.8 E 5412170.4 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 287.16
TOTAL DEPTH (m): 23.8
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

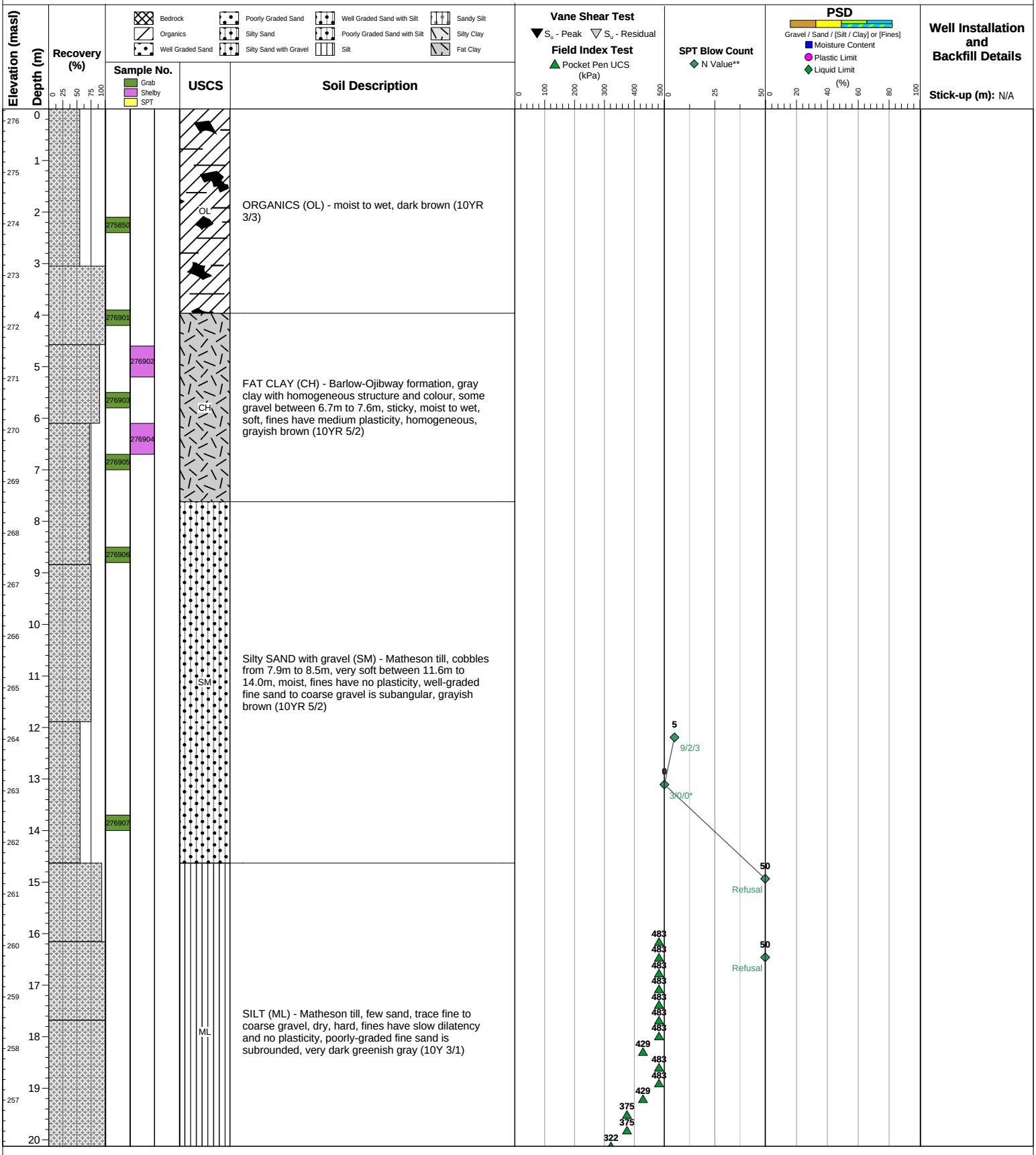
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-205
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Michael Stephens

DRILLING DATE: 16-Mar-24 **TO:** 18-Mar-24
COORDINATES: 474142.5 E 5413524.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.23
TOTAL DEPTH (m): 68.6
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-205
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Michael Stephens

DRILLING DATE: 16-Mar-24 **TO:** 18-Mar-24
COORDINATES: 474142.5 E 5413524.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.23
TOTAL DEPTH (m): 68.6
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Organics; Well Graded Sand; Poorly Graded Sand; Silty Sand; Silty Sand with Gravel; Well Graded Sand with Silt; Poorly Graded Sand with Silt; Silt; Sandy Silt; Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): N/A

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
256	0				
255	21		276908	CL-ML	SILTY CLAY (CL-ML) - Matheson till, 5cm sand lense at 21.3m, trace sand, moist, very stiff, fines have medium plasticity, very dark greenish gray (10Y 3/1)
254	22		276909	SW	Well-graded SAND (SW) - Matheson till, trace fine gravel, moist, medium dense, gap-graded medium sand is subangular to angular, gray (10YR 5/1)
253	23			SW-SM, ML, CL-ML	Well-graded SAND with silt (SW-SM) - Matheson till, few gravel, trace cobbles, dense, fines have no plasticity, well-graded fine sand to coarse gravel is subrounded to subangular, gray (10YR 5/1)
252	24			ML	SILT (ML) - Matheson till, trace gravel, trace sand, moist, medium, fines have slow dilatency and no plasticity, greenish gray (10Y 5/1)
251	25			CL-ML	SILTY CLAY (CL-ML) - Matheson till, dry to moist, very stiff, fines have medium plasticity, greenish gray (10Y 6/1)
250	26			ML	Sandy SILT (ML) - Matheson till, moist, very stiff, fines have slow dilatency and no plasticity, gap-graded fine sand, greenish gray (10Y 5/1)
249	27			CL-ML	SILTY CLAY (CL-ML) - Matheson till, 1 - 3mm thick laminations of light gray silt and dark gray clay, silt lense at 25.5m - 25.7m, moist, stiff, fines have low plasticity, gray (10YR 6/1)
248	28			ML	Sandy SILT (ML) - Matheson till, trace fine gravel, moist, very stiff, fines have slow dilatency and no plasticity, gap-graded fine sand, greenish gray (10Y 6/1)
247	29			ML	SILTY CLAY (CL-ML) - Matheson till, moist, stiff, fines have low plasticity, laminated, gray (10YR 6/1)
246	30		276910	SP-SM	Sandy SILT (ML) - Matheson till, trace fine to coarse gravel, sand lense at 28.3m - 28.5m, moist, very stiff, fines have slow dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
245	31			SP-SM	Poorly-graded SAND with silt (SP-SM) - Matheson till, dry to moist, loose, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
244	32				
243	33				
242	34			SM	Silty SAND (SM) - Matheson till, cobble at 34.1m, trace gravel, dry to moist, dense, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
241	35			SP-SM	Poorly-graded SAND with silt (SP-SM) - Matheson till, dry to moist, medium dense, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
240	36				
239	37				
238	38		276911	ML	Sandy SILT (ML) - Matheson till, trace gravel, moist, hard, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)
237	39			SW-SM,	Well-graded SAND with silt (SW-SM) - Matheson till, few gravel, moist, dense, fines have rapid dilatency and no plasticity, well-graded fine sand to coarse gravel is subrounded to subangular, gray (10YR 5/1)
236	40				Sandy SILT (ML) - Matheson till, trace fine to coarse

Vane Shear Test / Field Index Test values: 483, 483, 54, 27, 161, 27, 161, 27, 107, 27, 322, 215, 268, 268, 295, 295, 54, 161, 322, 27, 27, 27, 161, 107, 322, 107, 429, 215, 268, 402, 183, 349

SPT Blow Count values: 50 (Refusal); 22 (3/6/16); 50 (Refusal); 46 (8/14/32)

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-205
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Michael Stephens

DRILLING DATE: 16-Mar-24 **TO:** 18-Mar-24
COORDINATES: 474142.5 E 5413524.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.23
TOTAL DEPTH (m): 68.6
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock; Organics; Well Graded Sand; Poorly Graded Sand; Silty Sand; Silty Sand with Gravel; Well Graded Sand with Silt; Poorly Graded Sand with Silt; Silt; Sandy Silt; Silty Clay; Fat Clay

Sample No.: Grab; Shelby; SPT

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description	Vane Shear Test (kPa)	SPT Blow Count (N Value**)	PSD (%)
236–216	41–60	0–100	276912	ML	gravel, moist, hard, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, gray (10YR 5/1)	54		
235	41–42			SP	Poorly-graded SAND (SP) - Matheson till, moist, dense, poorly-graded fine sand to medium sand, gray (10YR 5/1)		28 (4/8/20)	
234–229	42–48			SW	Well-graded SAND (SW) - Matheson till, trace gravel from 47.5m - 48.2m, moist, medium dense, well-graded fine sand to medium sand is rounded to subrounded, homogeneous, gray (10YR 5/1)		50 Refusal	
227–219	49–57			SM	Silty SAND with gravel (SM) - Matheson till, silty sand with some large gravels between 50.3m - 50.9m, cobbles on at 51.2m - 53.6m and 63.1m - 63.4m, moist, medium dense, fines have no plasticity, well-graded fine sand to coarse sand is subrounded, homogeneous, grayish brown (10YR 5/2)		50 Refusal	

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-205
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Michael Stephens

DRILLING DATE: 16-Mar-24 **TO:** 18-Mar-24
COORDINATES: 474142.5 E 5413524.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 276.23
TOTAL DEPTH (m): 68.6
WATER LEVEL (mbgs): N/A

Bedrock, Organics, Well Graded Sand, Poorly Graded Sand, Silty Sand, Silty Sand with Gravel, Well Graded Sand with Silt, Poorly Graded Sand with Silt, Silt, Sandy Silt, Silty Clay, Fat Clay

Sample No.: Grab, Shelby, SPT

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Elevation (masl)	Depth (m)	Recovery (%)	USCS	Soil Description
215	61			
214	62			
213	63			
212	64			
211	65			
210	66		BR	BEDROCK (BR)
209	67			
208	68			
207	69			
206	70			
205	71			
	72			

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

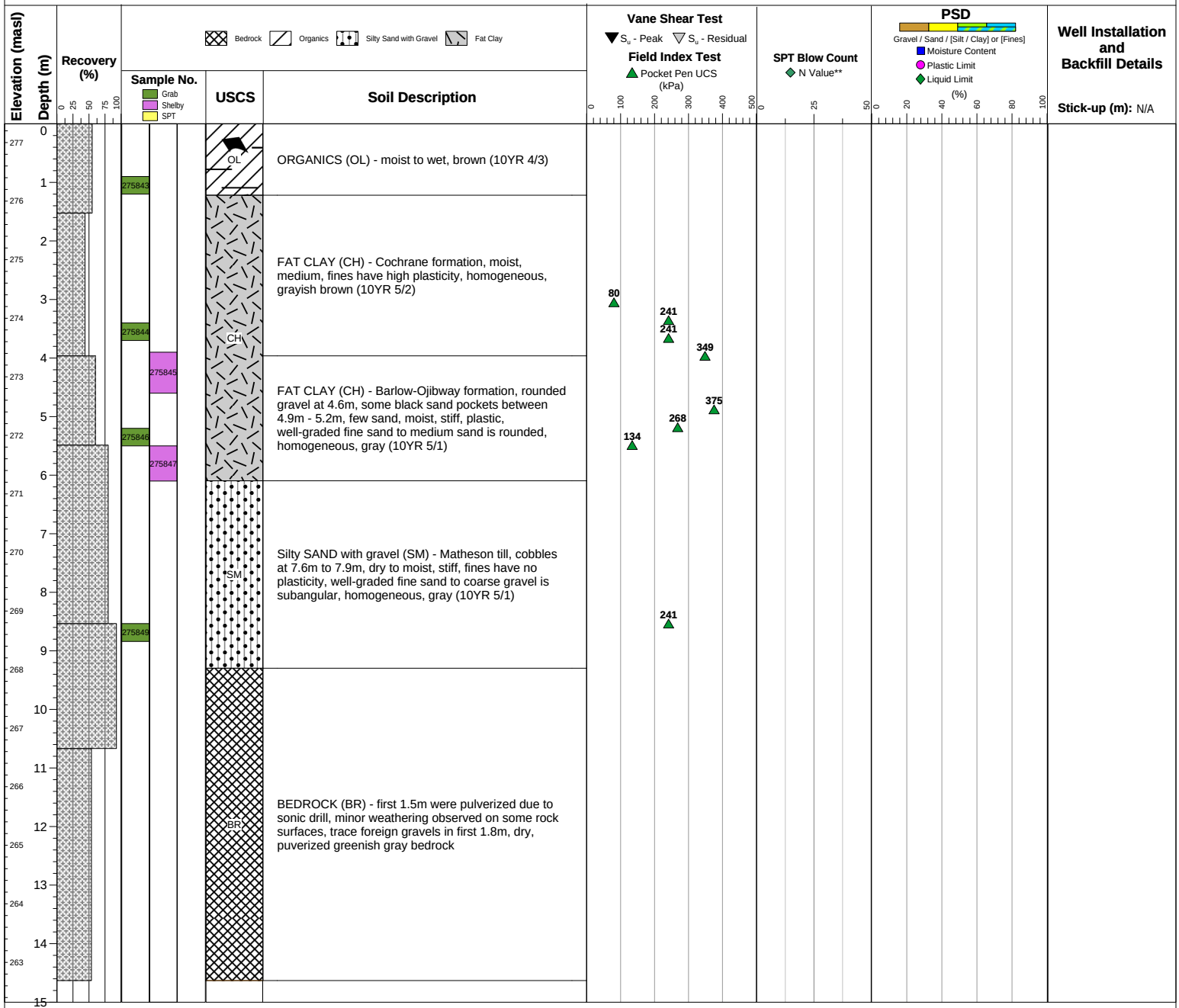
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-207
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Barbara Amar/Alice Xu

DRILLING DATE: 15-Mar-24 **TO:** 15-Mar-24
COORDINATES: 474234.8 E 5414555.3 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 277.32
TOTAL DEPTH (m): 14.6
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

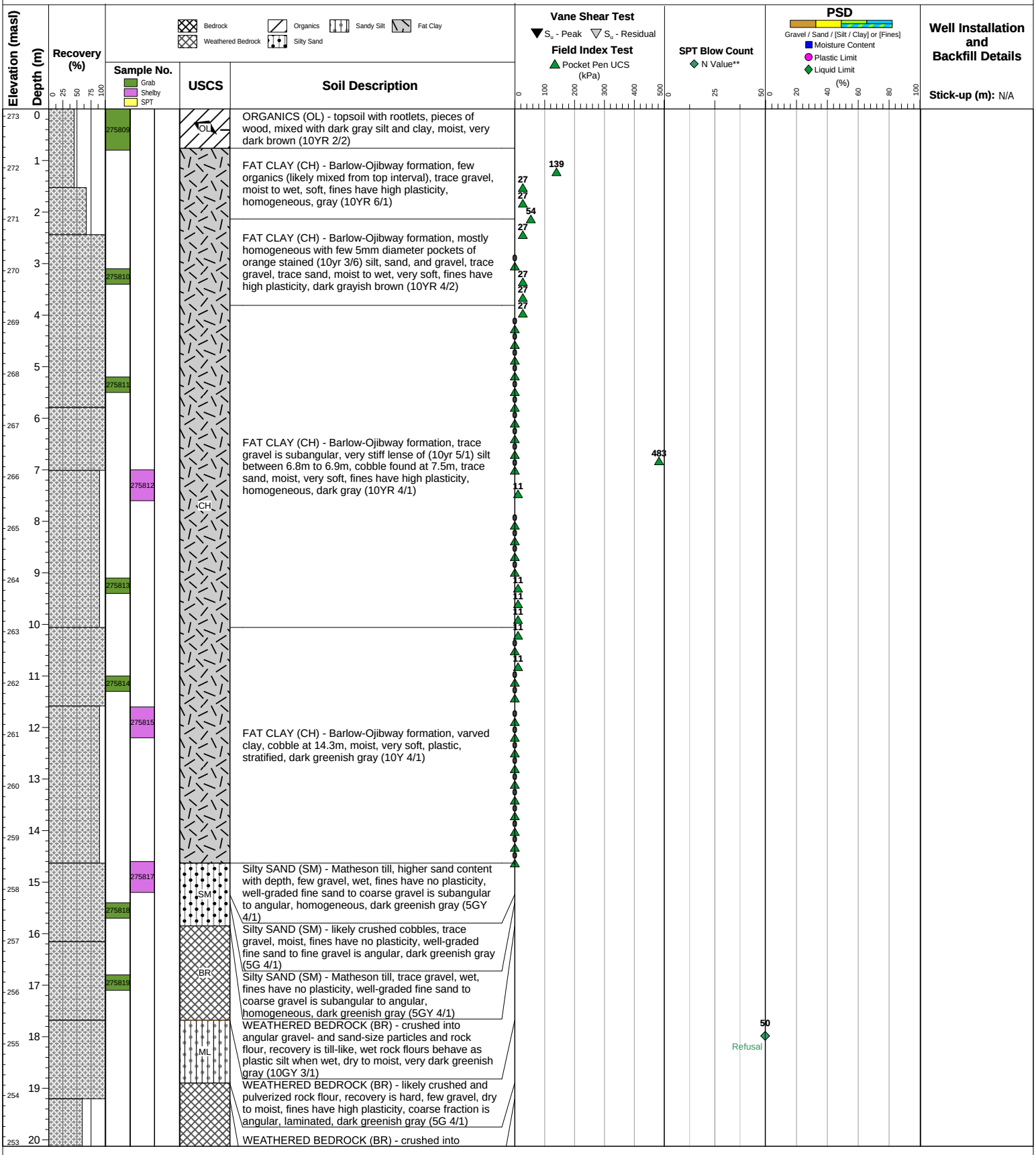
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-212
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Barbara Amar/Alice Xu/Clinton Loli

DRILLING DATE: 09-Mar-24 **TO:** 10-Mar-24
COORDINATES: 474392.4 E 5411192.2 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 273.14
TOTAL DEPTH (m): 35.7
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-212
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Barbara Amar/Alice Xu/Clinton Loli

DRILLING DATE: 09-Mar-24 **TO:** 10-Mar-24
COORDINATES: 474392.4 E 5411192.2 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 273.14
TOTAL DEPTH (m): 35.7
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab / Shelby / SPT)	USCS	Soil Description
253	20				angular cobble, coarse gravel-size and silt-size material, dry, greenish black (5GY 2.5/1)
252	21				
251	22				
250	23				
249	24				
248	25				WEATHERED BEDROCK (BR) - wet likely due to drilling with water, crushed into angular cobble and gravel size particles, orange staining (10yr 4/6) in fractures, more orange staining between 21.3m to 21.6m, dark greenish gray (5GY 4/1)
247	26				
246	27			BR	
245	28				
244	29				
243	30				
242	31				
241	32				
240	33				BEDROCK (BR) - competent, wet due to drilling, few white quartz veins from 1mm to 1cm thick, greenish black (10Y 2.5/1)
239	34				
238	35				
237	36				

Bedrock; Weathered Bedrock; Organics; Silty Sand; Sandy Silt; Fat Clay

Vane Shear Test: S_u - Peak; S_u - Residual
Field Index Test: Pocket Pen UCS (kPa) — 0, 100, 200, 300, 400, 500

SPT Blow Count: N Value** — 0, 25, 50

PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%) — 0, 20, 40, 60, 80, 100

Well Installation and Backfill Details

Stick-up (m): N/A

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

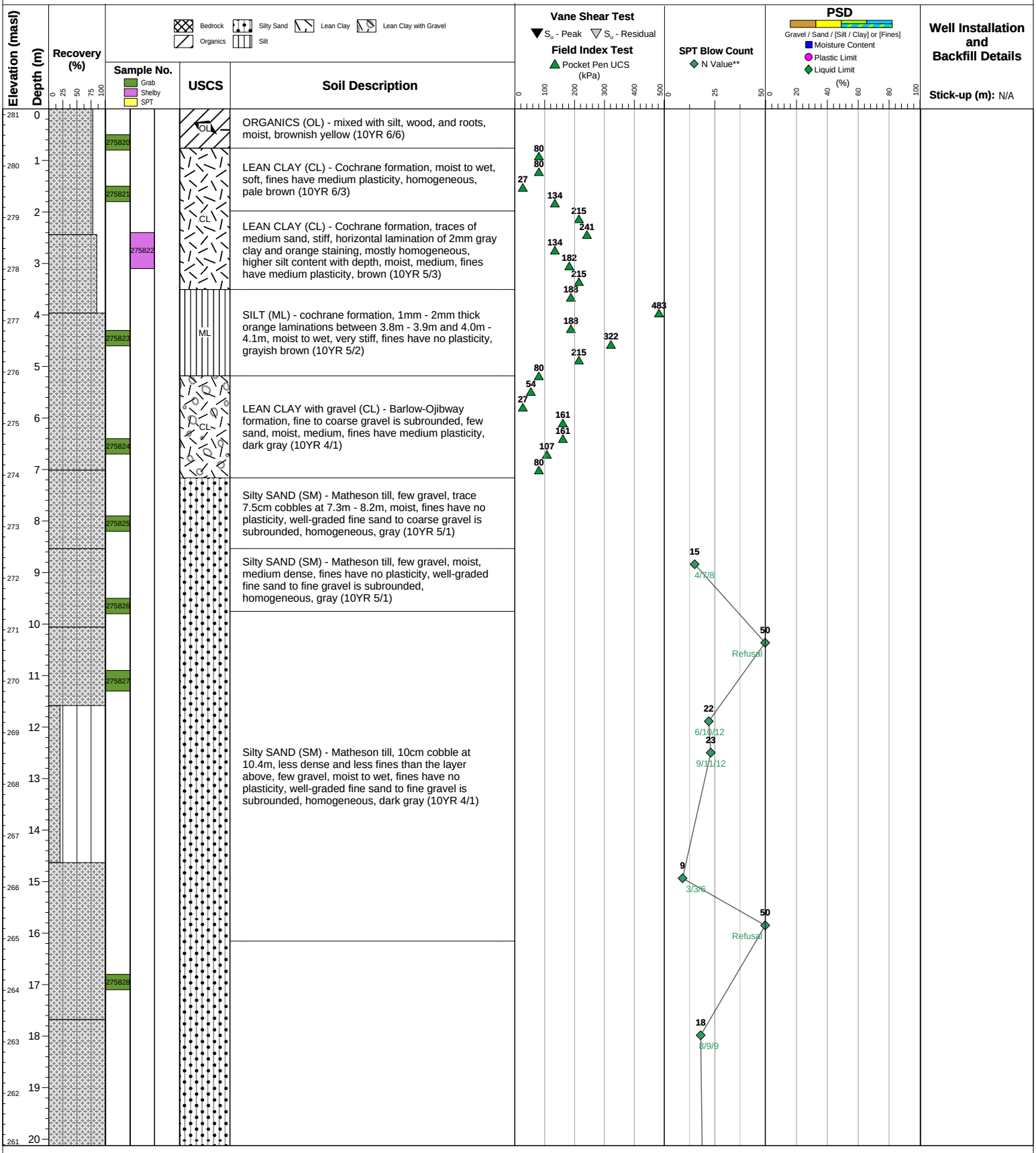
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-215
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Barbara Amar

DRILLING DATE: 11-Mar-24 **TO:** 13-Mar-24
COORDINATES: 473009.0 E 5413538.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 281.11
TOTAL DEPTH (m): 68.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-215
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Barbara Amar

DRILLING DATE: 11-Mar-24 **TO:** 13-Mar-24
COORDINATES: 473009.0 E 5413538.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 281.11
TOTAL DEPTH (m): 68.9
WATER LEVEL (mbgs): N/A

Elevation (masl) / Depth (m) | Recovery (%) | Sample No. (Grab, Shelby, SPT) | USCS | Soil Description

Bedrock, Organics, Silty Sand, Silt, Lean Clay, Lean Clay with Gravel

Vane Shear Test
S_u - Peak, S_u - Residual
Field Index Test
Pocket Pen UCS (kPa)

SPT Blow Count
N Value**

PSD
Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%)

Well Installation and Backfill Details
Stick-up (m): N/A

Depth (m)	Elevation (masl)	Sample No.	USCS	Soil Description
21	260		SM*	Silty SAND (SM) - Matheson till, wet, softer at 32.0m - 32.9m interval, few gravel, trace cobbles, dry to moist, very dense, fines have low plasticity, gap-graded fine sand to coarse gravel is subrounded, homogeneous, dark greenish gray (10Y 4/1)
28	253	275829		
33	248	275830		
36	245			Silty SAND (SM) - Matheson till, wet, very dense, fines have no plasticity, well-graded fine sand to medium sand, homogeneous, gray (10YR 5/1)
40	241			Silty SAND (SM) - Matheson till, moist, dense,

SPT Blow Count: 19 (13/9/10); 50 Refusal; 50 Refusal; 50 Refusal; 50 Refusal; 50 Refusal; 50 Refusal

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

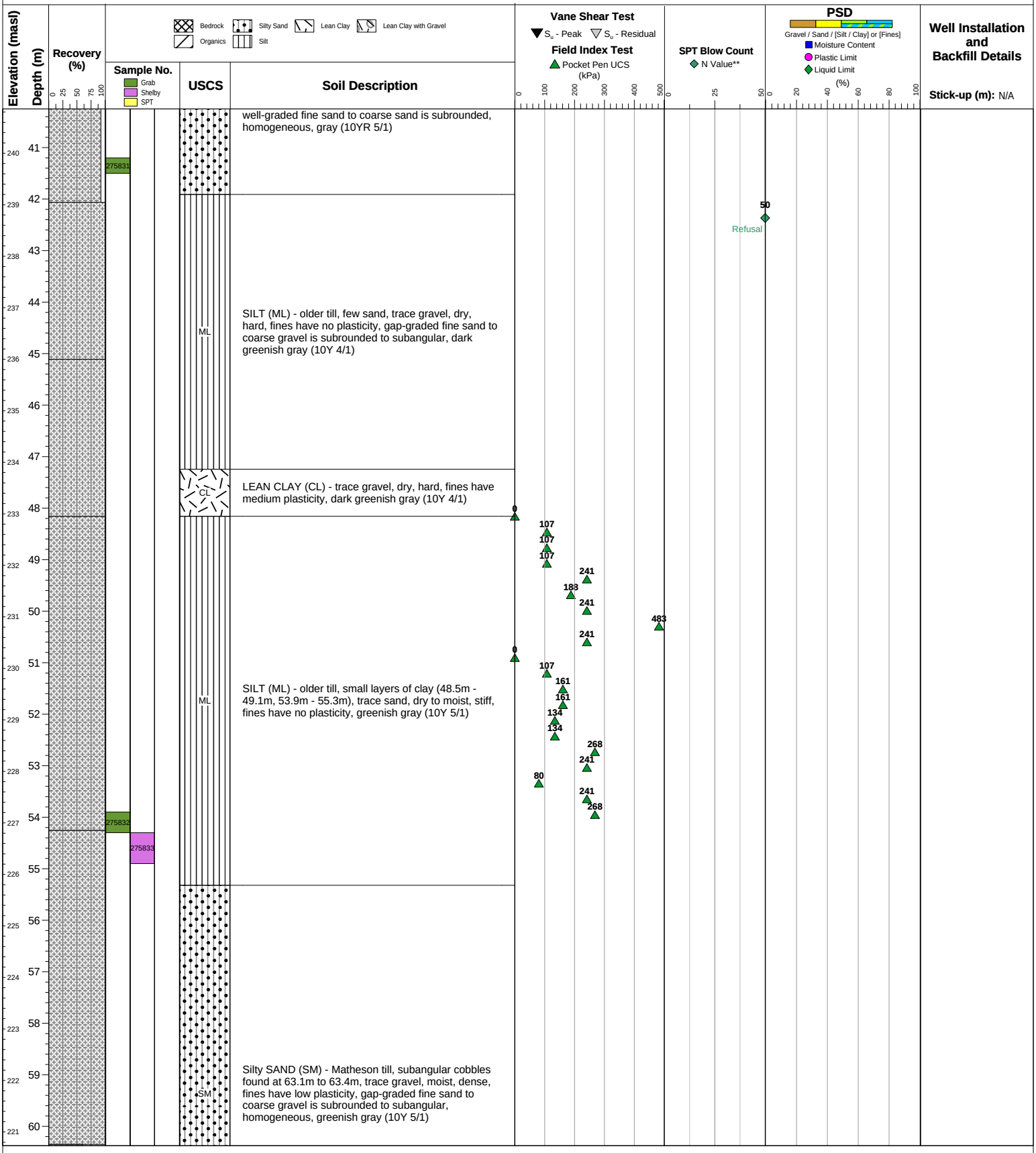
srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: SRK24-WRD-BH-215
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Barbara Amar

DRILLING DATE: 11-Mar-24 **TO:** 13-Mar-24
COORDINATES: 473009.0 E 5413538.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 281.11
TOTAL DEPTH (m): 68.9
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

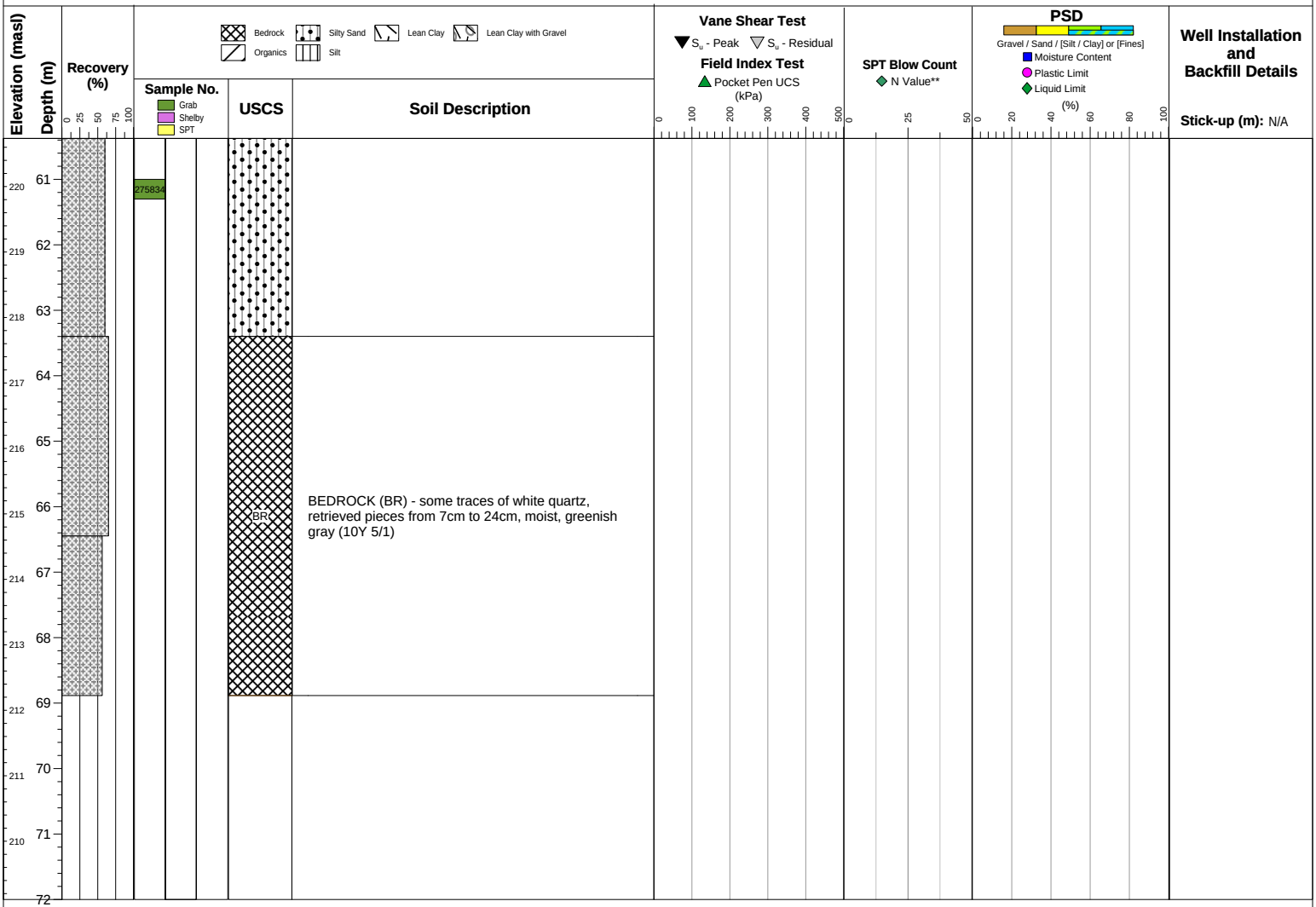
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-215
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Jasur Umarov/Barbara Amar

DRILLING DATE: 11-Mar-24 **TO:** 13-Mar-24
COORDINATES: 473009.0 E 5413538.8 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 281.11
TOTAL DEPTH (m): 68.9
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

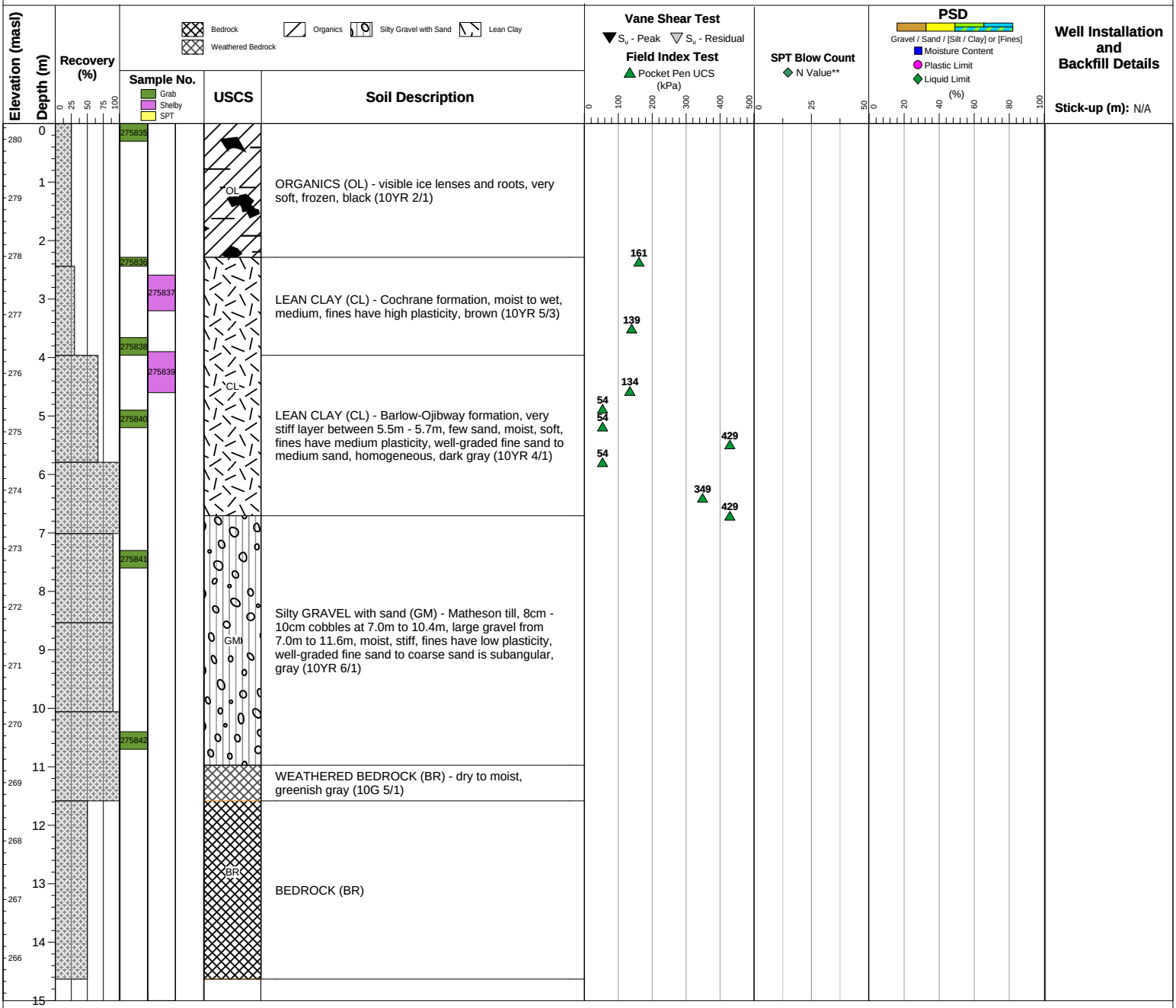
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-WRD-BH-218
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Alice Xu/Barbara Amar

DRILLING DATE: 13-Mar-24 **TO:** 14-Mar-24
COORDINATES: 473202.7 E 5414716.5 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 280.27
TOTAL DEPTH (m): 14.6
WATER LEVEL (mbgs): N/A



Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW04AB
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens/Erick Lino

DRILLING DATE: 11-Feb-24 **TO:** 12-Feb-24
COORDINATES: 470492.2 E 5411263.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 268.59
TOTAL DEPTH (m): 41.1
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock, Organics, Silty Sand, Silt, Lean Clay, Silty Clay, Fat Clay

Elevation (masl)	Depth (m)	Recovery (%)	Sample No. (Grab, Shelby, SPT)	USCS	Soil Description
268	0		202794	OL	ORGANICS (OL) - organic soil with visible roots and ice lenses, frozen, black (10YR 2/1)
	1			CL	LEAN CLAY with gravel (CL) - Cochrane formation, frozen, medium, fines have low plasticity, poorly-graded coarse sand to fine gravel, subrounded, homogeneous, light yellowish brown (10YR 6/4)
267			202795	OL	ORGANICS (OL) - organic soils with visible roots, moist to wet, black (10YR 2/1)
	2			CL	LEAN CLAY (CL) - Barlow-Ojibway formation, frozen, very stiff, fines have medium plasticity, homogeneous, gray (10YR 5/1)
266			202796	CH	FAT CLAY with gravel (CH) - Barlow-Ojibway formation, moist to wet, soft, fines have high plasticity, gap-graded fine gravel to fine gravel, subangular, homogeneous, gray (10YR 6/1)
	3				
265			202797		
	4				
264			202798		
	5				
263					
	6		202799		FAT CLAY (CH) - Barlow-Ojibway formation, few gravel, wet, very soft, fines have high plasticity, poorly-graded fine gravel to coarse gravel is subangular, homogeneous, gray (10YR 6/1)
262	7				
261	8				
260	9				
259	10				
258	11				
257			202800		
	12				
256					
	13				
255					
	14				
254			202801		FAT CLAY (CH) - Barlow-Ojibway formation, wet, very soft, fines have high plasticity, gray (10YR 5/1)
	15				
253					
	16				
252					
	17				
251					
	18		202802		
250					
	19				
249					
	20				

Vane Shear Test (S_u - Peak, S_u - Residual)
Field Index Test — Pocket Pen UCS (kPa): 322, 268, 483, 188, 215, 215, 161, 161, 107, 107, 107, 80, 322, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27, 54, 54, 27

SPT Blow Count — N Value**

PSD — Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): Well A 0.78, Well B 0.85

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details
Sand, Bentonite, PVC, Screen

srk consulting

CANADA NICKEL COMPANY

DRILLHOLE ID: ST24-BH-MW04AB
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens/Erick Lino

DRILLING DATE: 11-Feb-24 **TO:** 12-Feb-24
COORDINATES: 470492.2 E 5411263.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 268.59
TOTAL DEPTH (m): 41.1
WATER LEVEL (mbgs): N/A

PROJECT: Crawford Site Investigation 2024-QI
CLIENT: Canada Nickel Corporation

Bedrock, Organics, Silty Sand, Silt, Lean Clay, Silty Clay, Fat Clay

Elevation (masl)	Depth (m)	Recovery (%)	Sample No.	USCS	Soil Description
248	21				FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, wet, dark gray is soft, light gray is very soft, fines have high plasticity, stratified, gray (10YR 5/1)
247	22				
246	23		202803		FAT CLAY (CH) - Barlow-Ojibway formation, varved clay, wet, dark gray is soft, light gray is medium stiffness, fines have high plasticity, gray (10YR 5/1)
245	24				
244	25		202804	CL-ML	SILTY CLAY (CL-ML) - Barlow-Ojibway formation, clayey silt with rapid dilatency, wet, soft, fines have low plasticity, gray (10YR 5/1)
243	26		202805		
242	27			CL	LEAN CLAY (CL) - Barlow-Ojibway formation, wet, very soft, fines have slow dilatency and no plasticity, gray (10YR 5/1)
241	28				
240	29			SM	Silty SAND (SM) - Matheson till, trace fine to coarse gravel, trace cobbles, wet, fines have rapid dilatency and no plasticity, poorly-graded fine sand to medium sand, subrounded to subangular, gray (10YR 5/1)
239	30				
238	31		202806	ML	SILT (ML) - older till, few sand, trace gravel, trace cobbles, dry, hard, fines have slow dilatency and no plasticity, well-graded fine sand to coarse gravel, subrounded, very dark greenish gray (10Y 3/1)
237	32				
236	33				
235	34				
234	35				
233	36				
232	37				
231	38			BR	BEDROCK (BR) - moist to wet, dark olive gray (5Y 3/2)
230	39				
229	40				

Vane Shear Test: S_u - Peak, S_u - Residual
Field Index Test: Pocket Pen UCS (kPa)
SPT Blow Count: N Value**
PSD: Gravel / Sand / [Silt / Clay] or [Fines]; Moisture Content; Plastic Limit; Liquid Limit (%)

Well Installation and Backfill Details
Stick-up (m): Well A 0.78, Well B 0.85

Refusal

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details: Sand, Bentonite, PVC, Screen

srk consulting

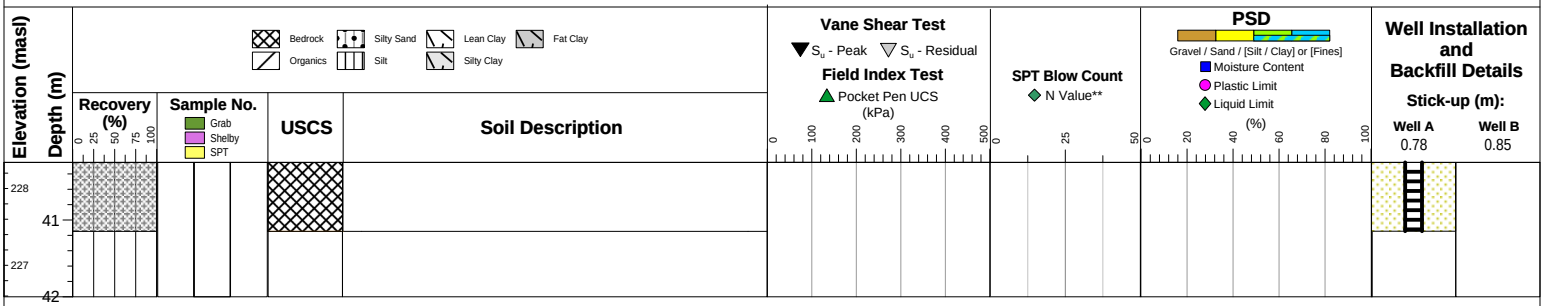
CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: ST24-BH-MW04AB
LOCATION: Impoundment Facility
PROJECT NO: CAPR003118
EQUIPMENT: Sonic Drill Model SDC 550-24
HOLE SIZE (m): 0.1016
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero/Michael Stephens/Erick Lino

DRILLING DATE: 11-Feb-24 **TO:** 12-Feb-24
COORDINATES: 470492.2 E 5411263.1 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): 268.59
TOTAL DEPTH (m): 41.1
WATER LEVEL (mbgs): N/A



Well Installation and Backfill Details

Stick-up (m):

Well A	Well B
0.78	0.85

Notes:
* Low N-values of 0 and 1 near the drilling bit are presumably caused by the sonic vibrations
** N-values of 50 are considered refusal and represent a blow count equal or higher than 50

Well Installation Details

Sand Bentonite PVC Screen

Appendix B: Test Pit Log

srk consulting

CANADA NICKEL COMPANY

PROJECT: Crawford Site Investigation 2024-QI

CLIENT: Canada Nickel Corporation

DRILLHOLE ID: SRK24-TMF-TP-01
LOCATION: Tailings Management Facility
PROJECT NO: CAPR003118
EQUIPMENT: SANY SY 155U
HOLE SIZE (m): N/A
CONTRACTOR: Choice Sonic
LOGGED BY: Andres R. Barrero

DRILLING DATE: 17-Mar-24 **TO:** 17-Mar-24
COORDINATES: 474853.0 E 5401914.0 N
DATUM: NAD83 UTM Zone 17N
GROUND EL (masl): N/A
TOTAL DEPTH (m): 4.6
WATER LEVEL (mbgs): N/A

DRAFT

Organics | Silty Gravel with Sand | Silty Sand with Gravel

Elevation (masl) / Depth (m)	Recovery (%)	Sample No. (Grab / Shelby / SPT)	USCS	Soil Description
0	N/A		OL	ORGANICS (OL) - peat
1		275972	SM	Silty SAND with gravel (SM) - trace cobbles, moist to wet, medium, fines have low plasticity, poorly-graded fine sand to fine gravel is rounded to subrounded, yellow (10YR 8/6)
2		275973		Silty SAND with gravel (SM) - older till, moist, very stiff, fines have low plasticity, poorly-graded fine sand to coarse sand is subrounded to subangular, yellow (10YR 7/6)
3			GM	Silty GRAVEL with sand (GM) - older till, moist, very stiff, fines have low plasticity, poorly-graded fine sand to fine gravel is subrounded to subangular, gray (10YR 6/1)
4				End of hole

Vane Shear Test (S_u - Peak, S_u - Residual)
Field Index Test Pocket Pen UCS (kPa) 0 100 200 300 400 500

SPT Blow Count N Value 0 25 50

PSD Gravel / Sand / [Silt / Clay] or [Fines]
Moisture Content
Plastic Limit
Liquid Limit
(%) 0 20 40 60 80 100

Well Installation and Backfill Details

Stick-up (m): N/A

Photo SRK24-TMF-TP-01:



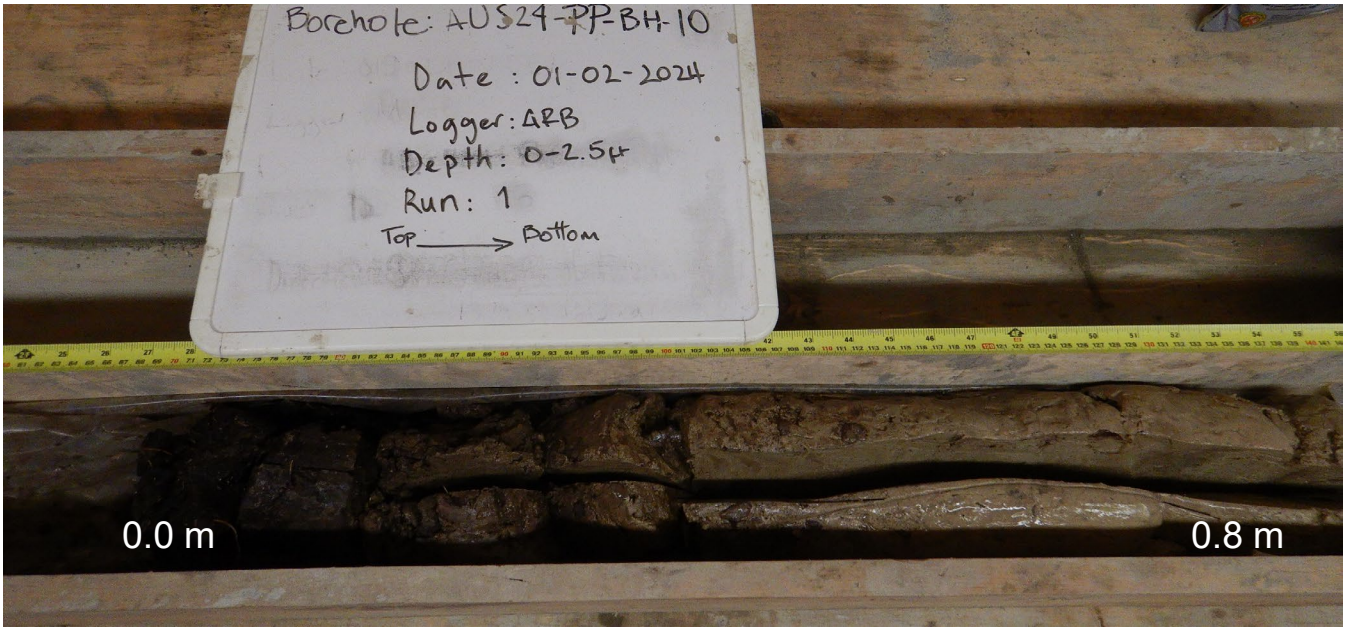
Note: Test terminated after machine reached refusal at 4.6 meters

Appendix C: Core Photologs

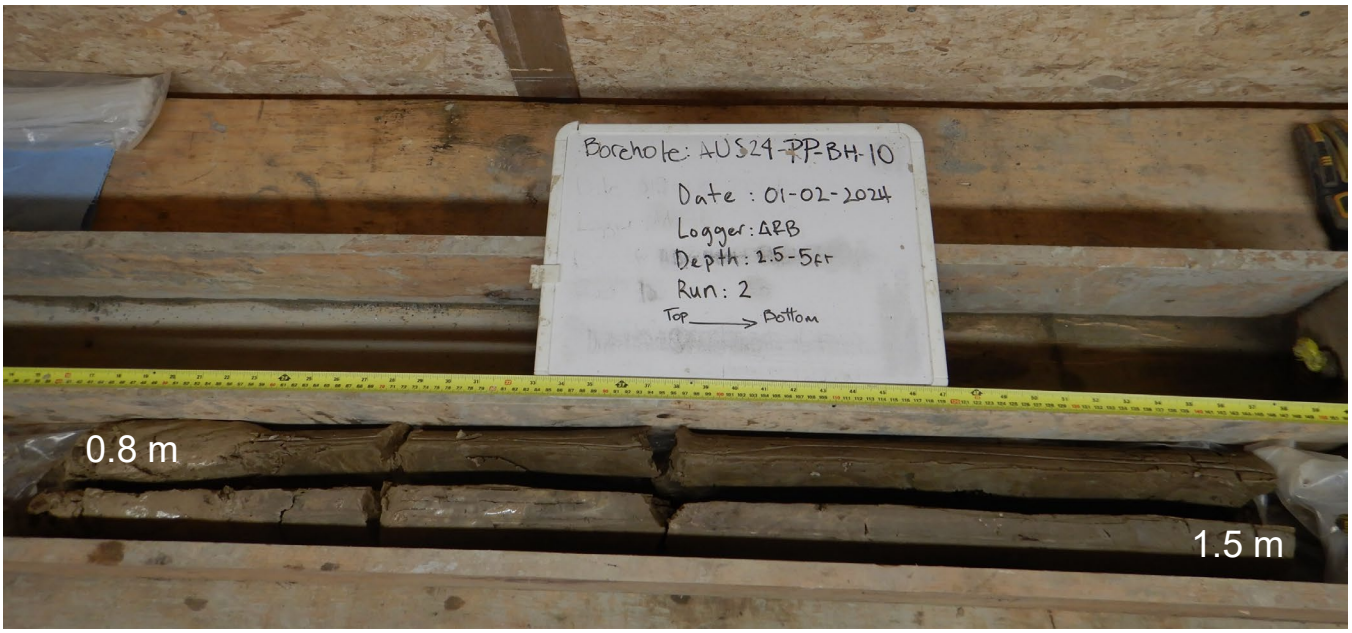
AUS24-PP-BH-10

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: January 2024	Approved:	Figure:

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



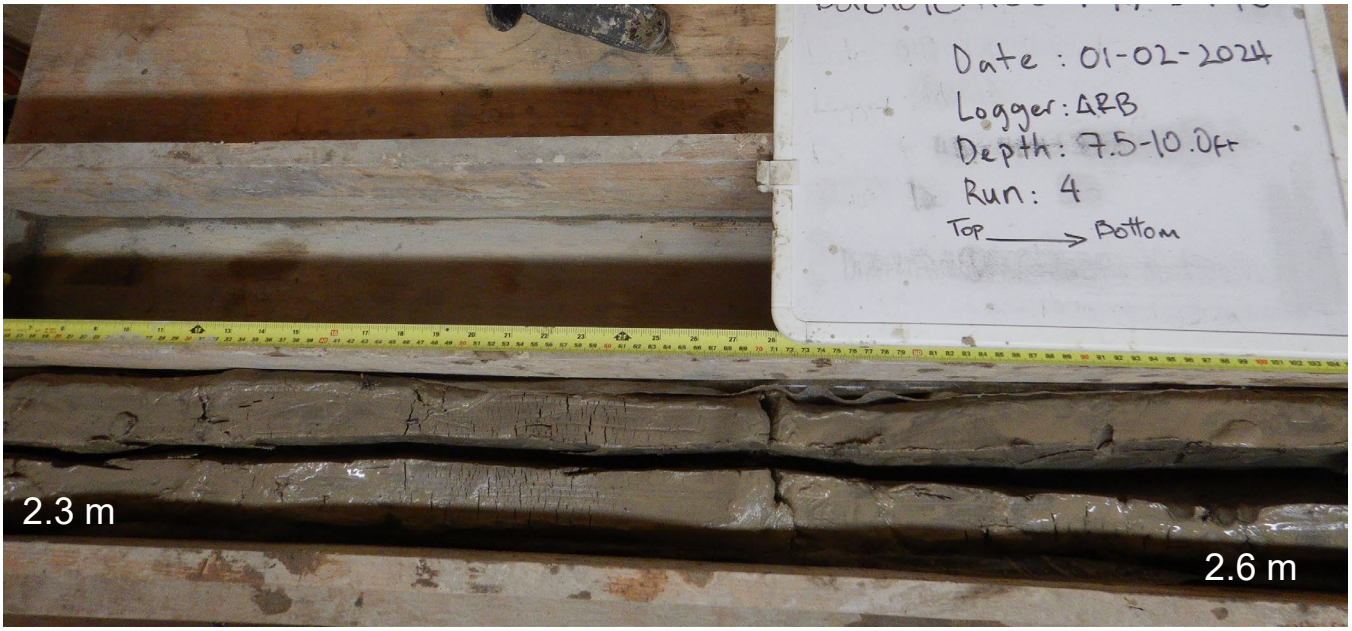
Depth (m): 0.0 -0.8



Depth (m): 0.8 – 1.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-10		
		Depth (m): 0.0 – 1.5		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 8**

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



Depth (m): 2.3 – 2.6



Depth (m): 2.5 – 3.0

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



Depth (m): 3.0 – 5.5



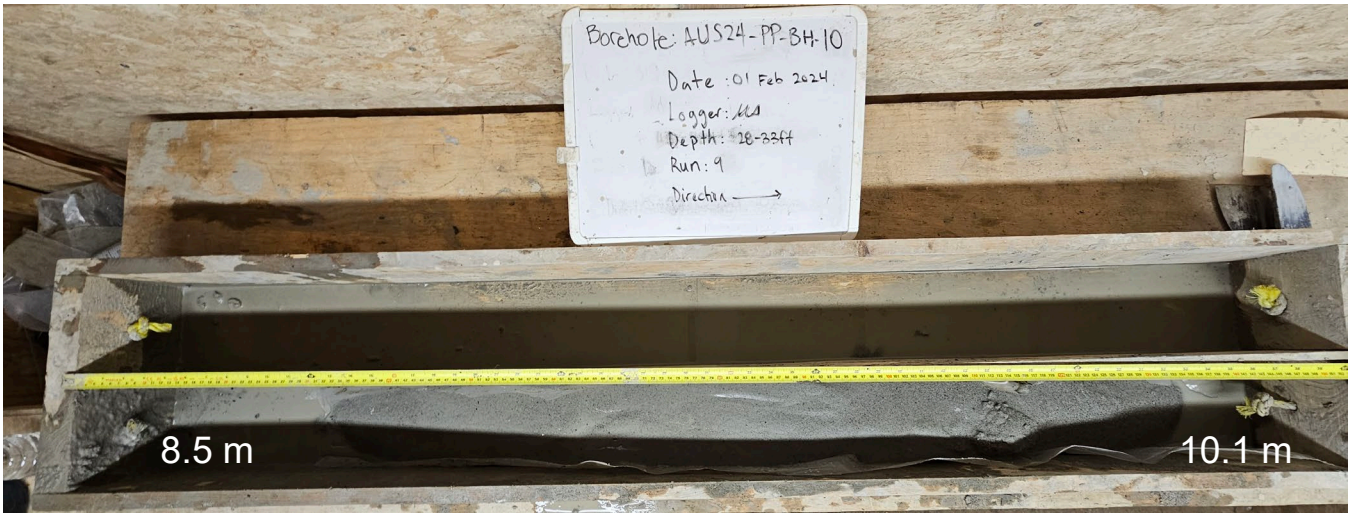
Depth (m): 5.5 – 7.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-10		
		Depth (m): 3.0 – 7.0		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 8**

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



Depth (m): 7.0 – 8.5



Depth (m): 8.5 – 10.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-10** **Depth (m): 7.0 – 10.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 8**

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



Depth (m): 10.1 – 11.6



Depth (m): 11.6 – 13.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-10** **Depth (m): 10.1 – 13.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 8**

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



Depth (m): 13.1 – 14.6



Depth (m): 14.6 – 16.2

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



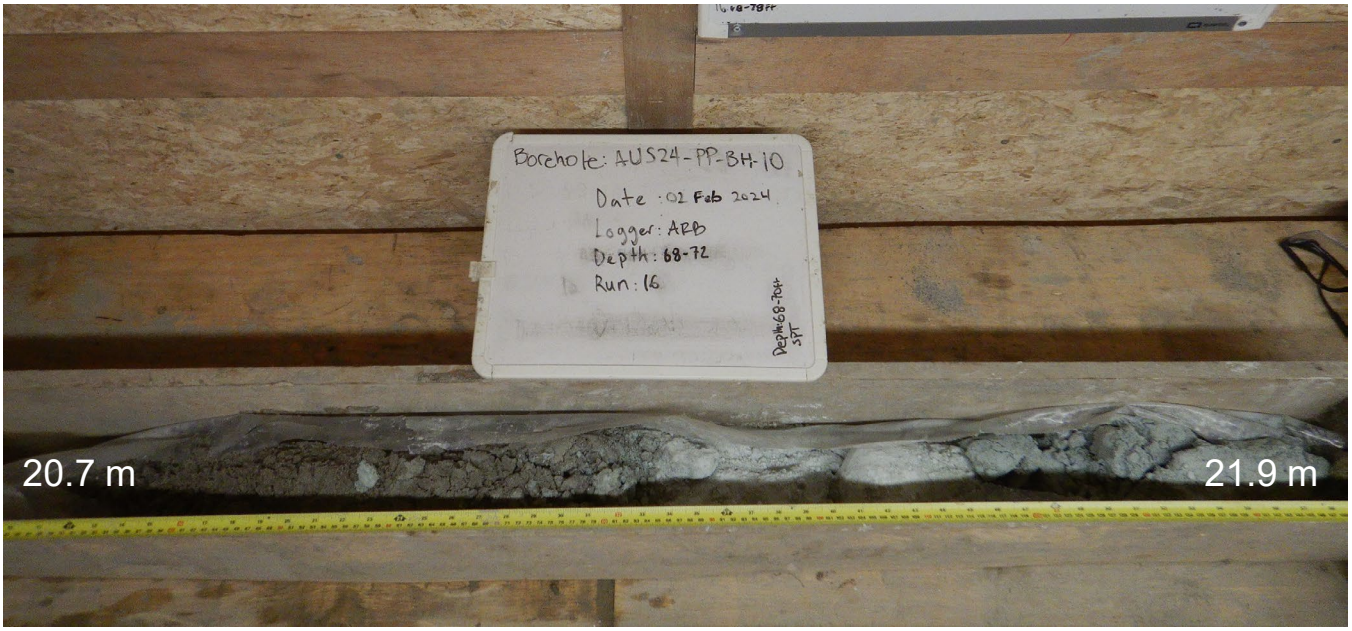
Depth (m): 16.2 – 17.7



Depth (m): 17.7 – 20.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-10** **Depth (m): 16.2 – 20.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 8**

Borehole ID: AUS24-PP-BH-10
Location: Process Plant



Depth (m): 20.7 – 21.9



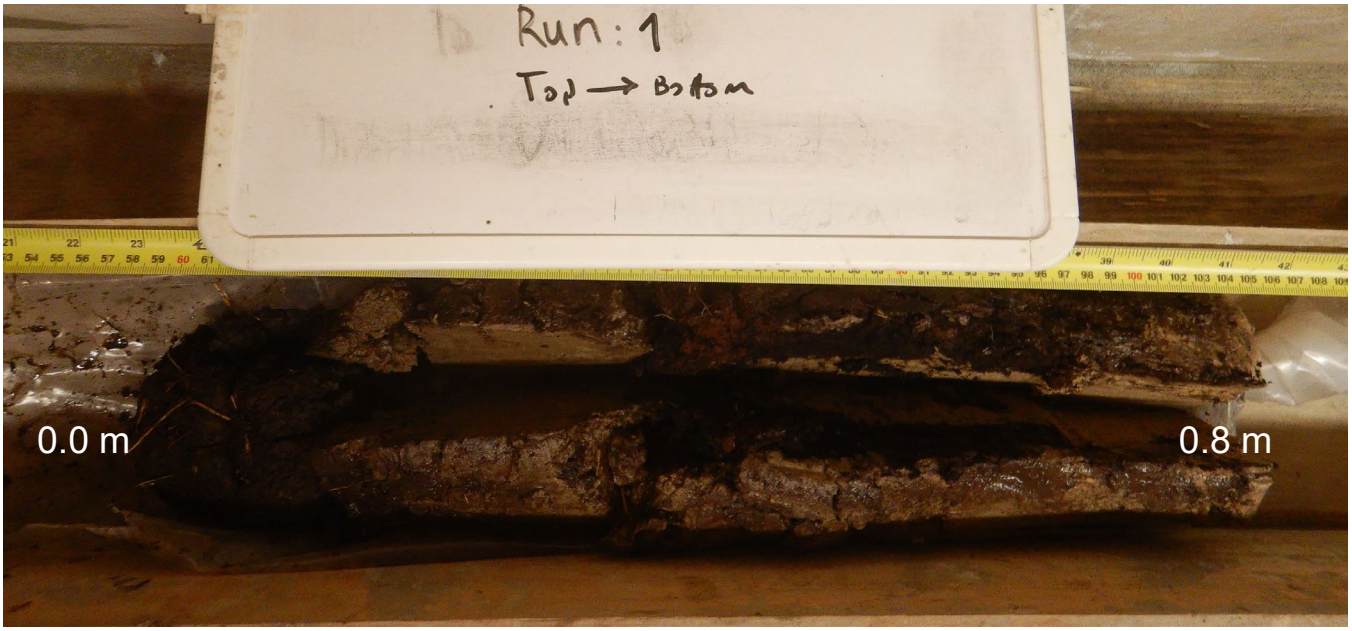
Depth (m): 21.9 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-10 **Depth (m): 20.7 – 26.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 8**

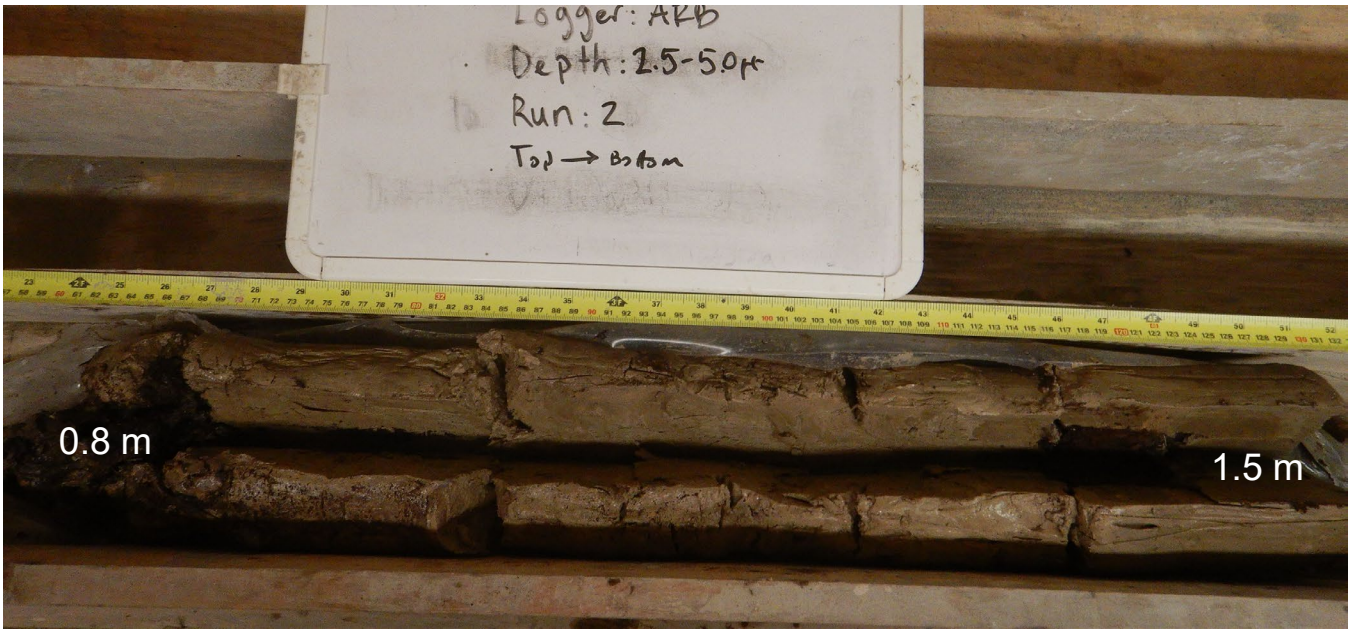
AUS24-PP-BH-11

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



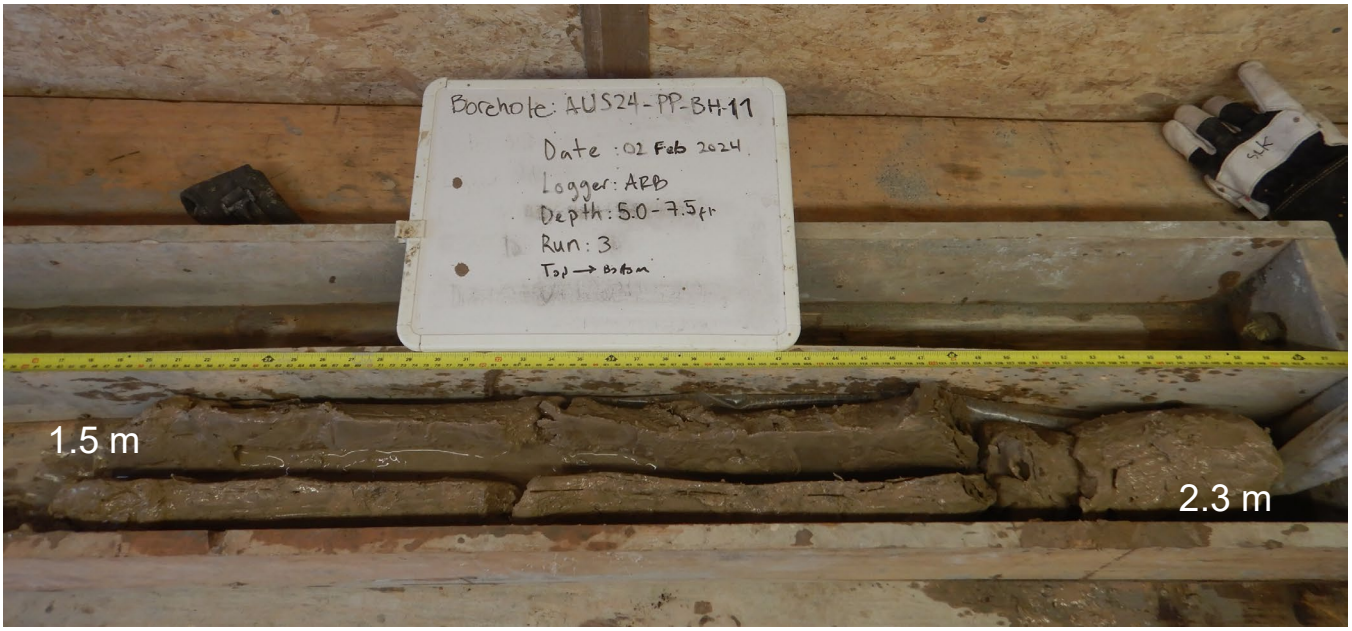
Depth (m): 0.0 – 0.8



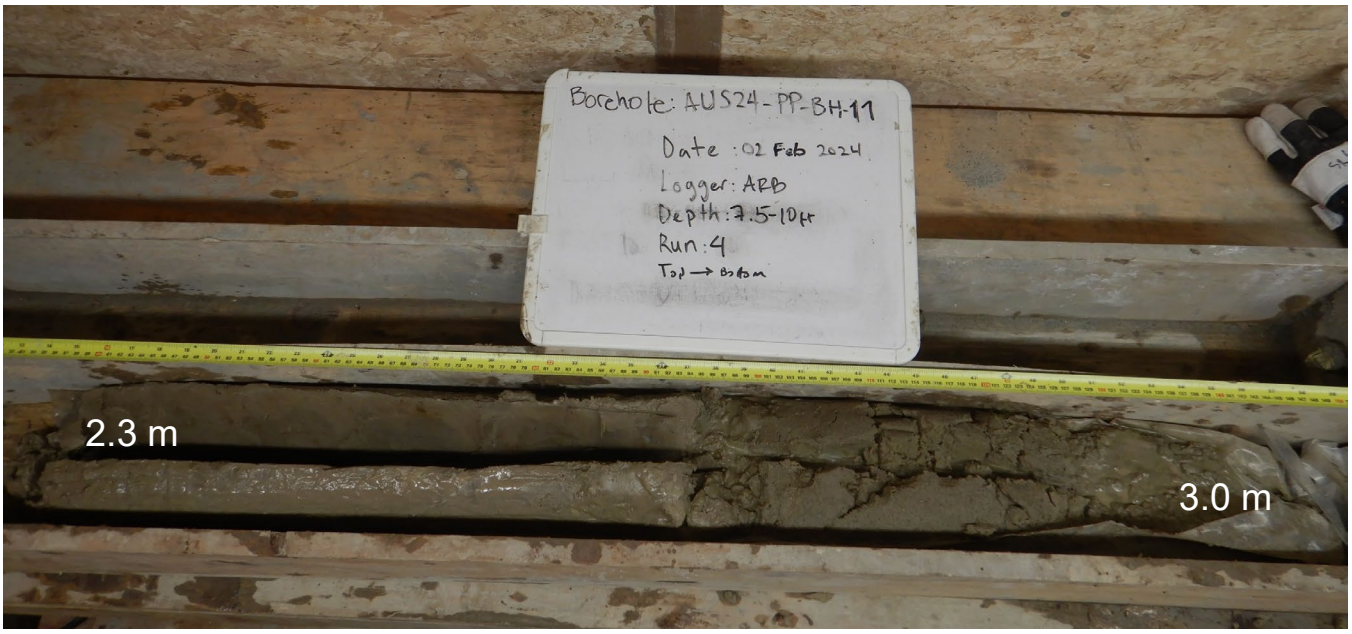
Depth (m): 0.8 – 1.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-11		
		Depth (m): 0.0 – 1.5		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



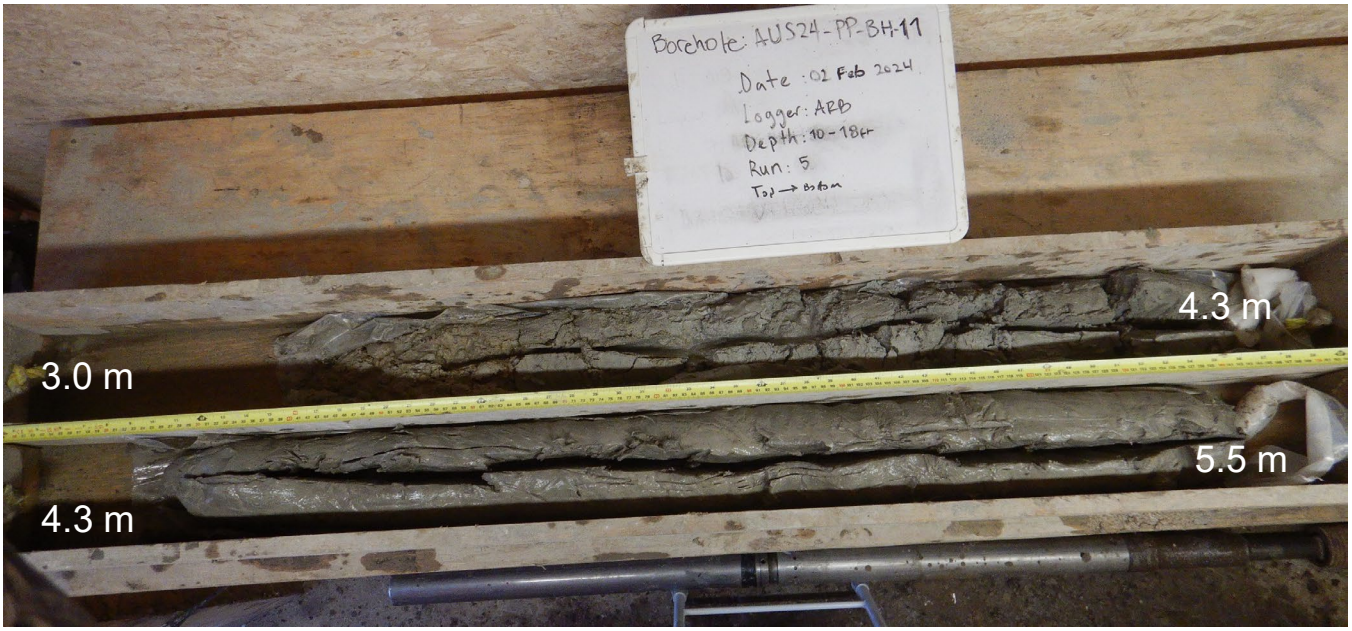
Depth (m): 1.5 – 2.3



Depth (m): 2.3 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-11		
		Depth (m): 1.5 – 3.0		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



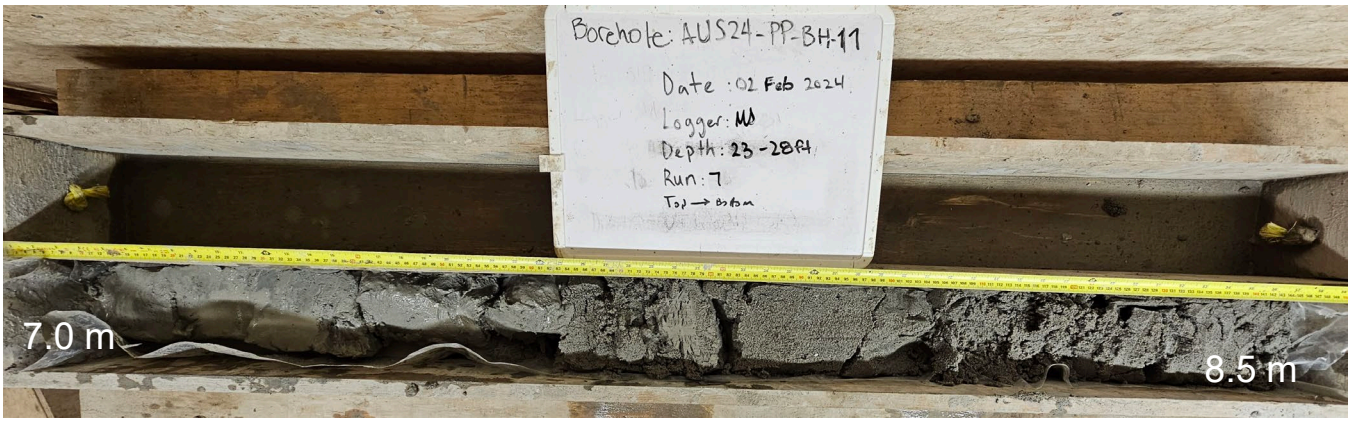
Depth (m): 3.0 – 5.5



Depth (m): 5.5 – 7.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-11		
		Depth (m): 3.0 – 7.0		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



Depth (m): 7.0 – 8.5



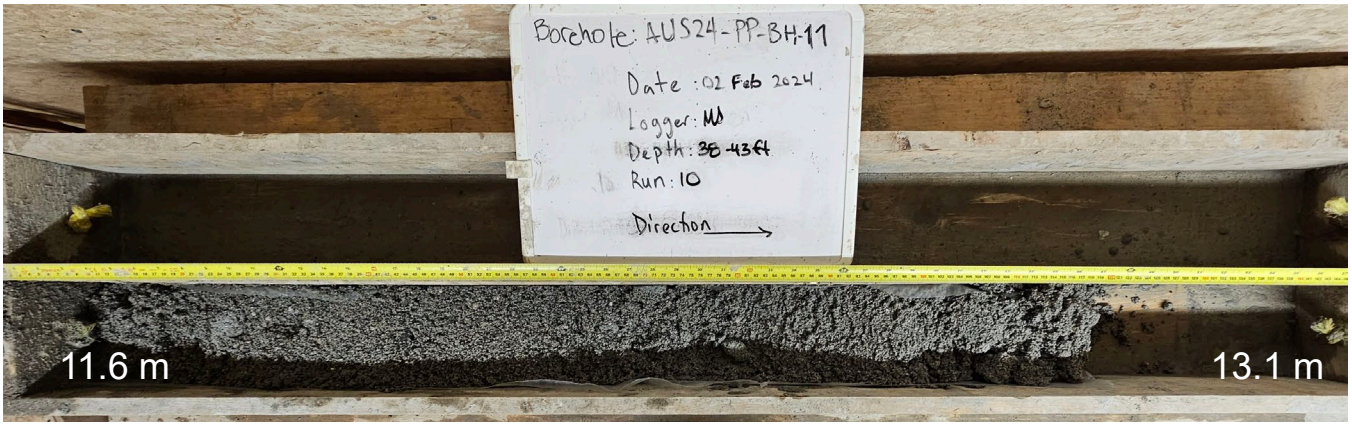
Depth (m): 8.5 – 10.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-11** **Depth (m): 7.0 – 10.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



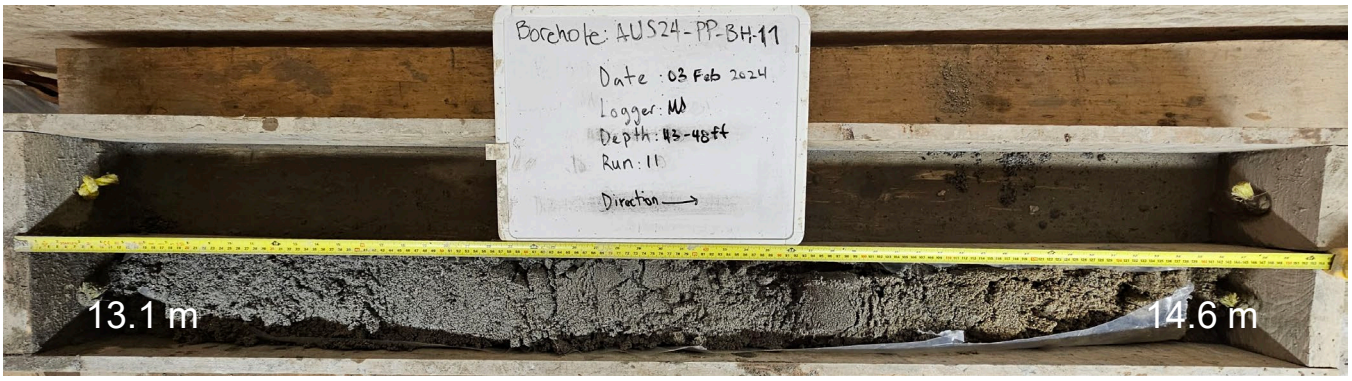
Depth (m): 10.1 – 11.6



Depth (m): 11.6 – 13.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-11** **Depth (m): 10.1 – 13.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



Depth (m): 13.1 – 14.6



Depth (m): 14.6 – 16.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-11** **Depth (m): 13.1 – 16.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



Depth (m): 16.2 – 17.7



Depth (m): 17.7 – 20.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-11 **Depth (m): 16.2 – 20.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



Depth (m): 20.7 – 23.8



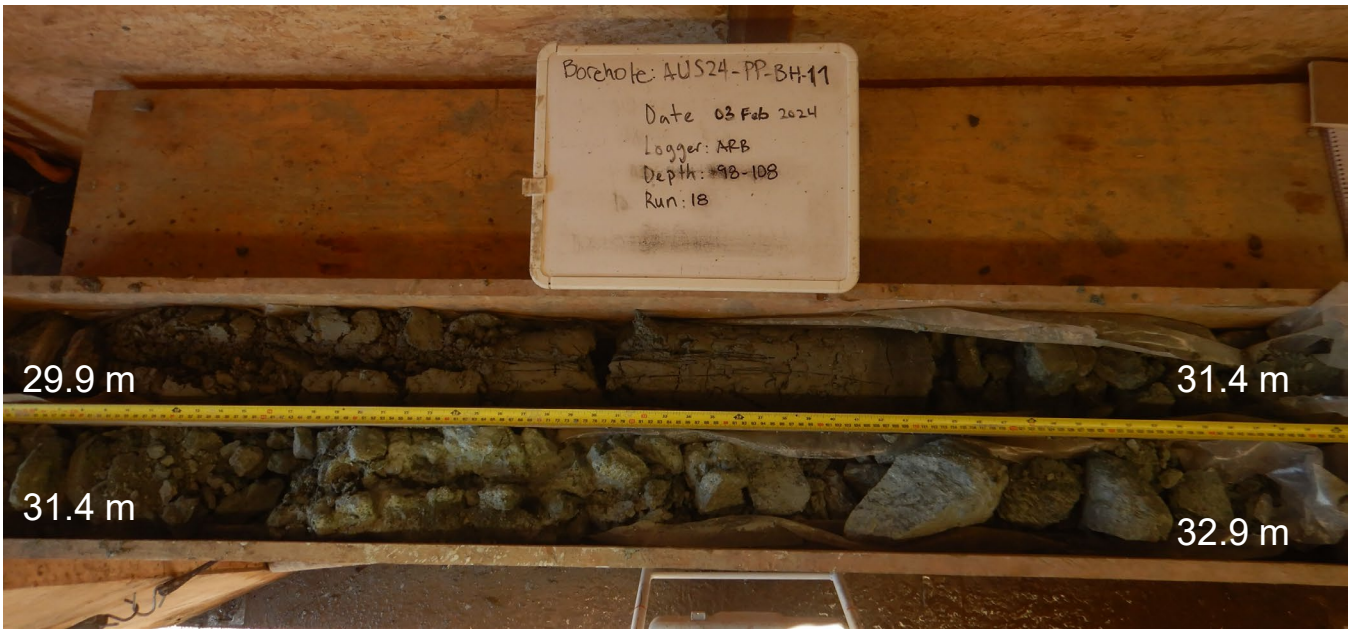
Depth (m): 23.8 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-11** **Depth (m): 20.7 – 26.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



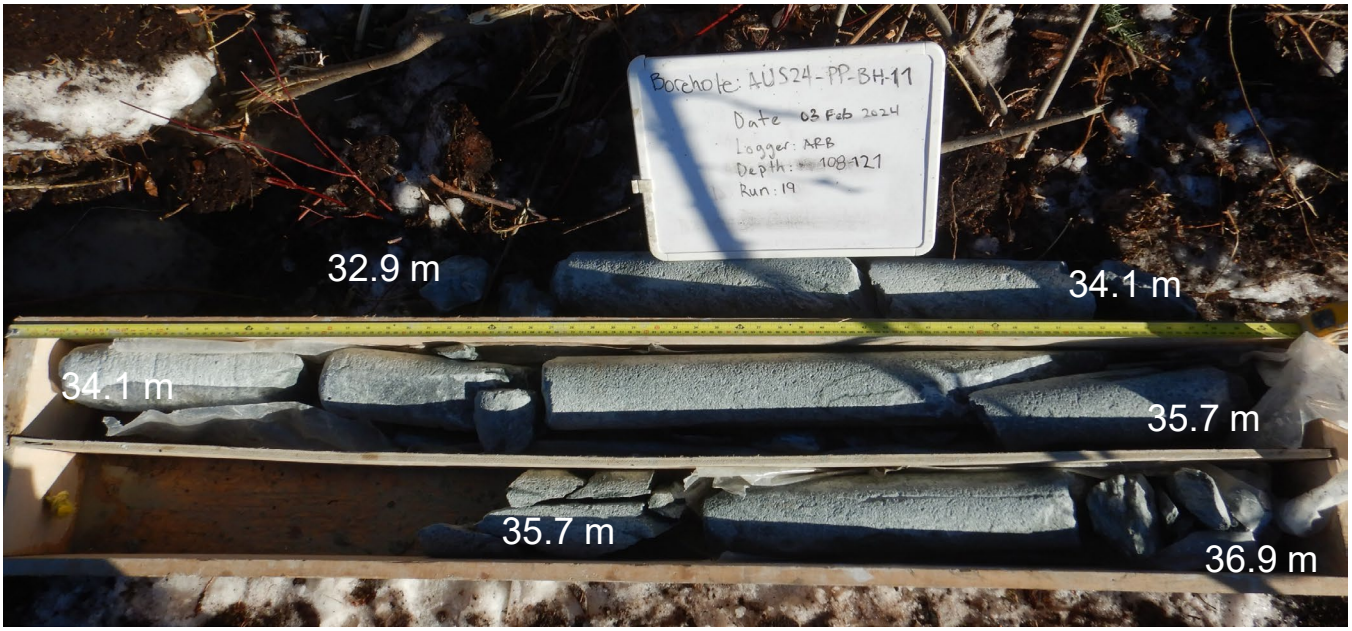
Depth (m): 26.8 – 29.9



Depth (m): 29.9 – 32.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-11** **Depth (m): 26.8 – 32.9**
Job No: CAPR000801	Crawford	Date: February 2024 / Approved: ARB / Figure: **9 of 10**

Borehole ID: AUS24-PP-BH-11
Location: Process Plant



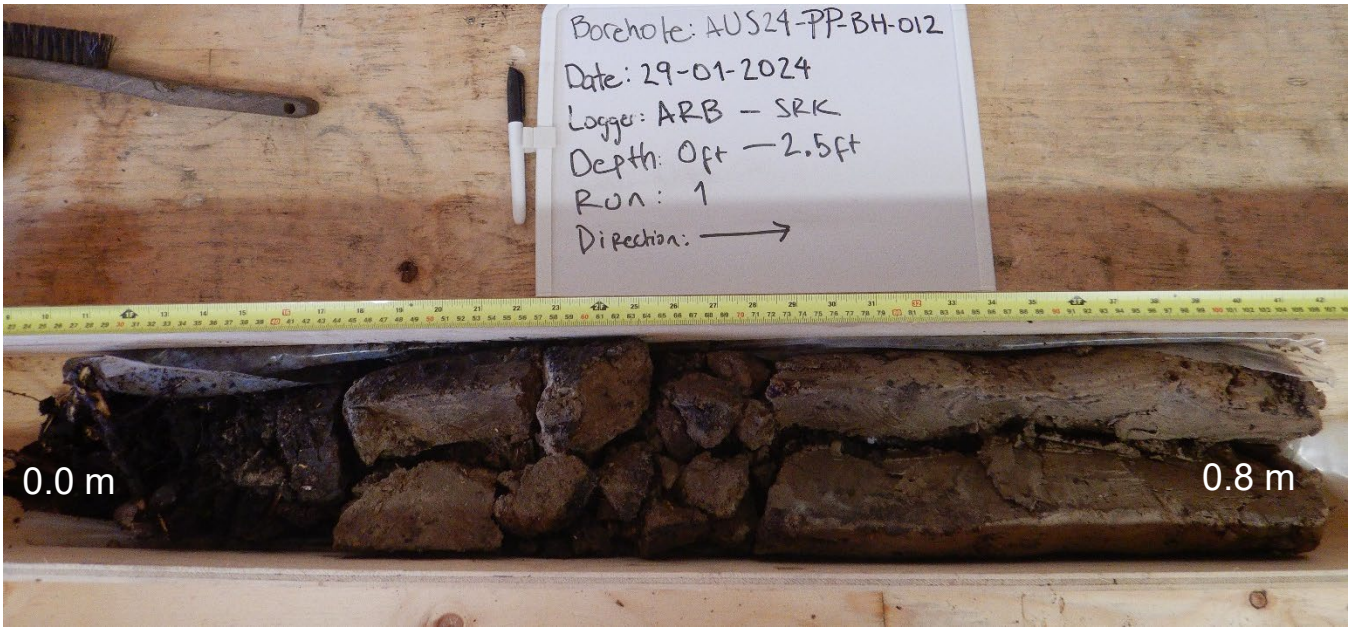
Depth (m): 32.9 – 36.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-11		
		Depth (m): 32.9 – 36.9		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 10**

AUS24-PP-BH-12

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: January 2024	Approved:	Figure:

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



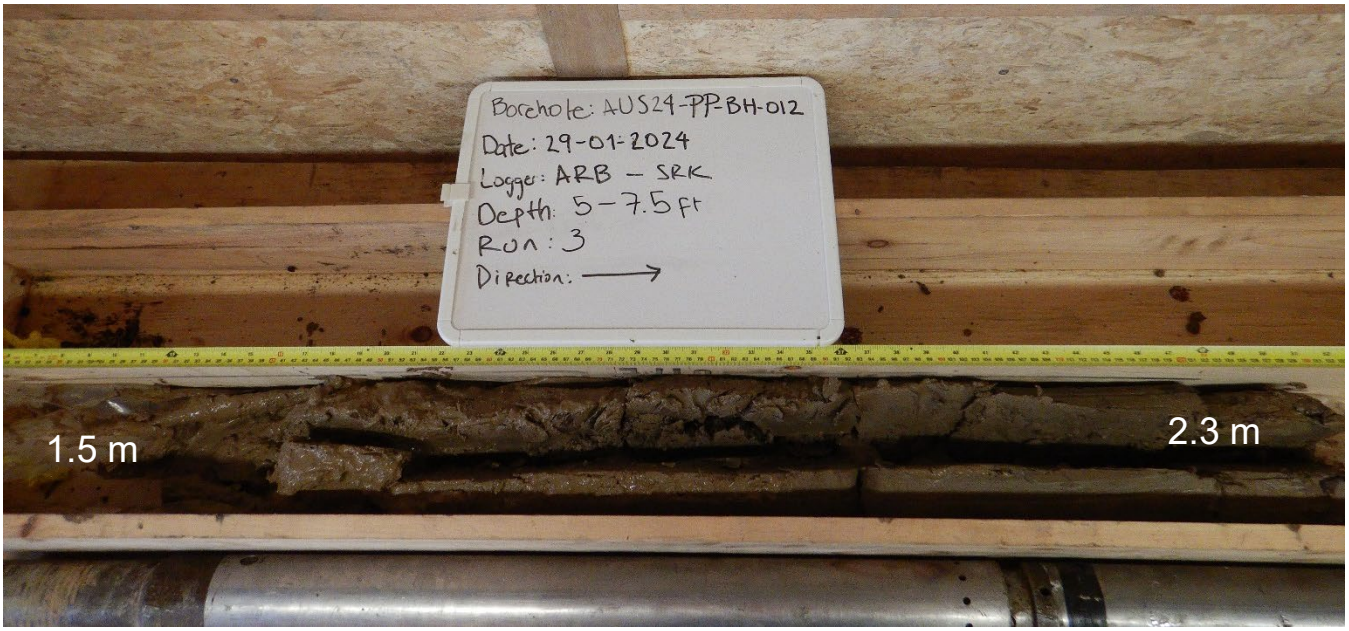
Depth (m): 0.0 – 0.8



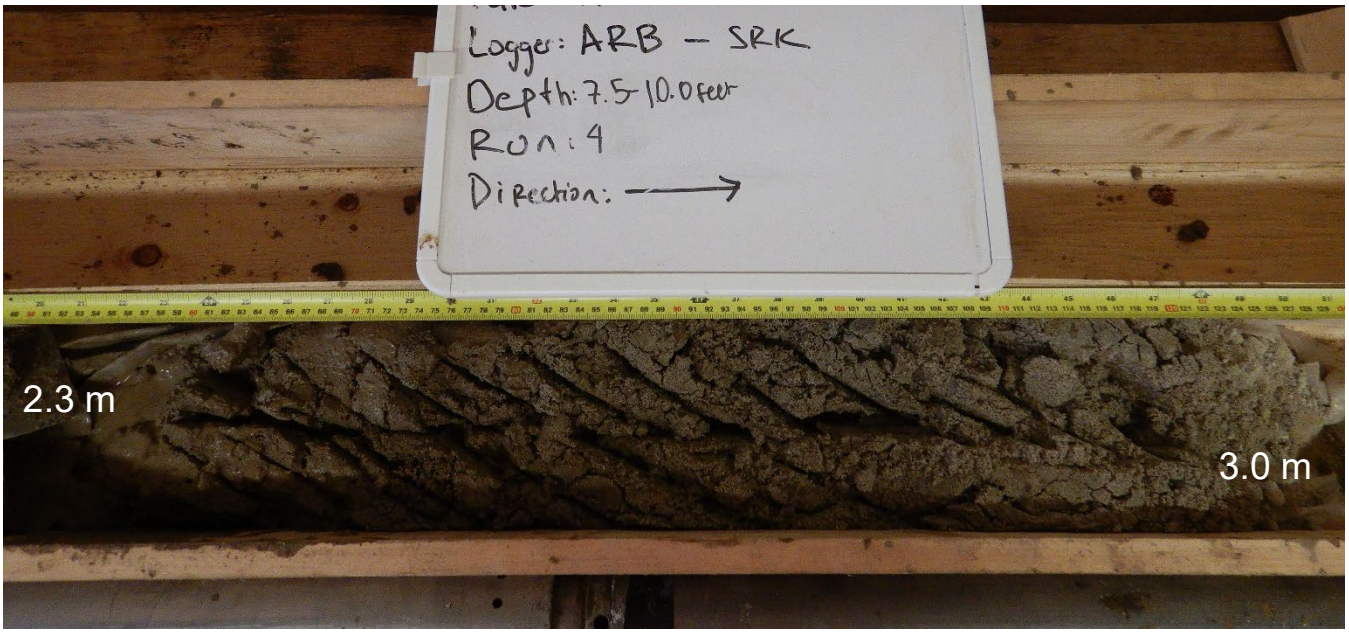
Depth (m): 0.8 – 1.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-12		
		Depth (m): 0.0 – 1.5		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **1 of 12**

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 1.5 – 2.3



Depth (m): 2.3 – 3.0

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 3.0 – 3.4



Depth (m): 3.4 – 3.8

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 3.8 – 4.2



Depth (m): 4.2 – 4.6

Borehole ID: AUS24-PP-BH-12
Location: Process Plant

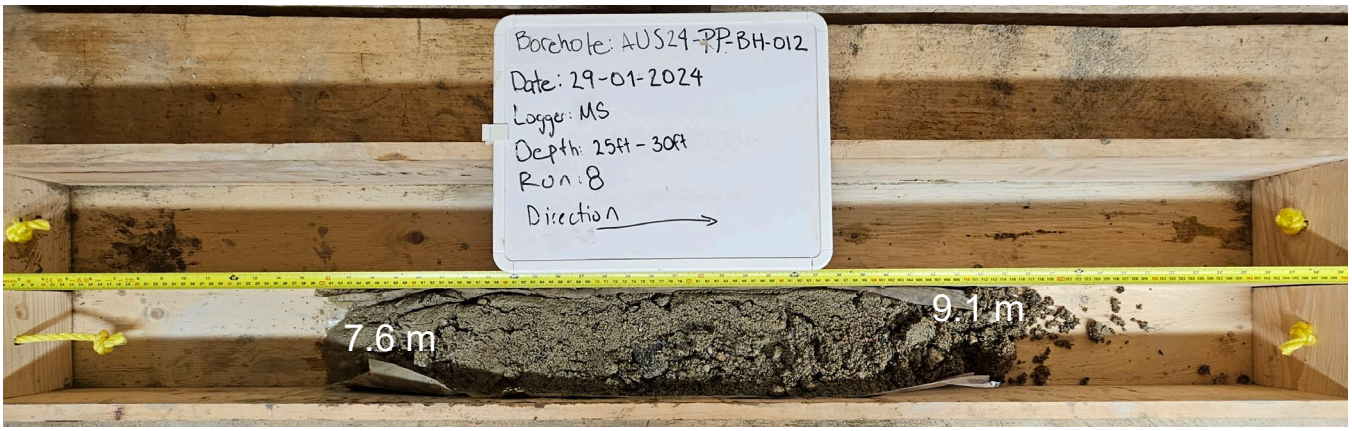


Depth (m): 4.6 – 6.1



Depth (m): 6.1 – 7.6

Borehole ID: AUS24-PP-BH-12
Location: Process Plant

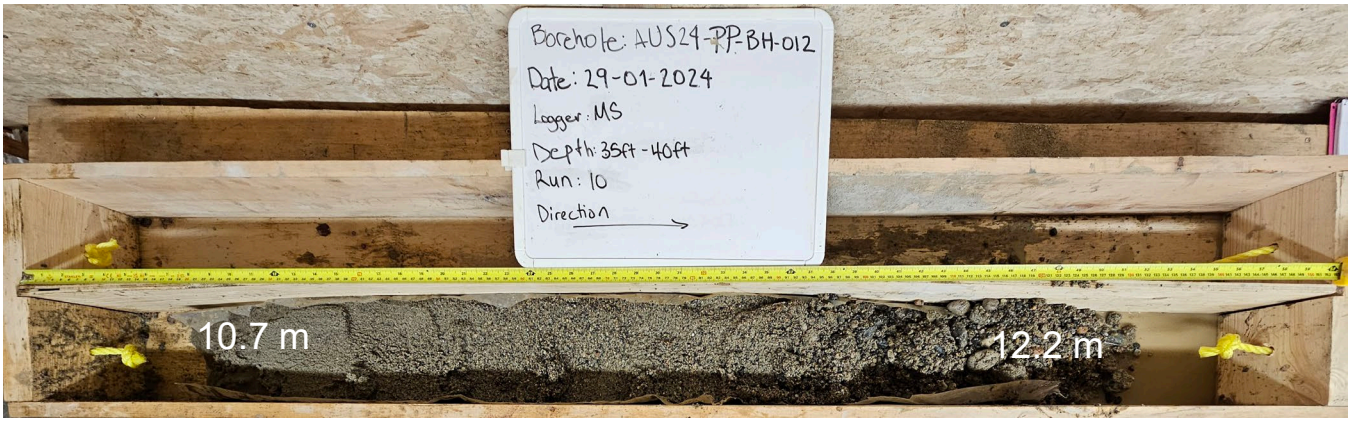


Depth (m): 7.6 – 9.1

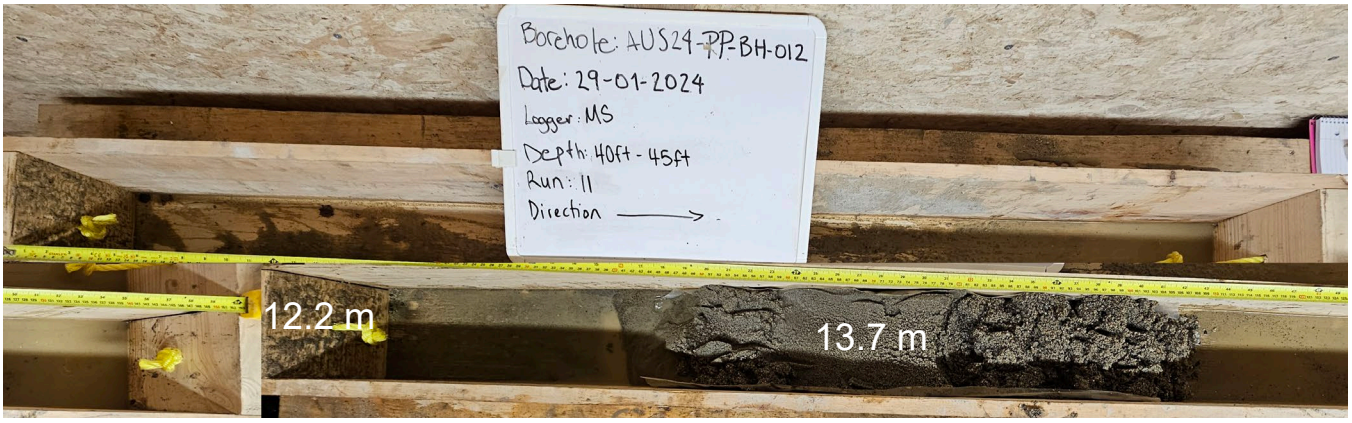


Depth (m): 9.1 – 10.7

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 10.7 – 12.2



Depth (m): 12.2 – 13.7

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 13.7 – 15.2



Depth (m): 15.2 – 16.8

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 16.8 – 17.7



Depth (m): 17.7 – 20.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-12		
		Depth (m): 16.8 – 20.7		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **9 of 12**

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



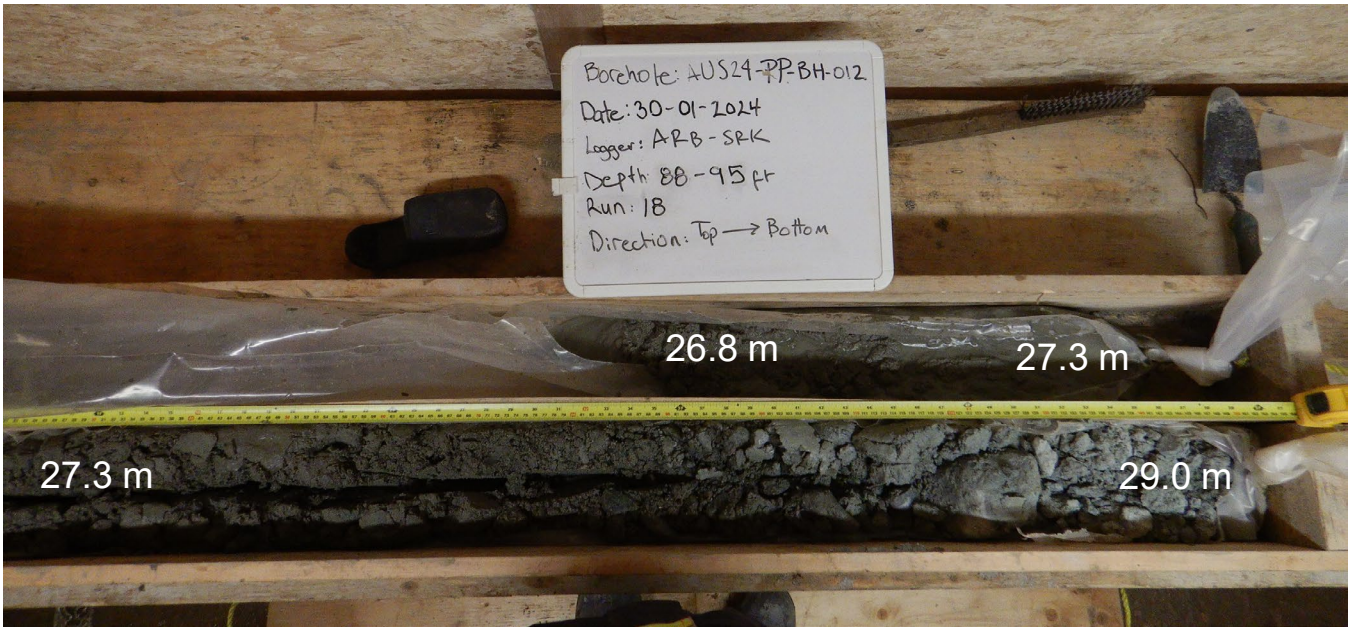
Depth (m): 20.7 – 23.8



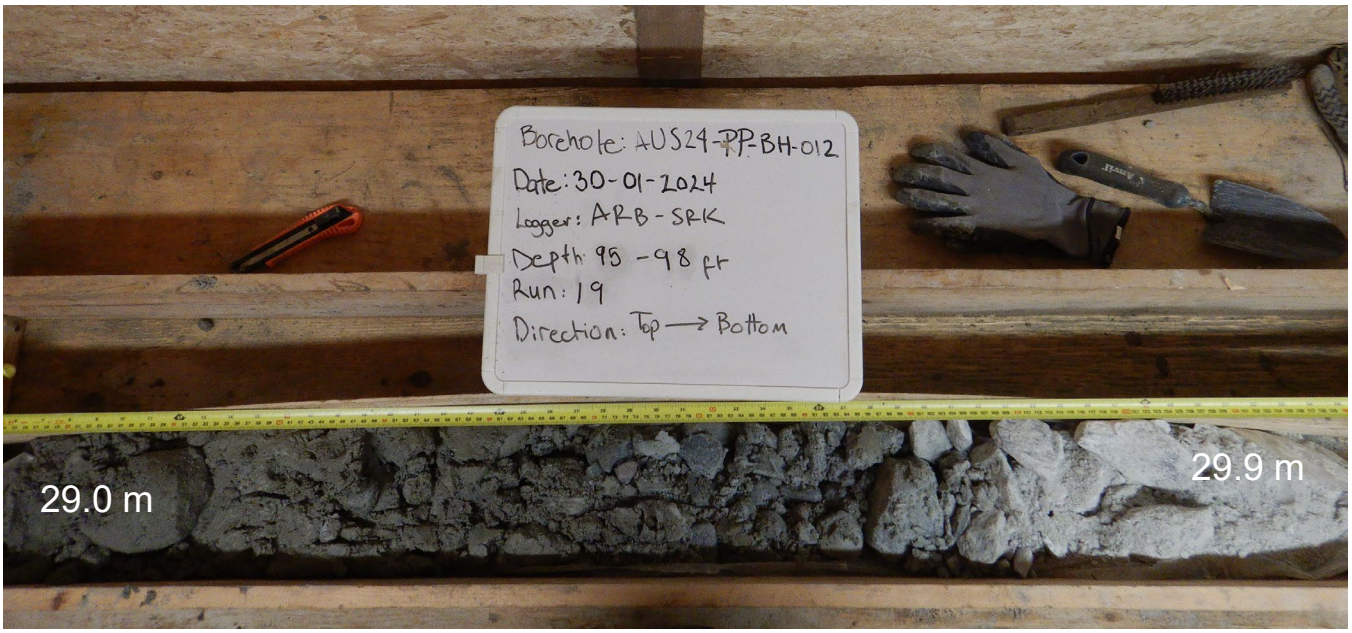
Depth (m): 23.8 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-12** **Depth (m): 20.7 – 26.8**		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **10 of 12**

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



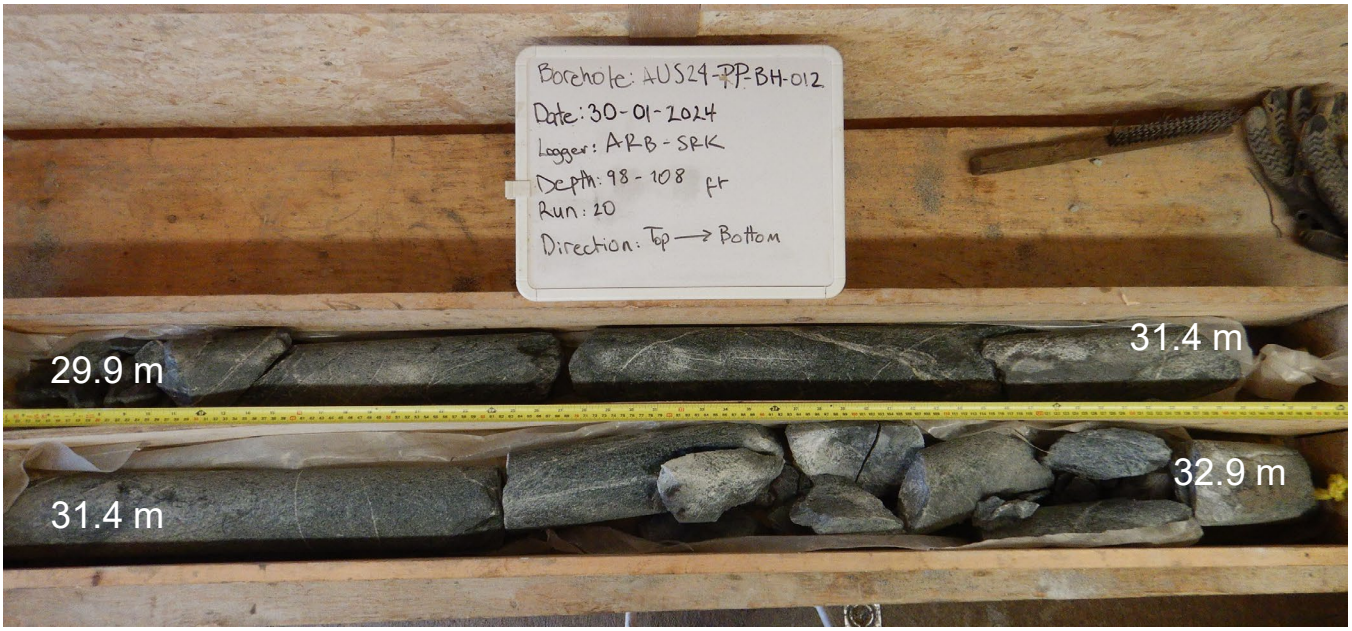
Depth (m): 26.8 – 29.0



Depth (m): 29.0 – 29.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-12		
		Depth (m): 26.8 – 29.9		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **11 of 12**

Borehole ID: AUS24-PP-BH-12
Location: Process Plant



Depth (m): 29.9 – 32.9

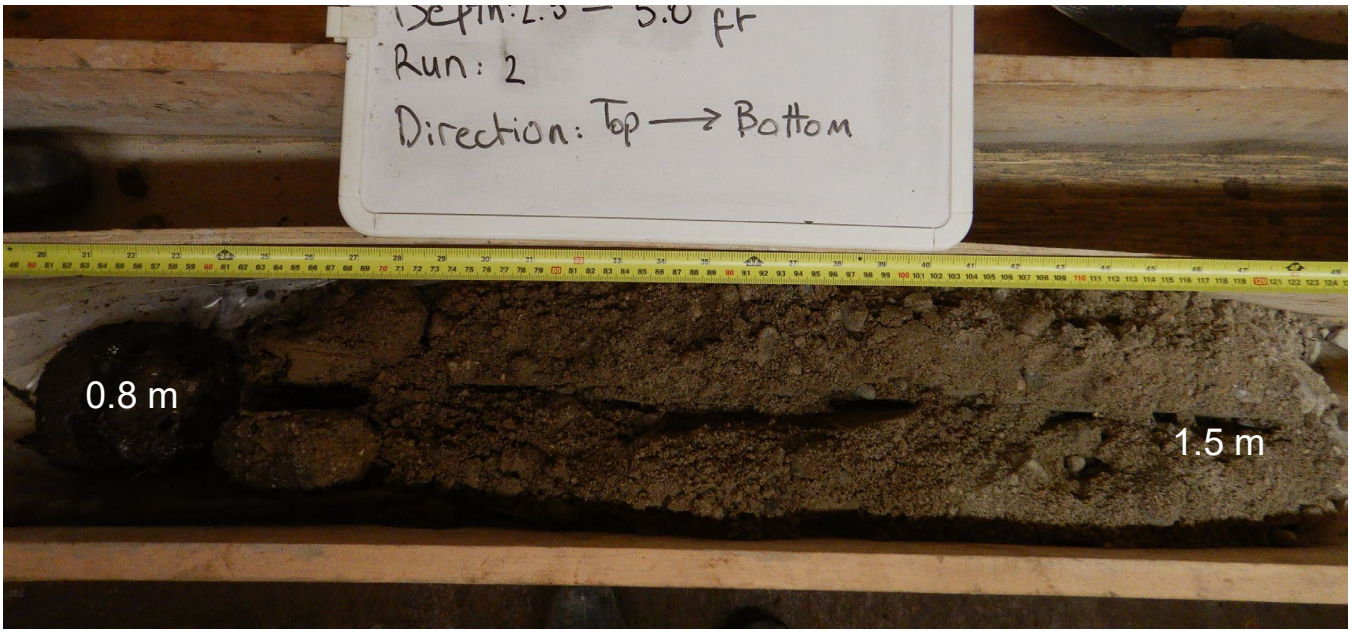
AUS24-PP-BH-14

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: January 2024	Approved:	Figure:

Borehole ID: AUS24-PP-BH-14
Location: Process Plant

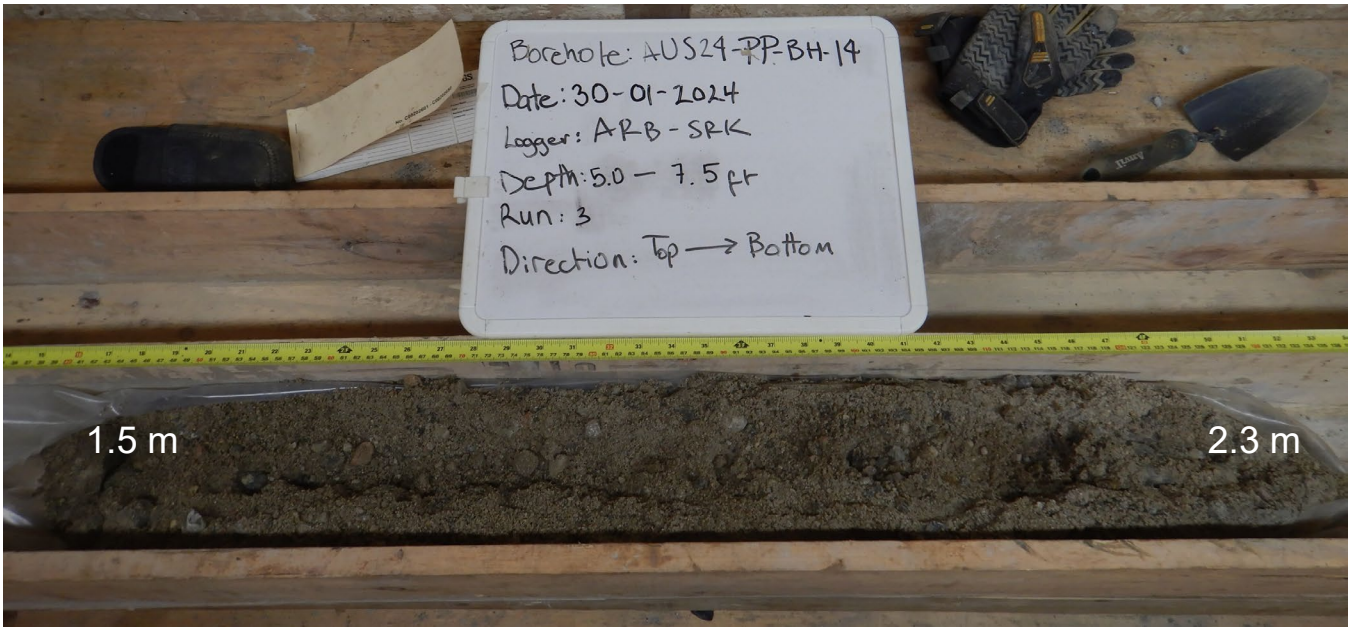


Depth (m): 0.0 – 0.8

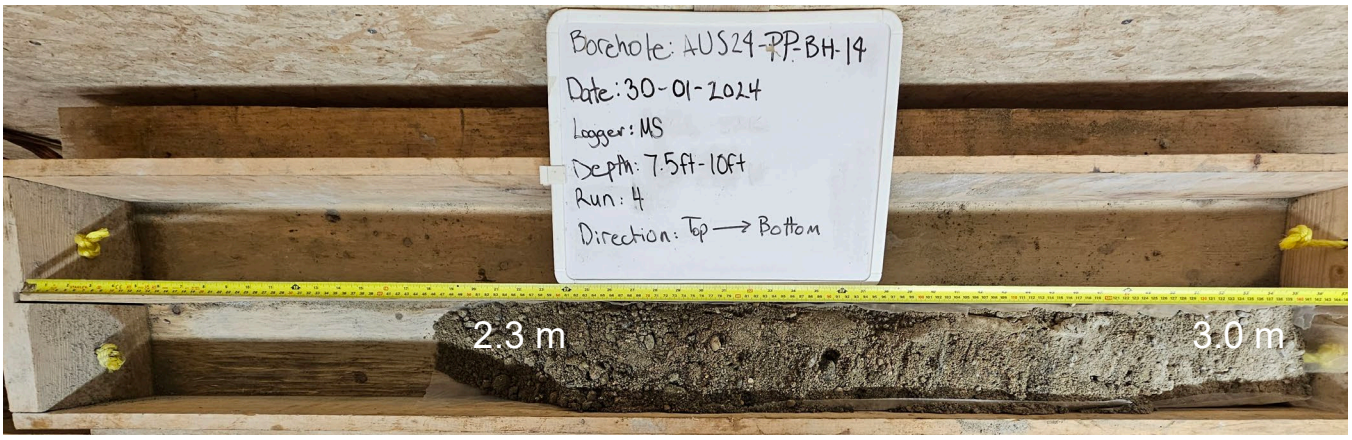


Depth (m): 0.8 – 1.5

Borehole ID: AUS24-PP-BH-14
Location: Process Plant



Depth (m): 1.5 – 2.3

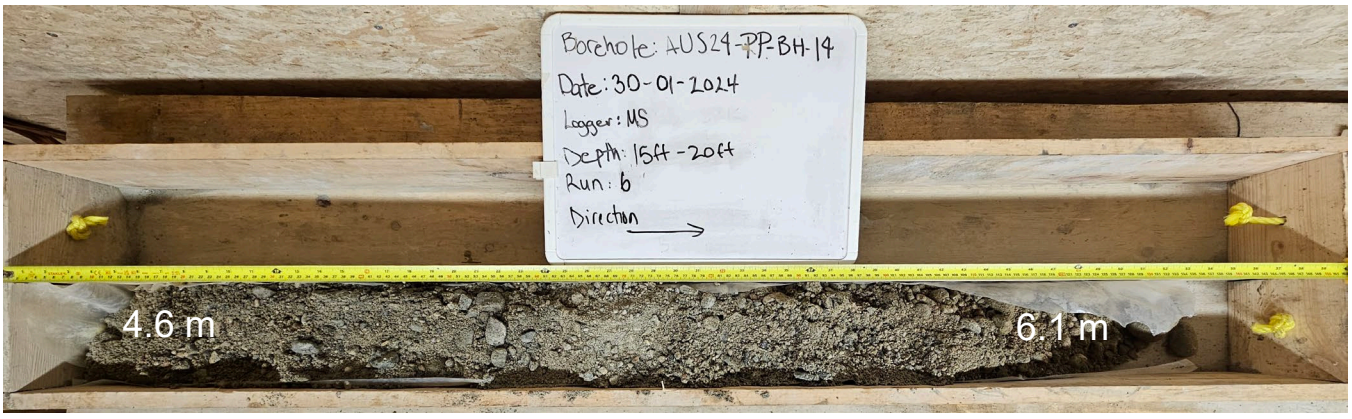


Depth (m): 2.3 – 3.0

Borehole ID: AUS24-PP-BH-14
Location: Process Plant

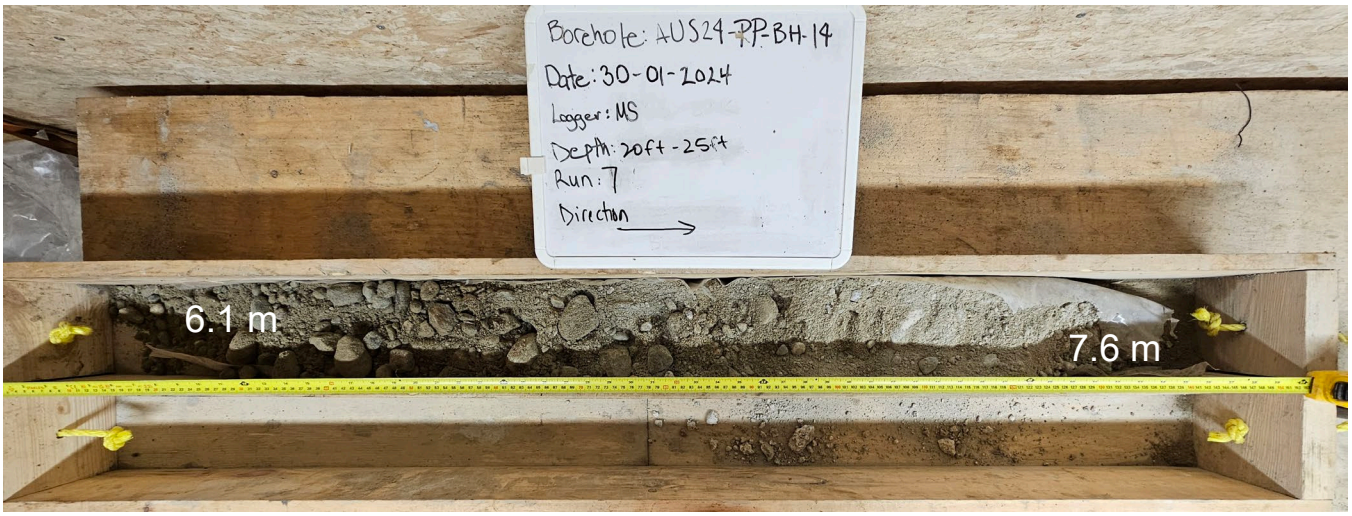


Depth (m): 3.0 – 4.6

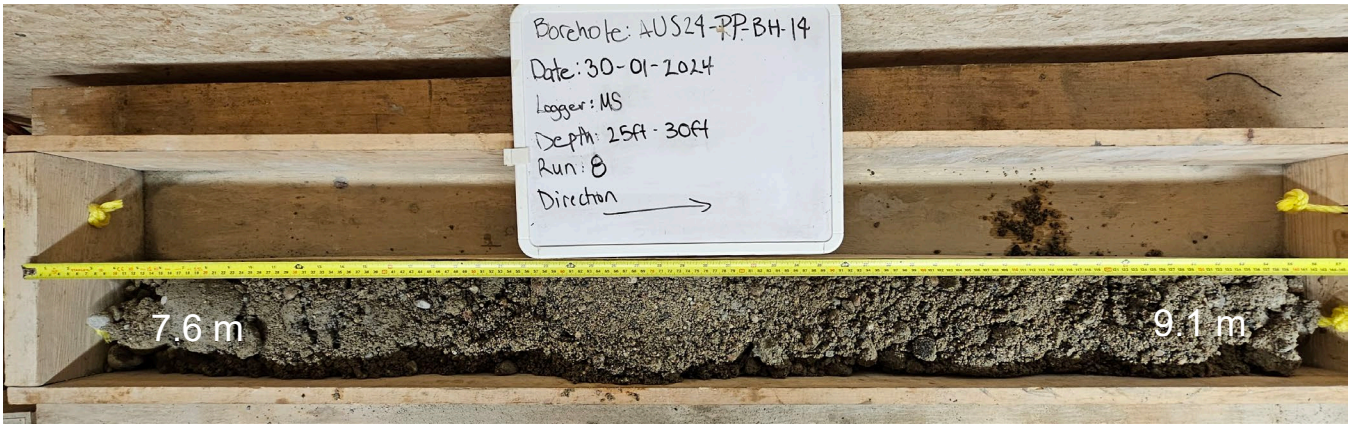


Depth (m): 4.6 – 6.1

Borehole ID: AUS24-PP-BH-14
Location: Process Plant



Depth (m): 6.1 – 7.6



Depth (m): 7.6 – 9.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-14** **Depth (m): 6.1 – 9.1**		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **4 of 10**

Borehole ID: AUS24-PP-BH-14
Location: Process Plant

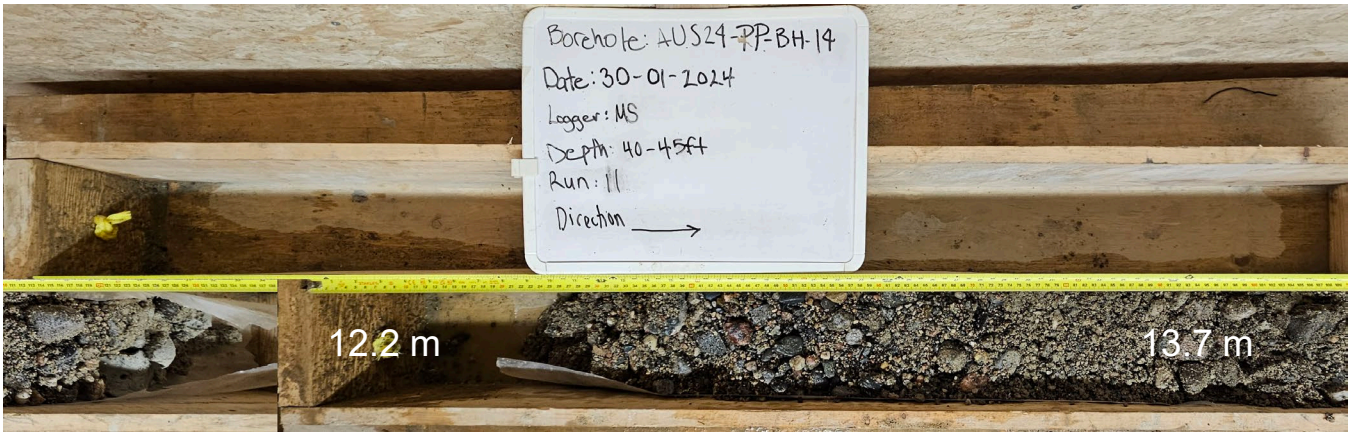


Depth (m): 9.1 – 10.7

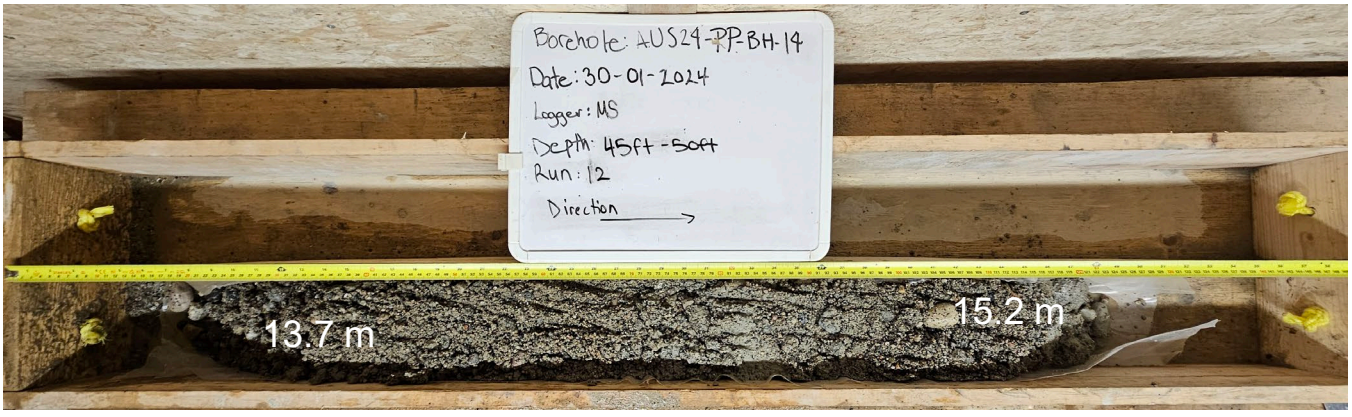


Depth (m): 10.7 – 12.2

Borehole ID: AUS24-PP-BH-14
Location: Process Plant



Depth (m): 12.2 – 13.7



Depth (m): 13.7 – 15.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-14** **Depth (m): 12.2 -15.2**		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **6 of 10**

Borehole ID: AUS24-PP-BH-14
Location: Process Plant



Depth (m): 15.2 – 16.8



Depth (m): 16.8 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-14** **Depth (m): 15.2 – 17.7**
Job No: CAPR000801	Crawford	Date: January 2024 | Approved: ARB | Figure: **7 of 10**

Borehole ID: AUS24-PP-BH-14
Location: Process Plant

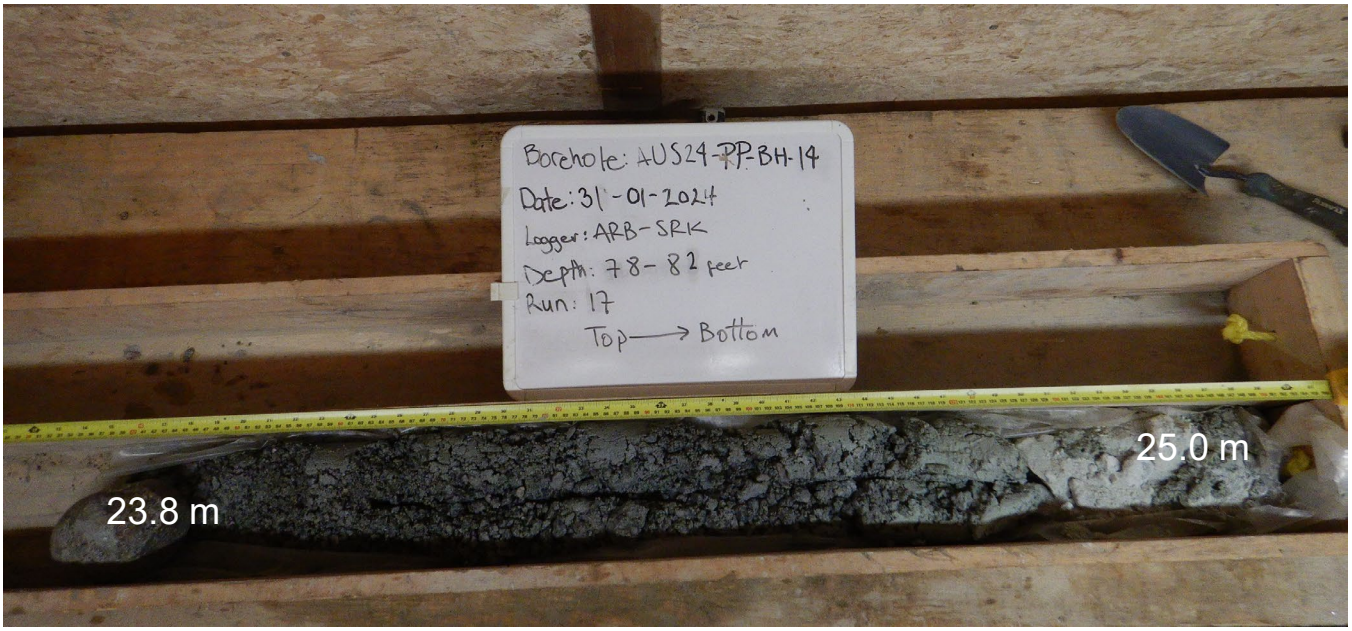


Depth (m): 17.7 – 20.7

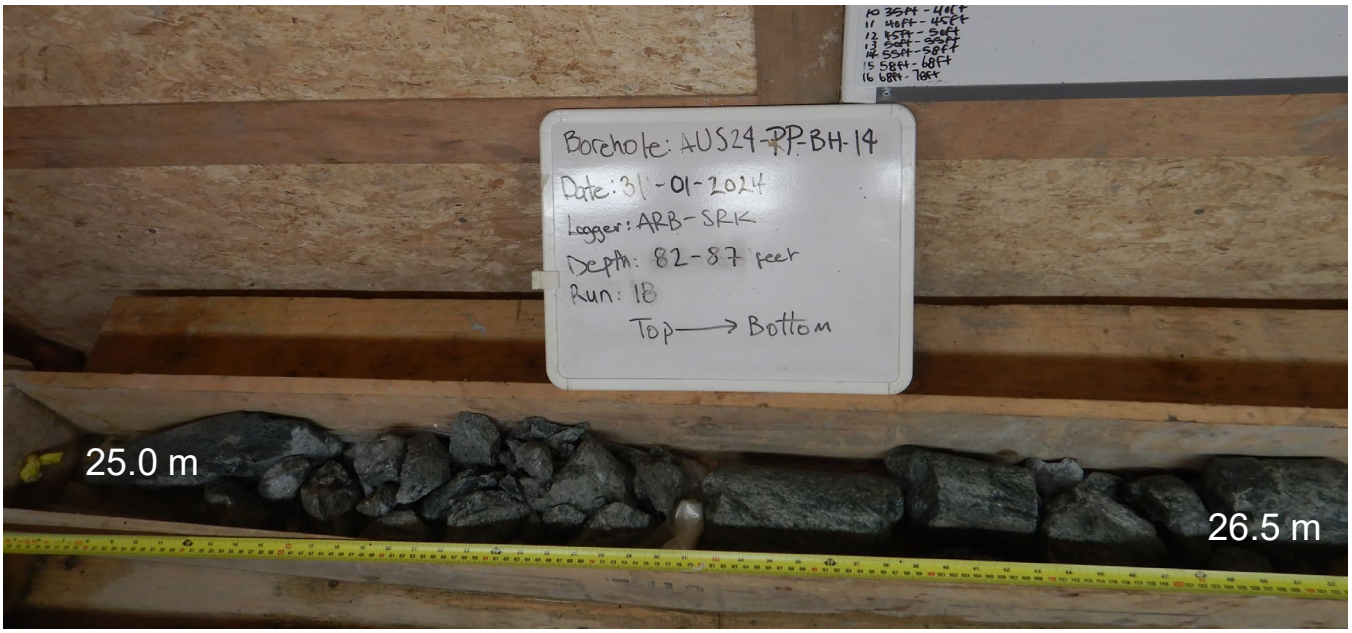


Depth (m): 20.7 – 23.8

Borehole ID: AUS24-PP-BH-14
Location: Process Plant



Depth (m): 23.8 – 25.0



Depth (m): 25.0 – 26.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-14** **Depth (m): 23.8 – 26.5**		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **9 of 10**

Borehole ID: AUS24-PP-BH-14
Location: Process Plant



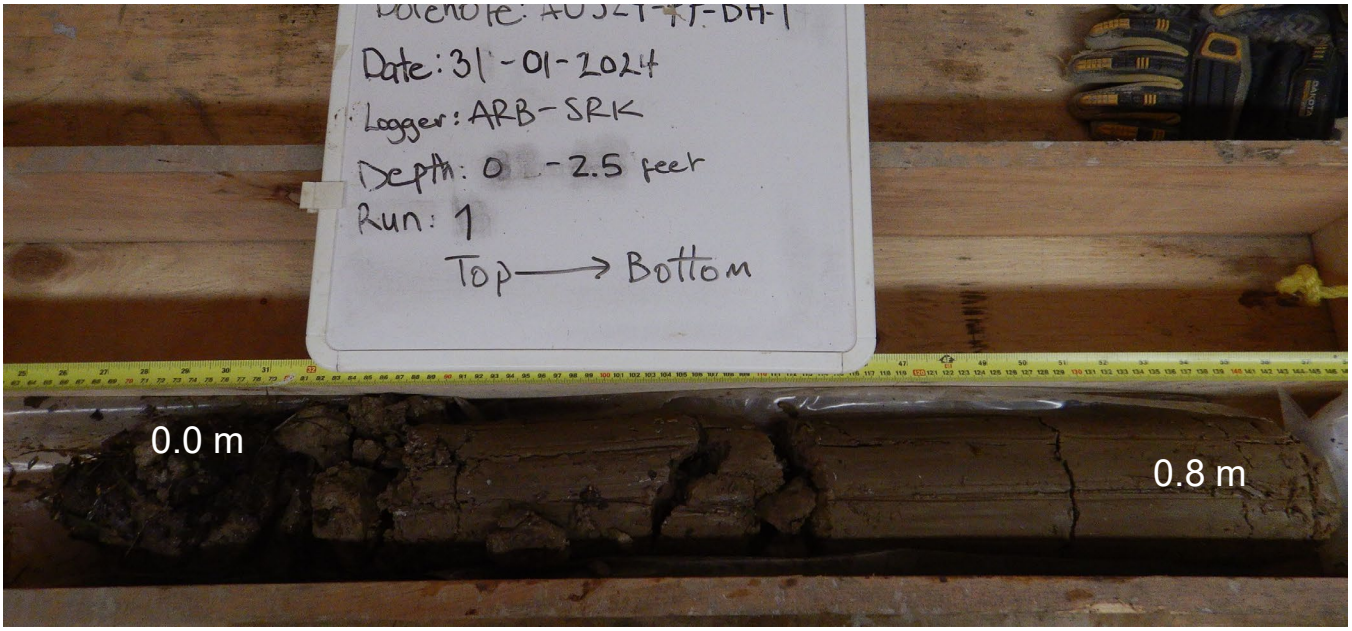
Depth (m): 26.5 – 29.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-14		
		Depth (m): 26.5 – 29.0		
Job No: CAPR000801	Crawford	Date: January 2024	Approved: ARB	Figure: **10 of 10**

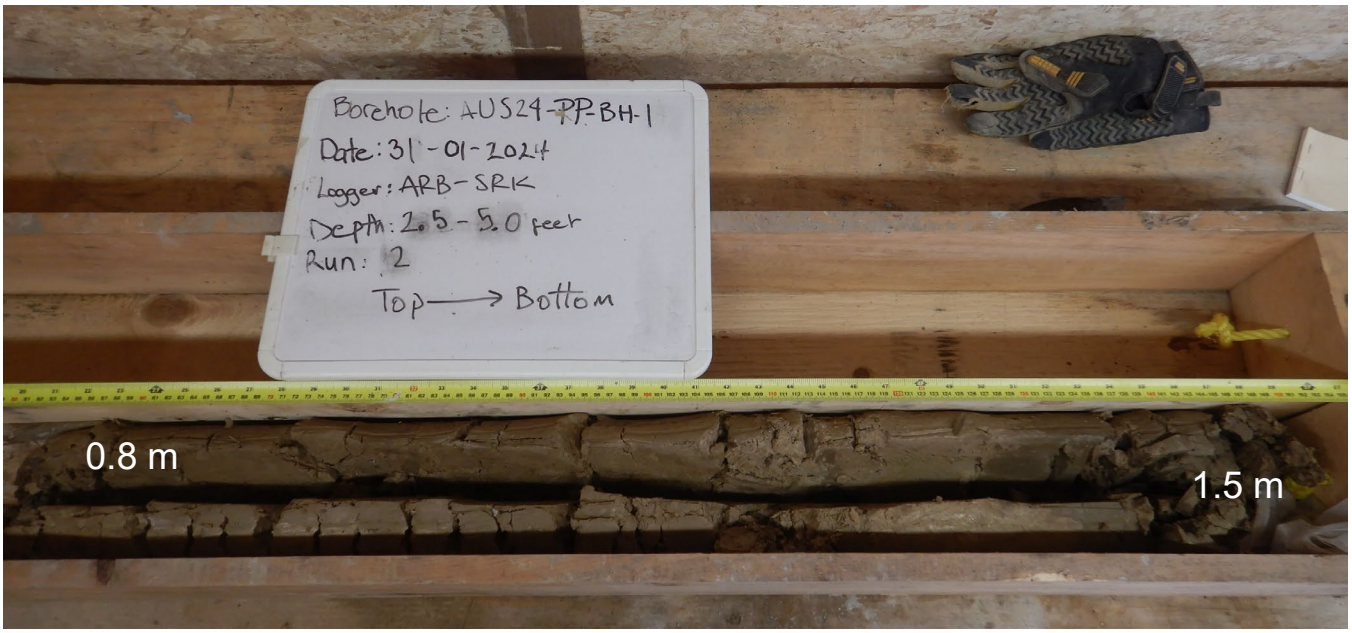
AUS24-PP-BH-16

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: January 2024	Approved:	Figure:

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



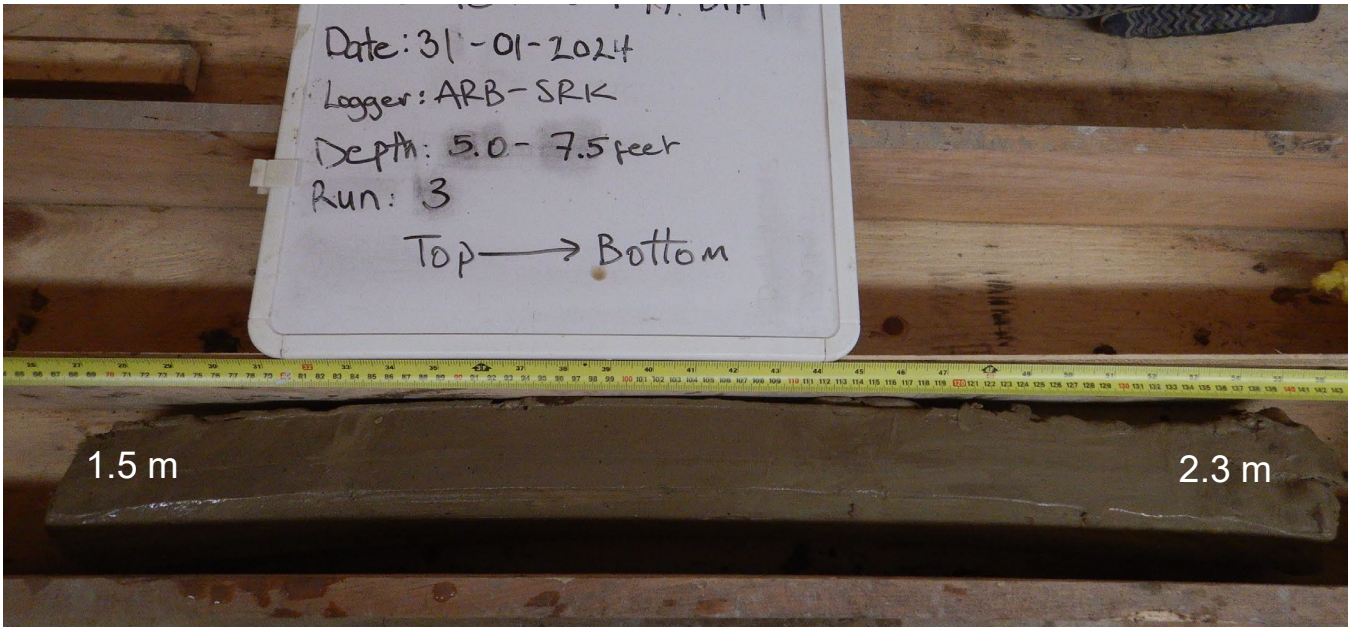
Depth (m): 0.0 – 0.8



Depth (m): 0.8 – 1.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		AUS24-PP-BH-16		
		Depth (m): 0.0 – 1.5		
Job No: CAPR000801	Crawford	Date: January/February 2024	Approved: ARB	Figure: **1 of 9**

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



Depth (m): 1.5 – 2.3



Depth (m): 2.4 – 5.5

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



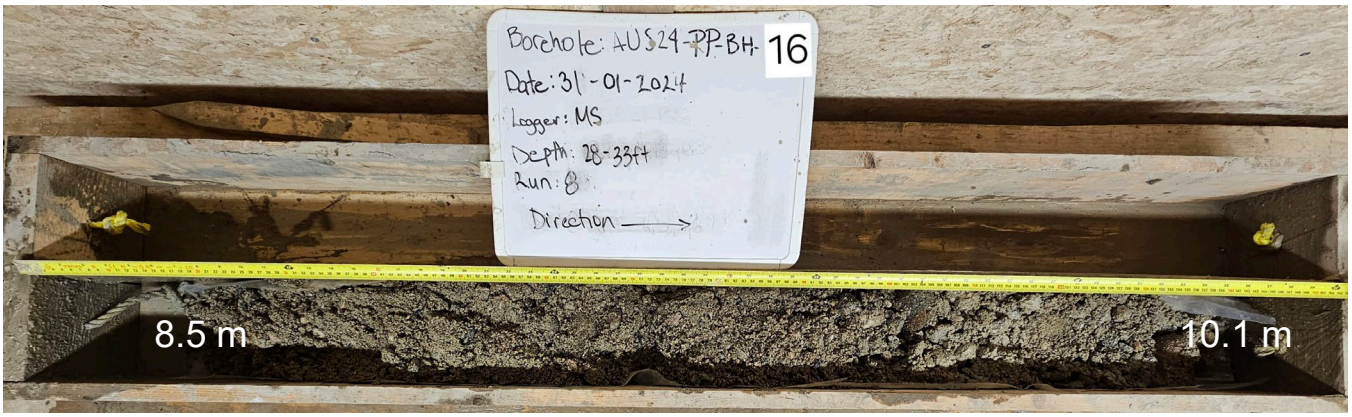
Depth (m): 5.5 – 7.0



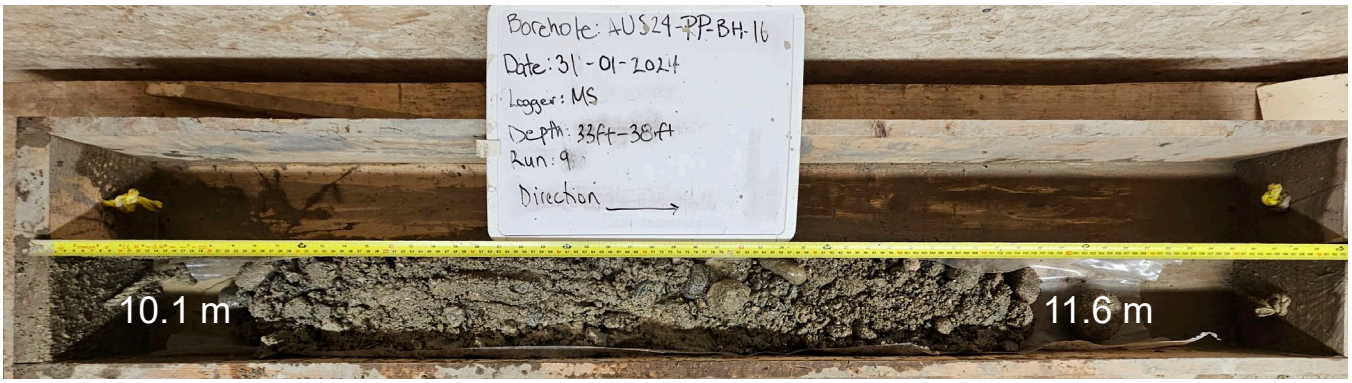
Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-16** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: January/February 2024	Approved: ARB	Figure: **3 of 9**

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



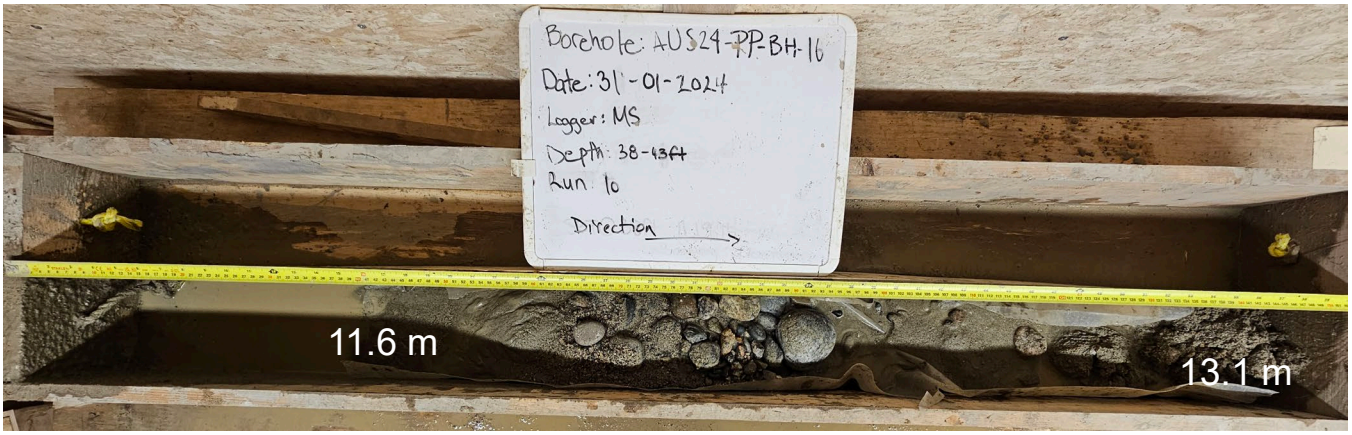
Depth (m): 8.5 – 10.1



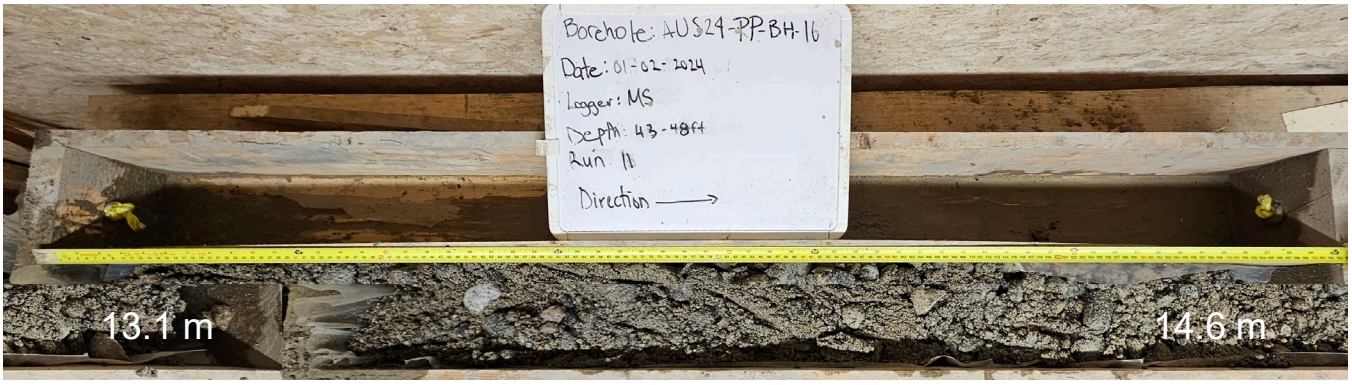
Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-16** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: January/February 2024	Approved: ARB	Figure: **4 of 9**

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



Depth (m): 11.6 – 13.1



Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-16** **Depth (m): 11.6 – 14.6**		
Job No: CAPR000801	Crawford	Date: January/February 2024	Approved: ARB	Figure: **5 of 9**

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-16** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: January/February 2024	Approved: ARB	Figure: **6 of 9**

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



Depth (m): 17.7 – 20.7



Depth (m): 20.7 – 23.8

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



Depth (m): 23.8 – 26.8



Depth (m): 26.8 – 27.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **AUS24-PP-BH-16** **Depth (m): 23.8 – 27.4**		
Job No: CAPR000801	Crawford	Date: January/February 2024	Approved: ARB	Figure: **8 of 9**

Borehole ID: AUS24-PP-BH-16
Location: Process Plant



Depth (m): 27.4 – 30.5

Combined24 -BH-04A

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 0.0 – 2.4



Depth (m): 2.4 – 5.5

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 5.5 – 7.0



Depth (m): 7.0 – 10.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-04A** **Depth (m): 5.5 – 10.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 10.1 – 13.1



Depth (m): 13.1 – 16.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-04A		
		Depth (m): 10.1 – 16.2		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 16.2 – 17.7



Depth (m): 17.7 – 20.7

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 20.7 – 23.8



Depth (m): 23.8 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-04A		
		Depth (m): 20.7 – 26.8		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 26.8 – 29.9



Depth (m): 29.9 – 32.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-04A **Depth (m): 26.8 – 32.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



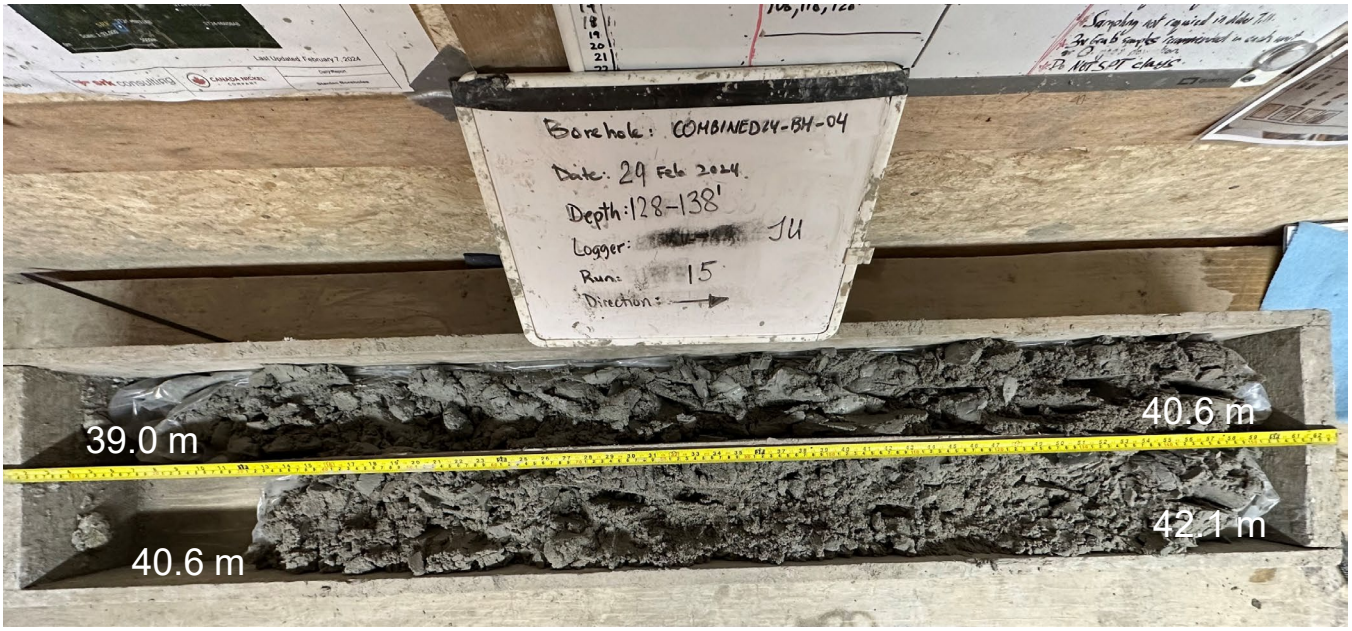
Depth (m): 32.9 – 36.0



Depth (m): 36.0 – 39.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-04A **Depth (m): 32.9 – 39.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 39.0 – 42.1



Depth (m): 42.1 – 45.1

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 45.1 – 48.2



Depth (m): 48.2 – 54.3

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 54.3 – 58.5



Depth (m): 58.5 – 60.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-04A** **Depth (m): 54.3 – 60.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 60.4 – 61.9



Depth (m): 61.9 – 63.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-04A		
		Depth (m): 60.4 – 63.4		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



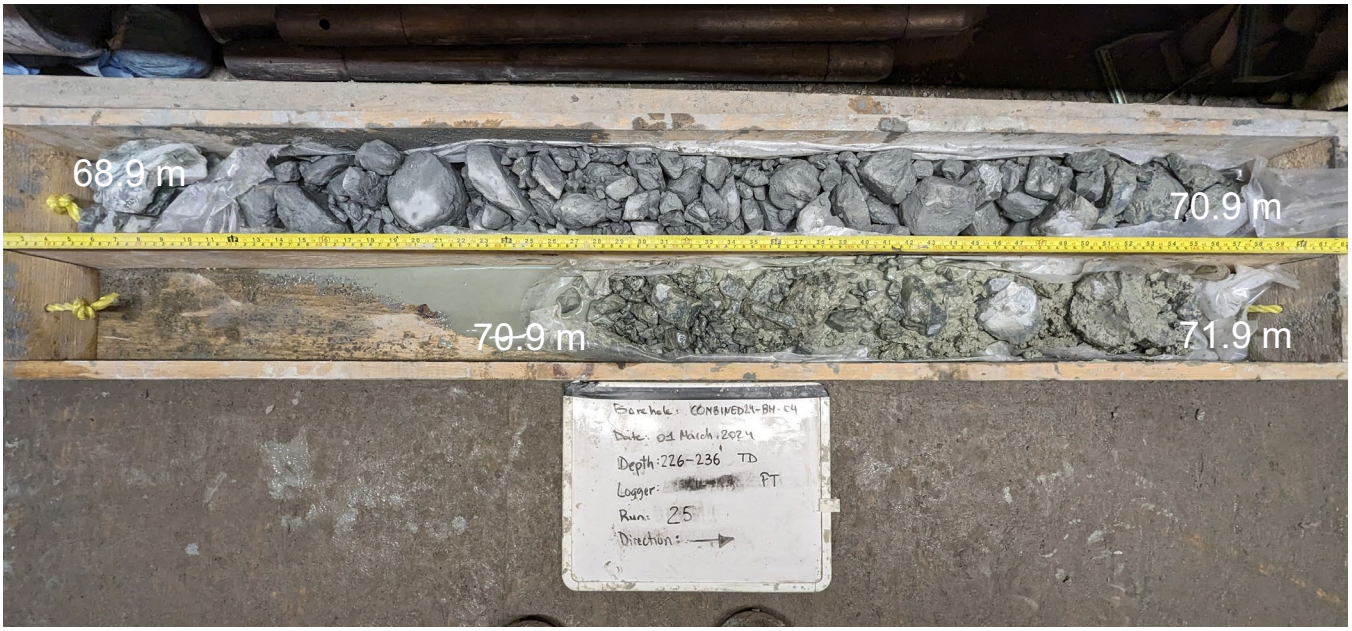
Depth (m): 63.4 – 67.1



Depth (m): 67.1 – 68.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-04A** **Depth (m): 63.4 – 68.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **12 of 13**

Borehole ID: Combined24-BH-04A
Location: East Stockpile



Depth (m): 68.9 – 71.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-04A** **Depth (m): 68.9 – 71.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **13 of 13**

Combined24 -BH-05A

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 0.0 – 2.4



Depth (m): 2.4 – 5.5

Borehole ID: Combined24-BH-05A
Location: East Stockpile



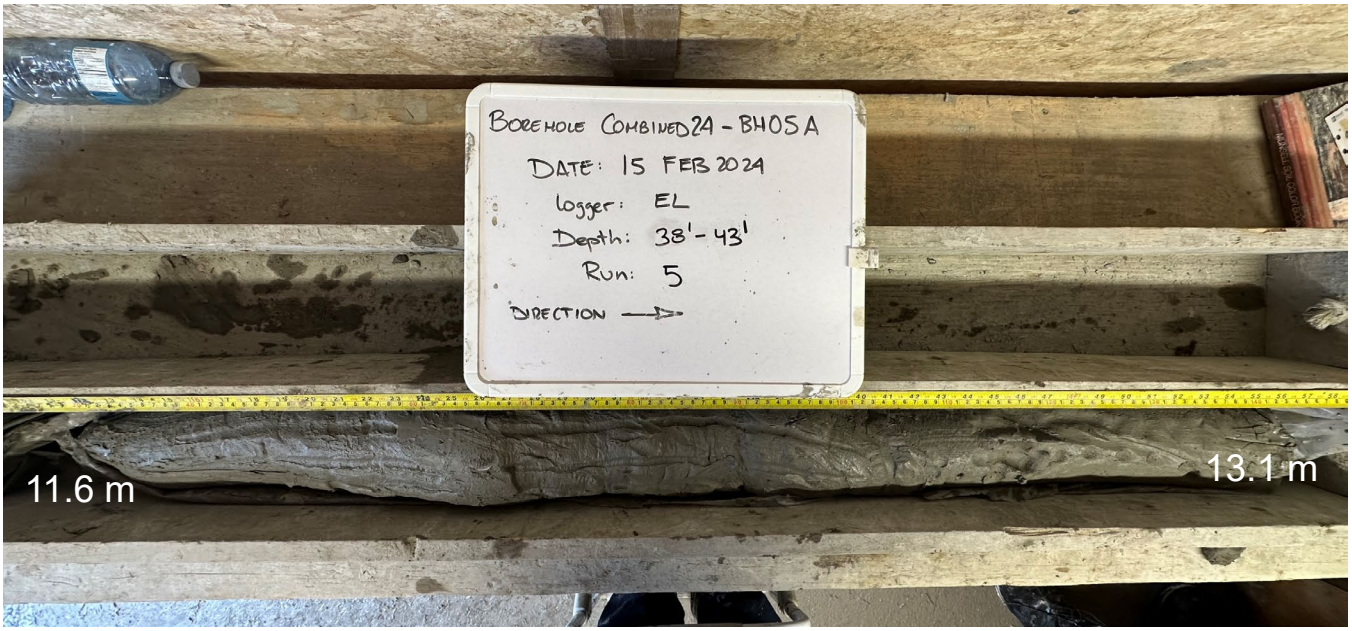
Depth (m): 5.5 – 8.5



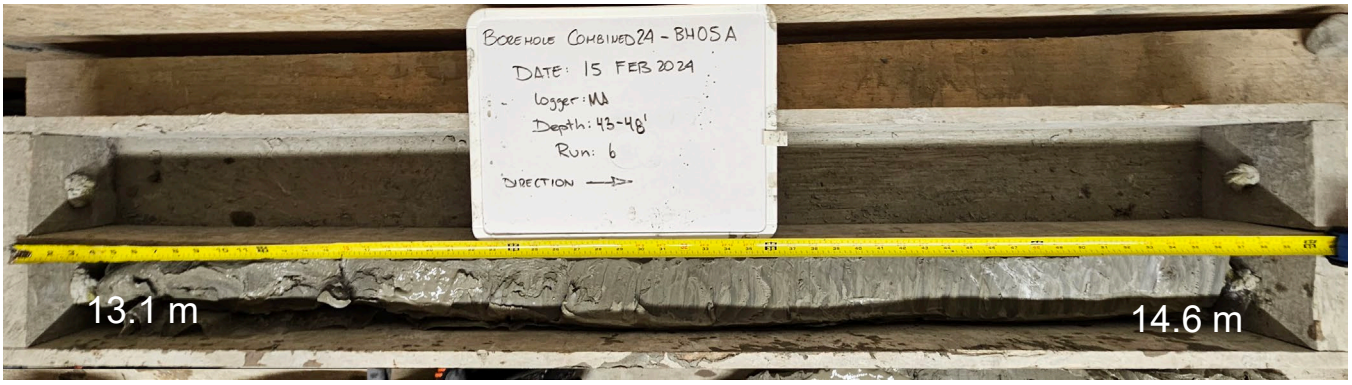
Depth (m): 8.5 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-05A** **Depth (m): 5.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 13**

Borehole ID: Combined24-BH-05A
Location: East Stockpile



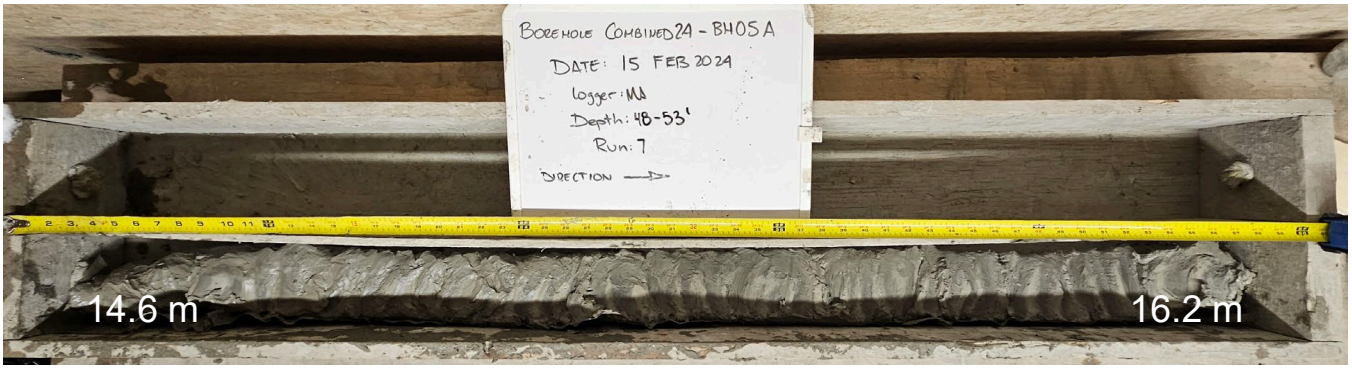
Depth (m): 11.6 – 13.1



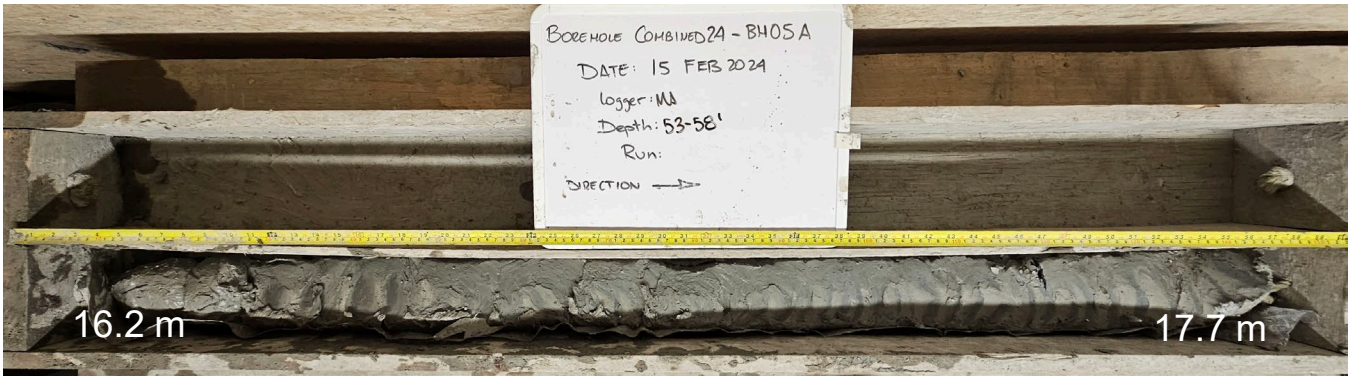
Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-05A		
		Depth (m): 11.6 – 14.6		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 13**

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 17.7 – 20.7



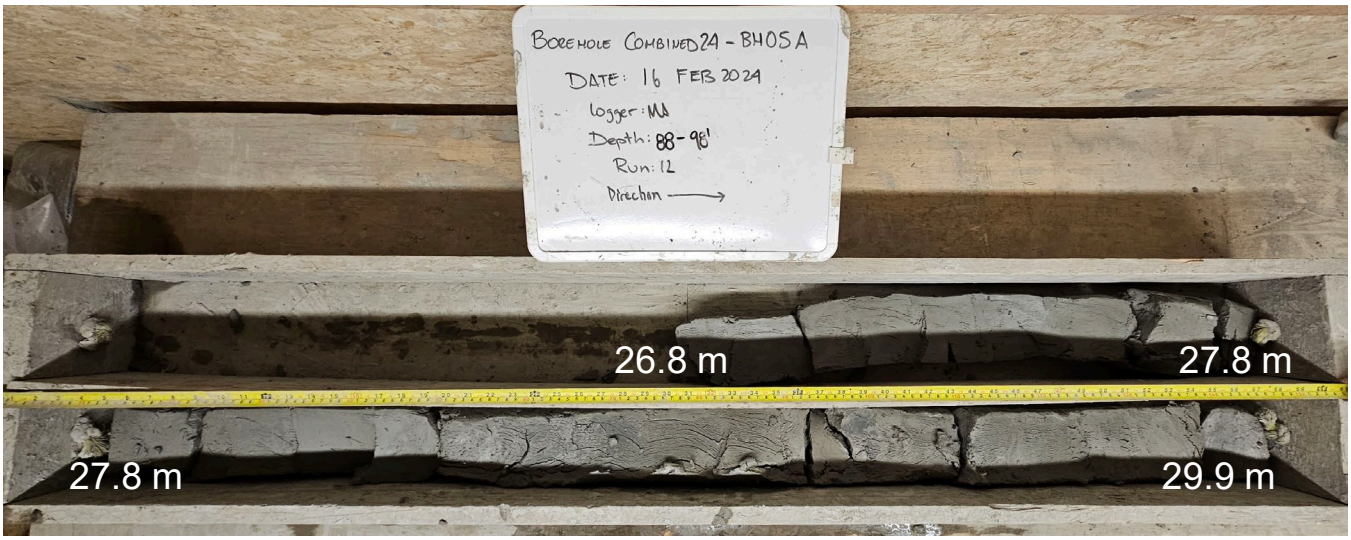
Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-05A** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 13**

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 23.8 – 26.8



Depth (m): 26.8 – 29.9

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 29.9 – 32.9



Depth (m): 32.9 – 36.0

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 36.0 – 39.0



Depth (m): 39.0 – 42.1

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 42.1 – 45.1



Depth (m): 45.1 – 48.2

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 48.2 – 51.2



Depth (m): 51.2 – 54.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-05A** **Depth (m): 48.2 – 54.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 13**

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 54.3 – 57.3



Depth (m): 57.3 – 60.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-05A		
		Depth (m): 54.3 – 60.4		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 13**

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 60.4 – 63.4



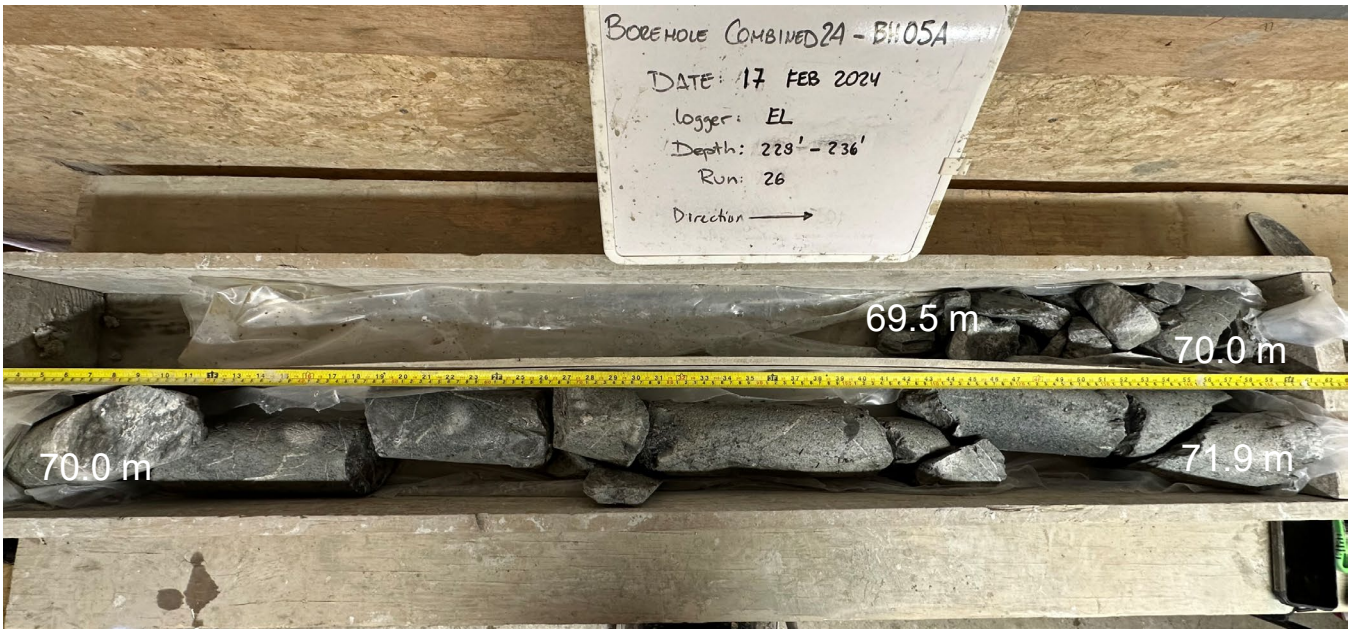
Depth (m): 63.4 – 66.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **Combined24-BH-05A** **Depth (m): 60.4 – 66.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **12 of 13**

Borehole ID: Combined24-BH-05A
Location: East Stockpile



Depth (m): 66.4 – 69.5



Depth (m): 69.5 – 71.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		Combined24-BH-05A		
		Depth (m): 66.4 – 71.9		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **13 of 13**

SRK24-LGE-BH-201

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



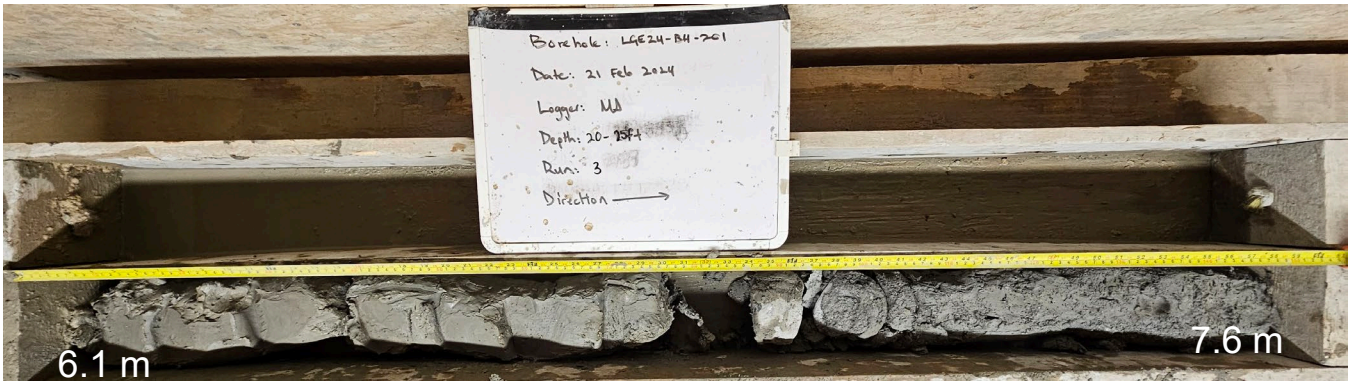
Depth (m): 0.0 – 3.0



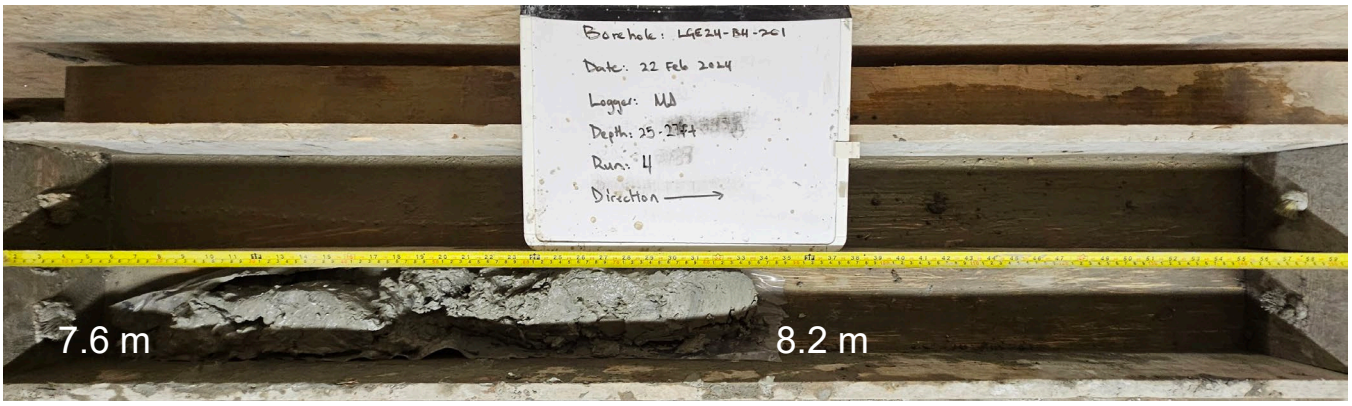
Depth (m): 3.0 – 6.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 0.0 – 6.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



Depth (m): 6.1 – 7.6



Depth (m): 7.6 – 8.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 6.1 – 8.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



Depth (m): 8.2 – 9.8



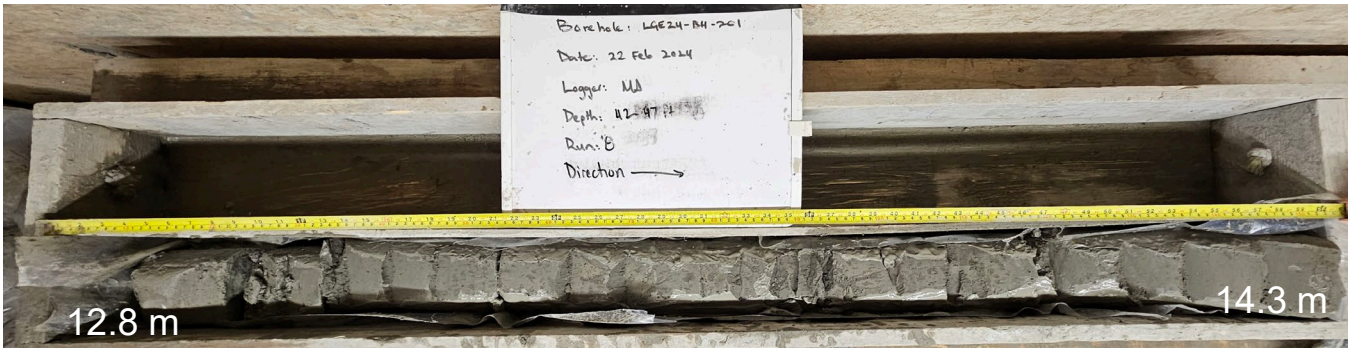
Depth (m): 9.8 – 11.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 8.2 – 11.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



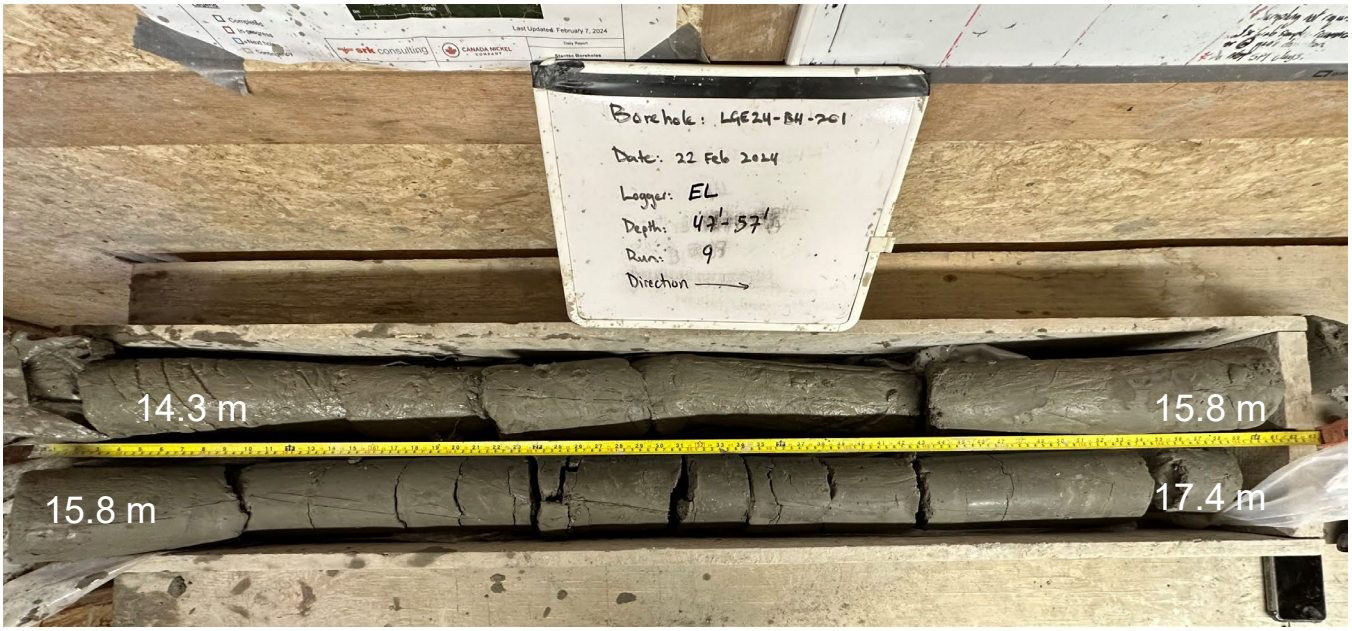
Depth (m): 11.3 – 12.8



Depth (m): 12.8 – 14.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 11.3 – 14.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile

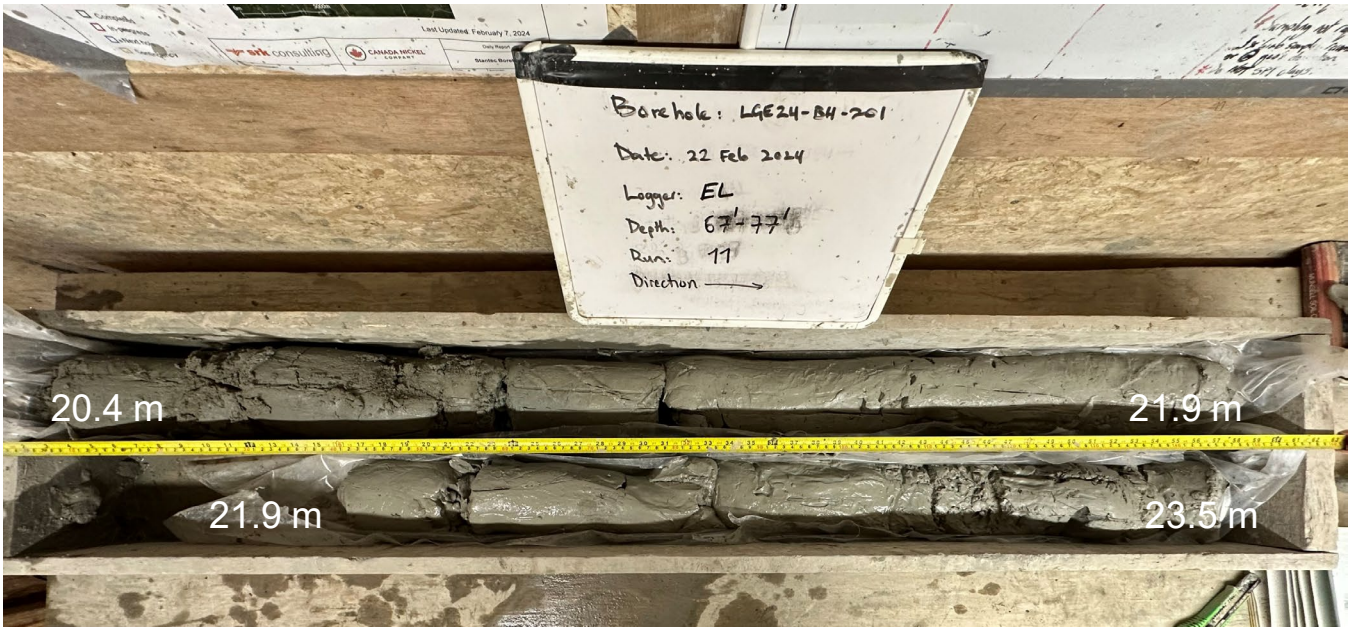


Depth (m): 14.3 – 17.4

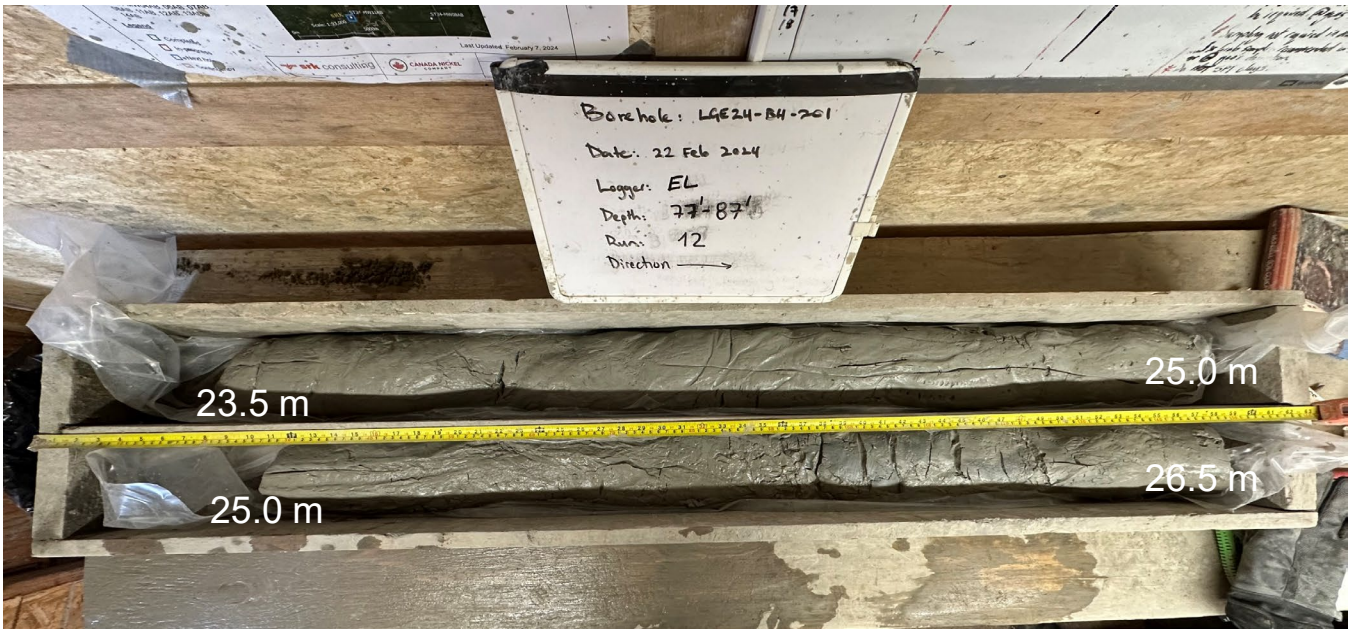


Depth (m): 17.4 – 20.4

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



Depth (m): 20.4 – 23.5



Depth (m): 23.5 – 26.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-201		
		Depth (m): 20.4 – 26.5		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile

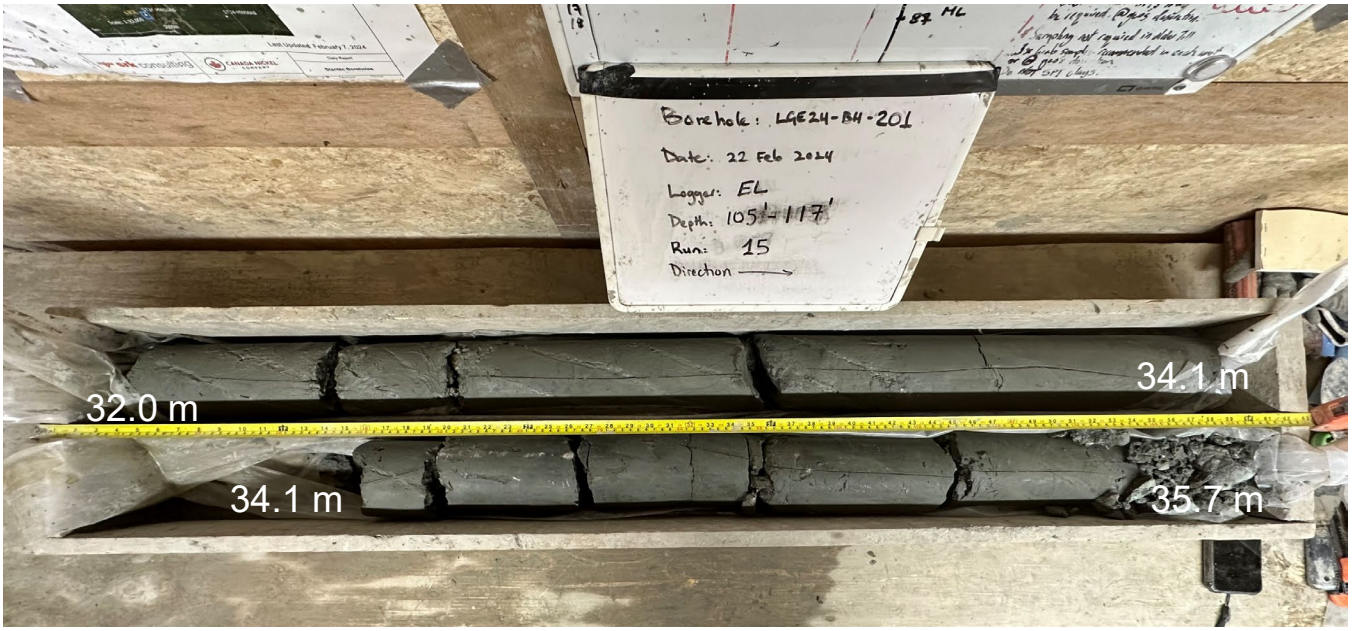


Depth (m): 26.5 – 29.0

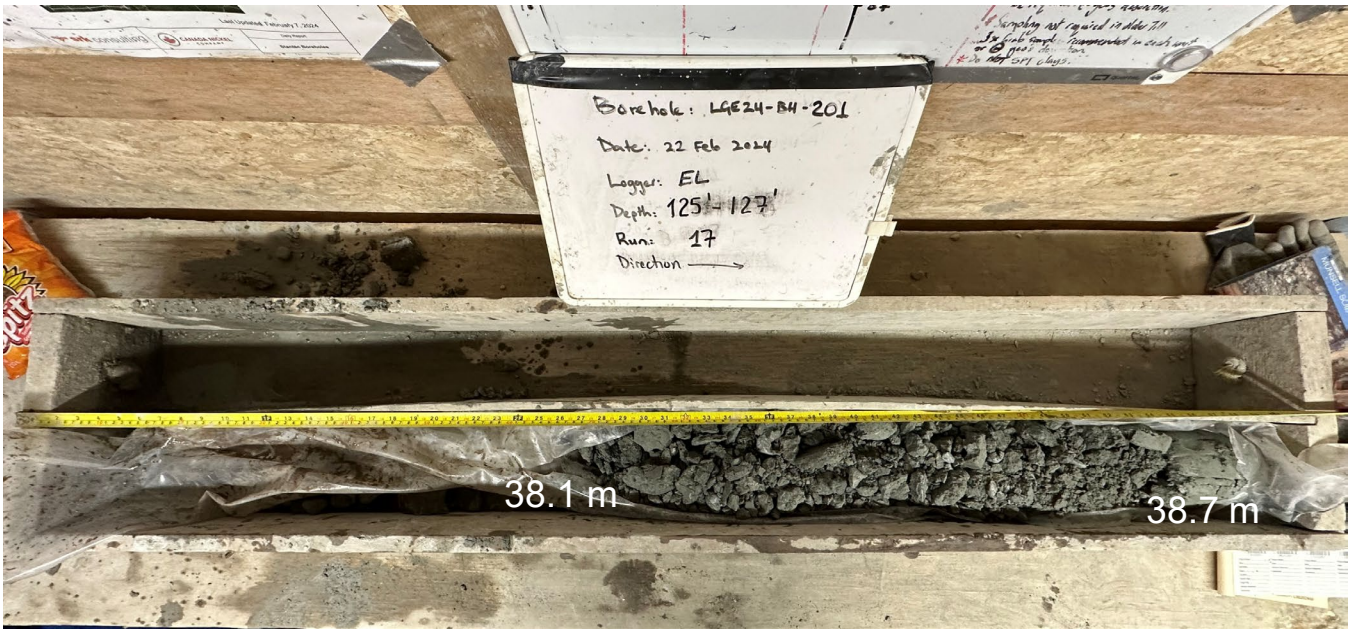


Depth (m): 29.0 – 32.0

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



Depth (m): 32.0 – 35.7



Depth (m): 38.1 – 38.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-201		
		Depth (m): 32.0 – 38.7		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



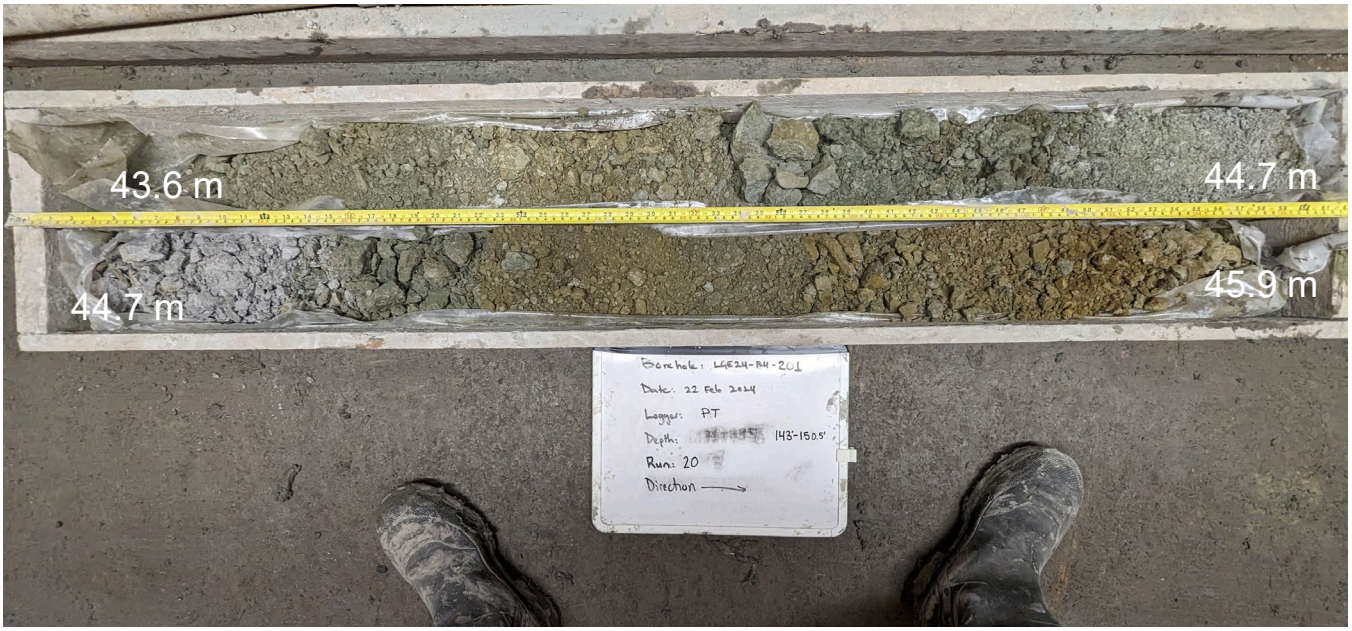
Depth (m): 38.7 – 41.1



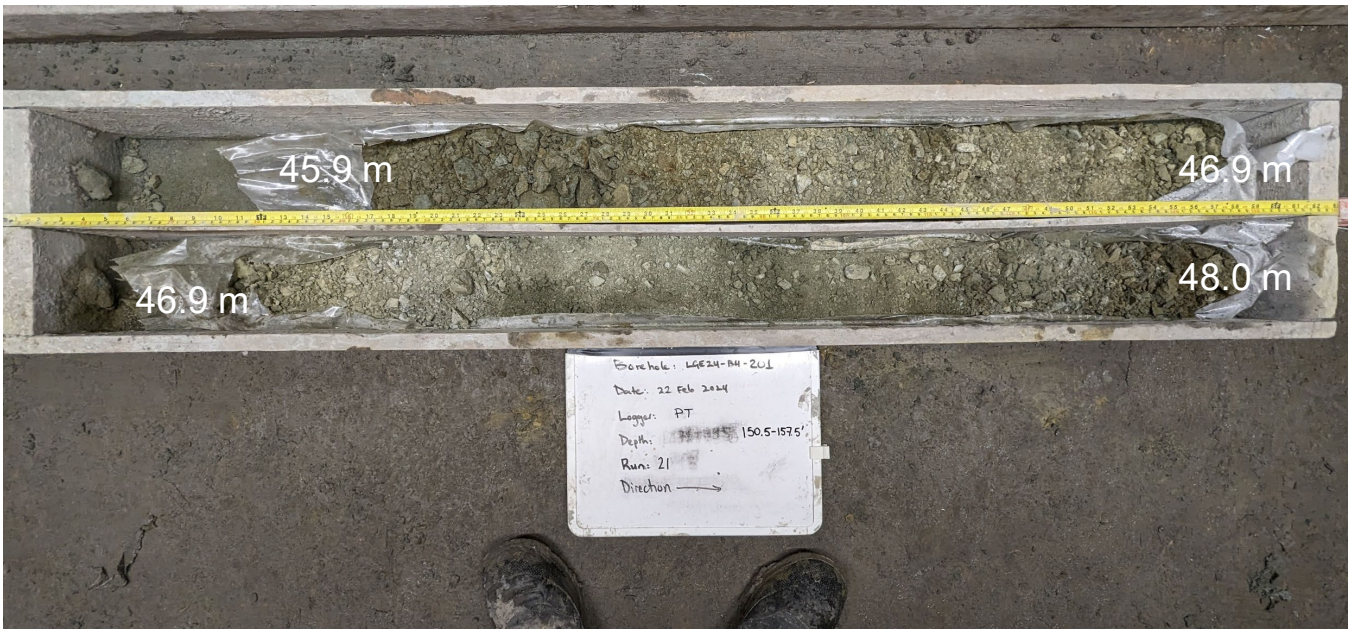
Depth (m): 41.1 – 43.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 38.7 – 43.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



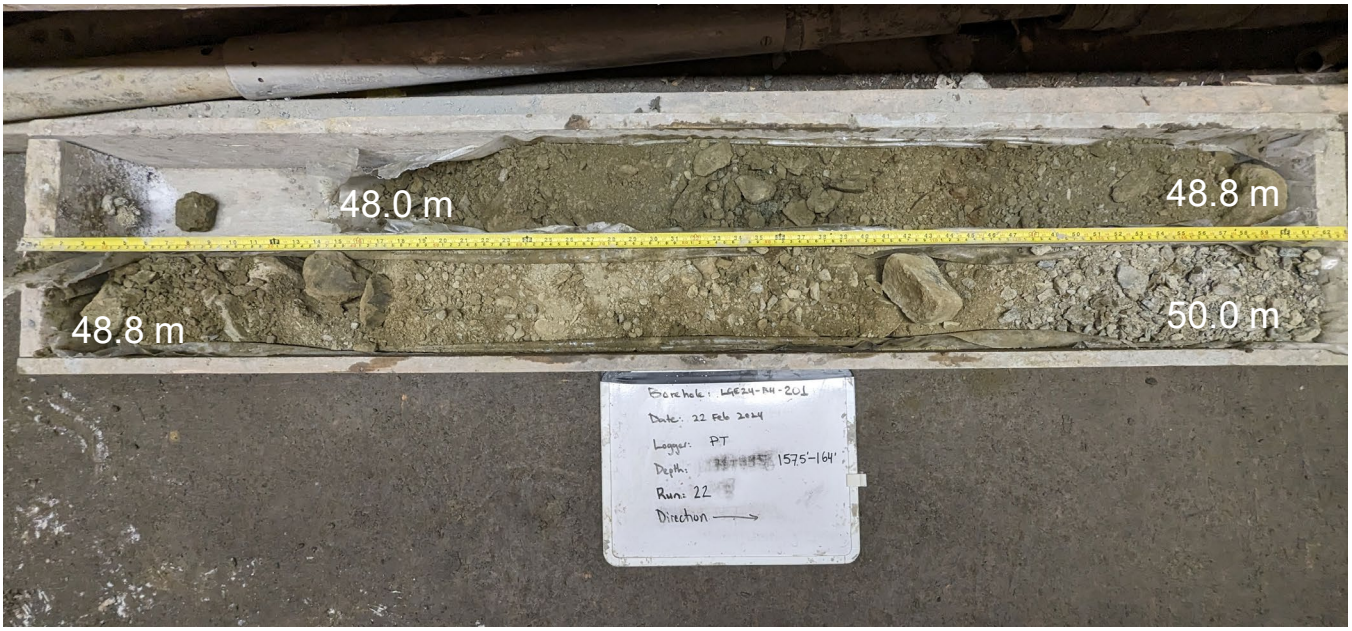
Depth (m): 43.6 – 45.9



Depth (m): 45.9 – 48.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 43.6 – 48.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 11**

Borehole ID: SRK24-LGE-BH-201
Location: East Stockpile



Depth (m): 48.0 – 50.0



Depth (m): 50.0 – 54.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-201** **Depth (m): 48.0 – 54.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 11**

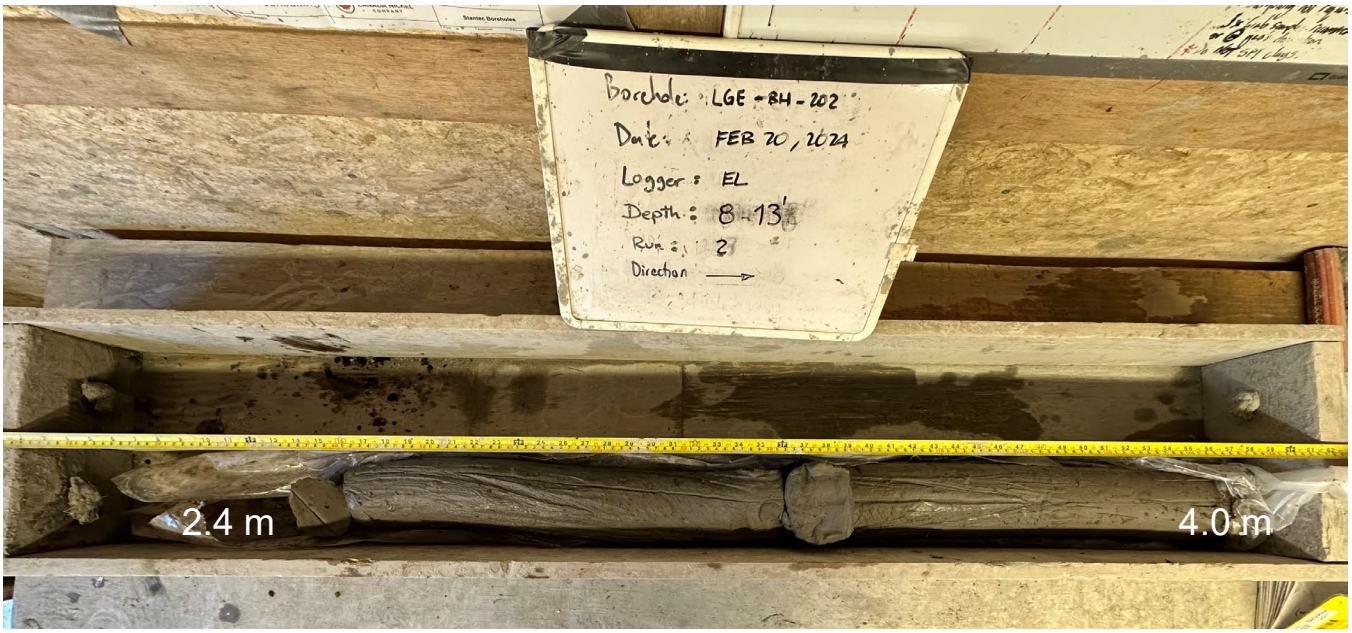
SRK24-LGE-BH-202

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: SRK24-LGE-BH-202
Location: East Stockpile



Depth (m): 0.0 – 2.4

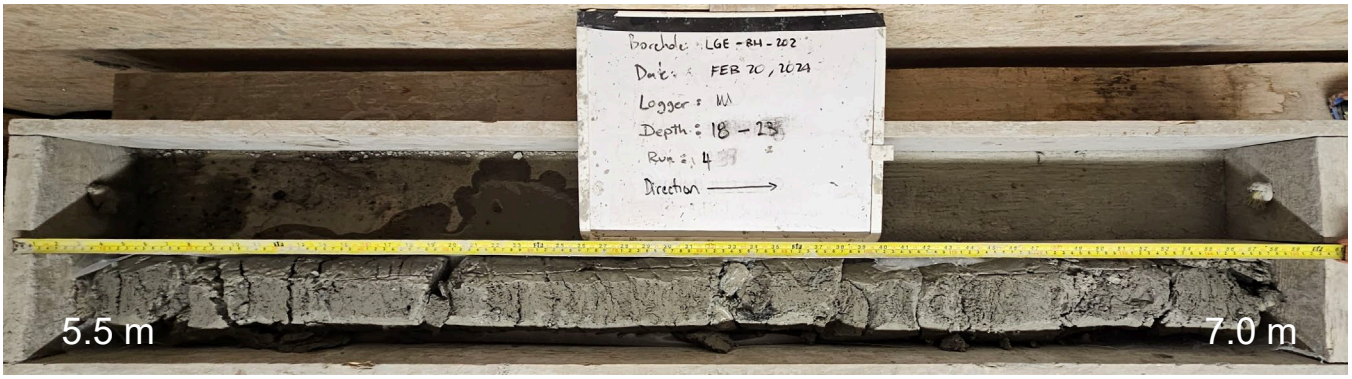


Depth (m): 2.4 – 4.0

Borehole ID: SRK24-LGE-BH-202
Location: East Stockpile



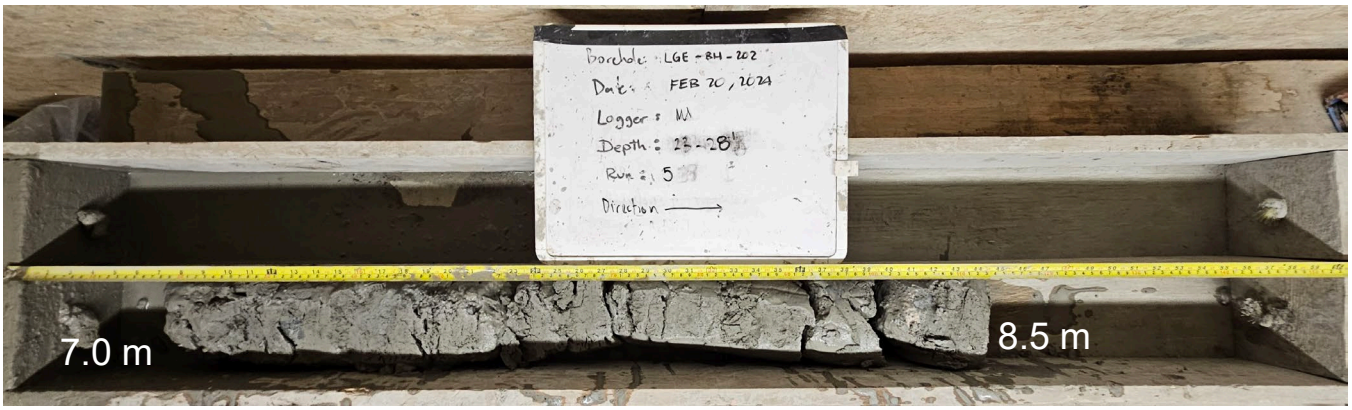
Depth (m): 4.0 – 5.5



Depth (m): 5.5 – 7.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-202** **Depth (m): 4.0 – 7.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 6**

Borehole ID: SRK24-LGE-BH-202
Location: East Stockpile



Depth (m): 7.0 – 8.5



Depth (m): 8.5 – 10.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-202** **Depth (m): 7.0 – 10.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 6**

Borehole ID: SRK24-LGE-BH-202
Location: East Stockpile



Depth (m): 10.1 – 11.6



Depth (m): 11.6 – 13.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-202** **Depth (m): 10.1 – 13.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 6**

Borehole ID: SRK24-LGE-BH-202
Location: East Stockpile



Depth (m): 13.1 – 16.2



Depth (m): 16.2 – 19.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-202** **Depth (m): 13.1 – 19.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 6**

Borehole ID: SRK24-LGE-BH-202
Location: East Stockpile



Depth (m): 19.2 – 22.3



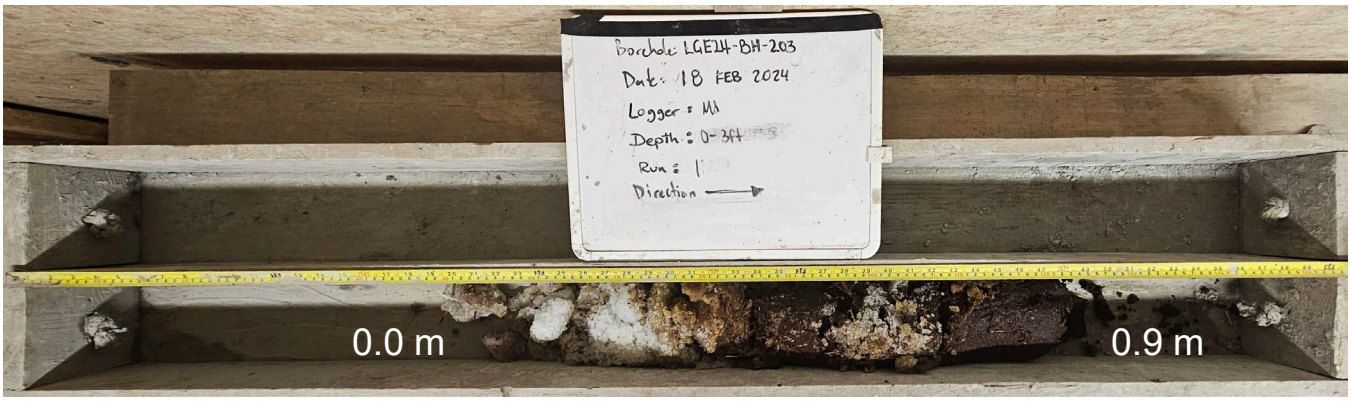
Depth (m): 22.3 – 25.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-202** **Depth (m): 19.2 – 25.3**
Job No: CAPR000801	Crawford	Date: February 2024 / Approved: ARB / Figure: **6 of 6**

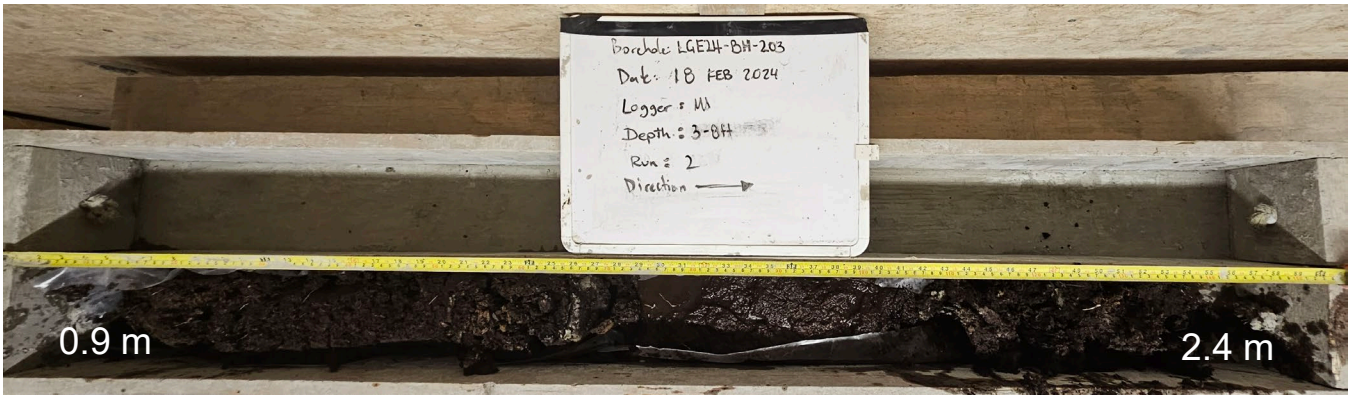
SRK24-LGE-BH-203

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



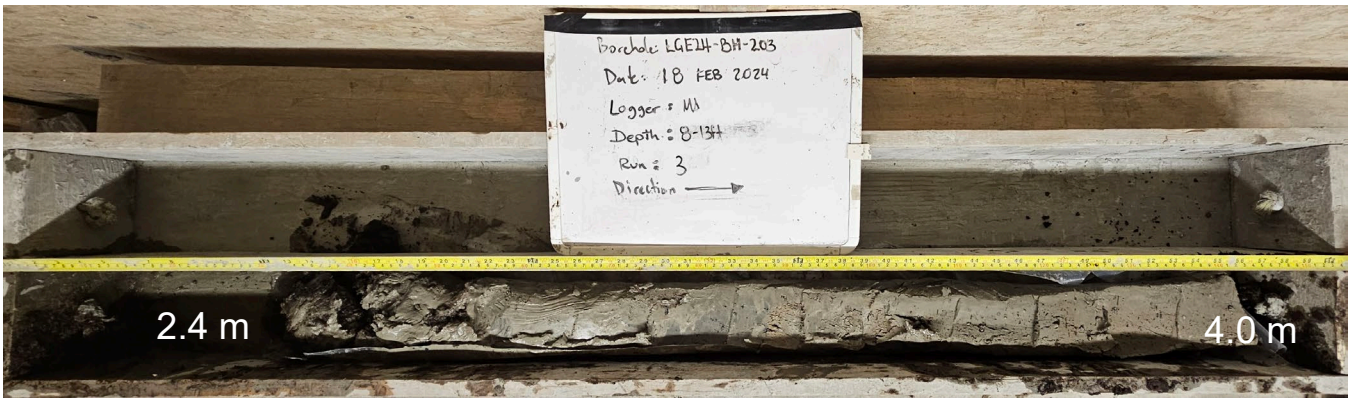
Depth (m): 0.0 – 0.9



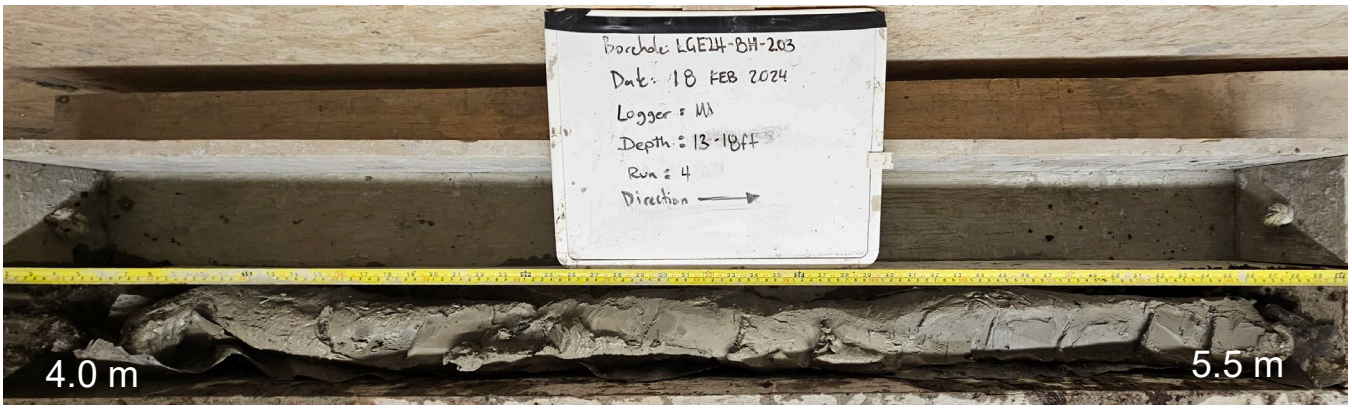
Depth (m): 0.9 – 2.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 0.0 – 2.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



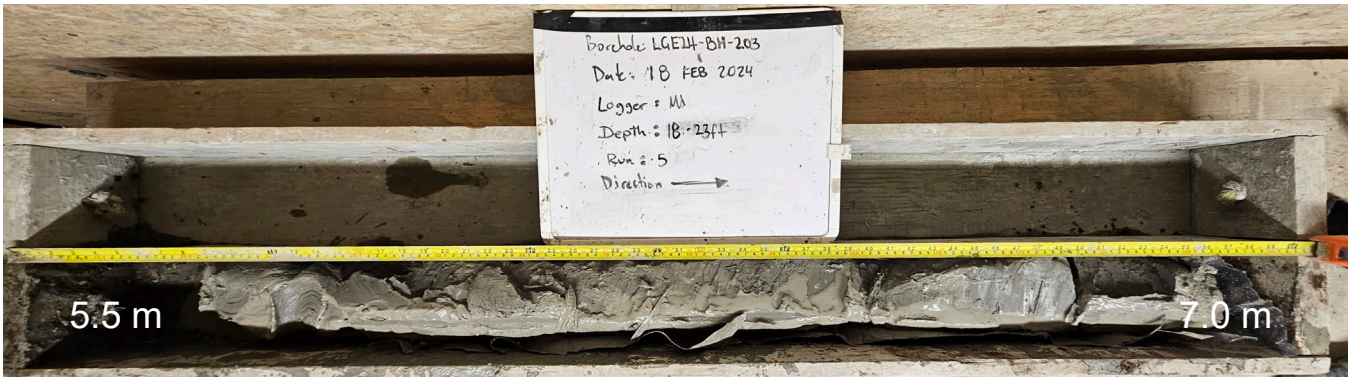
Depth (m): 2.4 – 4.0



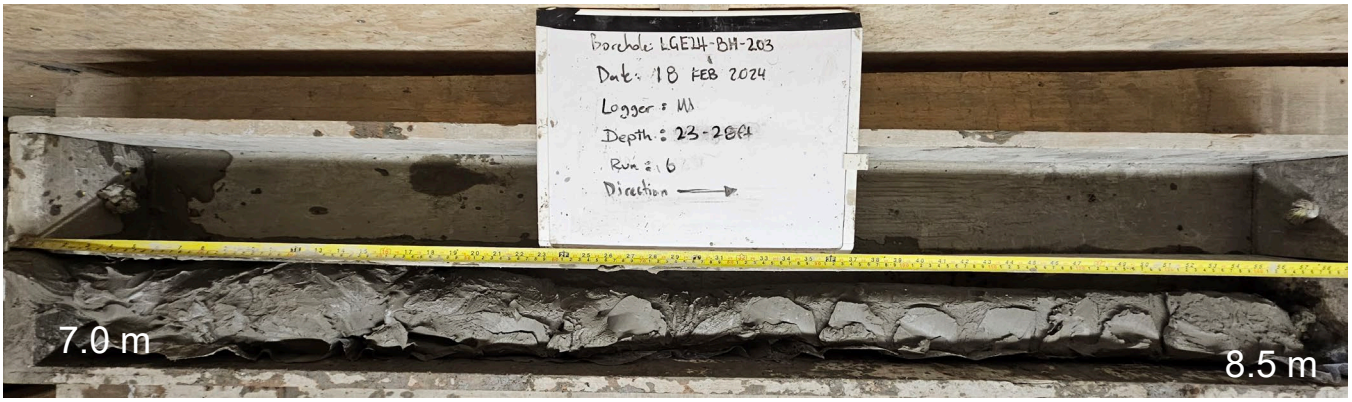
Depth (m): 4.0 – 5.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 2.4 – 5.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



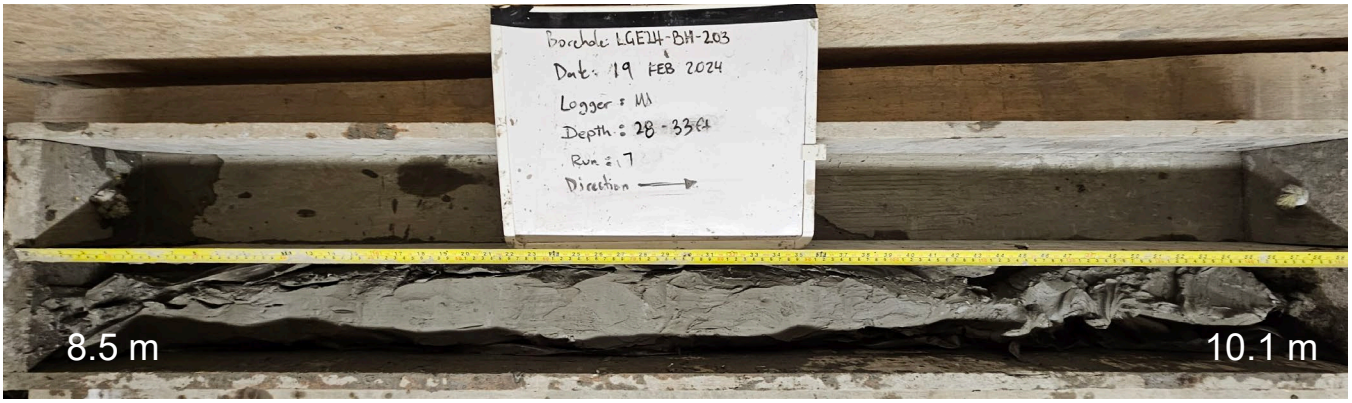
Depth (m): 5.5 – 7.0



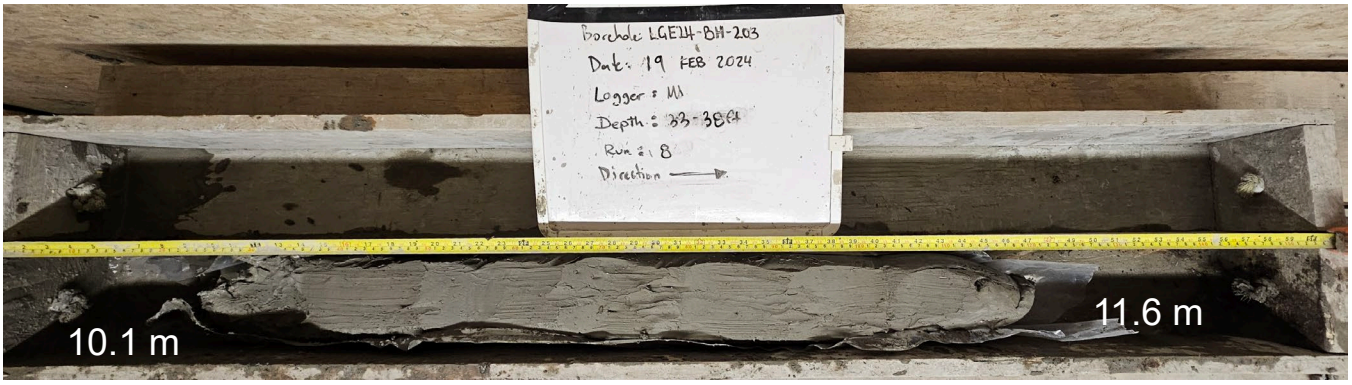
Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



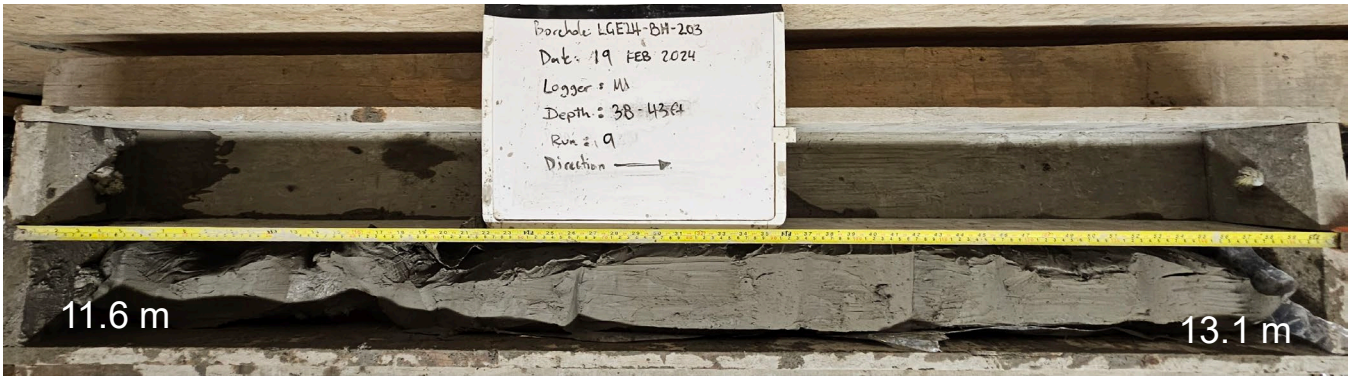
Depth (m): 8.5 – 10.1



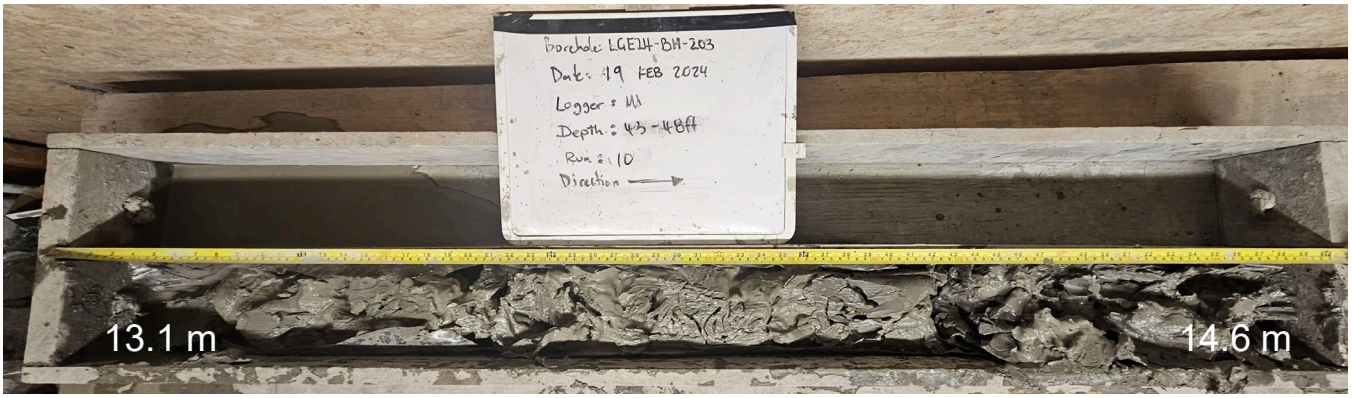
Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



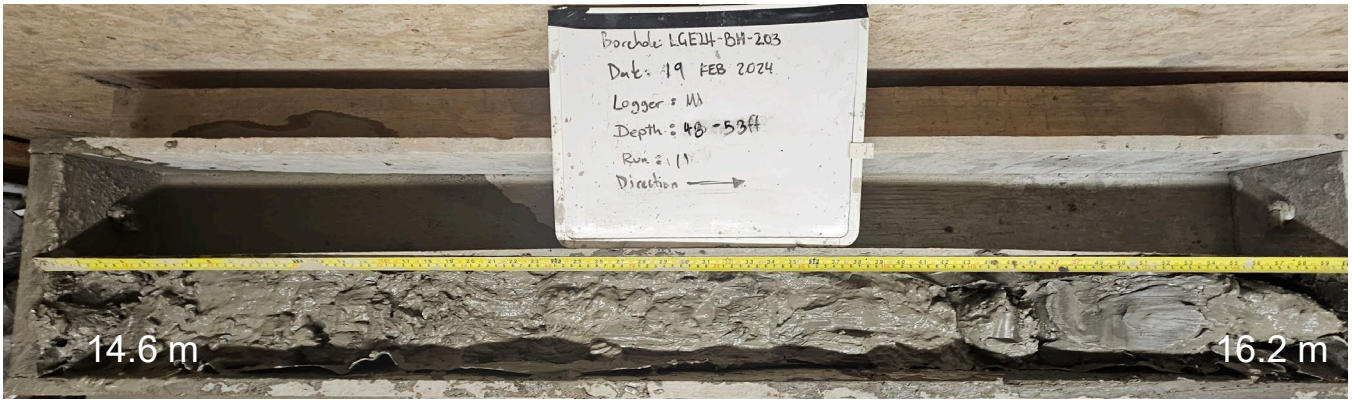
Depth (m): 11.6 – 13.1



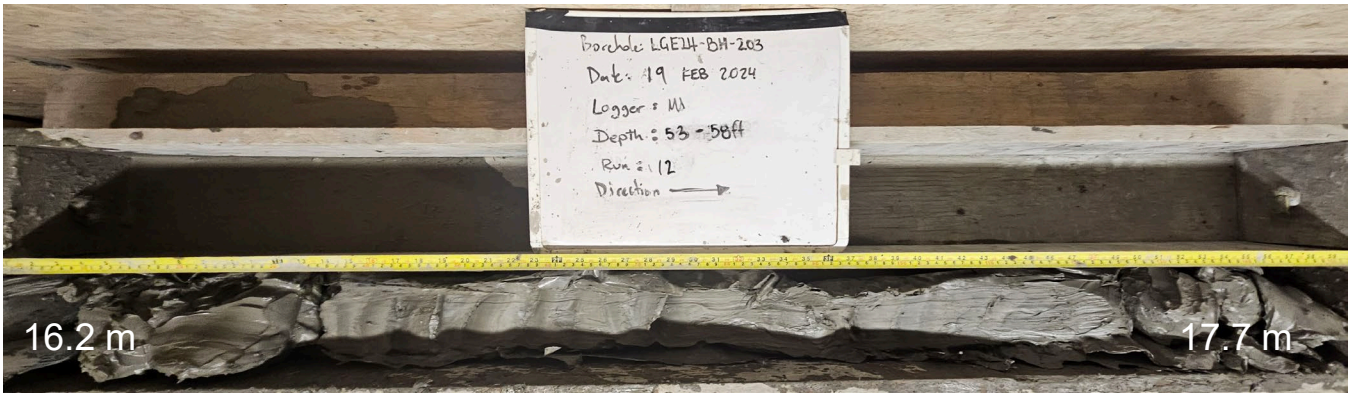
Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 11.6 – 14.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



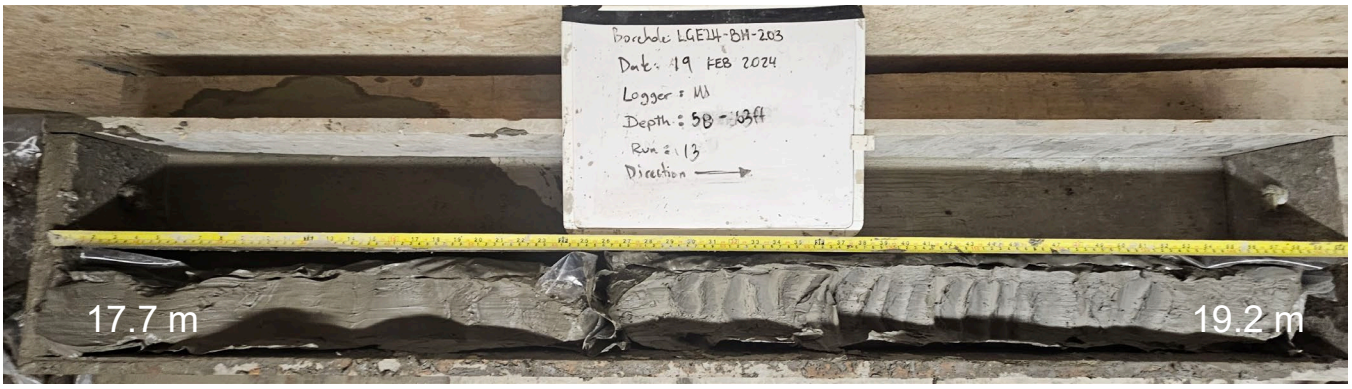
Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



Depth (m): 17.7 – 19.2



Depth (m): 19.2 – 22.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 17.7 – 22.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



Depth (m): 22.3 – 23.8



Depth (m): 23.8 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-203		
		Depth (m): 22.3 – 26.8		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



Depth (m): 26.8 – 29.9



Depth (m): 29.9 – 32.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-203		
		Depth (m): 26.8 – 32.9		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



Depth (m): 32.9 – 36.0



Depth (m): 36.0 – 39.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 32.9 – 39.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 11**

Borehole ID: SRK24-LGE-BH-203
Location: East Stockpile



Depth (m): 39.0 – 40.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-203** **Depth (m): 39.0 – 40.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 11**

SRK24-LGE-BH-204

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



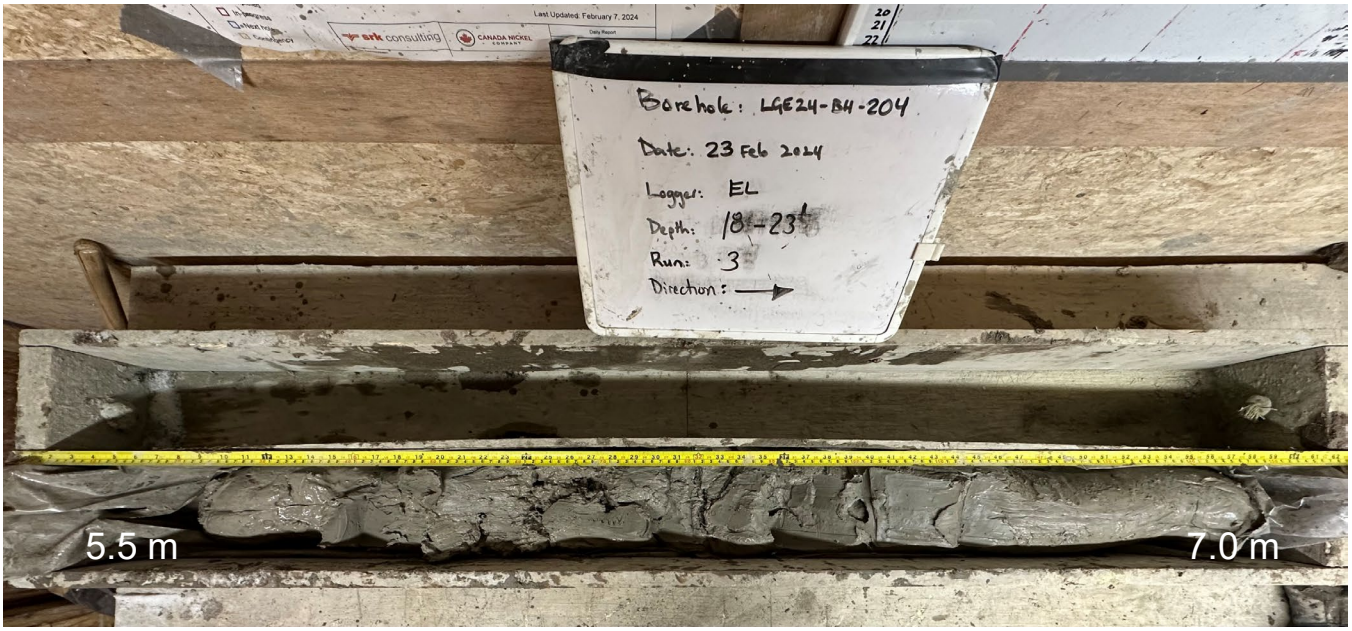
Depth (m): 0.0 – 2.4



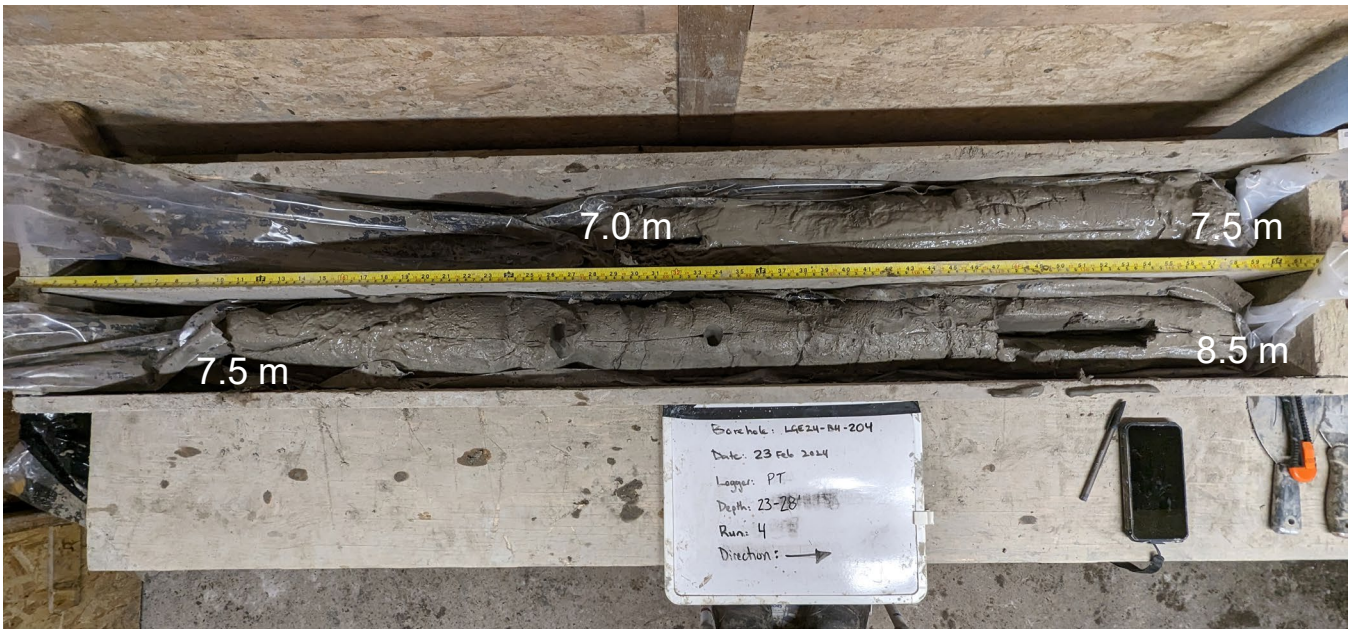
Depth (m): 2.4 – 5.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-204		
		Depth (m): 0.0 – 5.5		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 5.5 – 7.0



Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-204** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



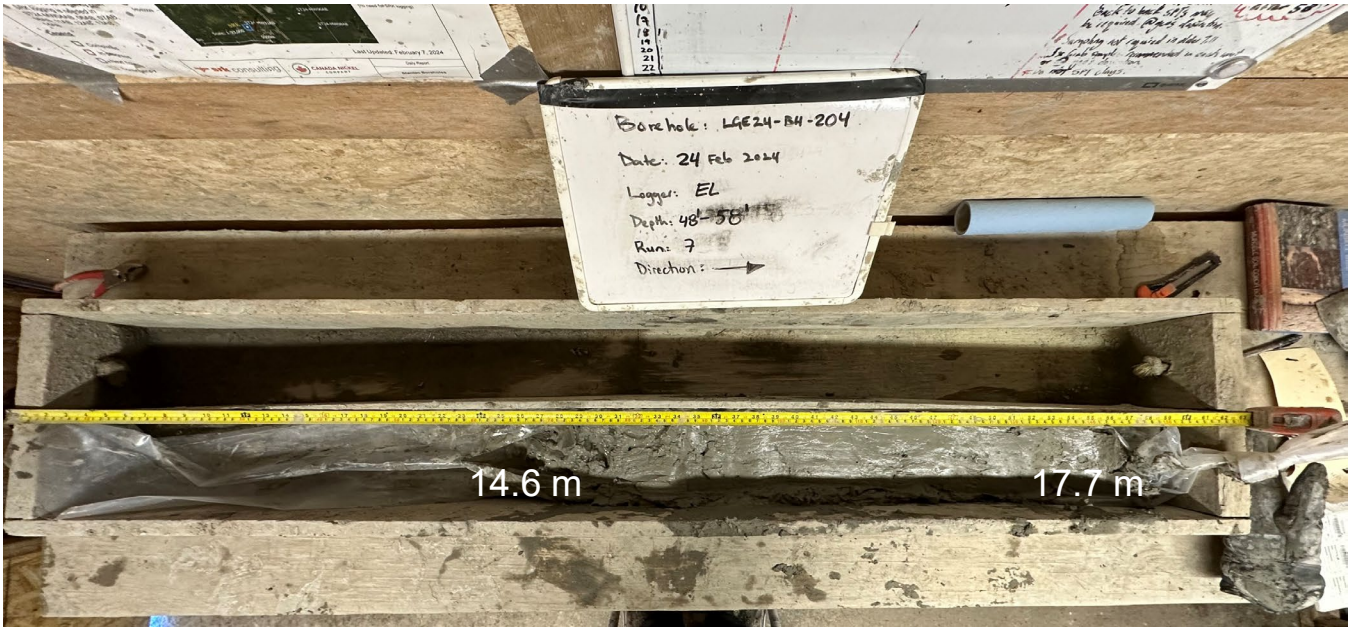
Depth (m): 8.5 – 11.6



Depth (m): 11.6 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-204** **Depth (m): 8.5 – 14.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 14.6 – 17.7



Depth (m): 17.7 – 20.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-204** **Depth (m): 14.6 – 20.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 20.1 – 23.8



Depth (m): 23.8 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-204		
		Depth (m): 20.1 – 26.8		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 26.8 – 29.9



Depth (m): 29.9 – 32.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-204** **Depth (m): 26.8 – 32.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 32.9 – 36.0



Depth (m): 36.0 – 39.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-204** **Depth (m): 32.9 – 39.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 39.0 – 40.8



Depth (m): 40.8 – 43.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-204		
		Depth (m): 39.0 – 43.6		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 9**

Borehole ID: SRK24-LGE-BH-204
Location: East Stockpile



Depth (m): 43.6 – 48.2

Depth (m):

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-204** **Depth (m): 43.6 -**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 9**

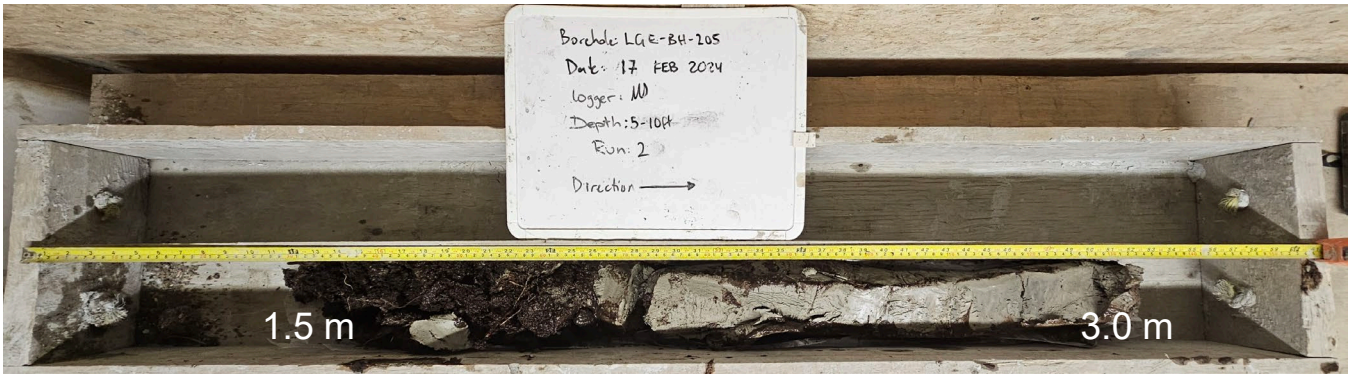
SRK24-LGE-BH-205

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



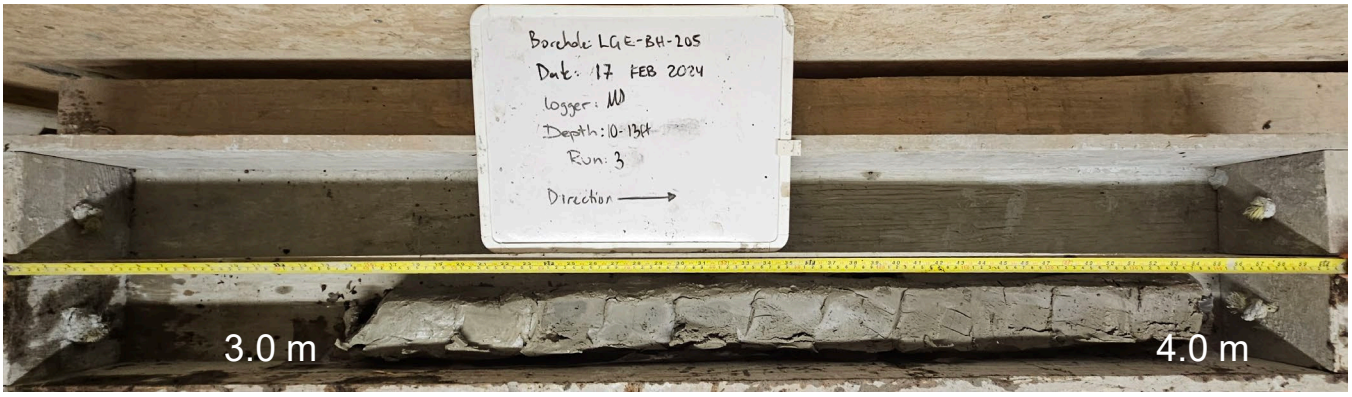
Depth (m): 0.0 – 1.5



Depth (m): 1.5 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-205** **Depth (m): 0.0 – 3.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



Depth (m): 3.0 – 4.0

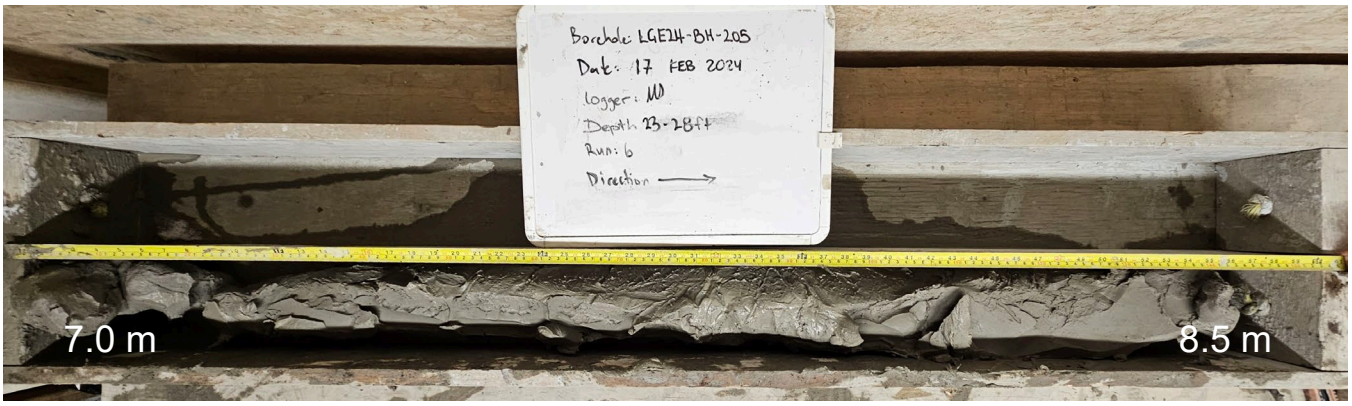


Depth (m): 4.0 – 5.5

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



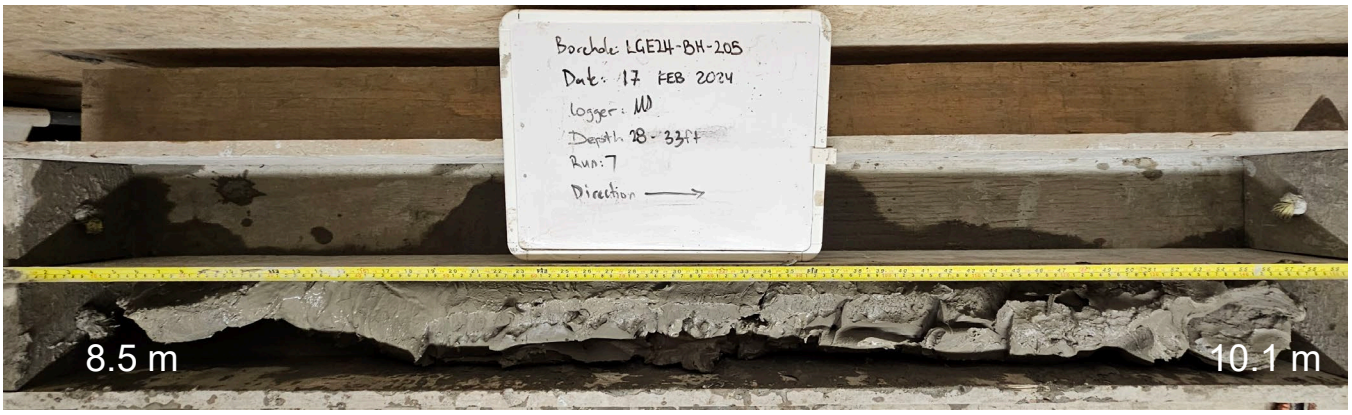
Depth (m): 5.5 – 7.0



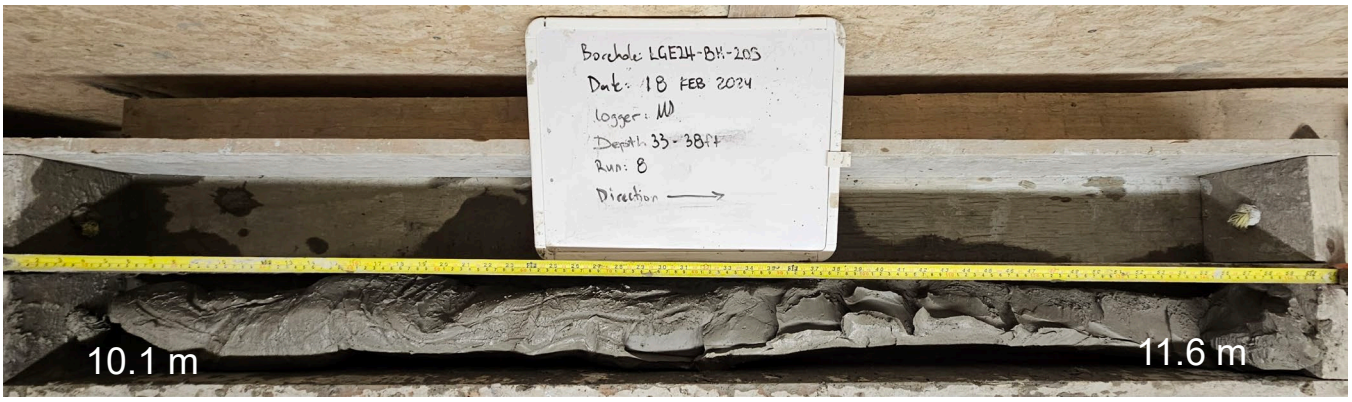
Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-205** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



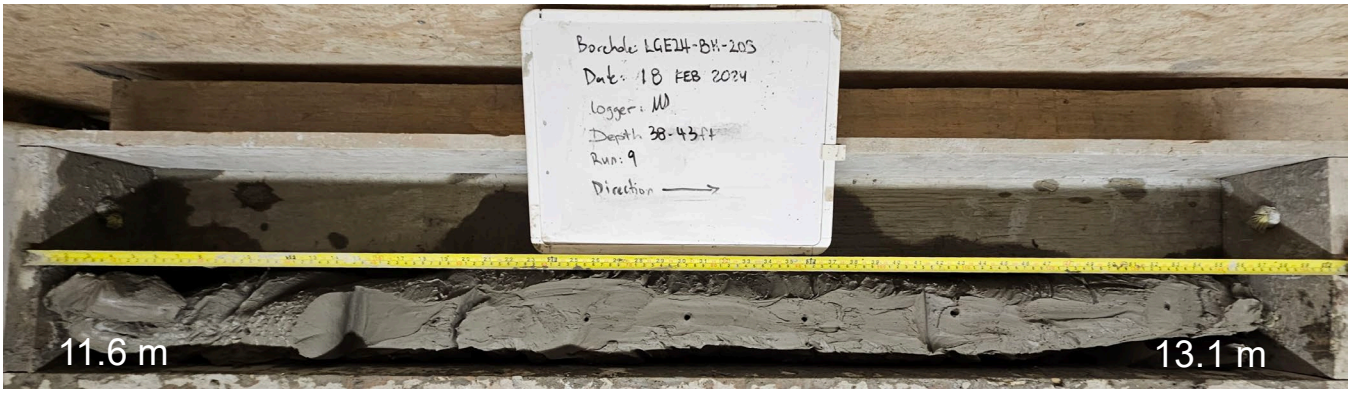
Depth (m): 8.5 – 10.1



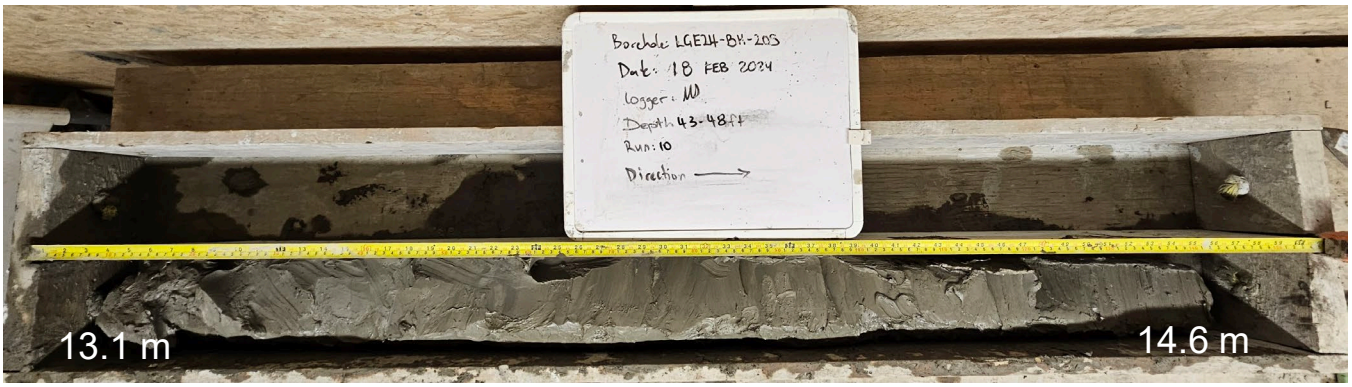
Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-205** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



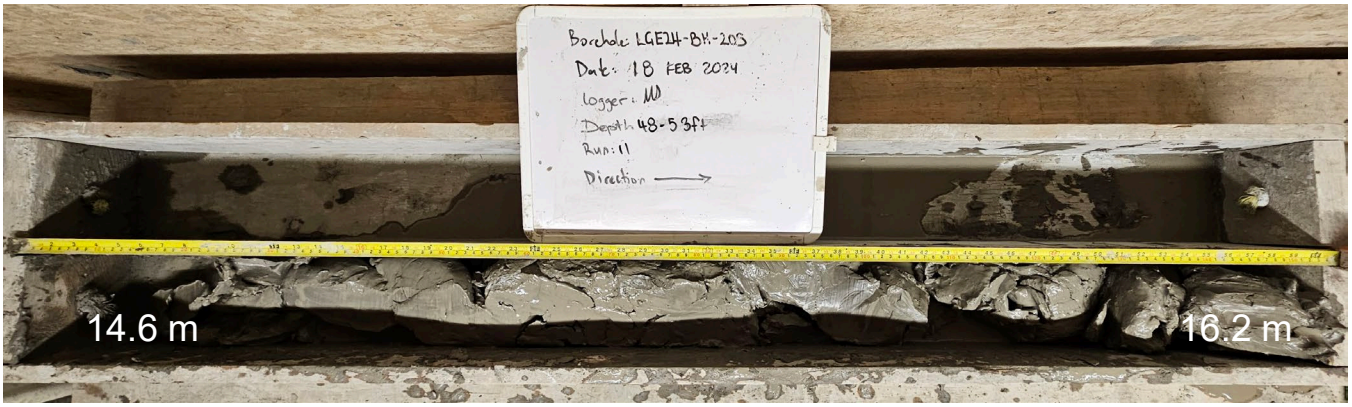
Depth (m): 11.6 – 13.1



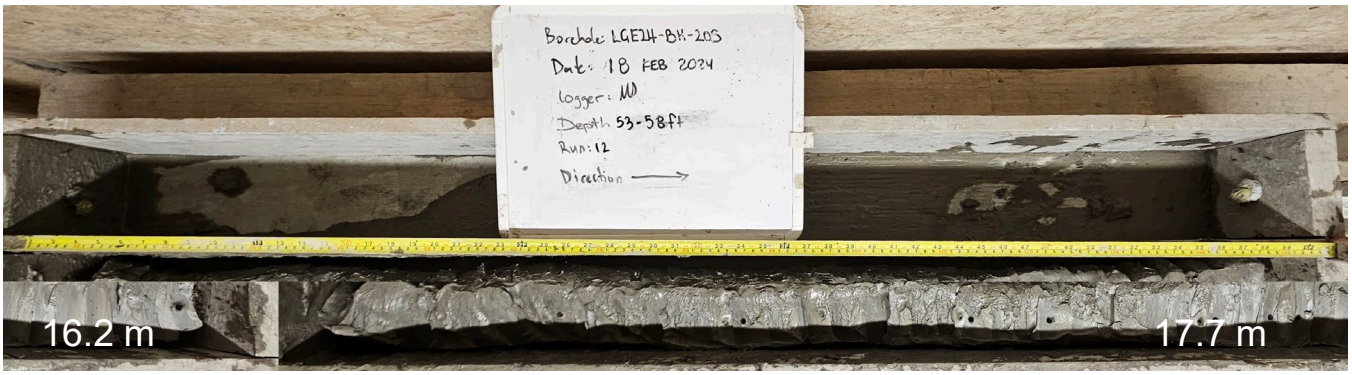
Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-205** **Depth (m): 11.6 – 14.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



Depth (m): 14.6 – 16.2



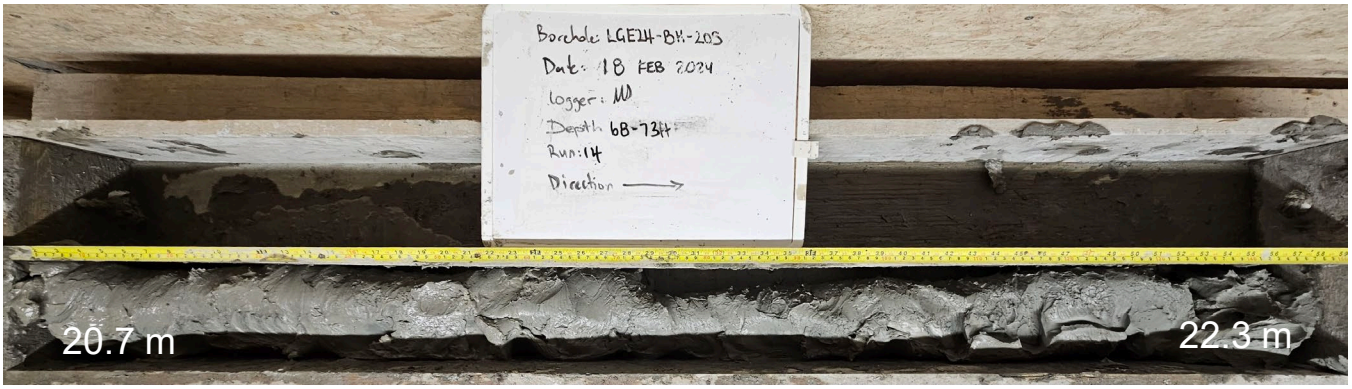
Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-205** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



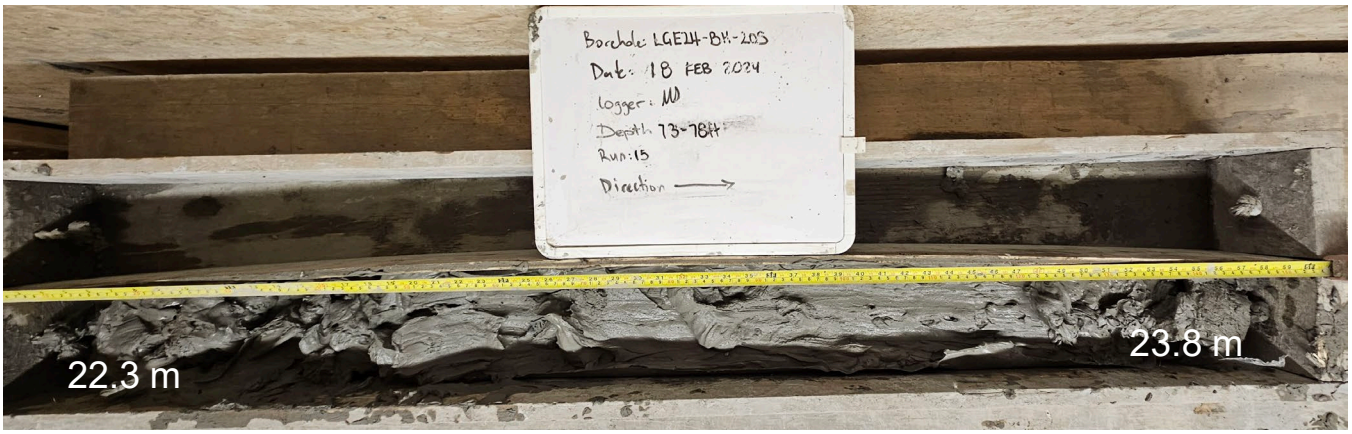
Depth (m): 17.7 – 20.7



Depth (m): 20.7 – 22.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-205		
		Depth (m): 17.7 – 22.3		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



Depth (m): 22.3 – 23.8



Depth (m): 23.8 – 25.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-LGE-BH-205		
		Depth (m): 22.3 – 25.3		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 9**

Borehole ID: SRK24-LGE-BH-205
Location: East Stockpile



Depth (m): 25.3 – 28.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-LGE-BH-205** **Depth (m): 25.3 – 28.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 9**

SRK24-WRD-BH-201

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 0.0 – 2.4



Depth (m): 2.4 – 4.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 0.0 – 4.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility

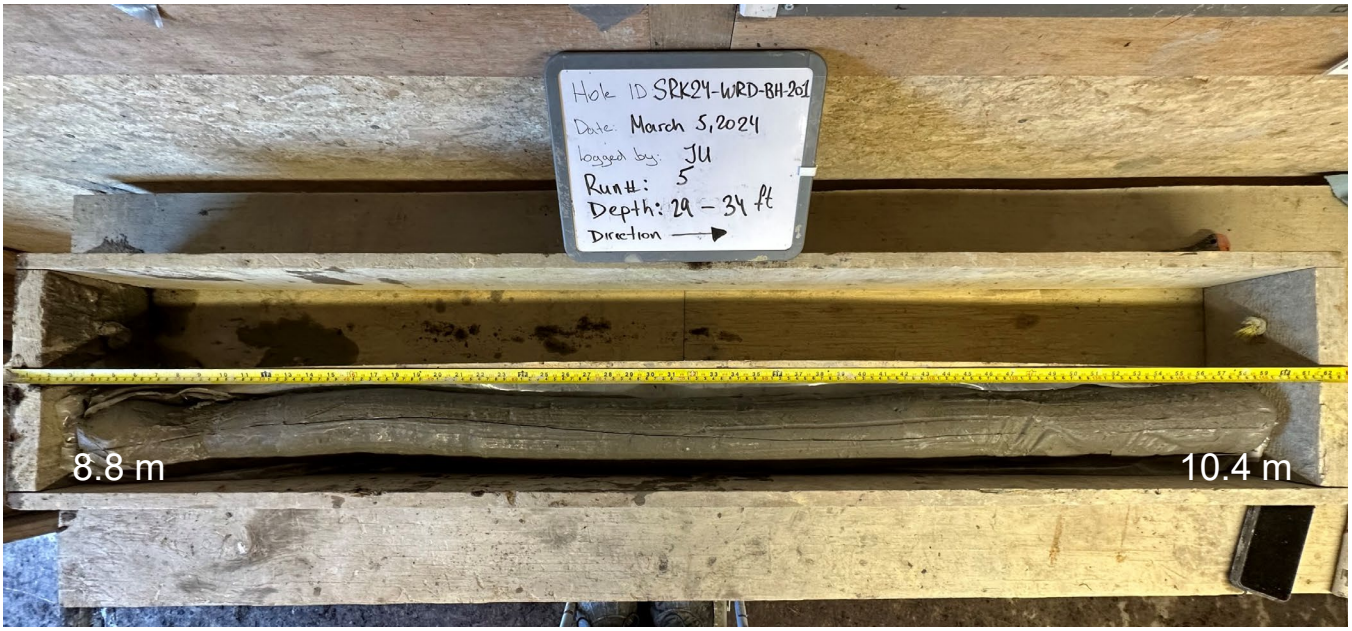


Depth (m): 4.0 – 5.5

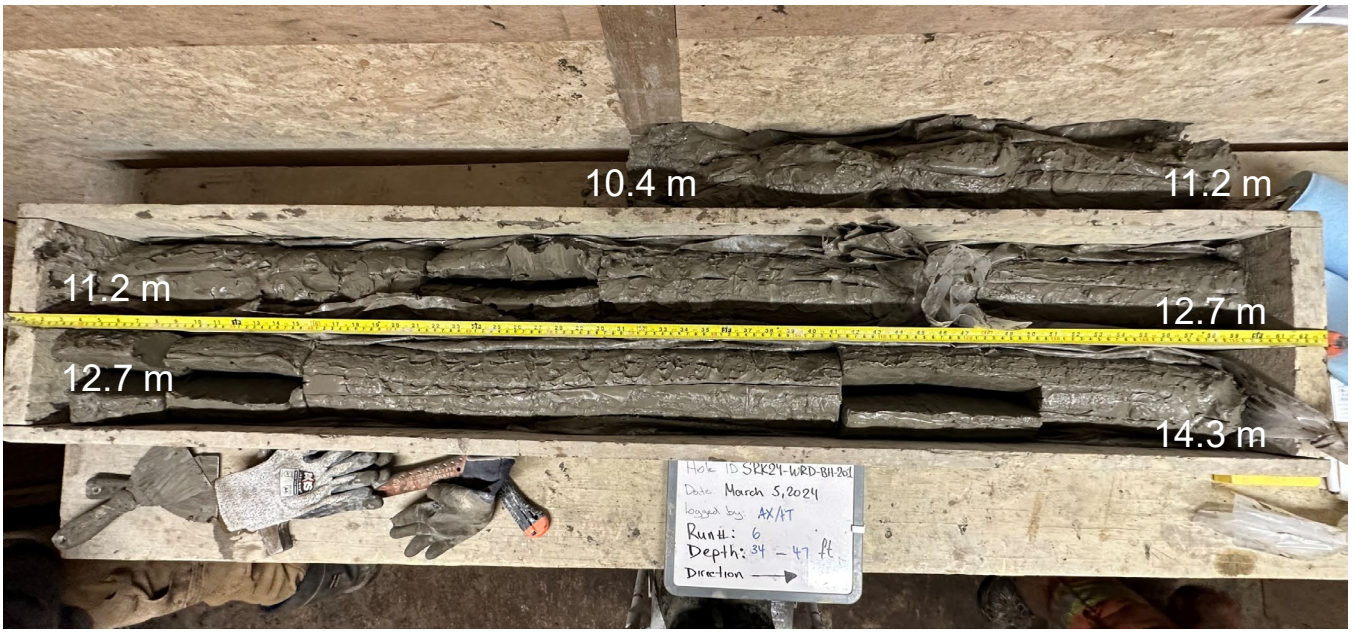


Depth (m): 5.5 – 8.8

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 8.8 – 10.4



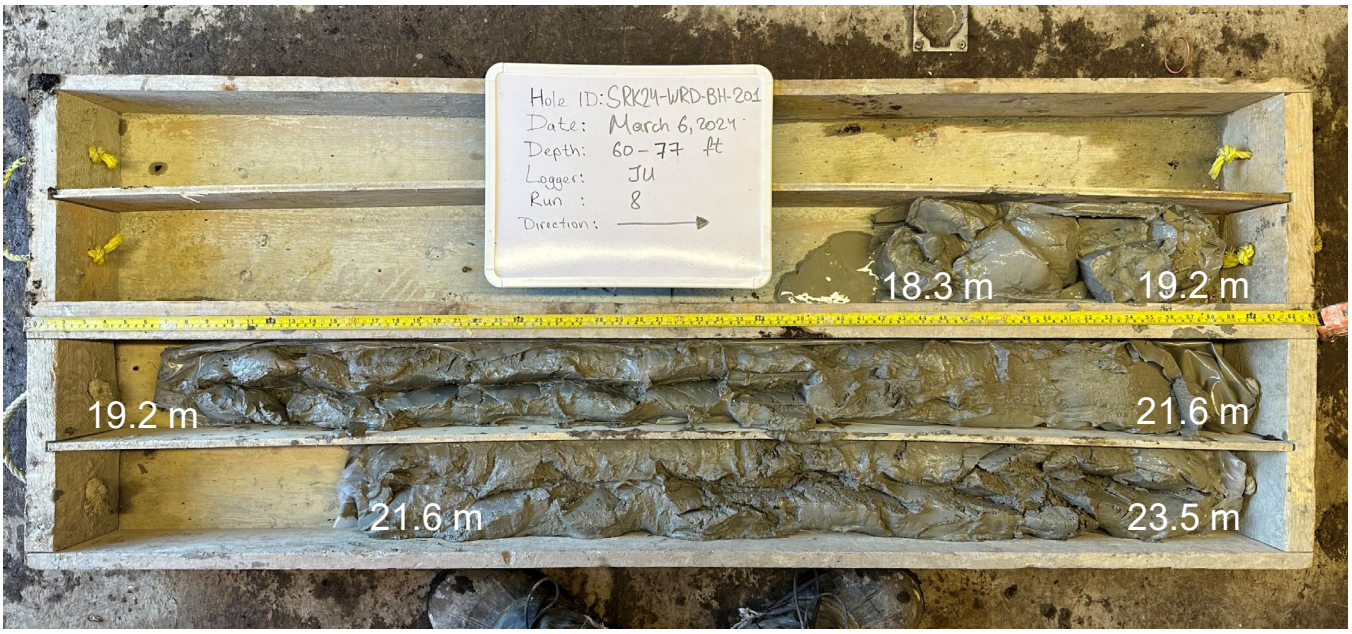
Depth (m): 10.4 – 14.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 8.8 – 14.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 14.3 – 18.3



Depth (m): 18.3 – 23.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 14.3 – 23.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 23.5 – 26.8



Depth (m): 26.8 – 29.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 23.5 – 29.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 29.9 – 32.9



Depth (m): 32.9 – 36.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 29.9 – 36.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 36.0 – 39.0



Depth (m): 39.0 – 42.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 36.0 – 42.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 42.1 – 45.1



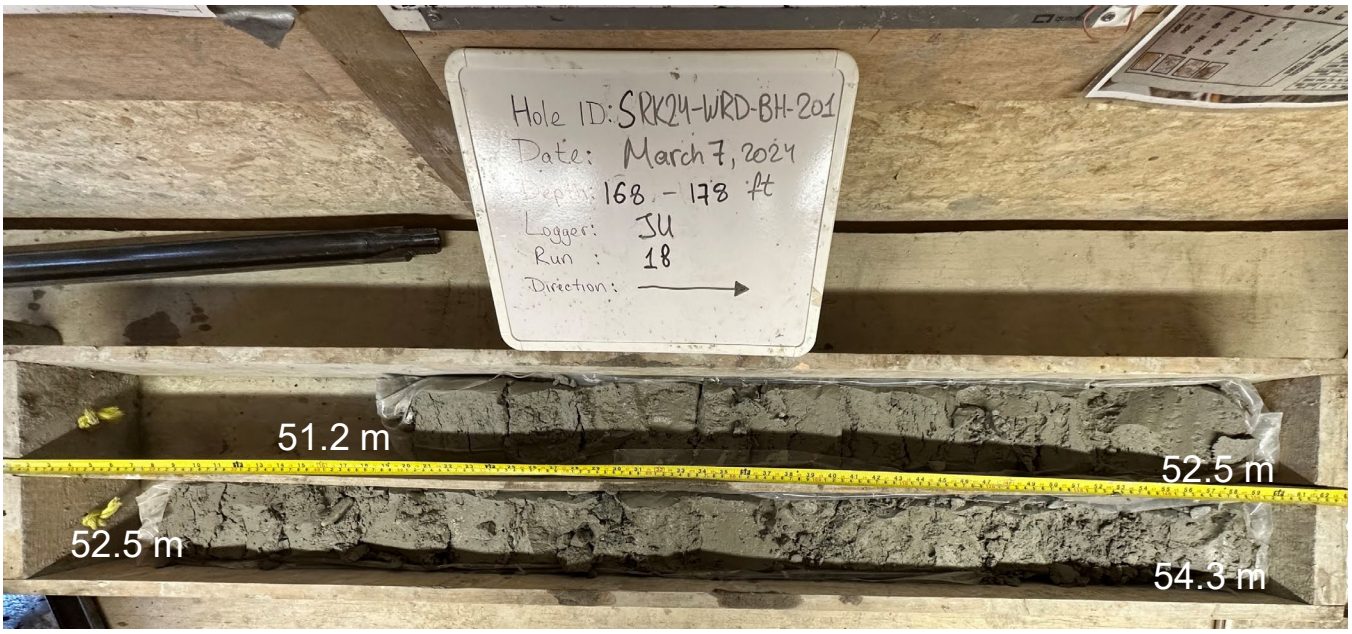
Depth (m): 45.1 – 48.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 42.1 – 48.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 48.2 – 51.2



Depth (m): 51.2 – 54.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-WRD-BH-201		
		Depth (m): 48.2 – 54.3		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 54.3 – 57.3



Depth (m): 57.3 – 60.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 54.3 – 60.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



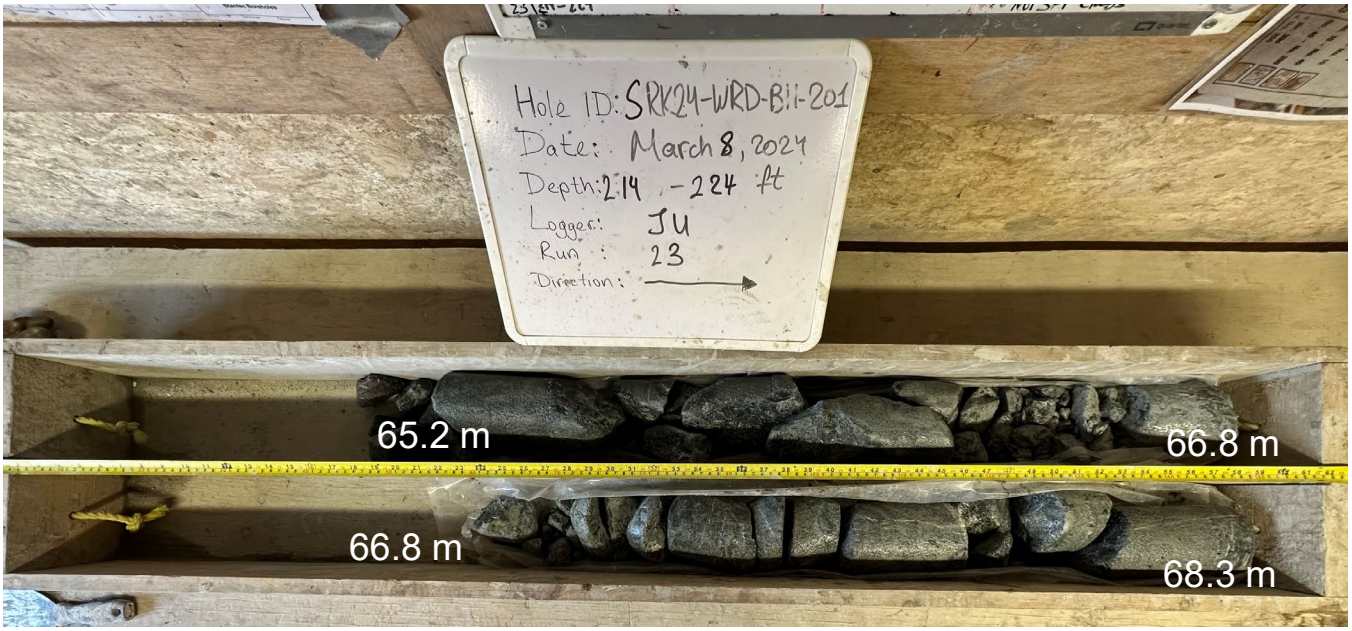
Depth (m): 60.4 – 63.4



Depth (m): 63.4 – 65.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-201** **Depth (m): 60.4 – 65.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 12**

Borehole ID: SRK24-WRD-BH-201
Location: Impoundment Facility



Depth (m): 65.2 – 68.3

SRK24-WRD-BH-202

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-202
Location: Impoundment Facility



Depth (m): 0.0 – 1.5



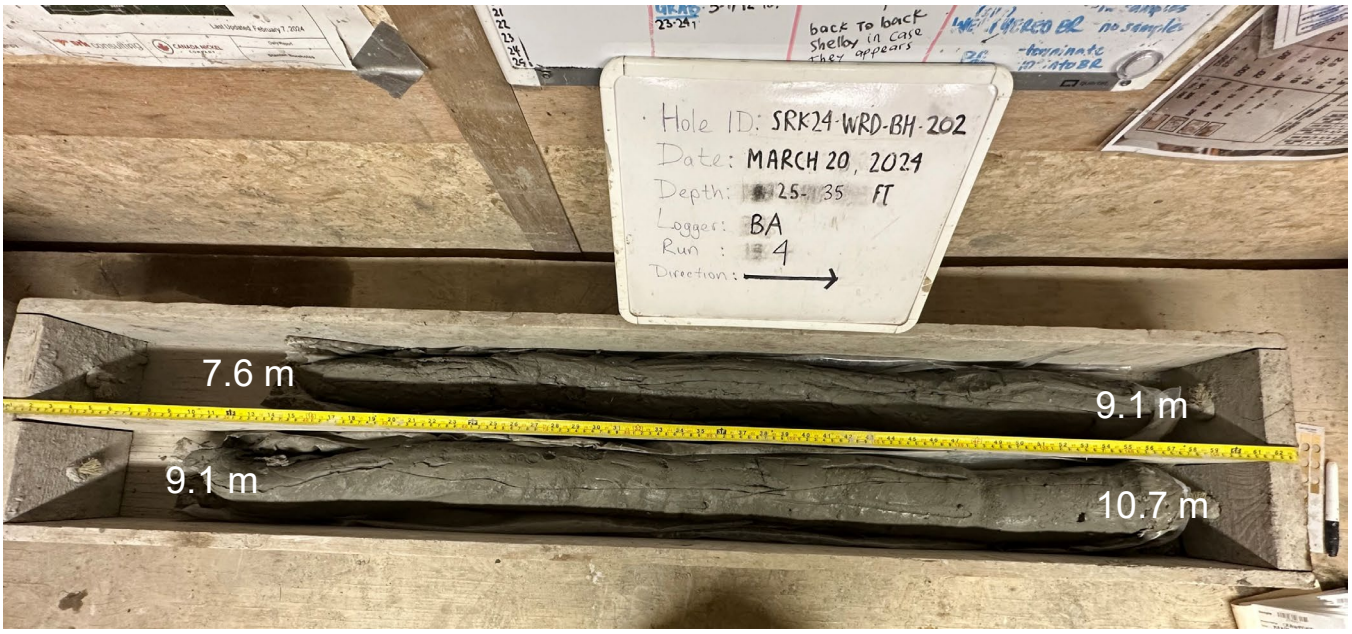
Depth (m): 1.5 – 4.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-202** **Depth (m): 0.0 – 4.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 5**

Borehole ID: SRK24-WRD-BH-202
Location: Impoundment Facility



Depth (m): 4.6 – 7.6



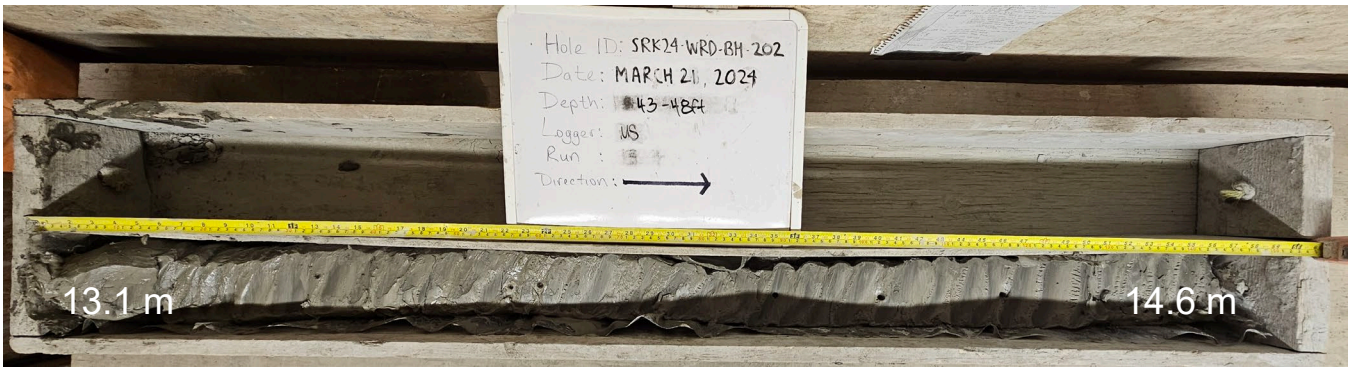
Depth (m): 7.6 – 10.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-202** **Depth (m): 4.6 – 10.7**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **2 of 5**

Borehole ID: SRK24-WRD-BH-202
Location: Impoundment Facility



Depth (m): 10.7 – 13.1



Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-202** **Depth (m): 10.7 – 14.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 5**

Borehole ID: SRK24-WRD-BH-202
Location: Impoundment Facility



Depth (m): 14.6 – 17.7



Depth (m): 17.7 – 20.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-202** **Depth (m): 14.6 – 20.7**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **4 of 5**

Borehole ID: SRK24-WRD-BH-202
Location: Impoundment Facility



Depth (m): 20.7 – 22.3



Depth (m): 22.3 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-WRD-BH-202 **Depth (m): 20.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **5 of 5**

SRK24-WRD-BH-205

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility

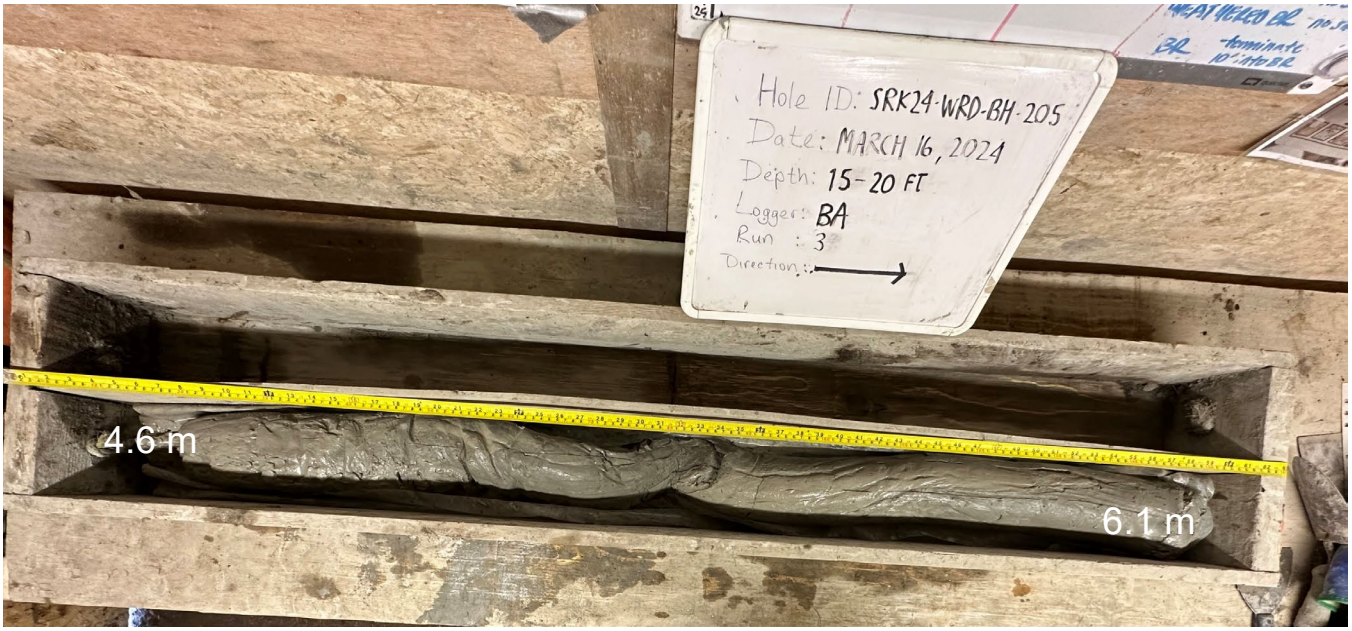


Depth (m): 0.0 – 3.0



Depth (m): 3.0 – 4.6

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 4.6 – 6.1



Depth (m): 6.1 – 8.8

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 8.8 – 11.9



Depth (m): 11.9 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-WRD-BH-205		
		Depth (m): 8.8 – 14.6		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 13**

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 17.7 – 20.7



Depth (m): 20.7 – 23.8

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 23.8 – 26.8



Depth (m): 26.8 – 29.9

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 29.9 – 32.9



Depth (m): 32.9 – 36.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-205** **Depth (m): 29.9 – 36.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **7 of 13**

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 36.0 – 39.0



Depth (m): 39.0 – 42.1

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 42.1 – 45.1



Depth (m): 45.1 – 48.2

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 48.2 – 51.2



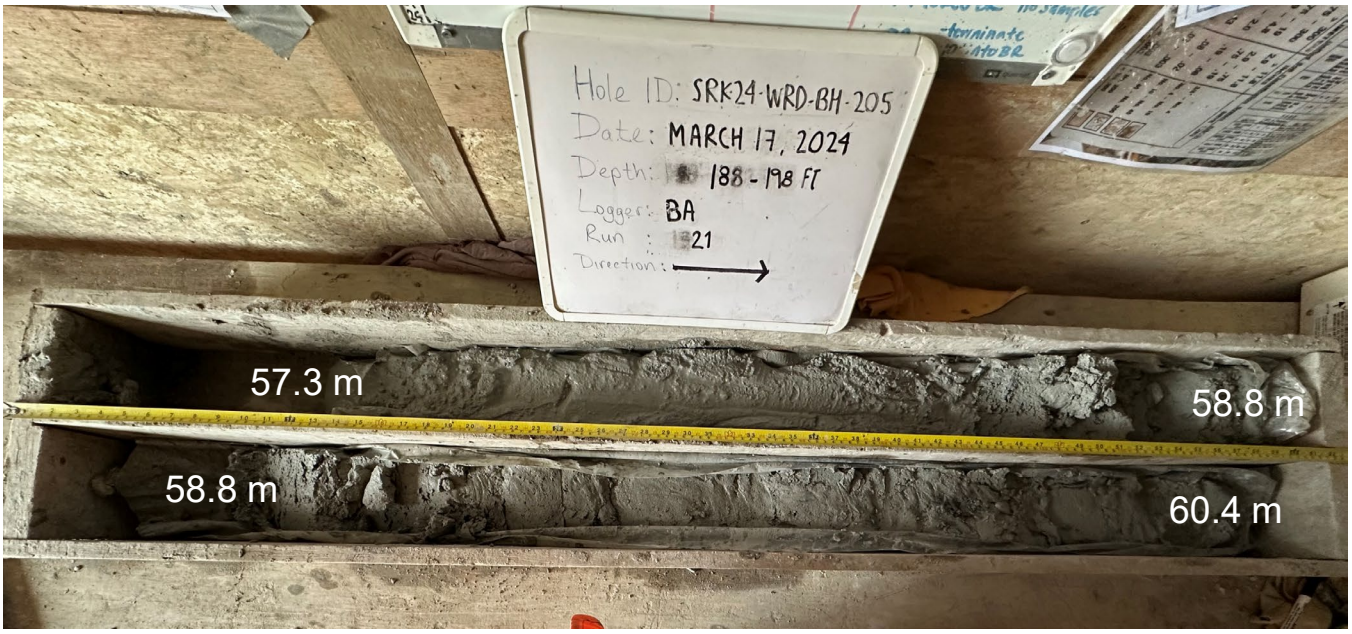
Depth (m): 51.2 – 54.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-205** **Depth (m): 48.2 – 54.3**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **10 of 13**

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 54.3 – 57.3



Depth (m): 57.3 – 60.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-205** **Depth (m): 54.3 – 60.4**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **11 of 13**

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 60.4 – 63.4



Depth (m): 63.4 – 65.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-205** **Depth (m): 60.4 – 65.5**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **12 of 13**

Borehole ID: SRK24-WRD-BH-205
Location: Impoundment Facility



Depth (m): 65.5 – 68.6

SRK24-WRD-BH-207

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-207
Location: Impoundment Facility



Depth (m): 0.0 – 1.5



Depth (m): 1.5 – 4.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-207** **Depth (m): 0.0 – 4.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 3**

Borehole ID: SRK24-WRD-BH-207
Location: Impoundment Facility



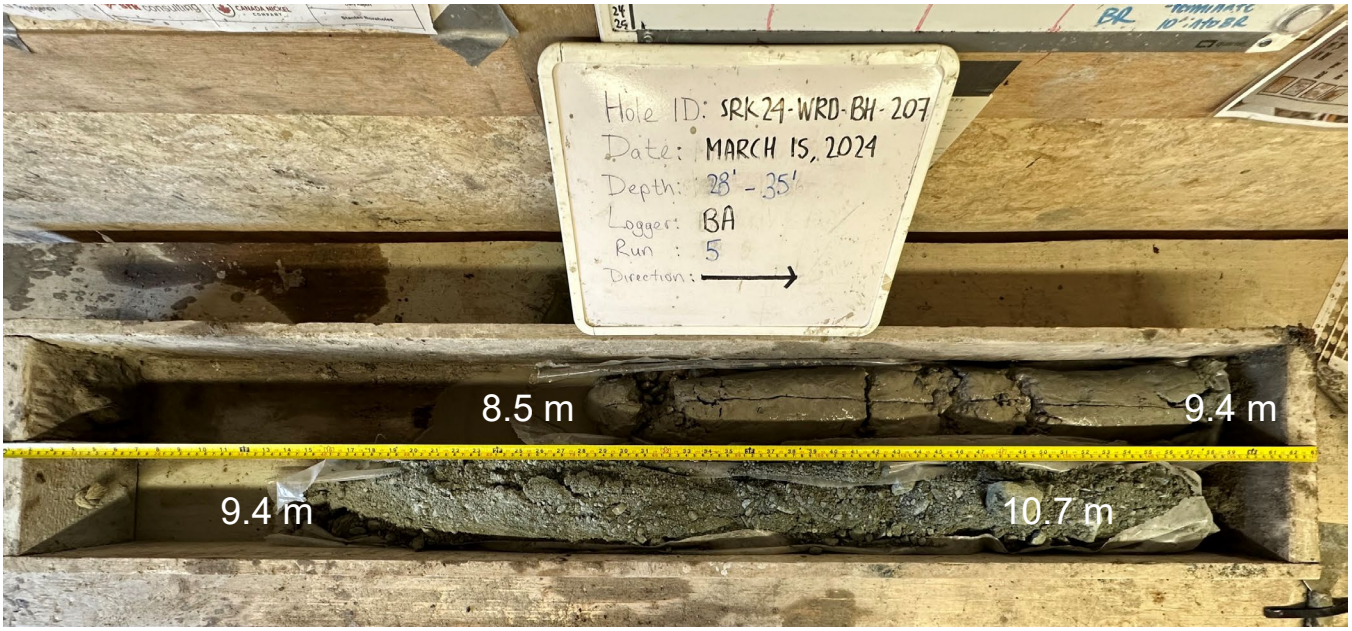
Depth (m): 4.0 – 5.5



Depth (m): 5.5 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-WRD-BH-207		
		Depth (m): 4.0 – 8.5		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **2 of 3**

Borehole ID: SRK24-WRD-BH-207
Location: Impoundment Facility



Depth (m): 8.5 – 10.7



Depth (m): 10.7 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-207** **Depth (m): 8.5 – 14.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 3**

SRK24-WRD-BH-212

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 0.0 – 1.5

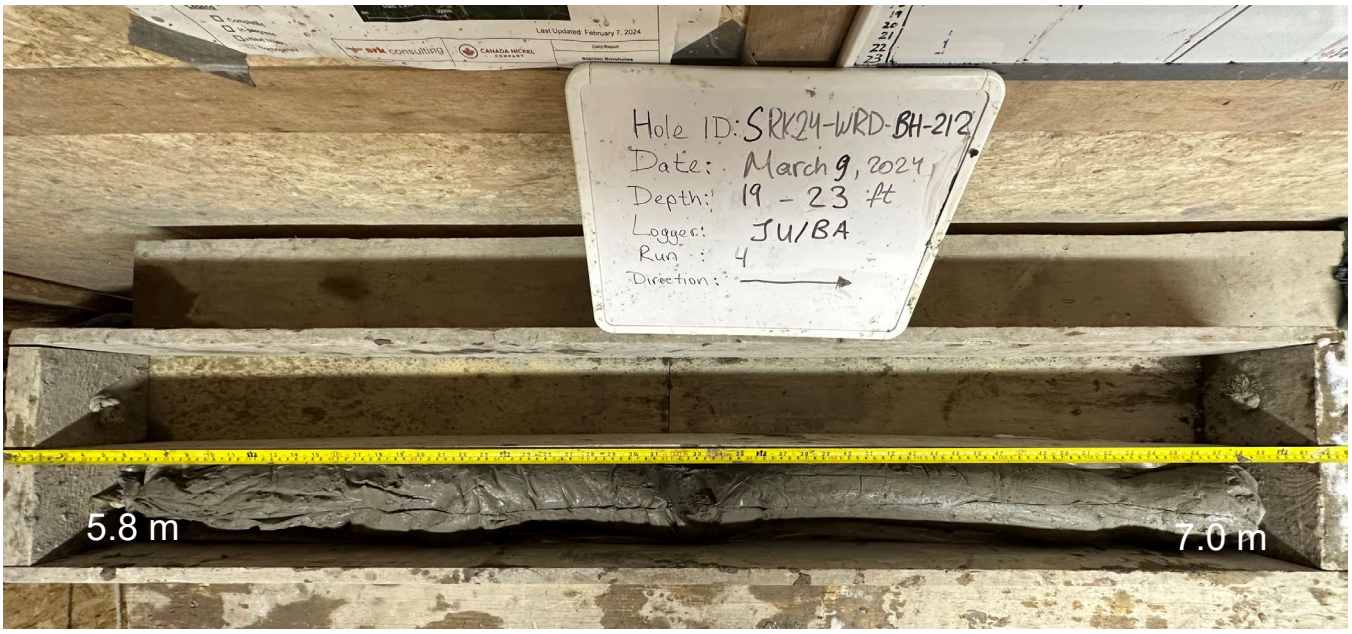


Depth (m): 1.5 – 2.4

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 2.4 – 5.8



Depth (m): 5.8 – 7.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-212** **Depth (m): 2.4 – 7.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **2 of 7**

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 7.0 – 10.1



Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-212** **Depth (m): 7.0 – 11.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 7**

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 11.6 – 14.6



Depth (m): 14.6 – 16.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-212** **Depth (m): 11.6 – 16.2**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **4 of 7**

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 16.2 – 17.7



Depth (m): 17.7 – 19.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-212** **Depth (m): 16.2 – 19.2**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **5 of 7**

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 19.2 – 21.6



Depth (m): 21.6 – 28.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-212** **Depth (m): 19.2 – 28.3**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **6 of 7**

Borehole ID: SRK24-WRD-BH-212
Location: Impoundment Facility



Depth (m): 28.3 – 32.6



Depth (m): 32.6 – 35.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-212** **Depth (m): 28.3 – 35.7**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **7 of 7**

SRK24-WRD-BH-215

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 0.0 – 2.4



Depth (m): 2.4 – 4.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 0.0 – 4.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 12**

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility

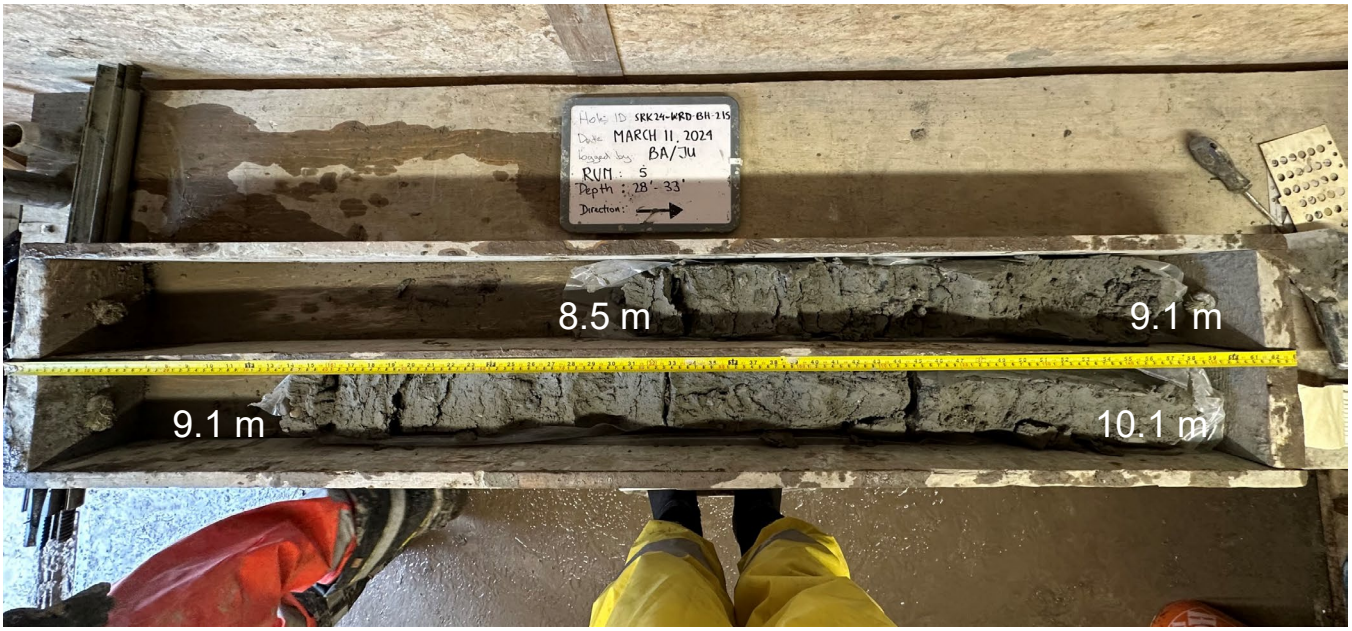


Depth (m): 4.0 – 7.0



Depth (m): 7.0 – 8.5

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 8.5 – 10.1



Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 12**

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 11.6 – 14.6



Depth (m): 14.6 – 17.7

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 17.7 – 20.7



Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **5 of 12**

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 23.8 – 26.8



Depth (m): 26.8 – 29.9

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 29.9 – 32.9



Depth (m): 32.9 – 36.0

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 36.0 – 39.0



Depth (m): 39.0 – 42.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 36.0 – 42.1**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **8 of 12**

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 42.1 – 45.1

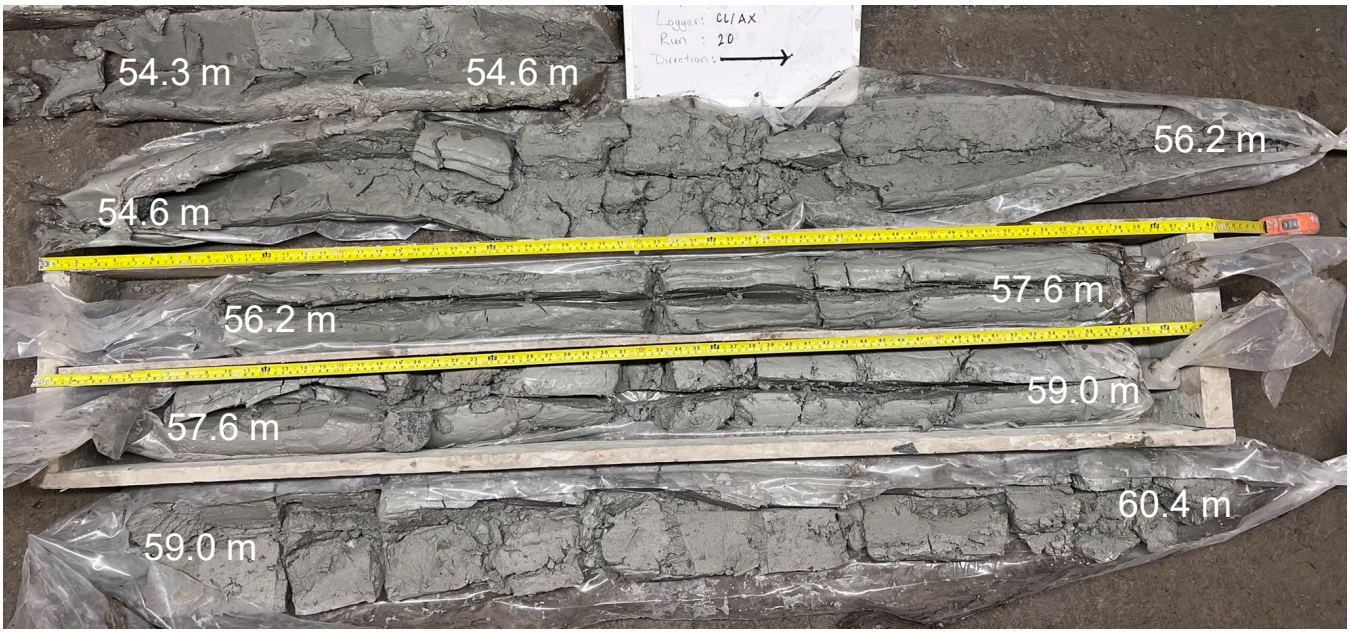


Depth (m): 45.1 – 48.2

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 48.2 – 54.3



Depth (m): 54.3 – 60.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 48.2 – 60.4**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **10 of 12**

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



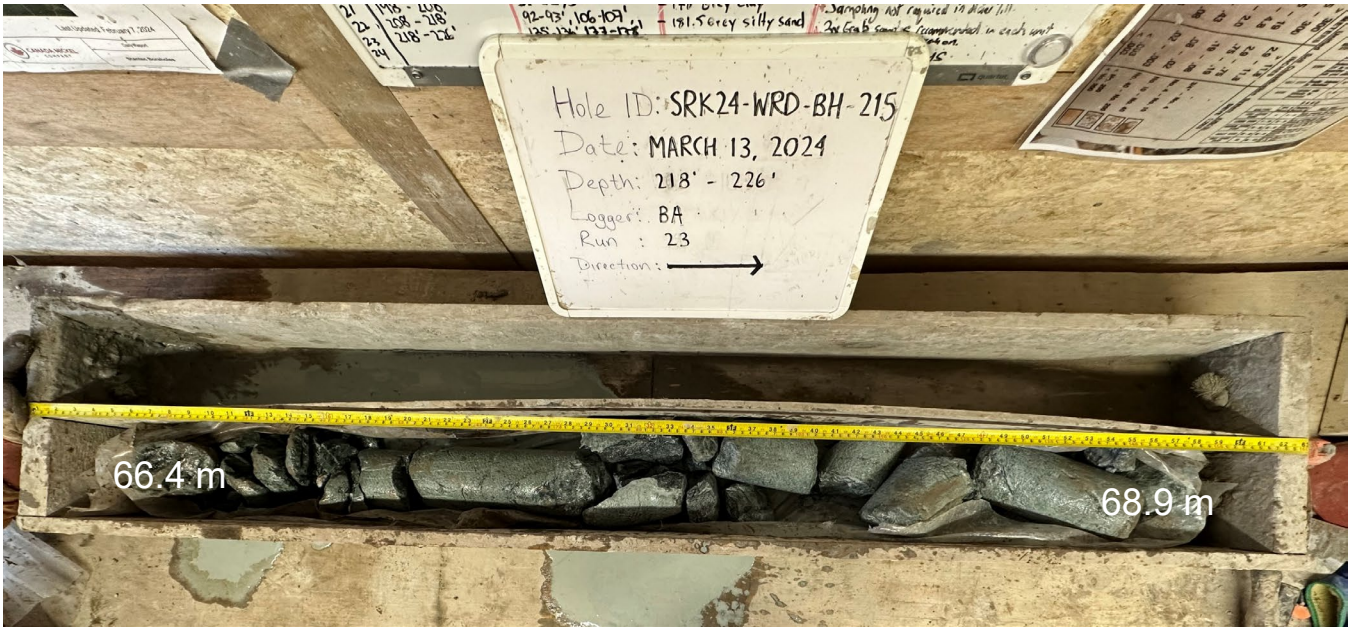
Depth (m): 60.4 – 63.4



Depth (m): 63.4 – 66.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 60.4 – 66.4**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **11 of 12**

Borehole ID: SRK24-WRD-BH-215
Location: Impoundment Facility



Depth (m): 66.4 – 68.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-215** **Depth (m): 66.4 – 68.9**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **12 of 12**

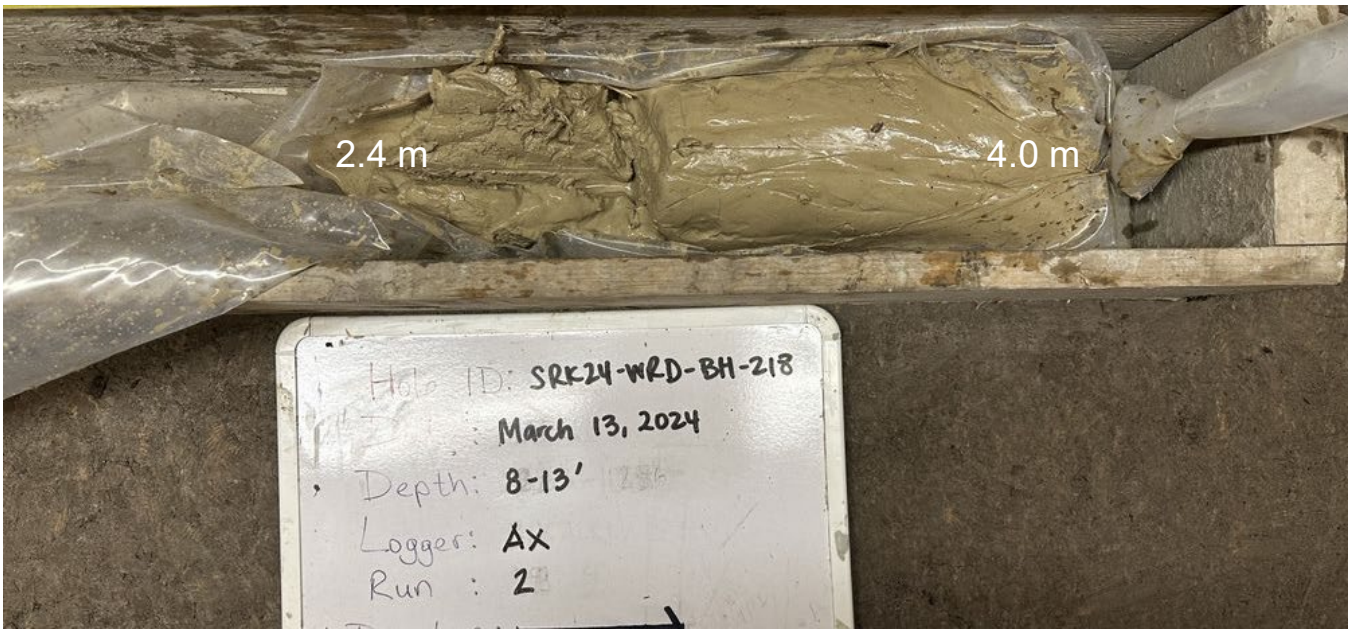
SRK24-WRD-BH-218

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-WRD-BH-218
Location: Impoundment Facility



Depth (m): 0.0 – 2.4



Depth (m): 2.4 – 4.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-218** **Depth (m): 0.0 – 4.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 4**

Borehole ID: SRK24-WRD-BH-218
Location: Impoundment Facility



Depth (m): 4.0 – 5.8



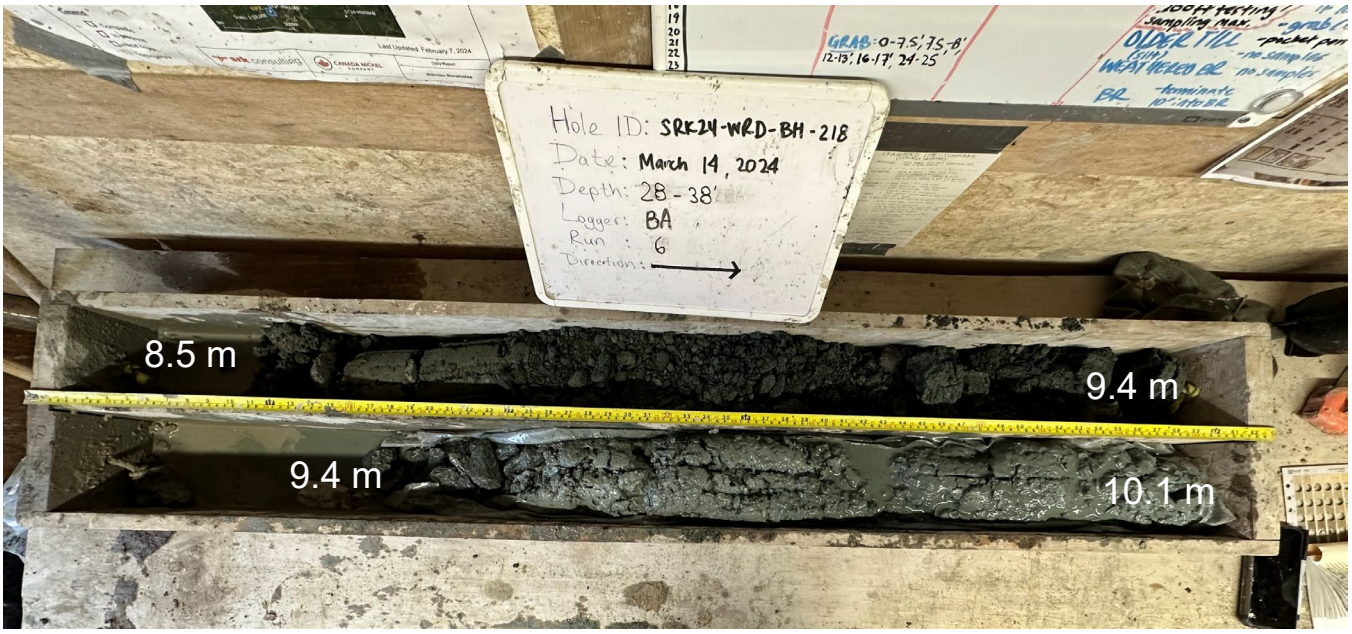
Depth (m): 5.8 – 7.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-218** **Depth (m): 4.0 – 7.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **2 of 4**

Borehole ID: SRK24-WRD-BH-218
Location: Impoundment Facility

NO PHOTO

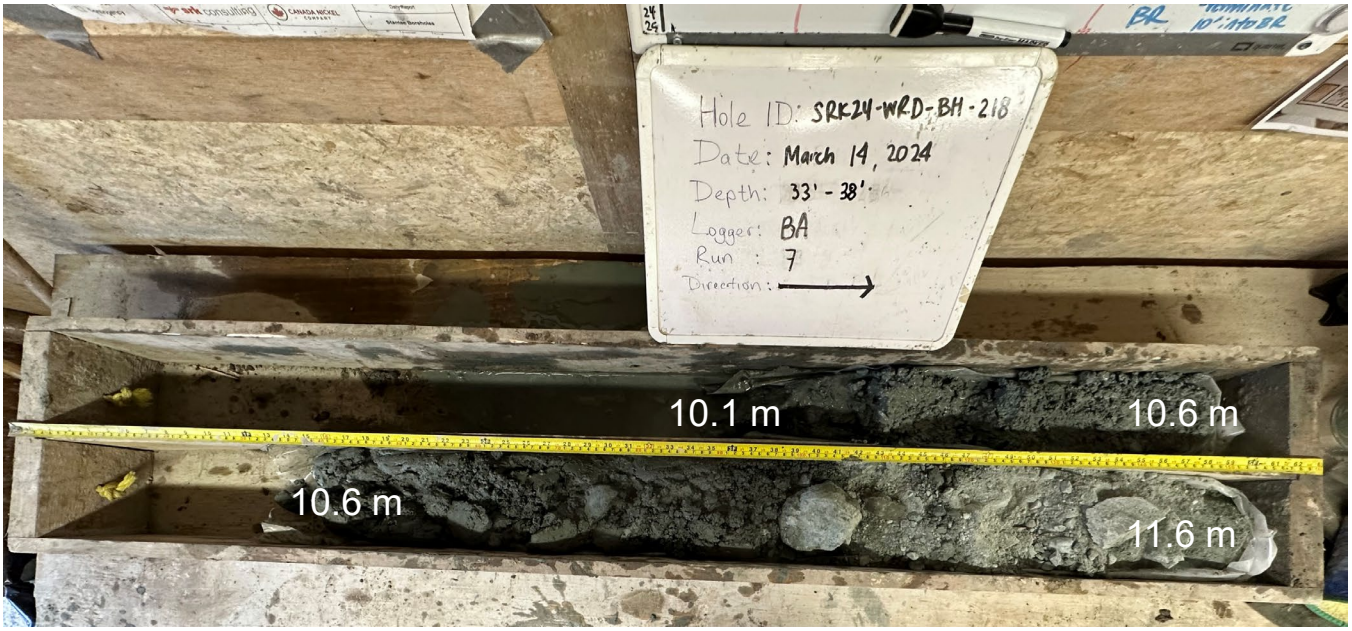
Depth (m): 7.0 – 8.5



Depth (m): 8.5 – 10.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-218** **Depth (m): 7.0 – 10.1**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 4**

Borehole ID: SRK24-WRD-BH-218
Location: Impoundment Facility



Depth (m): 10.1 – 11.6



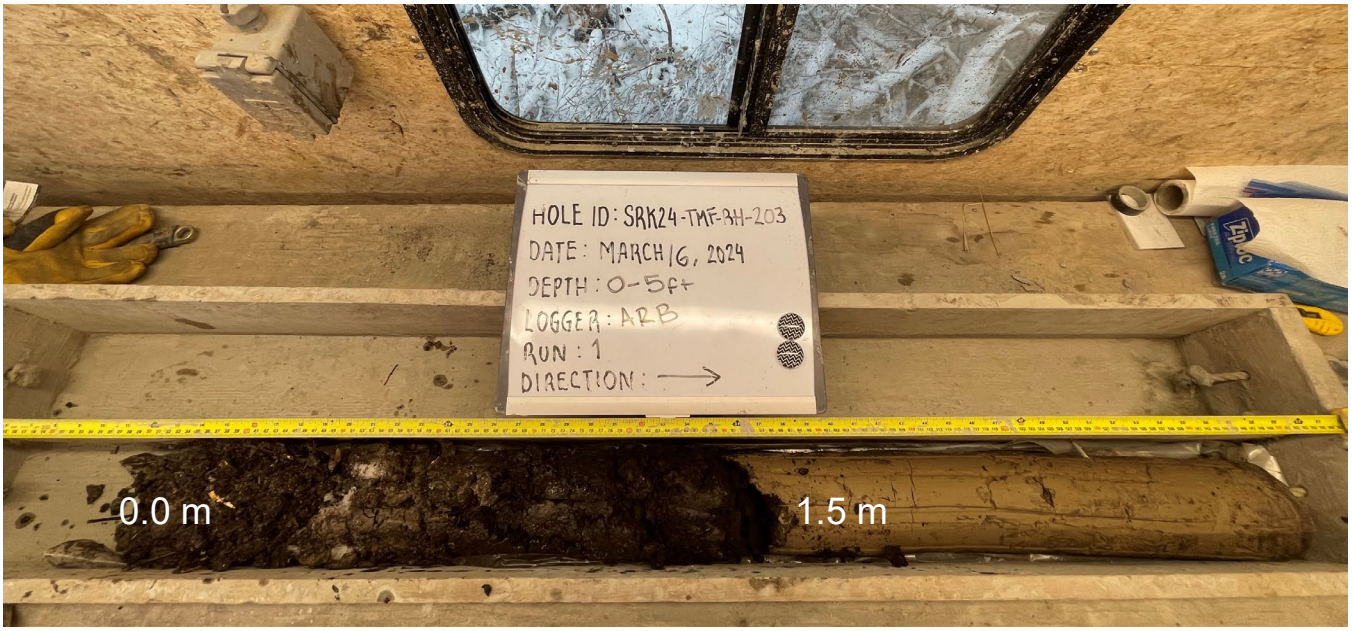
Depth (m): 11.6 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-WRD-BH-218** **Depth (m): 10.1 -14.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **4 of 4**

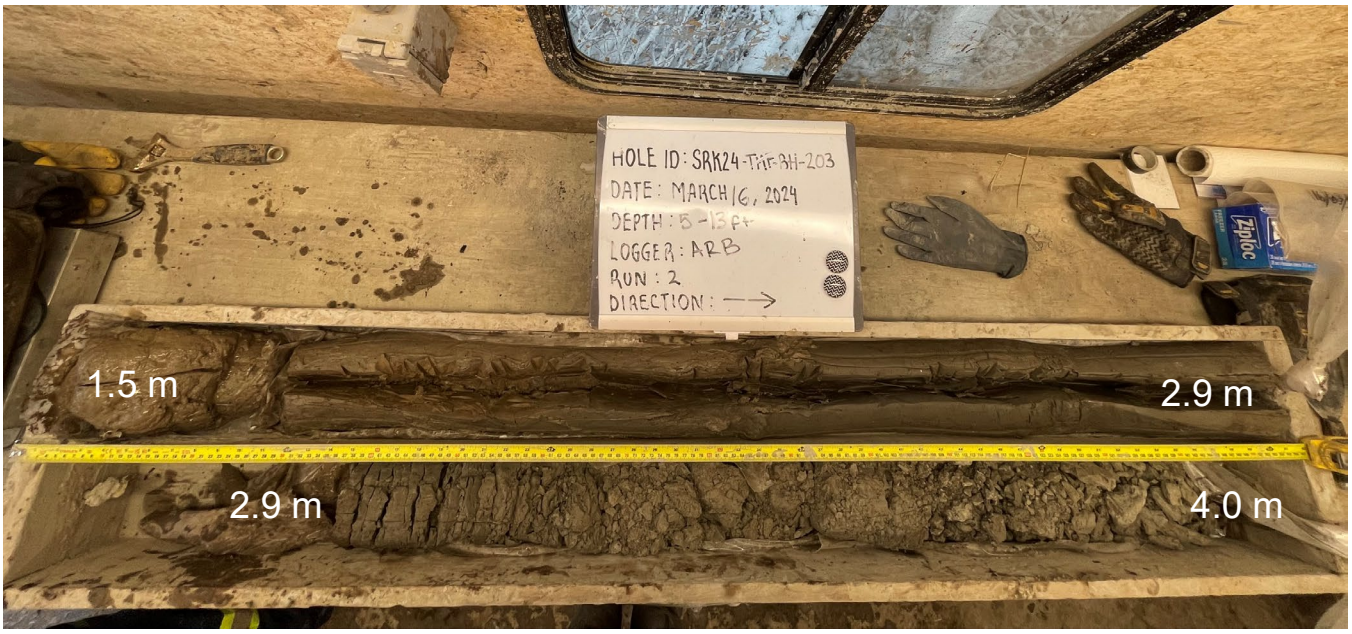
SRK24-TMF-BH-203

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-TMF-BH-203
Location: Tailings Management Facility



Depth (m): 0.0 – 1.5



Depth (m): 1.5 – 4.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-TMF-BH-203** **Depth (m): 0.0 – 4.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 1**

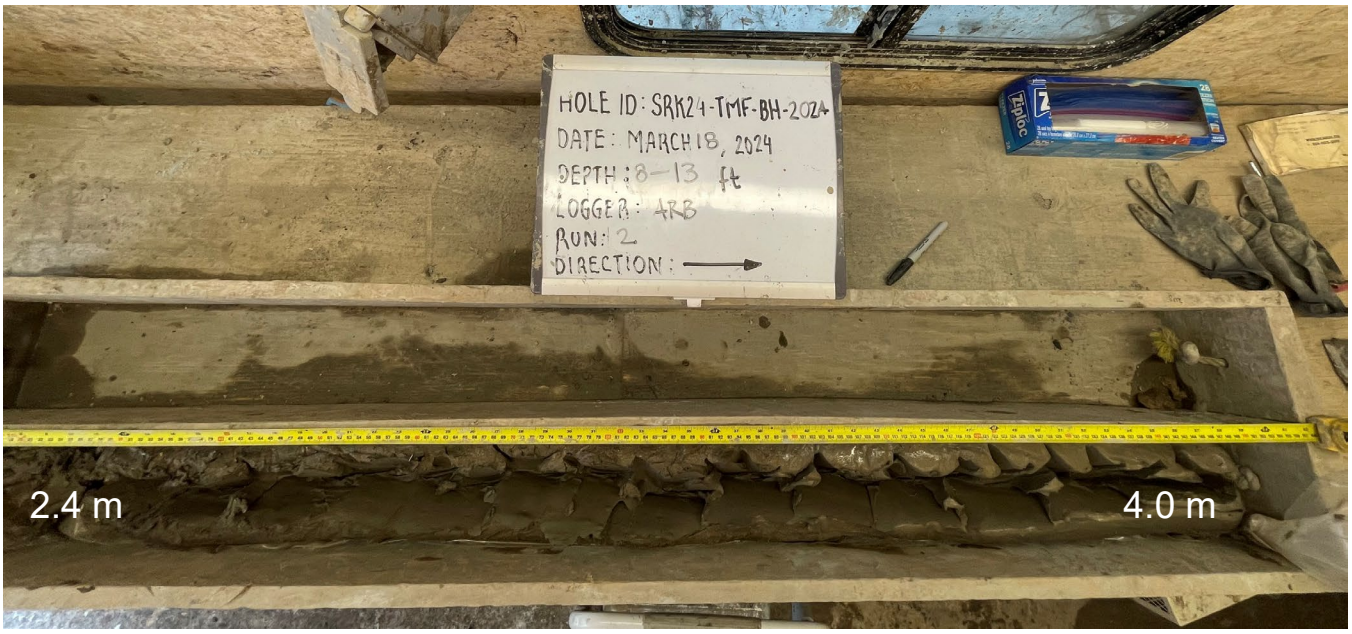
SRK24-TMF-BH-202A

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-TMF-BH-202A
Location: Tailings Management Facility



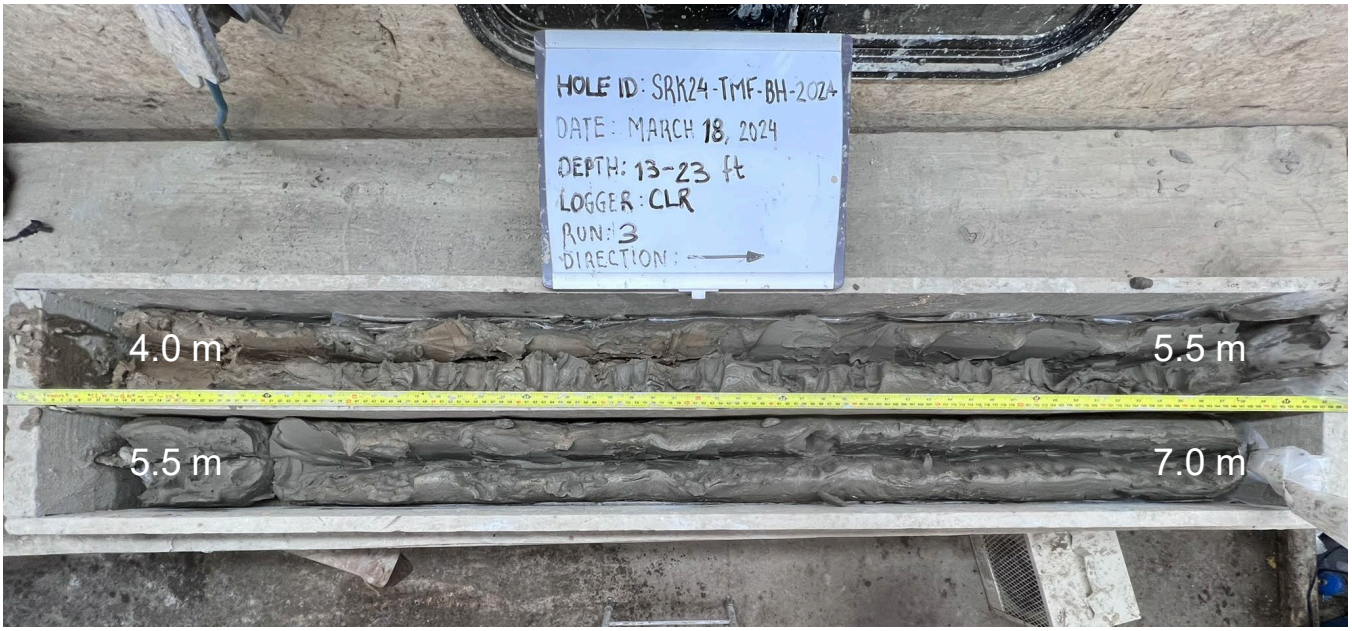
Depth (m): 0.0 – 2.4



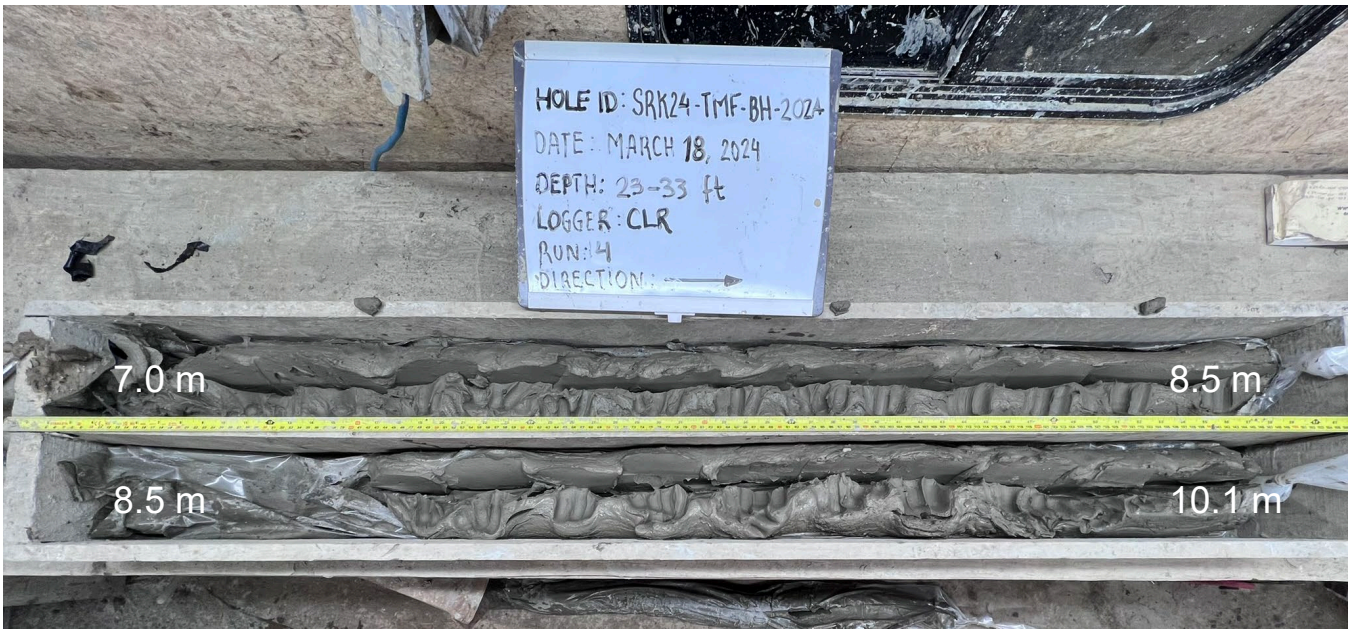
Depth (m): 2.4 – 4.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SRK24-TMF-BH-202A		
		Depth (m): 0.0 – 4.0		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 6**

Borehole ID: SRK24-TMF-BH-202A
Location: Tailings Management Facility



Depth (m): 4.0 – 7.0



Depth (m): 7.0 – 10.1

Borehole ID: SRK24-TMF-BH-202A
Location: Tailings Management Facility



Depth (m): 10.1 – 11.6



Depth (m): 11.6 – 14.6

Borehole ID: SRK24-TMF-BH-202A
Location: Tailings Management Facility

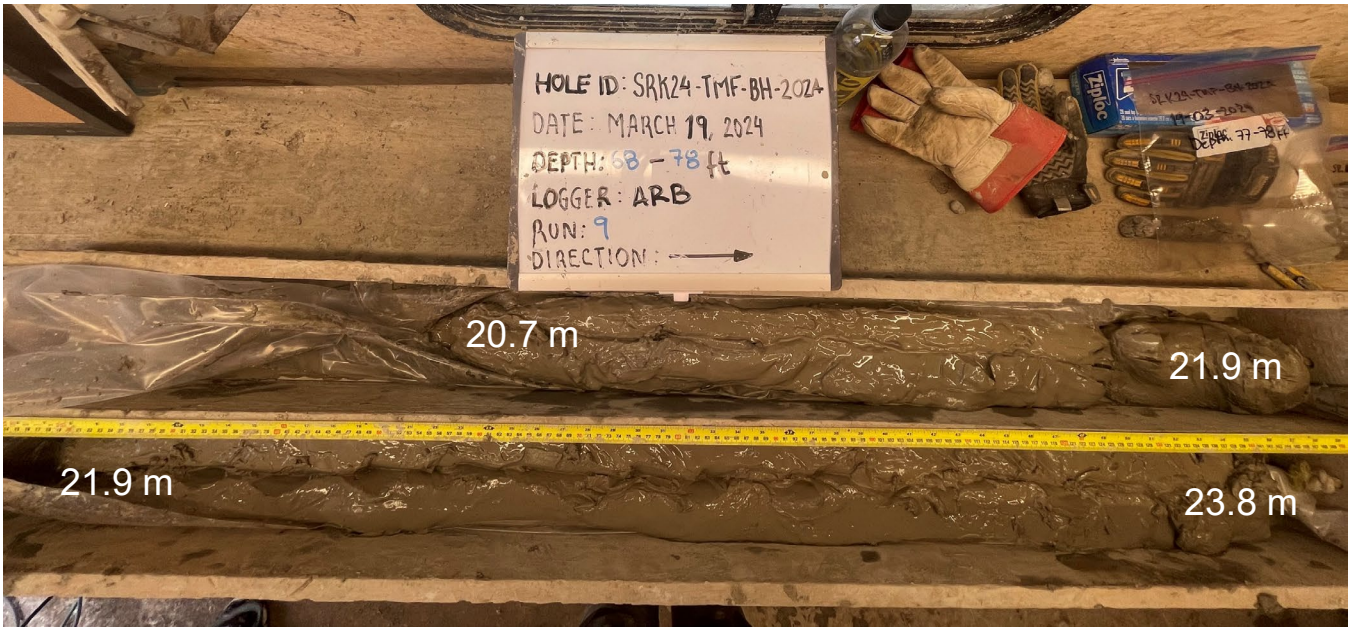


Depth (m): 14.6 – 17.7



Depth (m): 17.7 – 20.7

Borehole ID: SRK24-TMF-BH-202A
Location: Tailings Management Facility

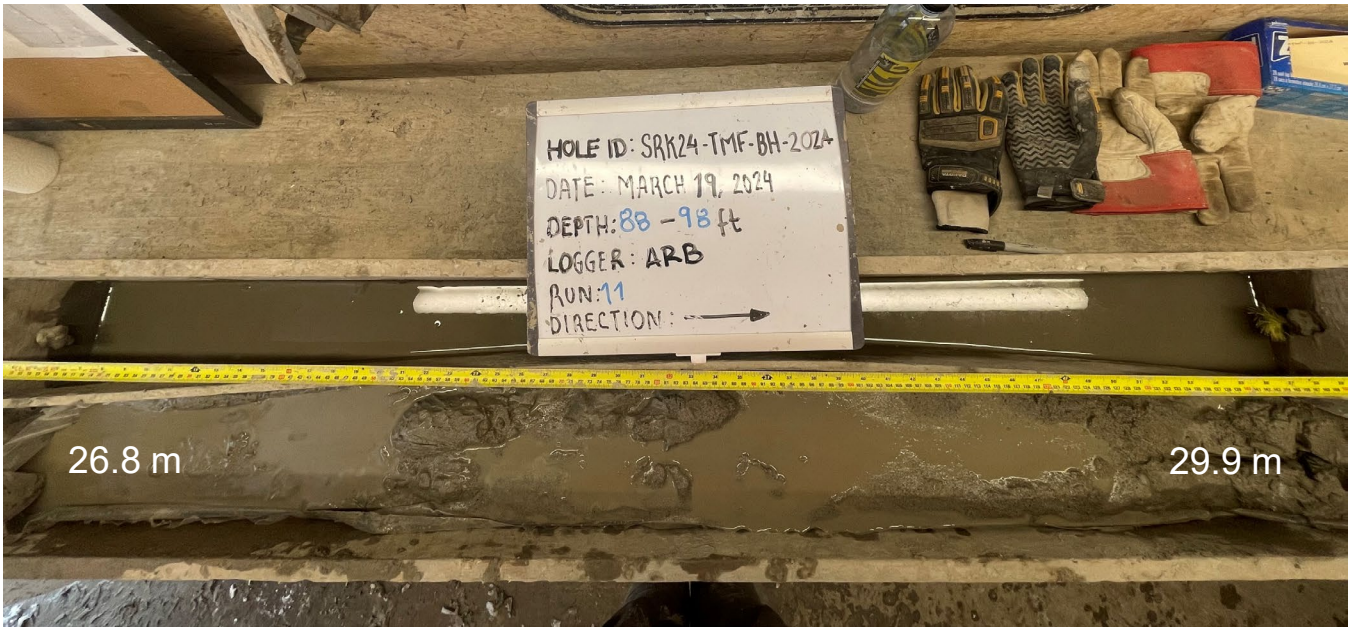


Depth (m): 20.7 – 23.8



Depth (m): 23.8 – 26.8

Borehole ID: SRK24-TMF-BH-202A
Location: Tailings Management Facility



Depth (m): 26.8 – 29.9

Depth (m):

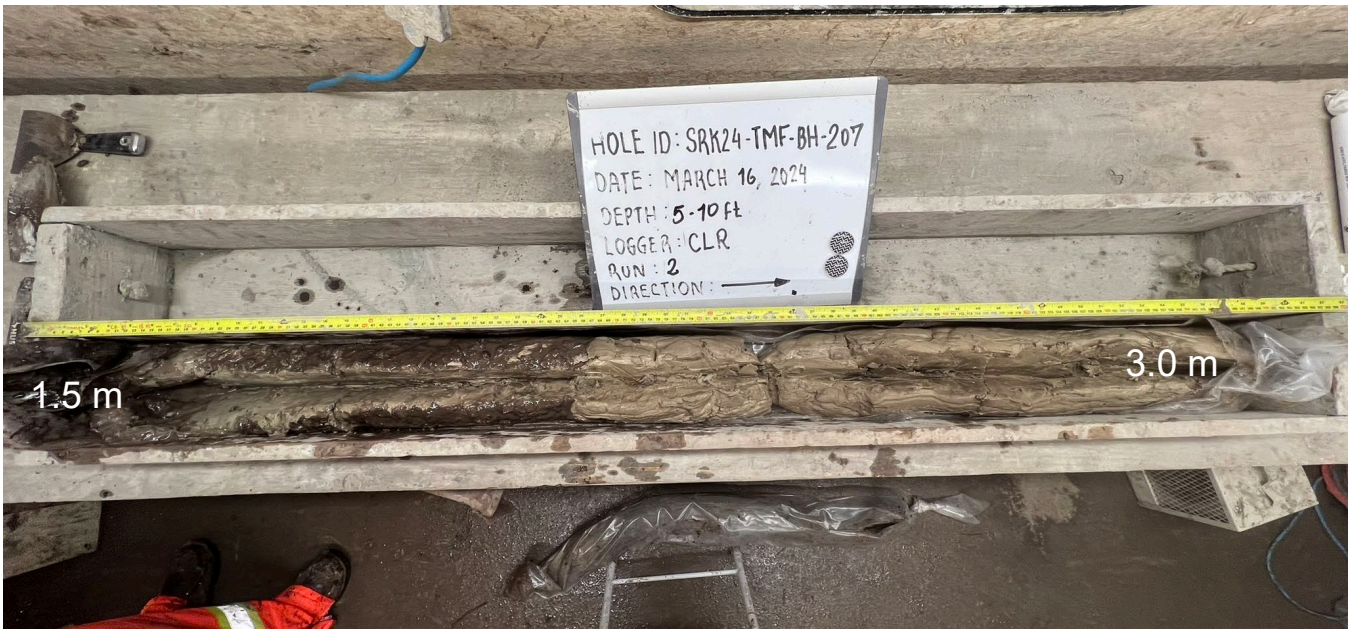
SRK24-TMF-BH-207

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 0.0 – 1.5



Depth (m): 1.5 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-TMF-BH-207** **Depth (m): 0.0 – 3.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 10**

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility

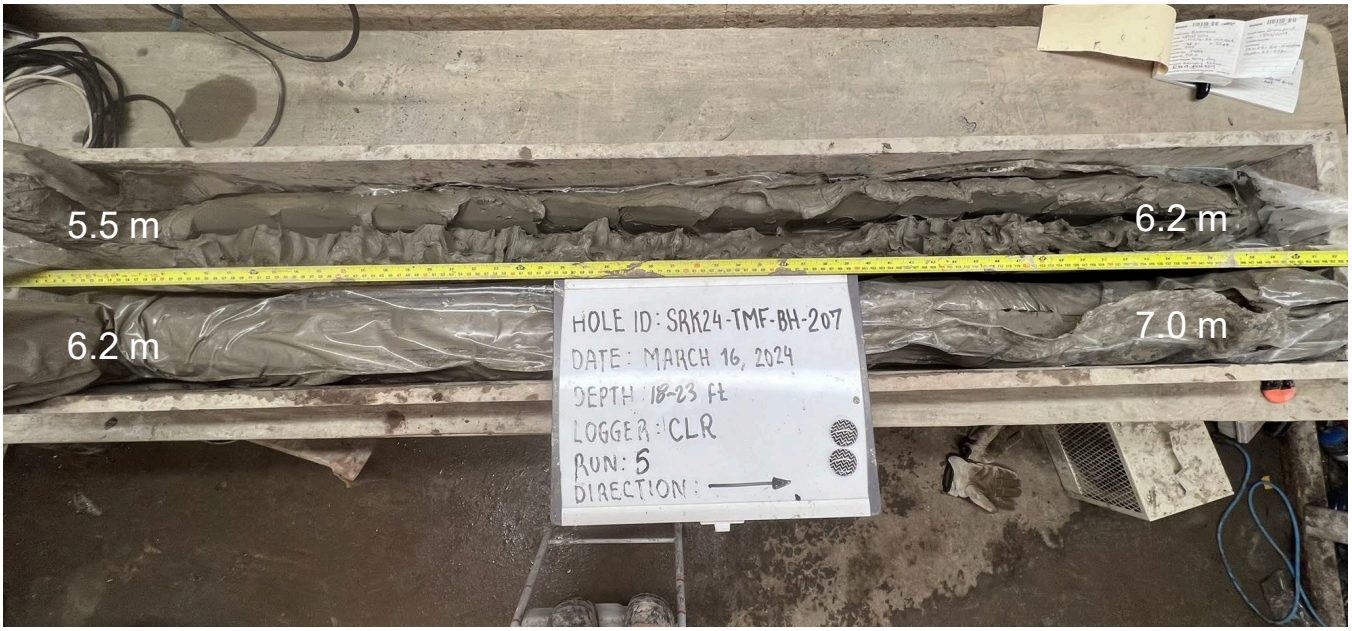


Depth (m): 3.0 – 4.0

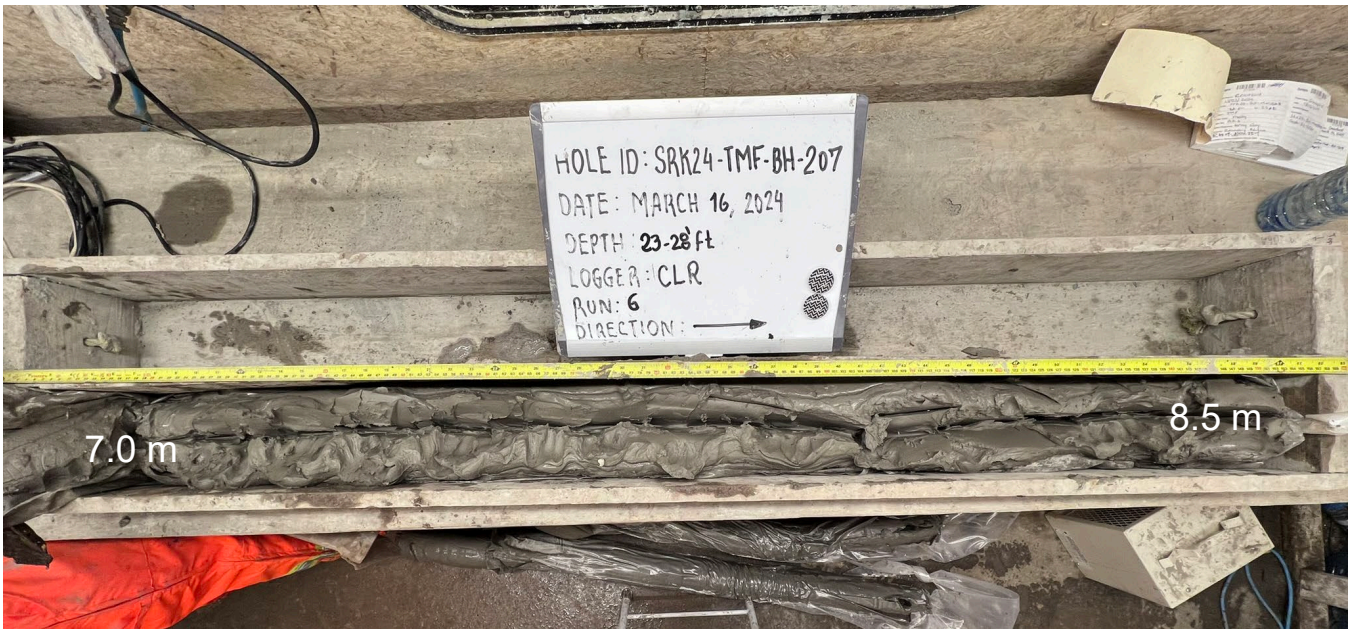


Depth (m): 4.0 – 5.5

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 5.5 – 7.0



Depth (m): 7.0 – 8.5

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 8.5 – 10.1

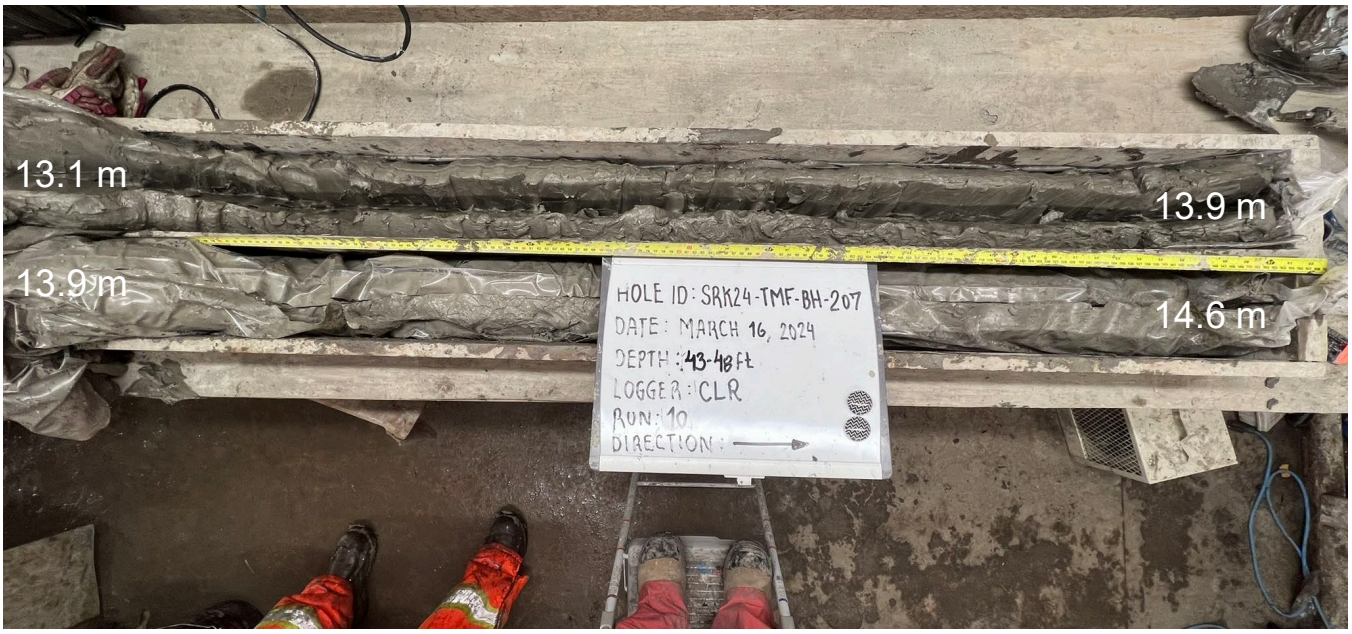


Depth (m): 10.1 – 11.6

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 11.6 – 13.1

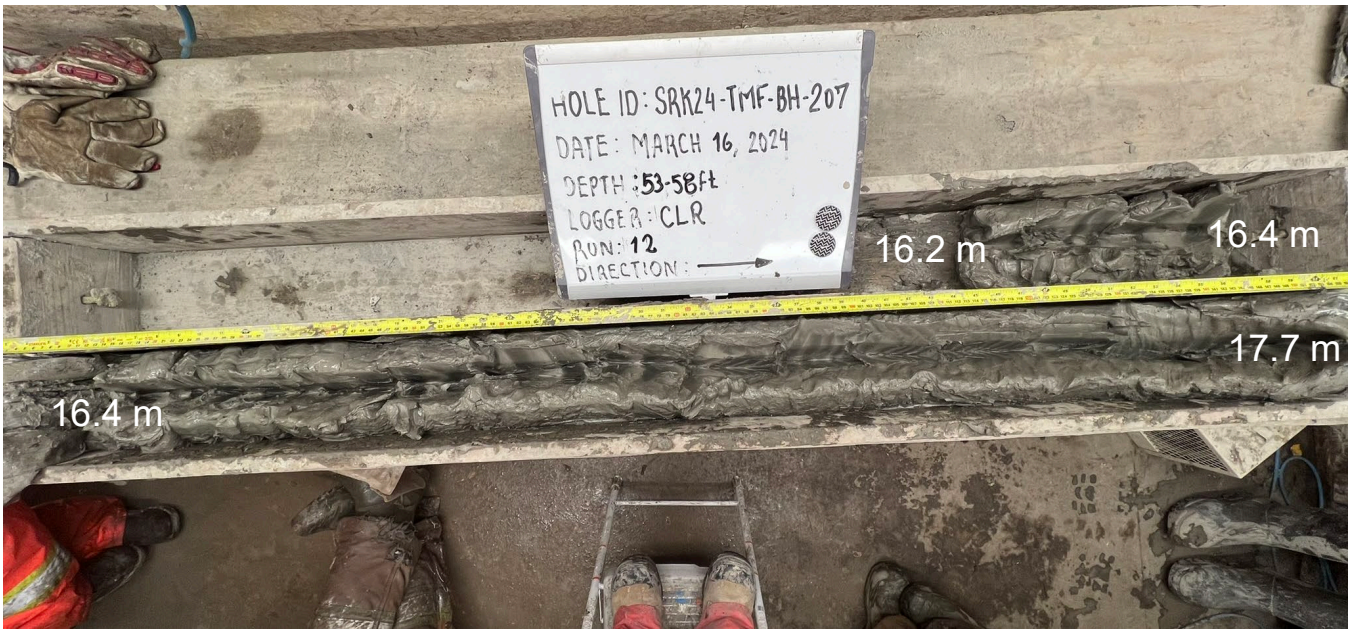


Depth (m): 13.1 – 14.6

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



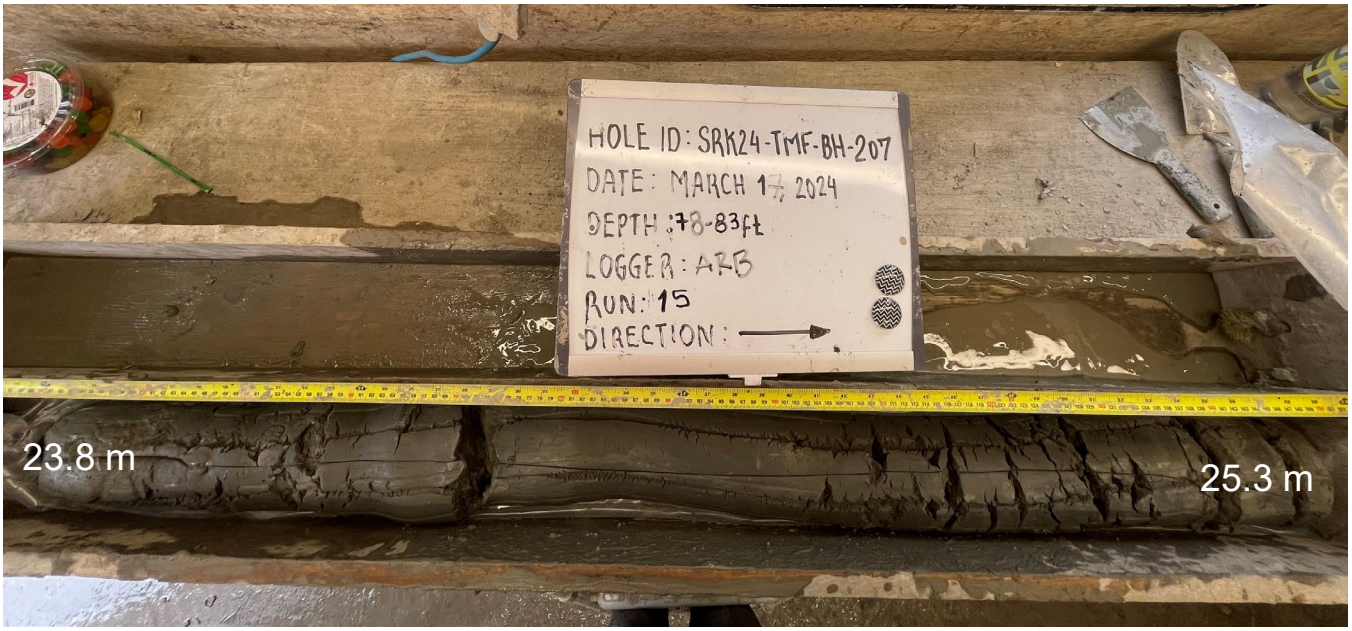
Depth (m): 17.7 – 20.7



Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-TMF-BH-207** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **7 of 10**

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 23.8 – 25.3

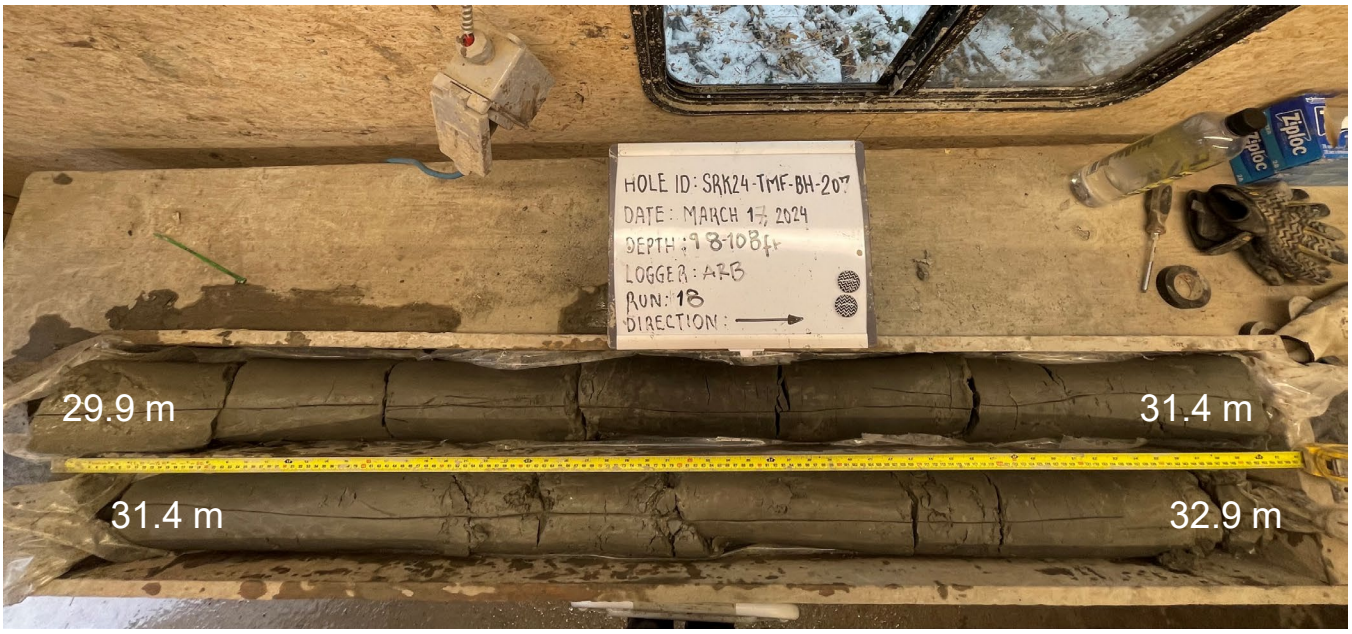


Depth (m): 25.3 – 26.8

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 26.8 – 29.9

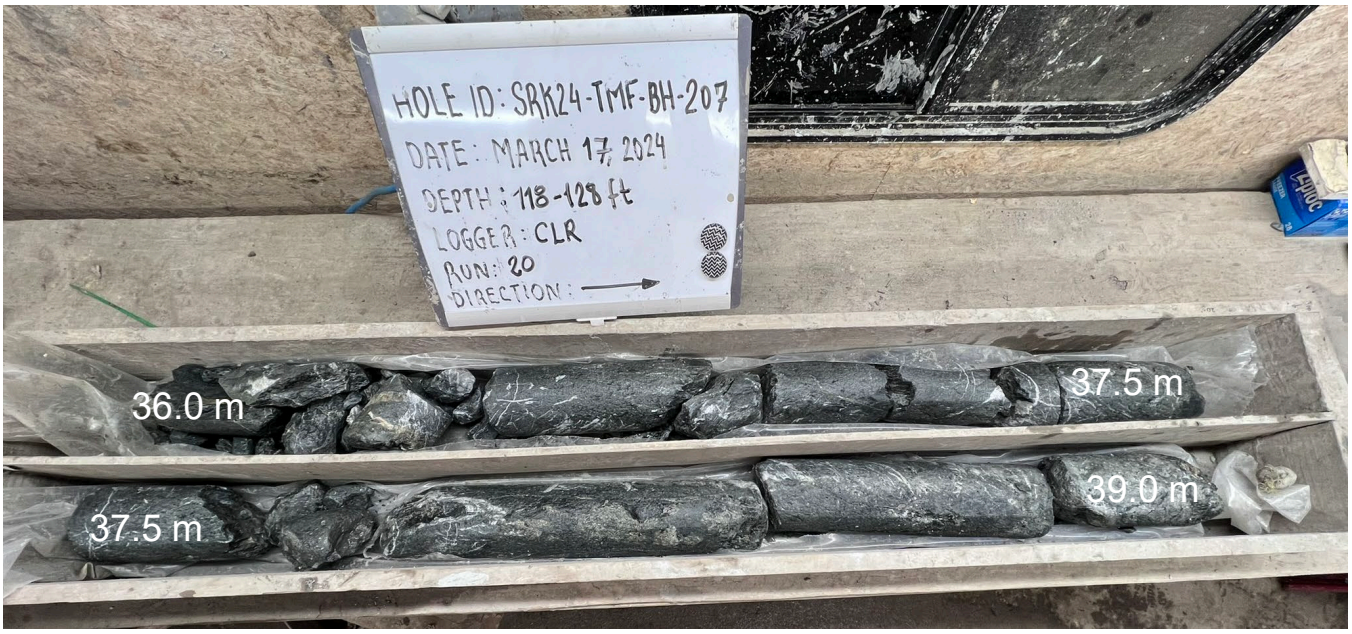


Depth (m): 29.9 – 32.9

Borehole ID: SRK24-TMF-BH-207
Location: Tailings Management Facility



Depth (m): 32.9 – 36.0



Depth (m): 36.0 – 39.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SRK24-TMF-BH-207** **Depth (m): 32.9 – 39.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **10 of 10**

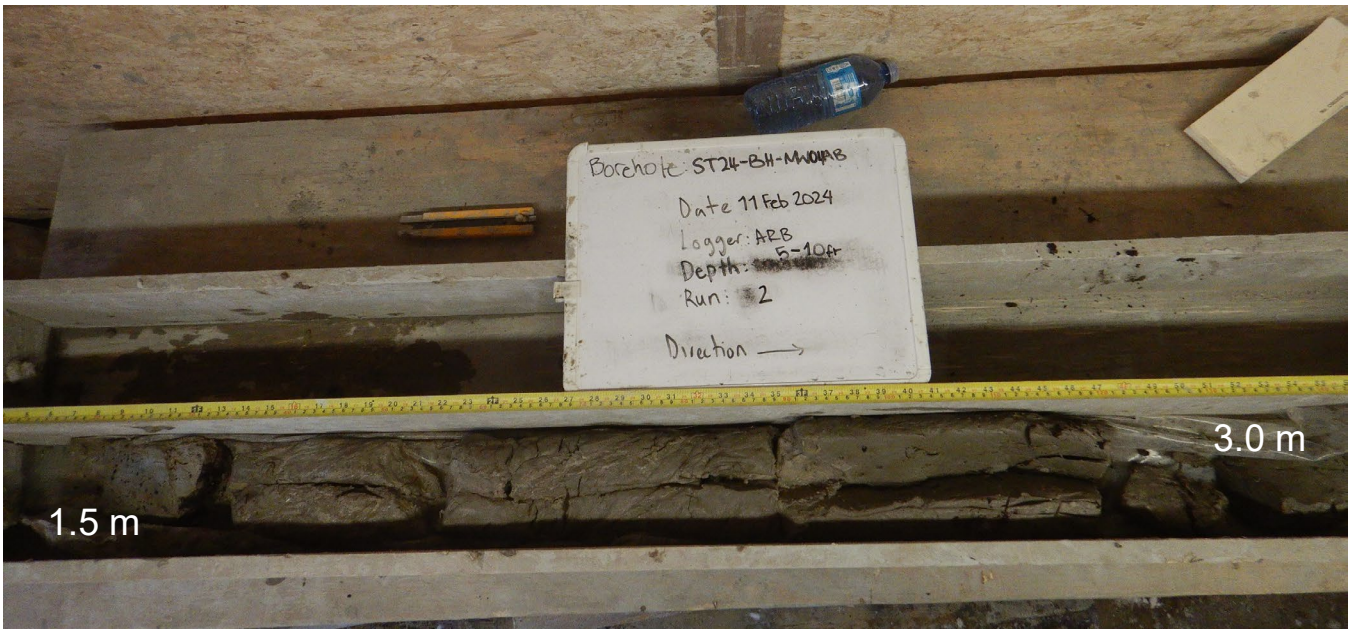
ST24-BH-MW-04AB

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



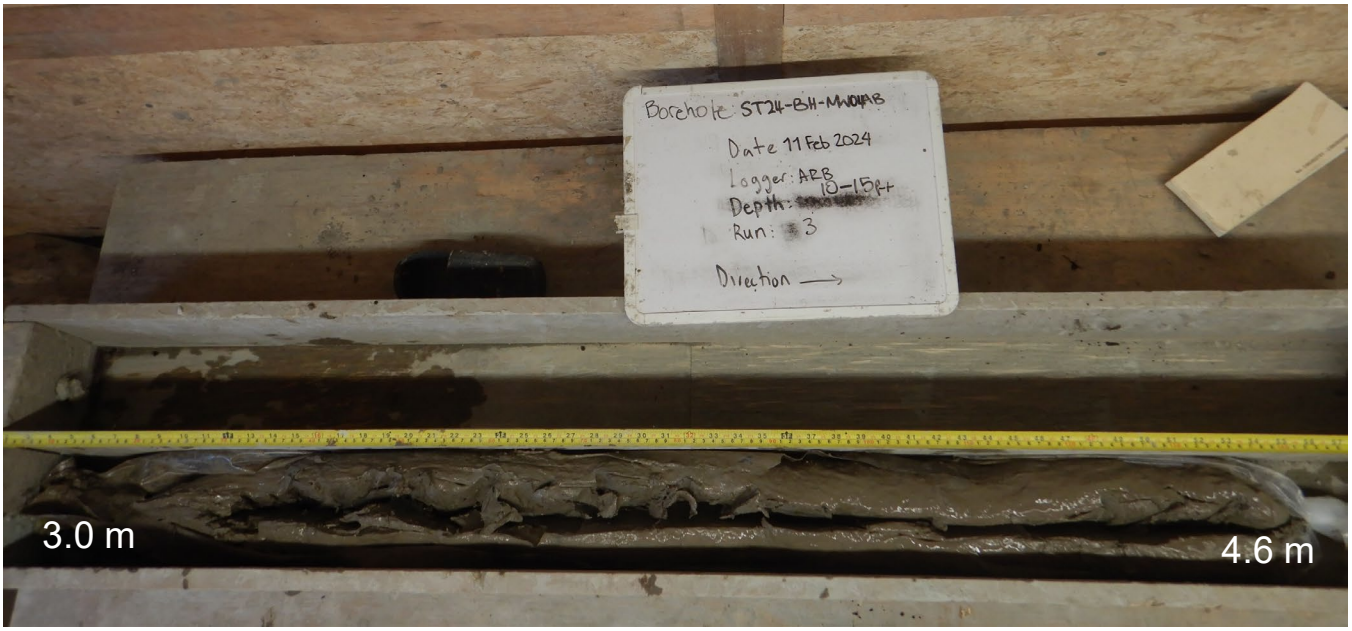
Depth (m): 0.0 – 1.5



Depth (m): 1.5 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SR24-BH-MW-04AB		
		Depth (m): 0.0 – 3.0		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



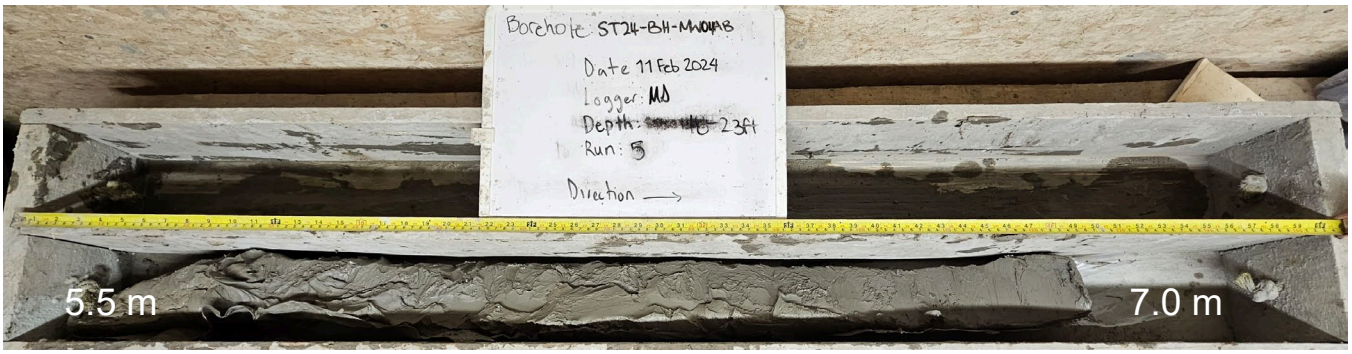
Depth (m): 3.0 – 4.6



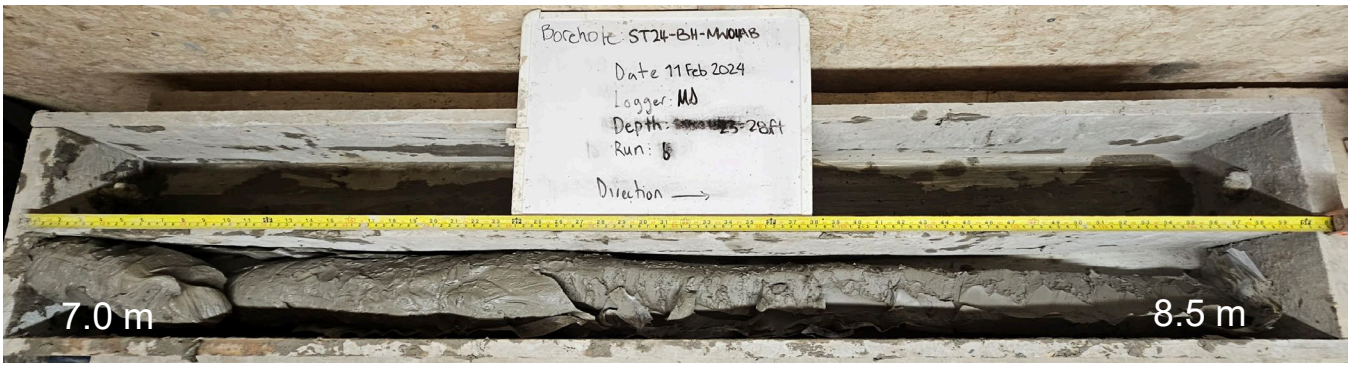
Depth (m): 4.6 – 5.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 3.0 – 5.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



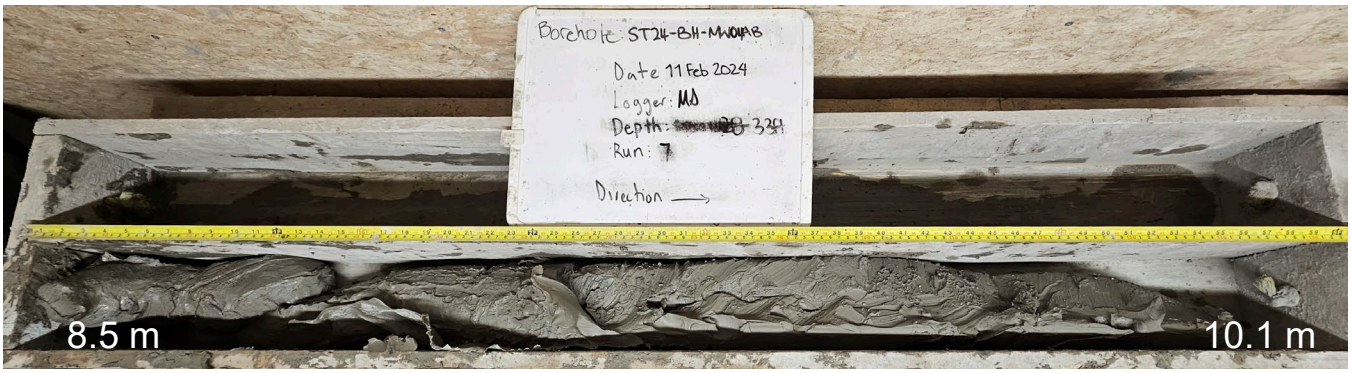
Depth (m): 5.5 – 7.0



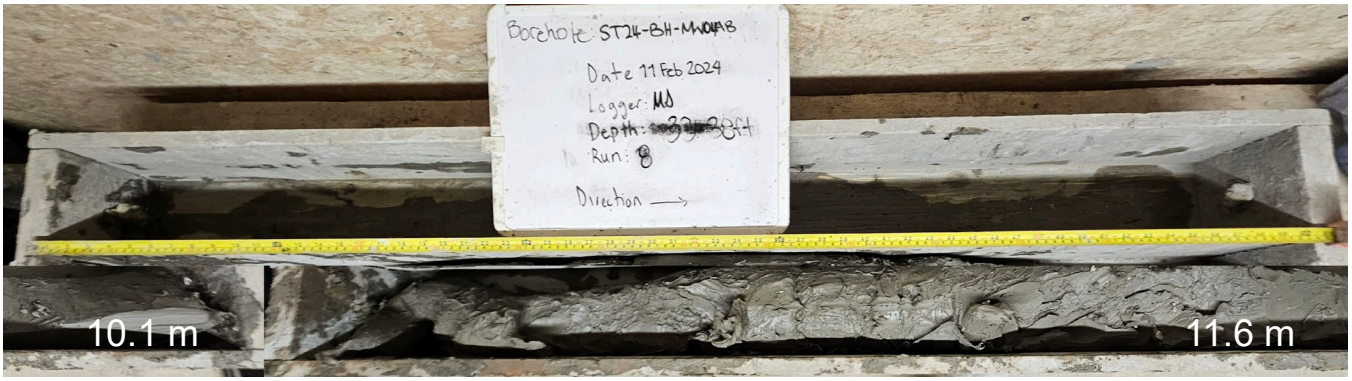
Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



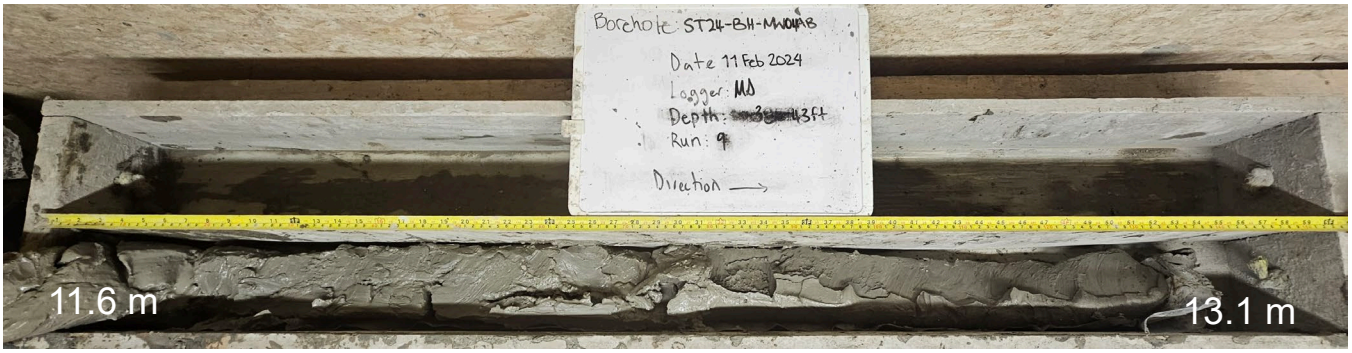
Depth (m): 8.5 – 10.1



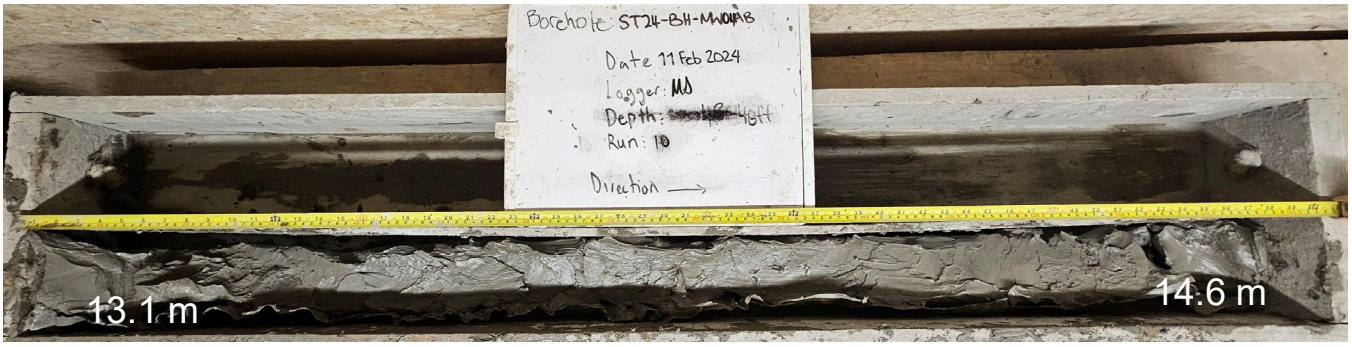
Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



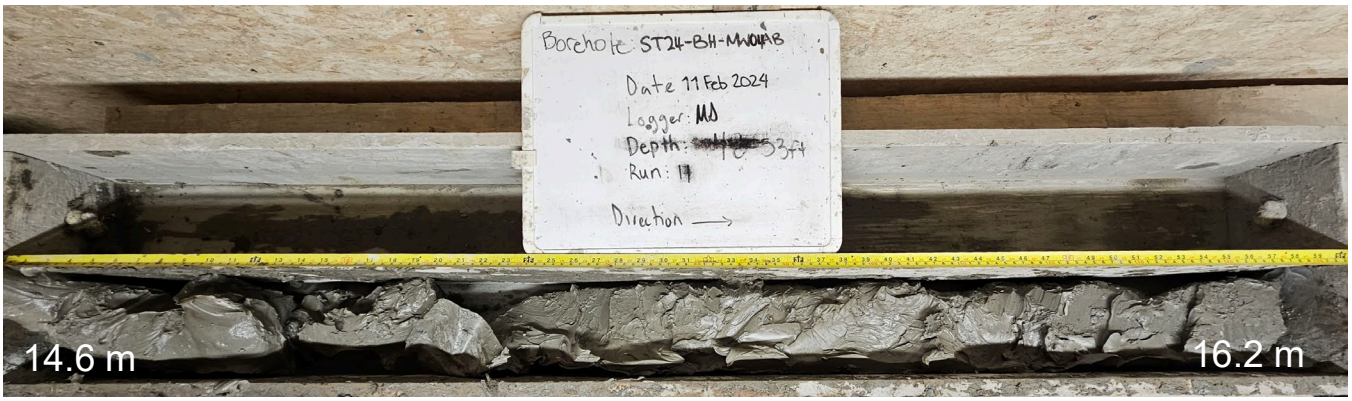
Depth (m): 11.6 – 13.1



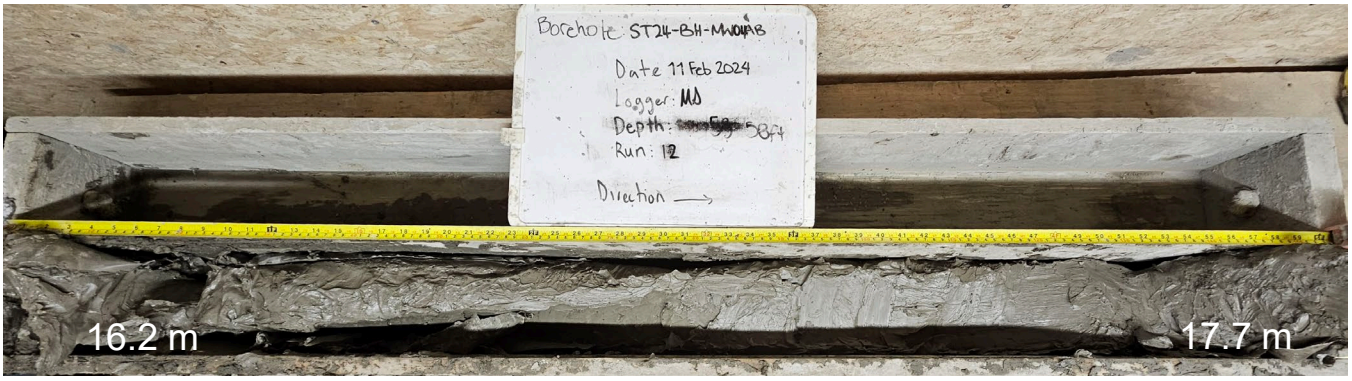
Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 11.6 – 14.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



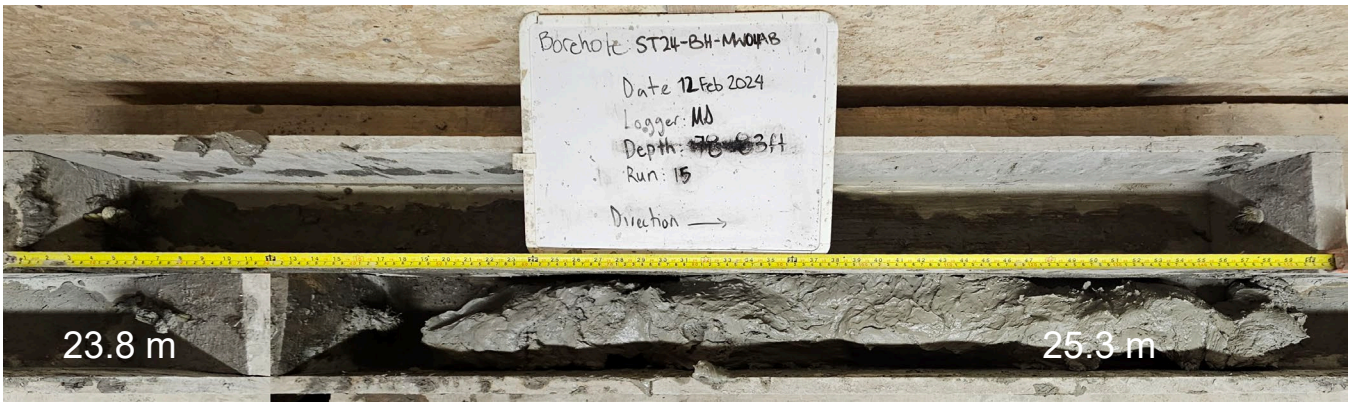
Depth (m): 17.7 – 20.7



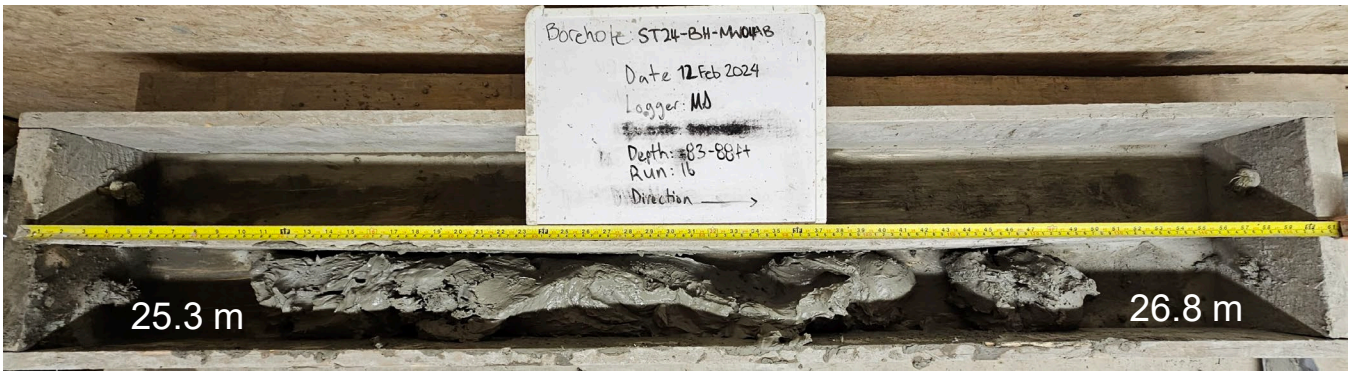
Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



Depth (m): 23.8 – 25.3



Depth (m): 25.3 – 26.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 23.8 – 26.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



Depth (m): 26.8 – 29.9



Depth (m): 29.9 – 32.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 26.8 – 32.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



Depth (m): 32.9 – 34.0



Depth (m): 34.0 – 36.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 32.9 – 36.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 11**

Borehole ID: ST24-BH-MW-04AB
Location: Impoundment Facility



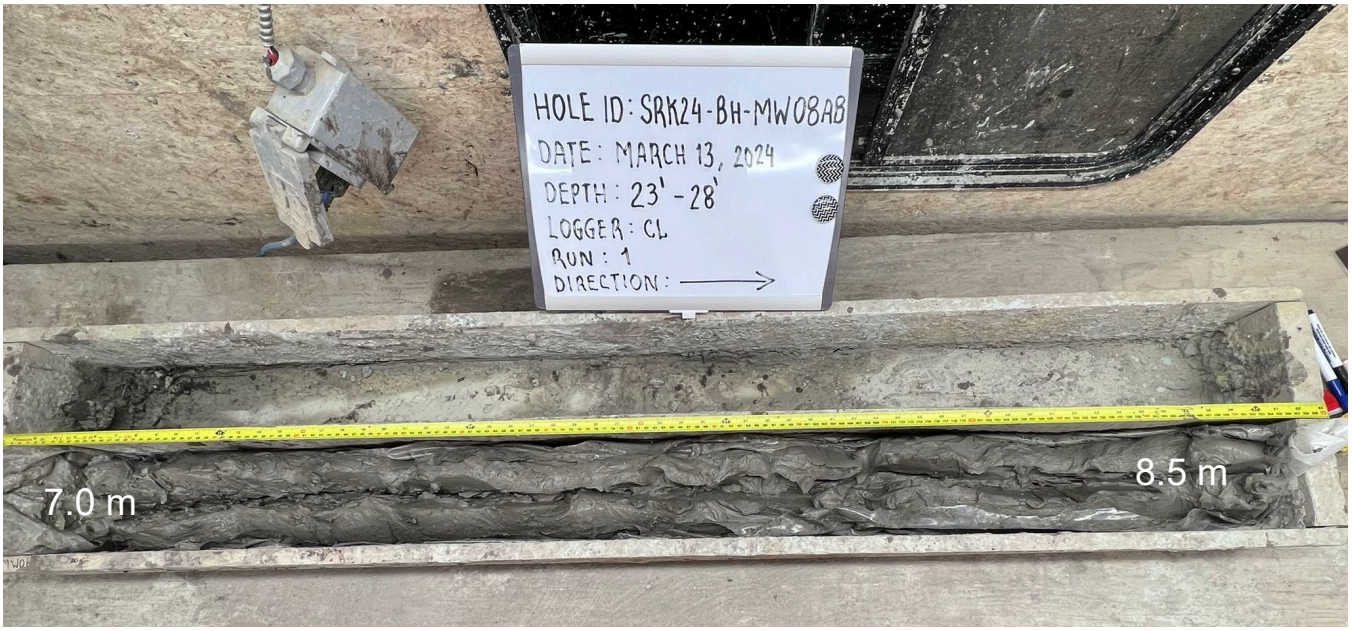
Depth (m): 36.0 – 41.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-04AB** **Depth (m): 36.0 – 41.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 11**

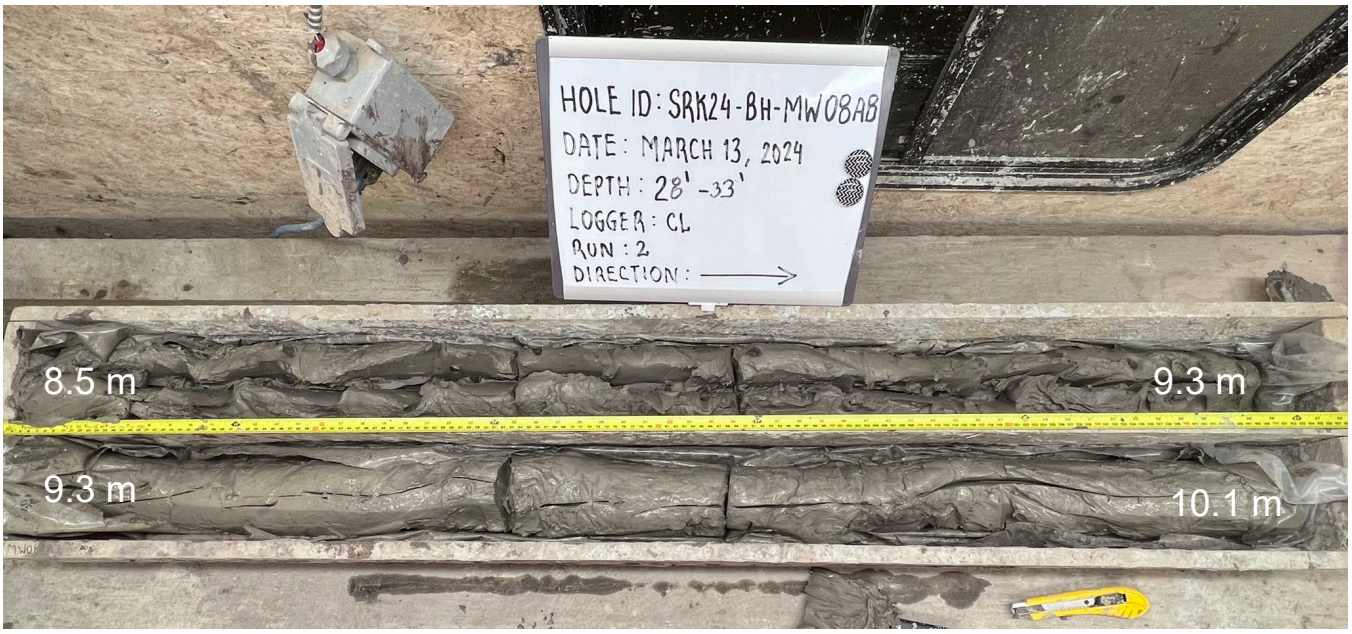
SRK24-BH-MW-08AB

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility



Depth (m): 7.0 – 8.5



Depth (m): 8.5 – 10.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-08AB** **Depth (m): 7.0 – 10.1**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 9**

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility

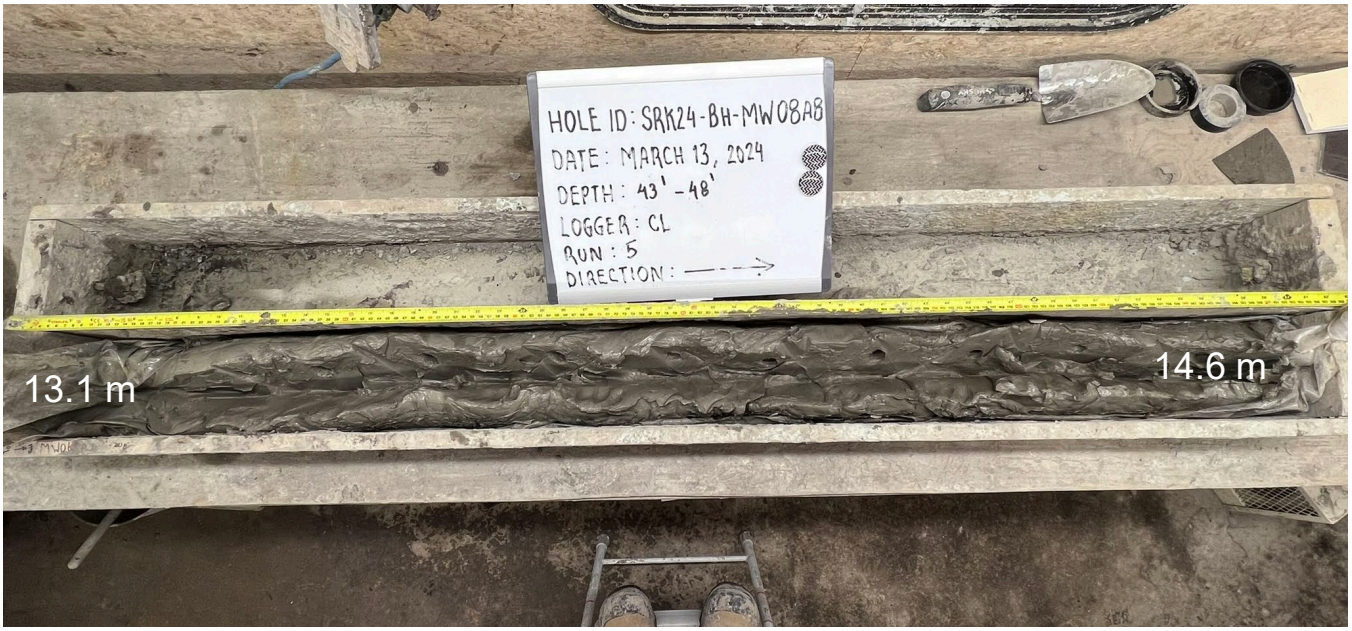


Depth (m): 10.1 – 11.6



Depth (m): 11.6 – 13.1

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility

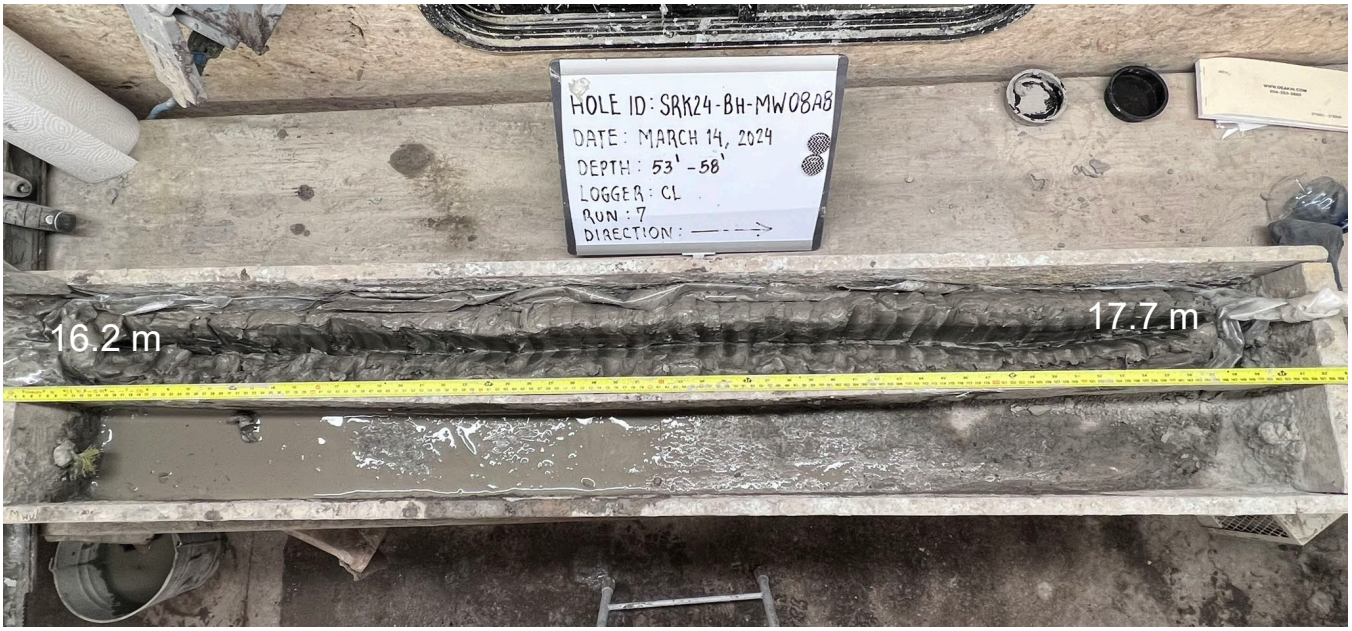


Depth (m): 13.1 – 14.6



Depth (m): 14.6 – 16.2

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility



Depth (m): 16.2 – 17.7



Depth (m): 17.7 – 20.7

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility



Depth (m): 20.7 – 23.8



Depth (m): 23.8 – 26.8

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility



Depth (m): 26.8 – 29.9



Depth (m): 29.9 – 32.9

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility



Depth (m): 32.9 – 36.0



Depth (m): 36.0 – 39.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-08AB** **Depth (m): 32.9 – 39.0**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **7 of 9**

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility

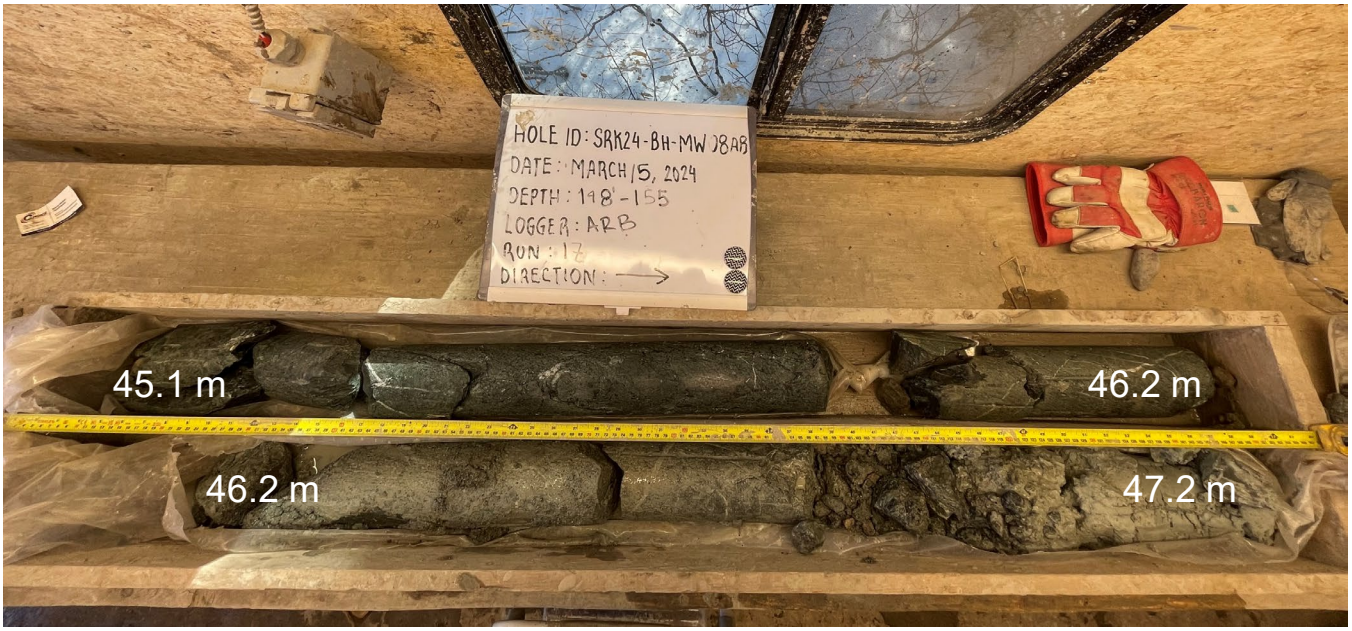


Depth (m): 39.0 – 42.1



Depth (m): 42.1 – 45.1

Borehole ID: ST24-BH-MW-08AB
Location: Tailings Management Facility



Depth (m): 45.1 – 47.2

ST24-BH-MW-10A

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: March 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-10A
Location: Monitoring Wells



Depth (m): 54.3 – 57.3



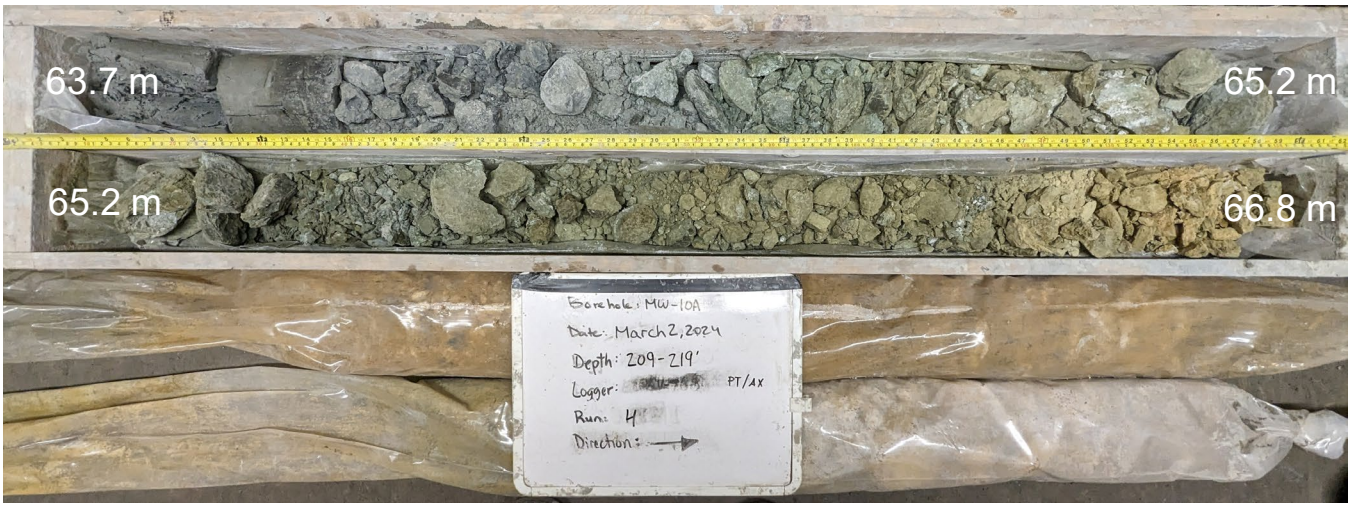
Depth (m): 57.3 – 59.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-10A** **Depth (m): 54.3 – 59.3**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **1 of 5**

Borehole ID: ST24-BH-MW-10A
Location: Monitoring Wells



Depth (m): 59.3 – 63.7



Depth (m): 63.7 – 66.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-10A** **Depth (m): 59.3 – 66.8**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **2 of 5**

Borehole ID: ST24-BH-MW-10A
Location: Monitoring Wells



Depth (m): 66.8 – 68.6



Depth (m): 68.6 – 73.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-10A** **Depth (m): 66.8 – 73.2**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **3 of 5**

Borehole ID: ST24-BH-MW-10A
Location: Monitoring Wells



Depth (m): 73.2 – 75.3



Depth (m): 75.3 – 78.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-10A** **Depth (m): 73.2 – 78.6**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **4 of 5**

Borehole ID: ST24-BH-MW-10A
Location: Monitoring Wells



Depth (m):



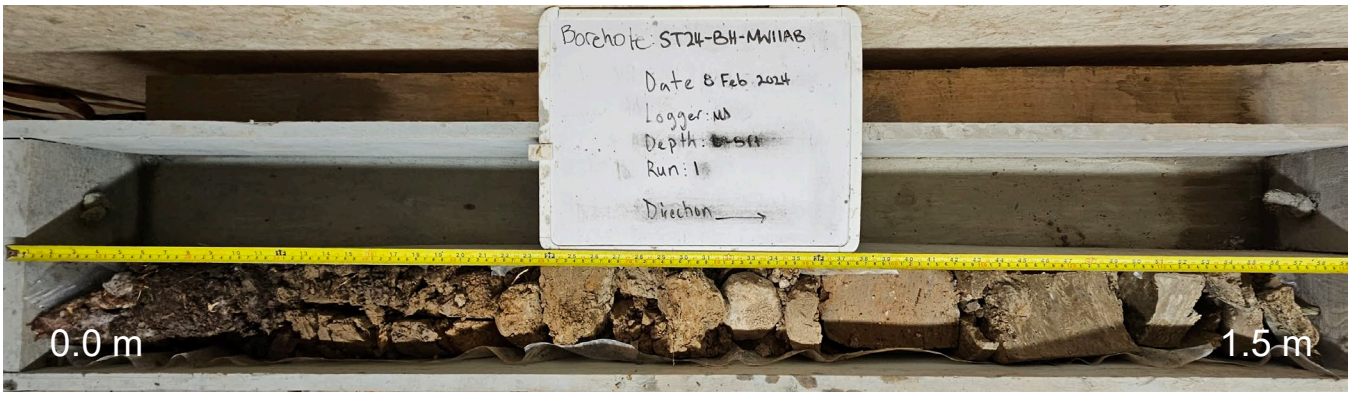
Depth (m): 80.2 – 82.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-10A** **Depth (m): - 82.8**		
Job No: CAPR000801	Crawford	Date: March 2024	Approved: ARB	Figure: **5 of 5**

ST24-BH-MW-11AB

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



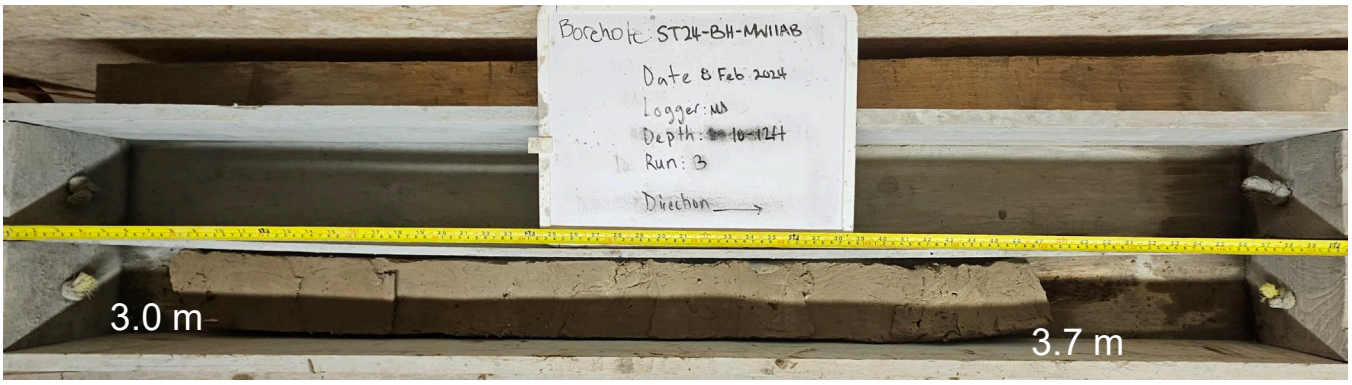
Depth (m): 0.0 – 1.5



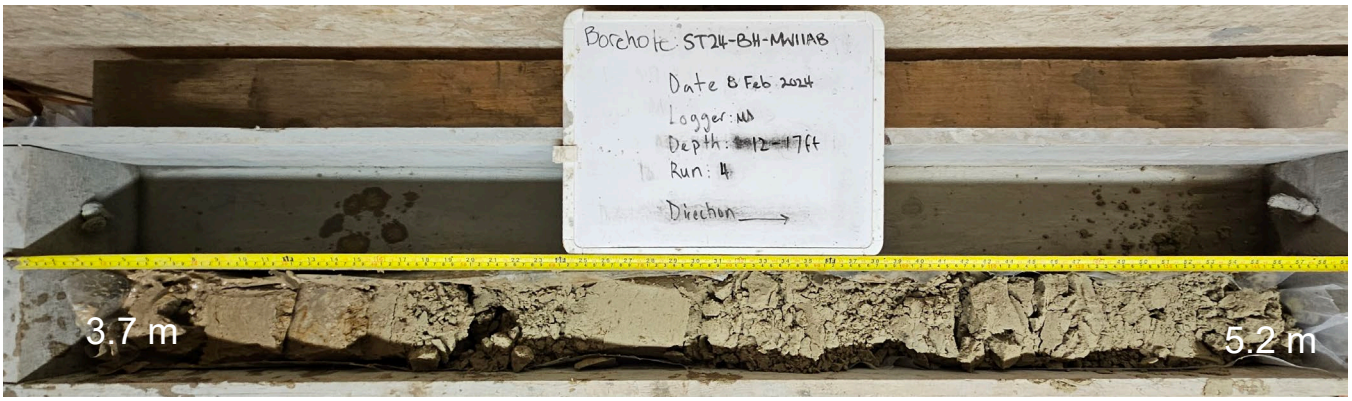
Depth (m): 1.5 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 0.0 – 3.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



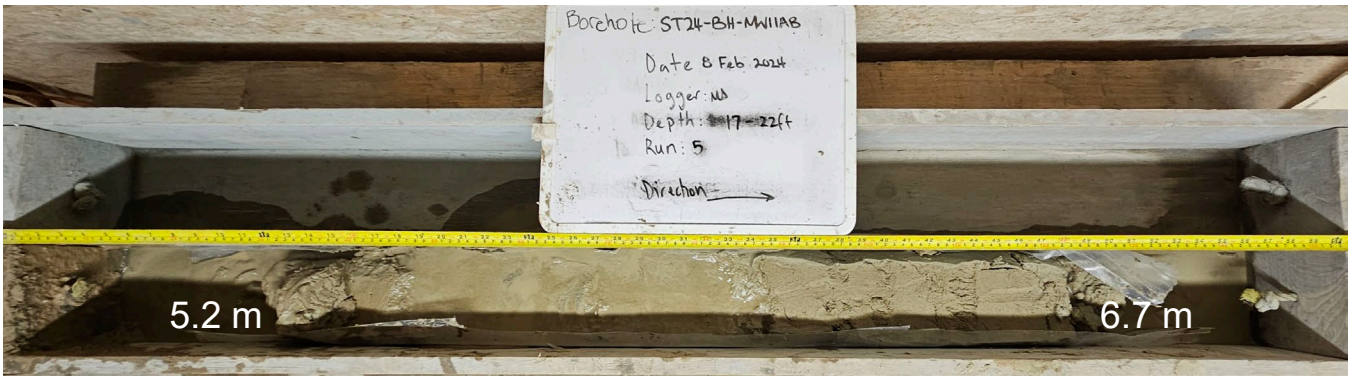
Depth (m): 3.0 – 3.7



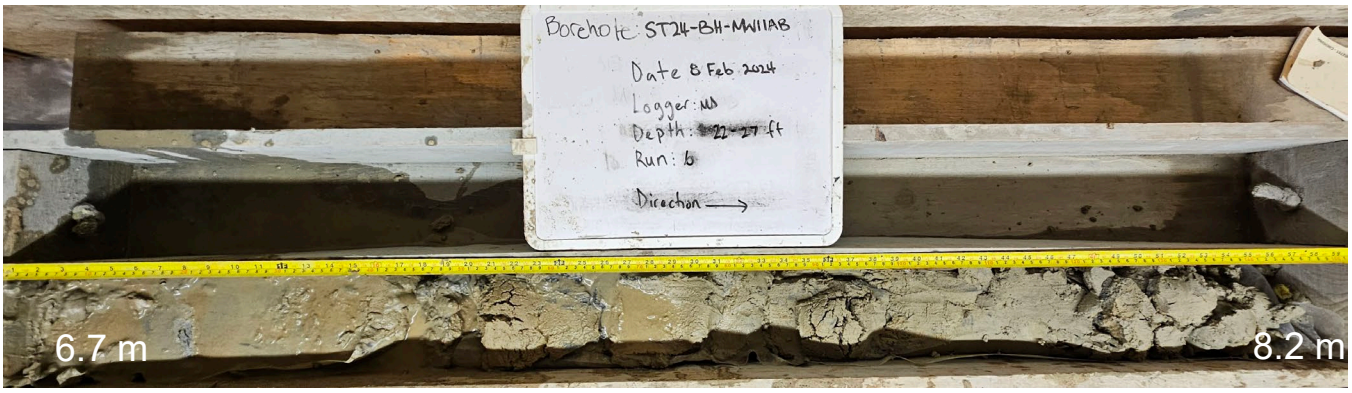
Depth (m): 3.7 – 5.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 3.0 – 5.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



Depth (m): 5.2 – 6.7



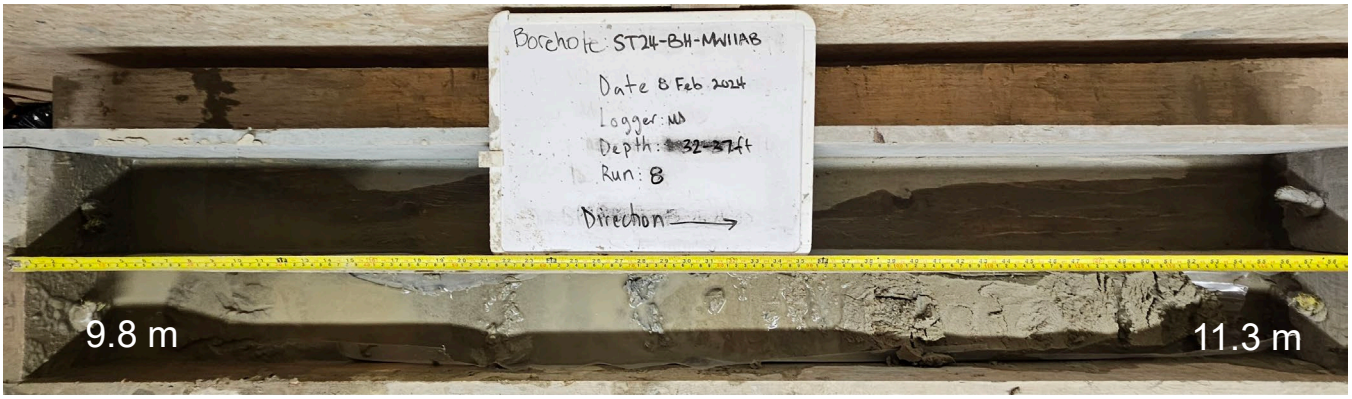
Depth (m): 6.7 – 8.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 5.2 – 8.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



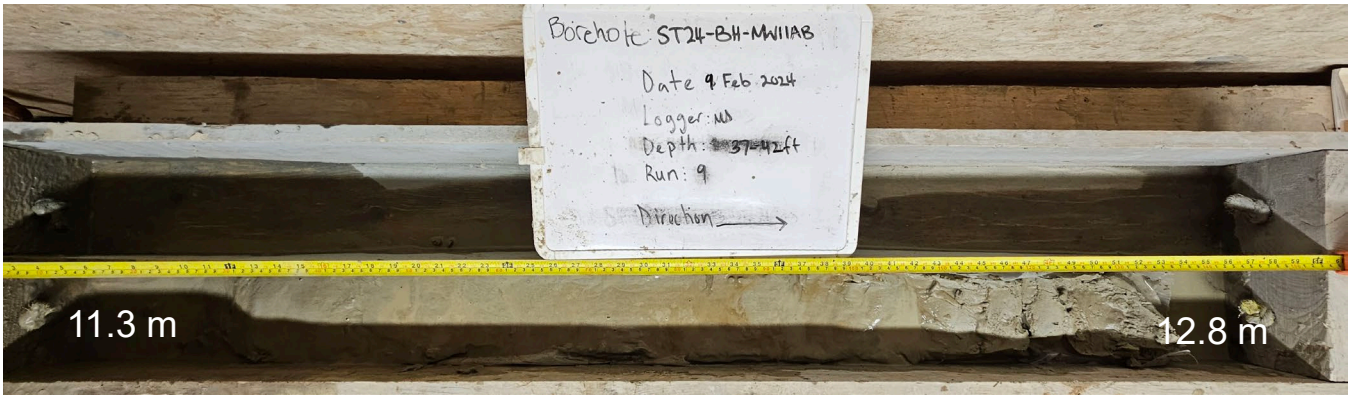
Depth (m): 8.2 – 9.8



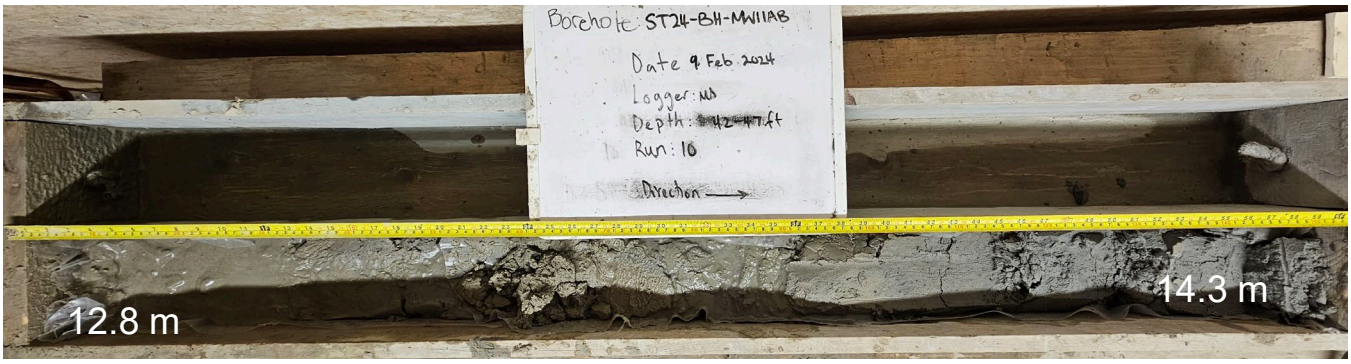
Depth (m): 9.8 – 11.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 8.2 – 11.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



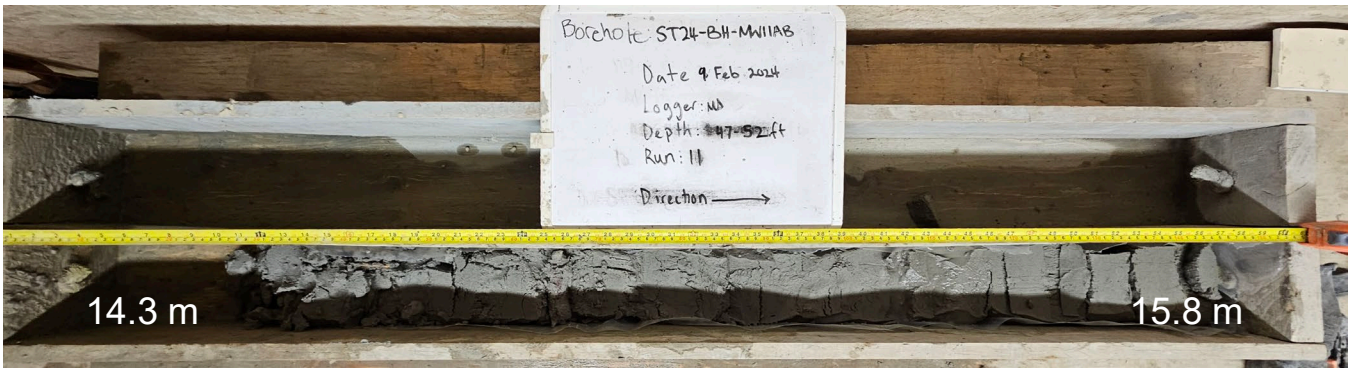
Depth (m): 11.3 – 12.8



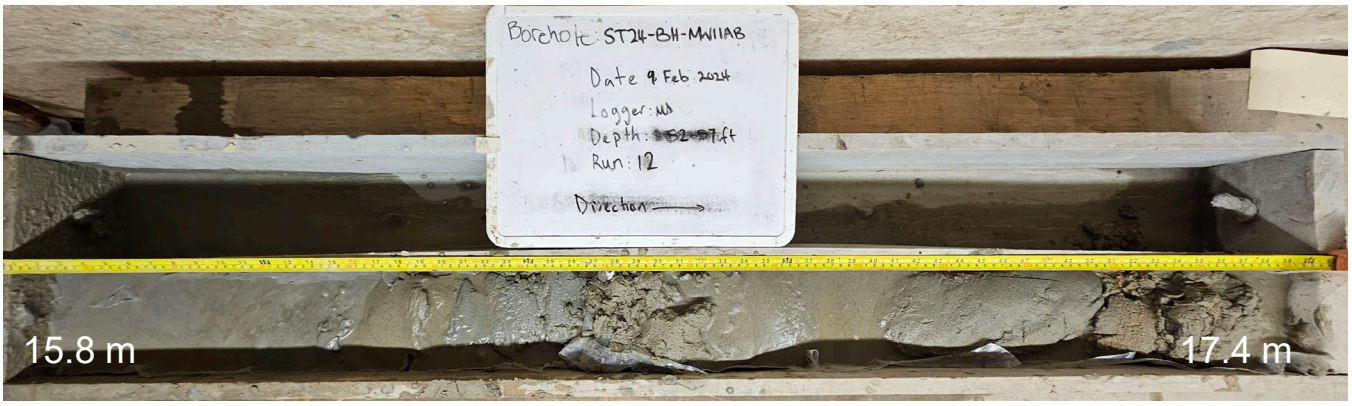
Depth (m): 12.8 – 14.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 11.3 – 14.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



Depth (m): 14.3 – 15.8



Depth (m): 15.8 – 17.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 14.3 – 17.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



Depth (m): 17.4 – 20.4



Depth (m): 20.4 – 21.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 17.4 – 21.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 8**

Borehole ID: ST24-BH-MW-11AB
Location: Monitoring Wells



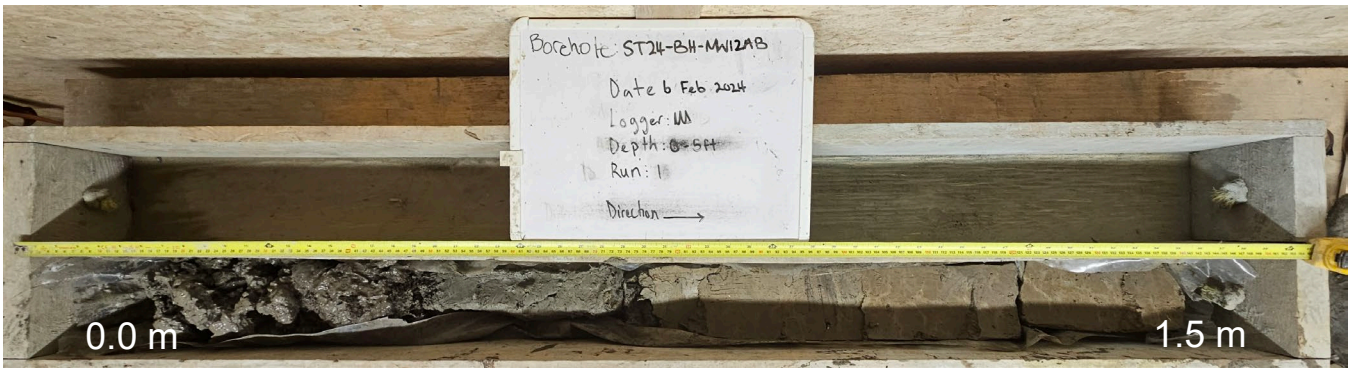
Depth (m): 21.9 – 22.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-11AB** **Depth (m): 21.9 – 22.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 8**

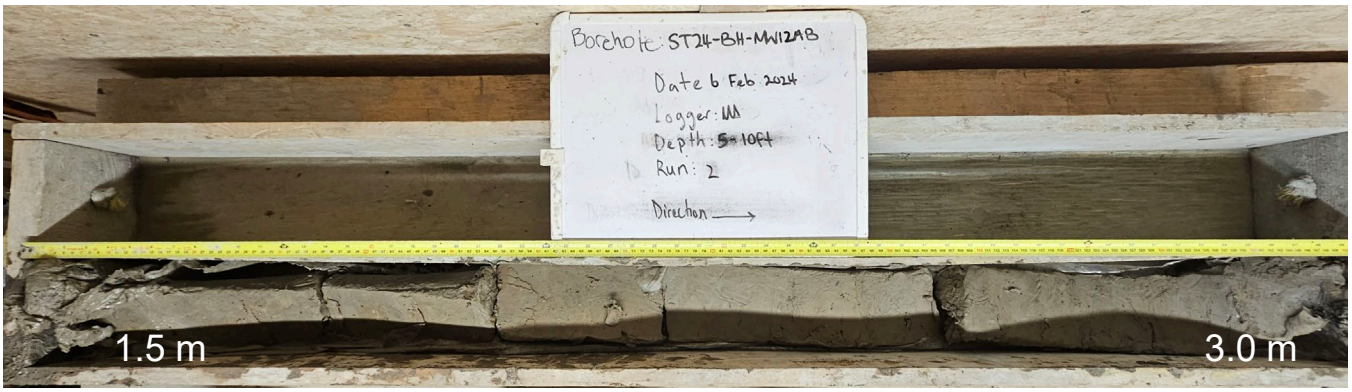
ST24-BH-MW-12AB

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



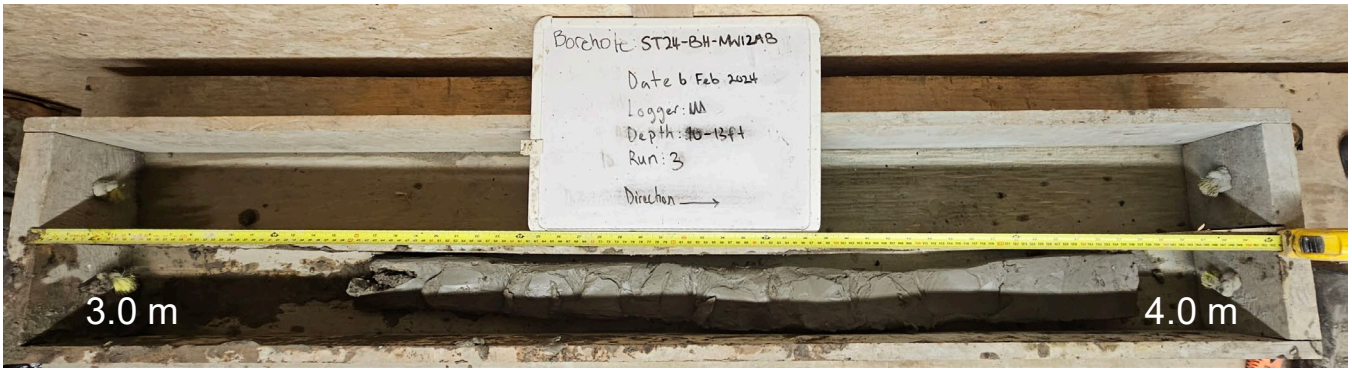
Depth (m): 0.0 – 1.5



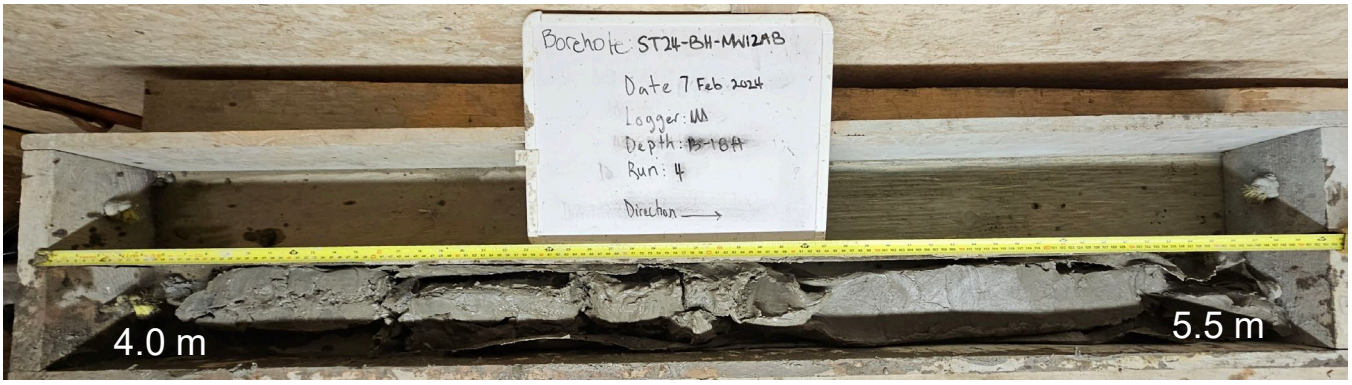
Depth (m): 1.5 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 0.0 – 3.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



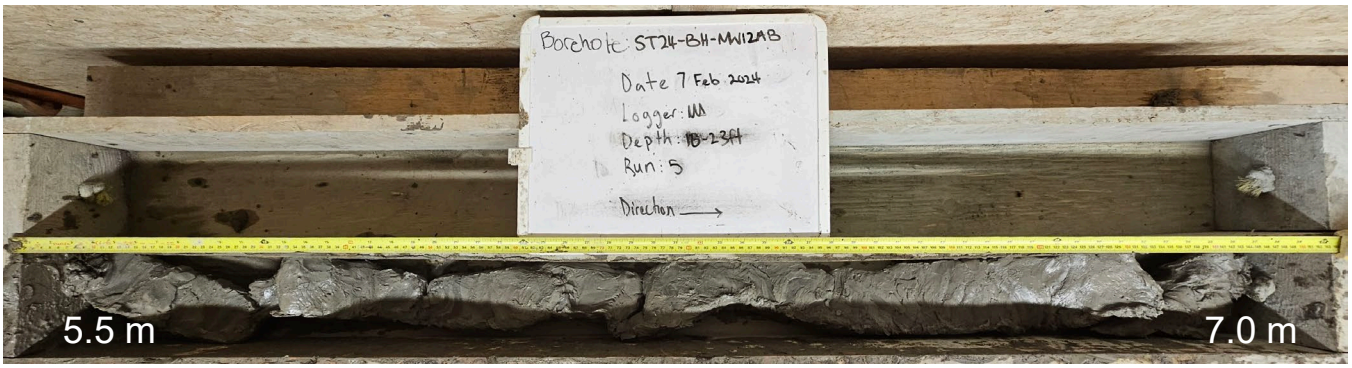
Depth (m): 3.0 – 4.0



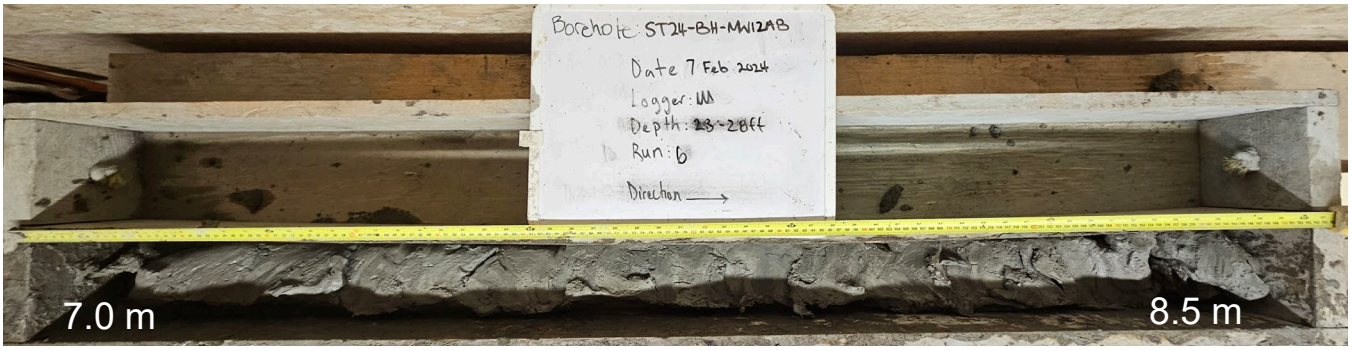
Depth (m): 4.0 – 5.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 3.0 – 5.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **2 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



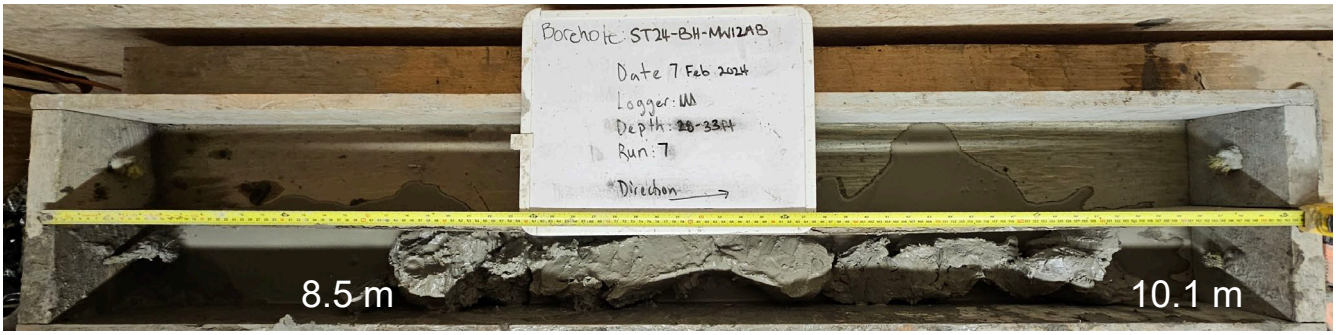
Depth (m): 5.5 – 7.0



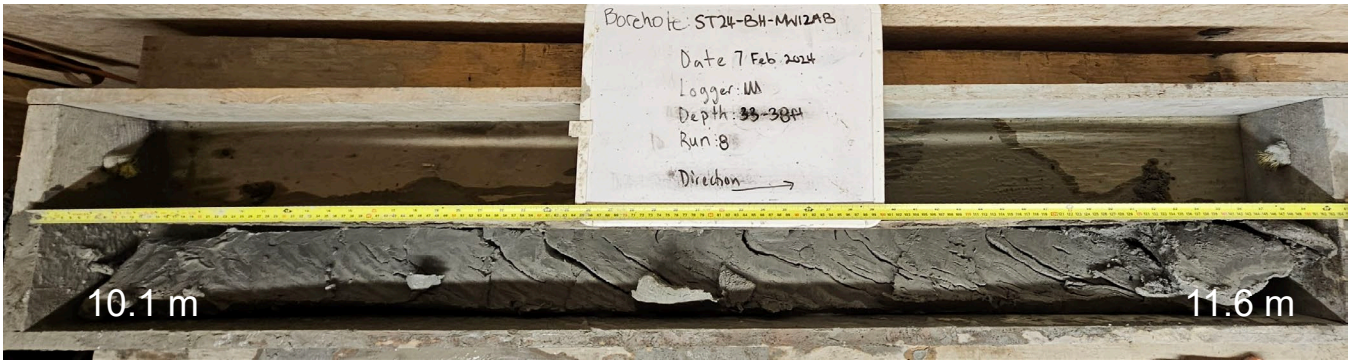
Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



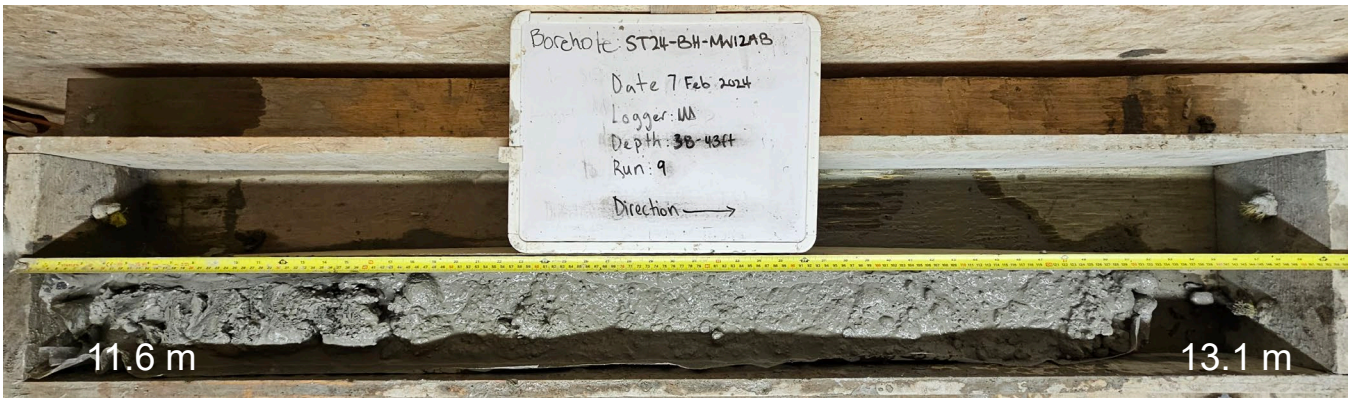
Depth (m): 8.5 – 10.1



Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



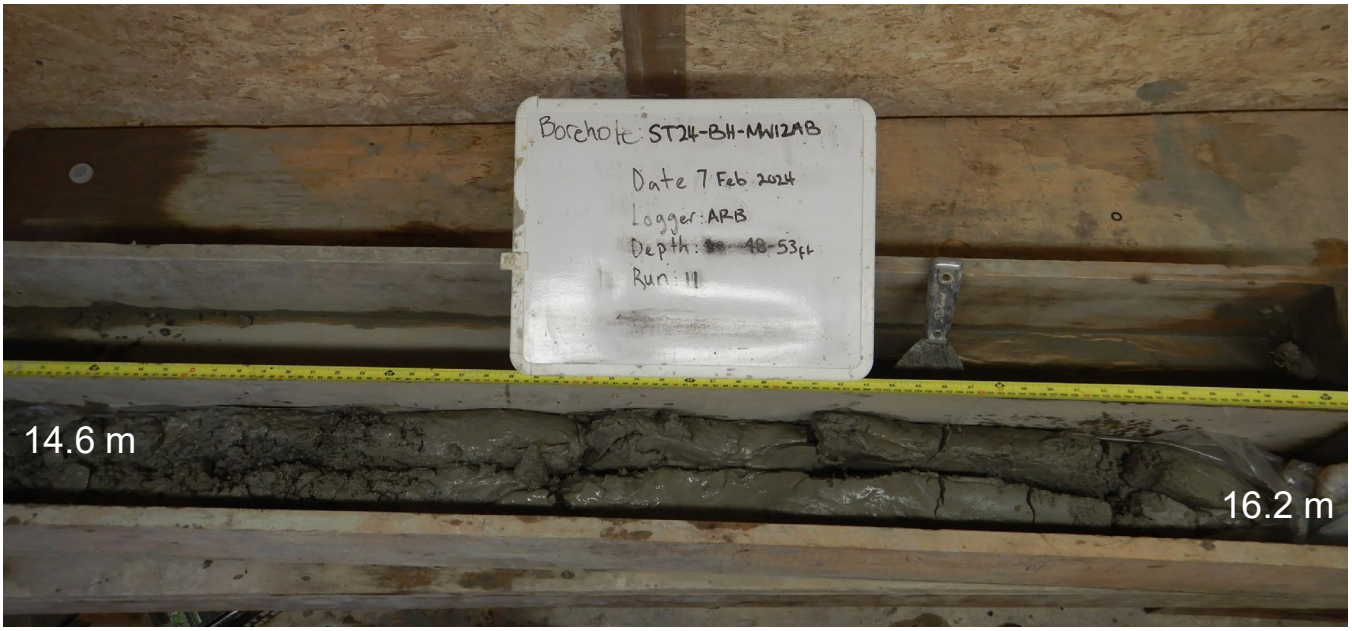
Depth (m): 11.6 – 13.1



Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 11.6 – 14.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



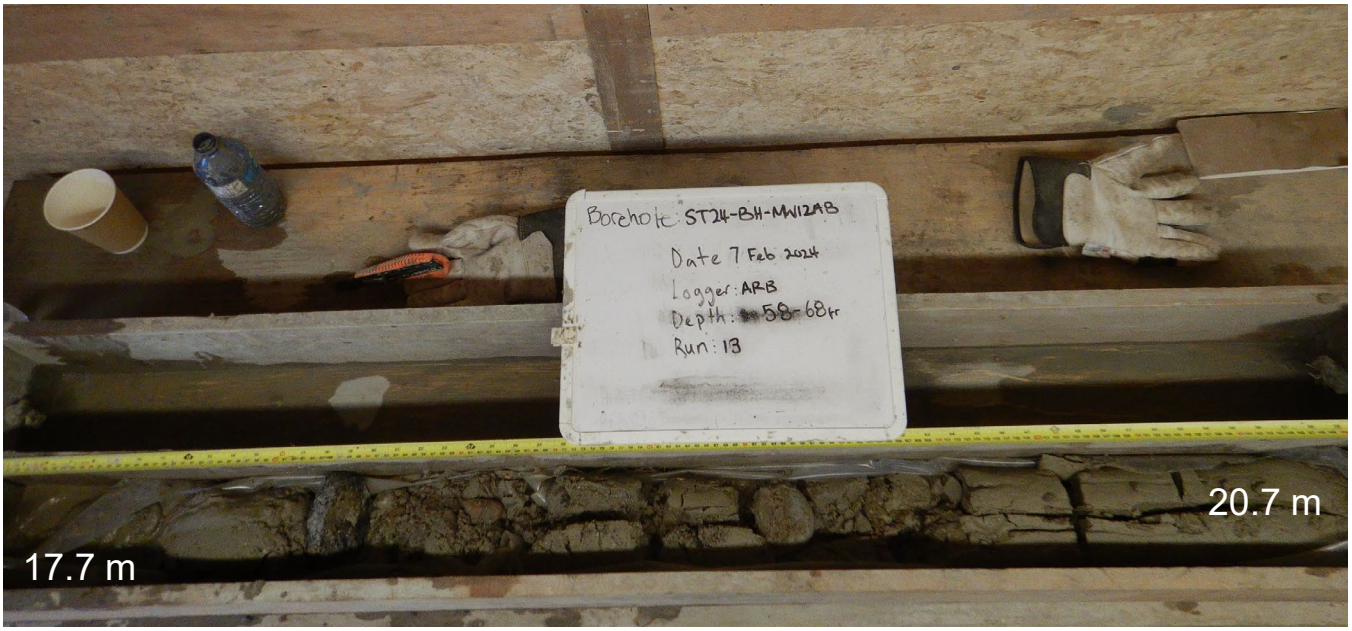
Depth (m): 14.6 – 16.2



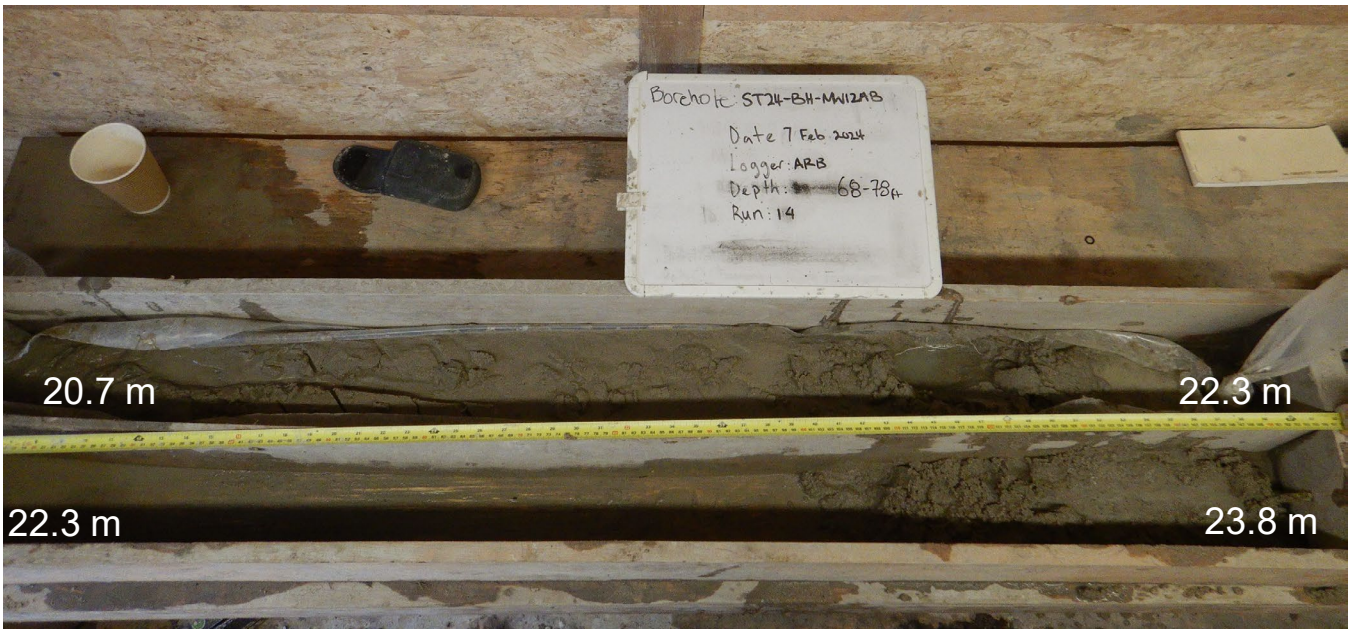
Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



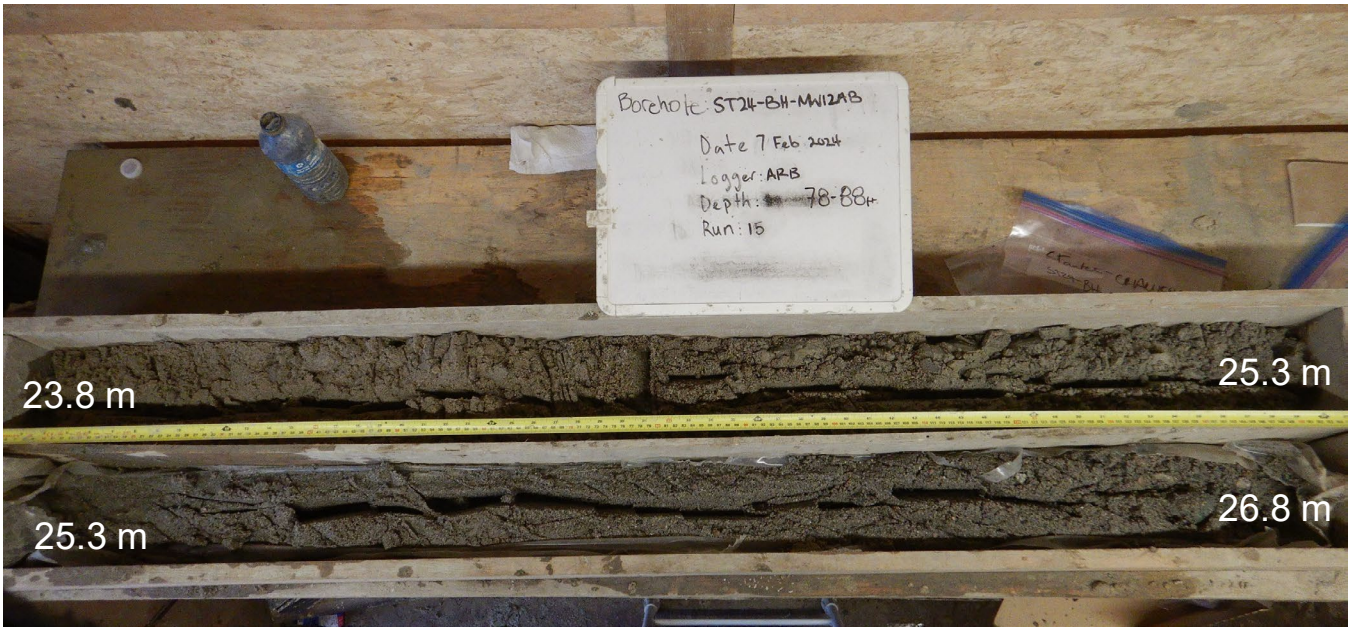
Depth (m): 17.7 – 20.7



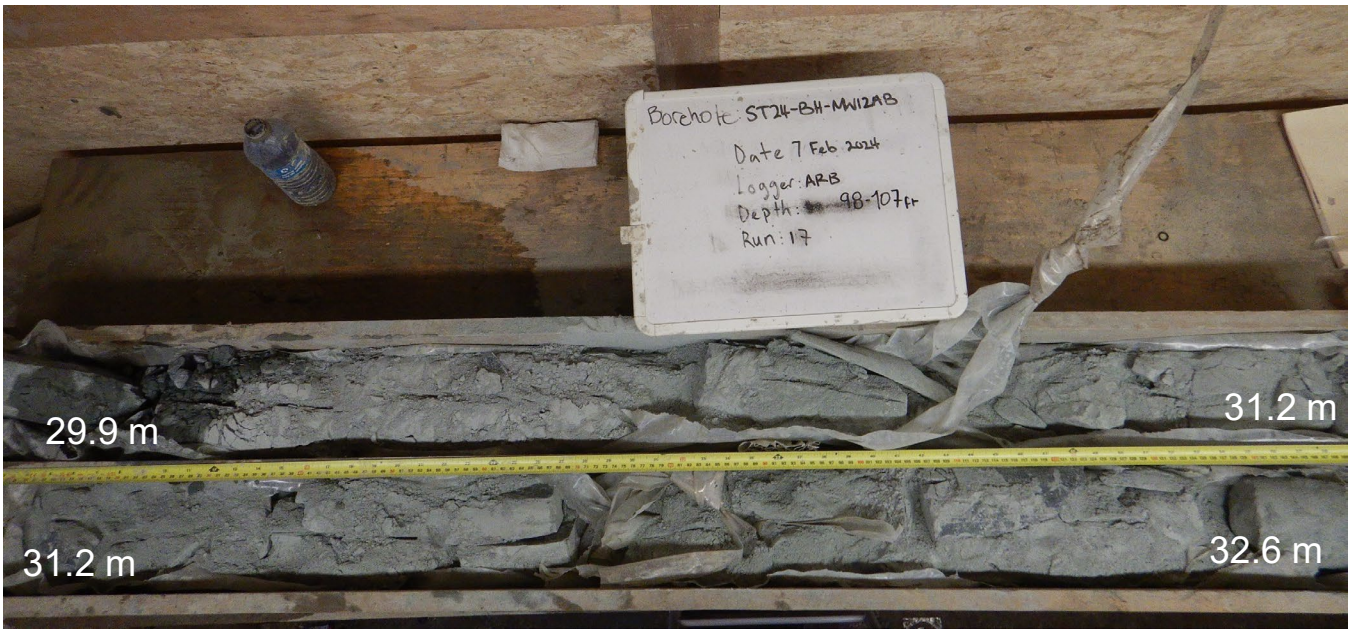
Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-12AB** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 8**

Borehole ID: ST24-BH-MW-12AB
Location: Monitoring Wells



Depth (m): 23.8 – 26.8



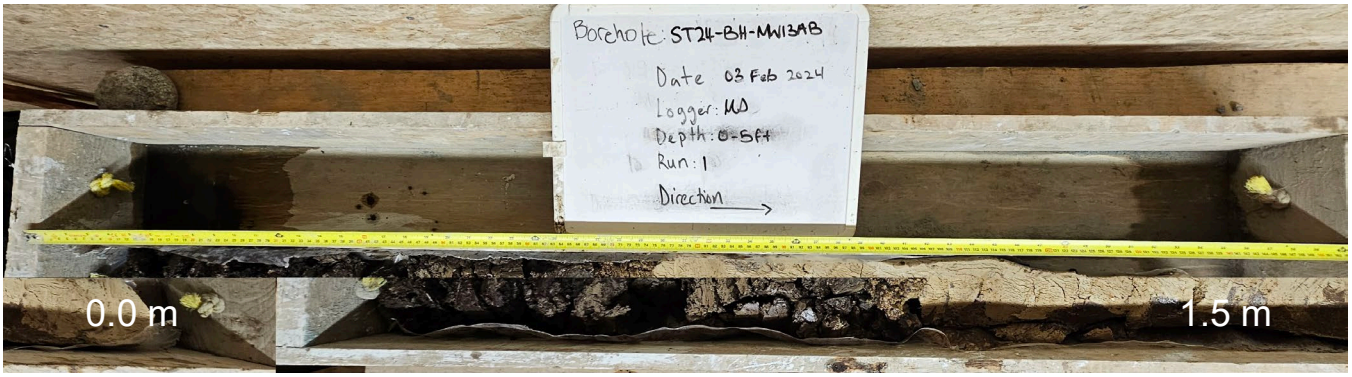
Depth (m): 29.9 – 32.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		SR24-BH-MW-12AB		
		Depth (m): 23.8 – 32.6		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 8**

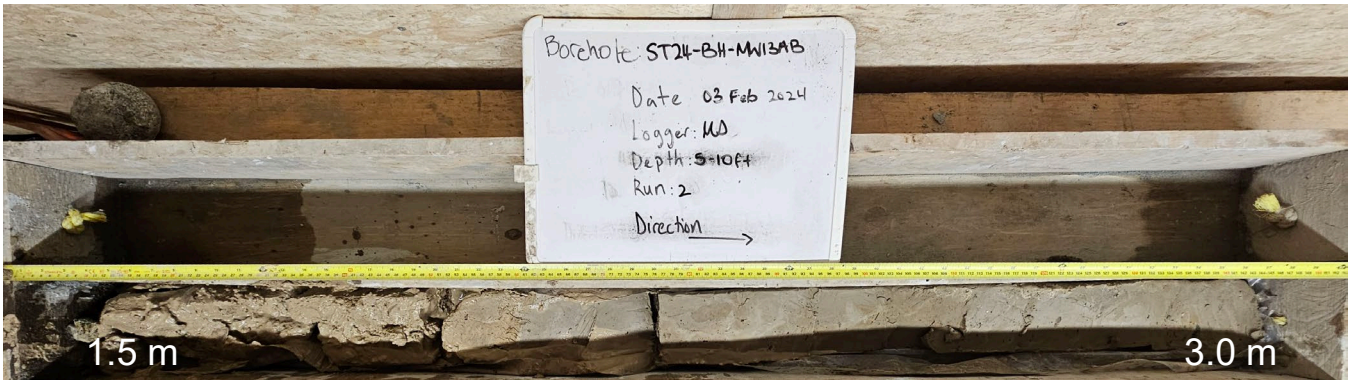
ST24-BH-MW-13AB

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells

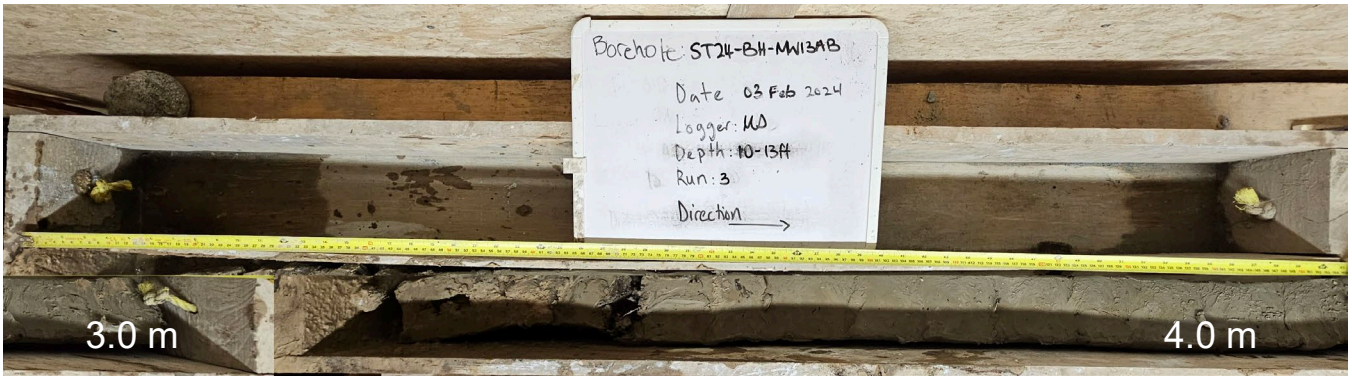


Depth (m): 0.0 – 1.5



Depth (m): 1.5 – 3.0

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells

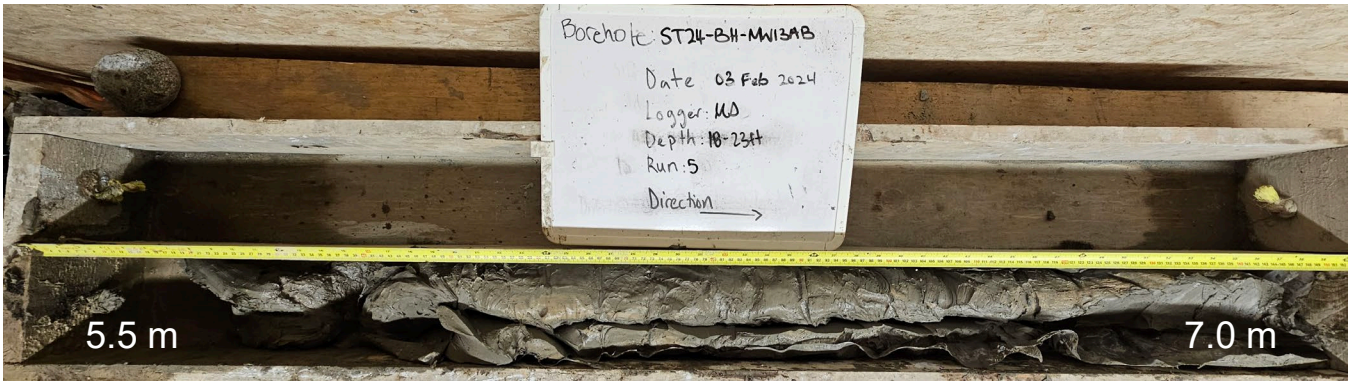


Depth (m): 3.0 – 4.0

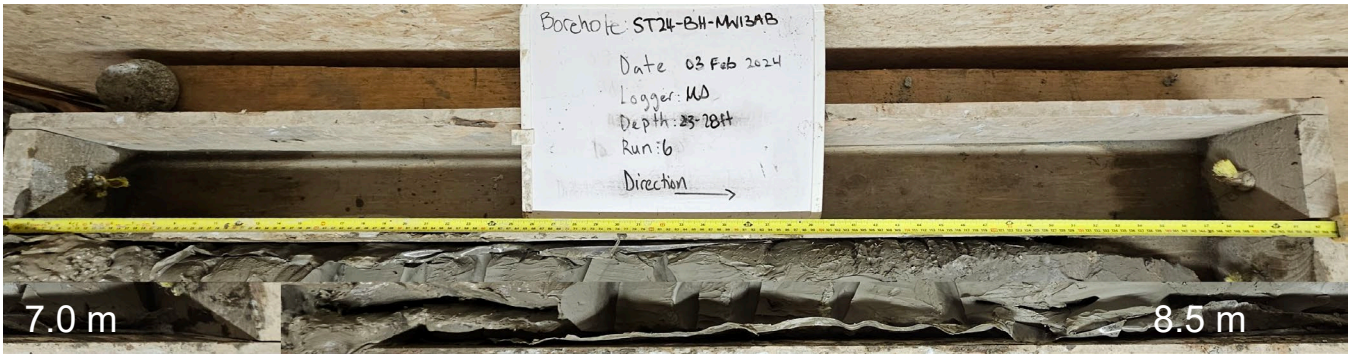


Depth (m): 4.0 – 5.5

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



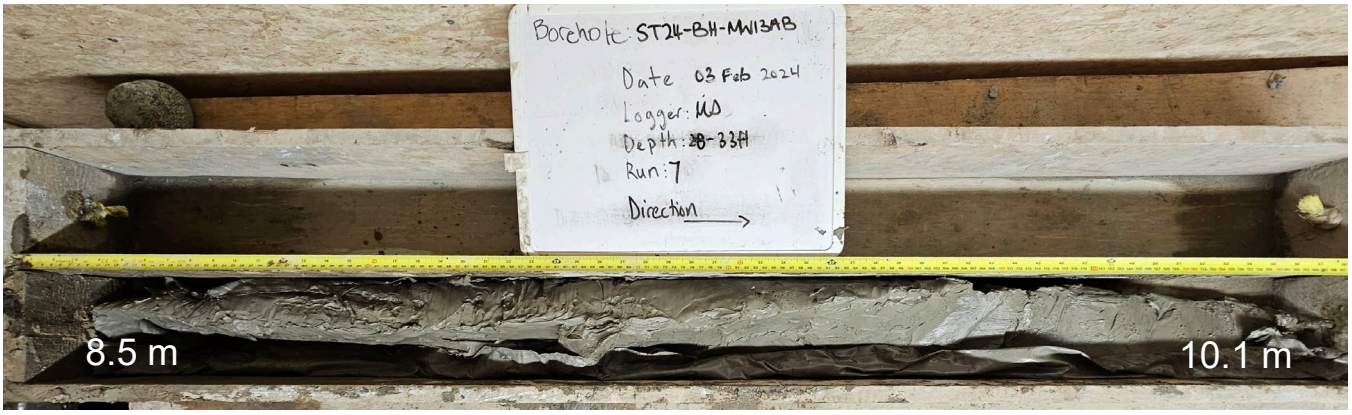
Depth (m): 5.5 – 7.0



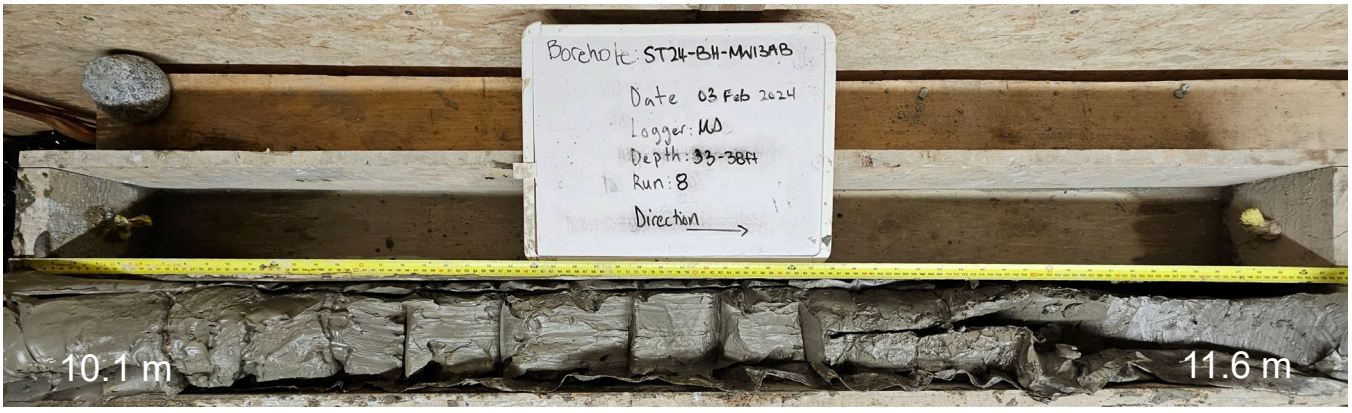
Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells

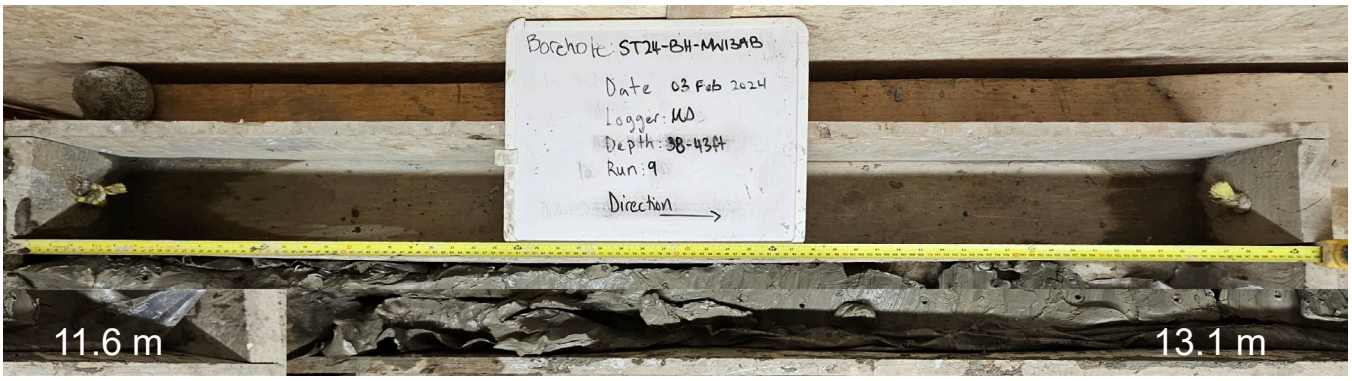


Depth (m): 8.5 – 10.1

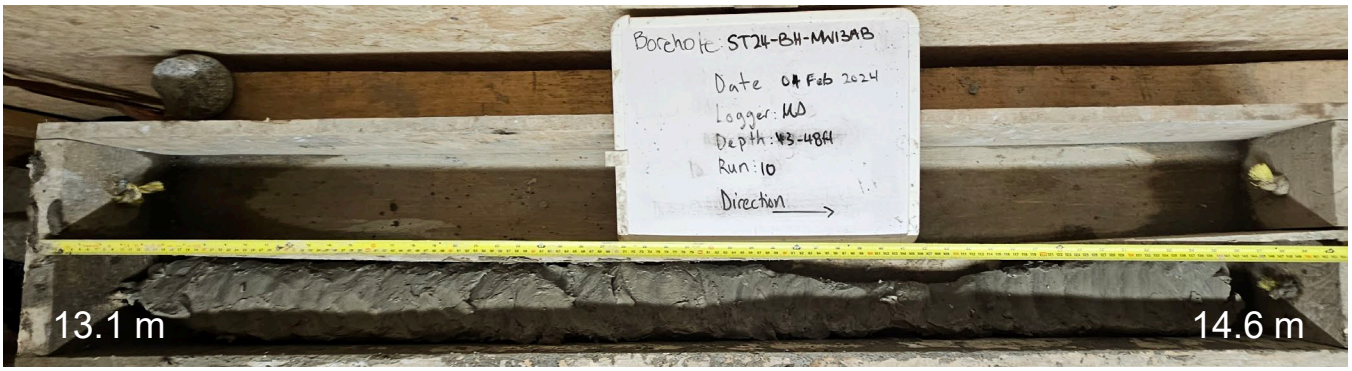


Depth (m): 10.1 – 11.6

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells

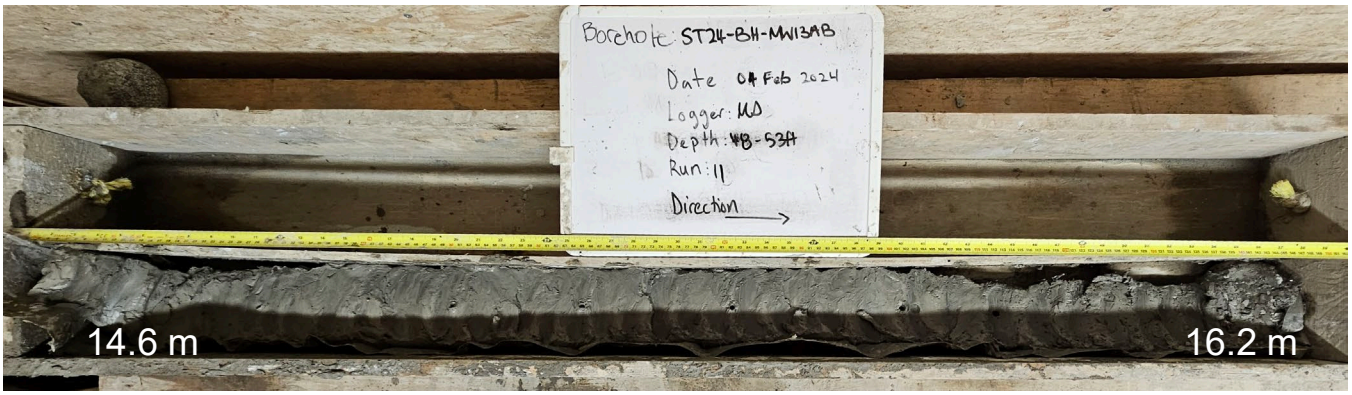


Depth (m): 11.6 – 13.1

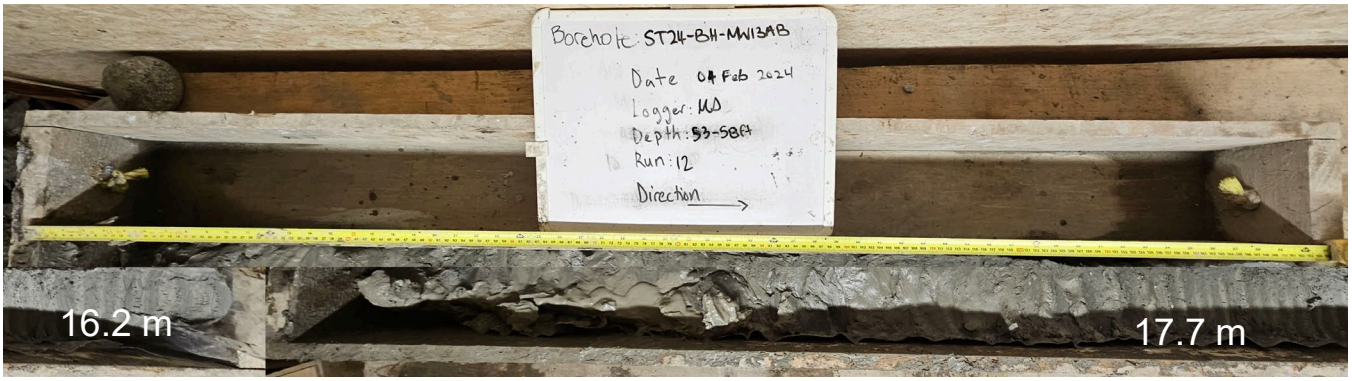


Depth (m): 13.1 – 14.6

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 14.6 – 16.2



Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



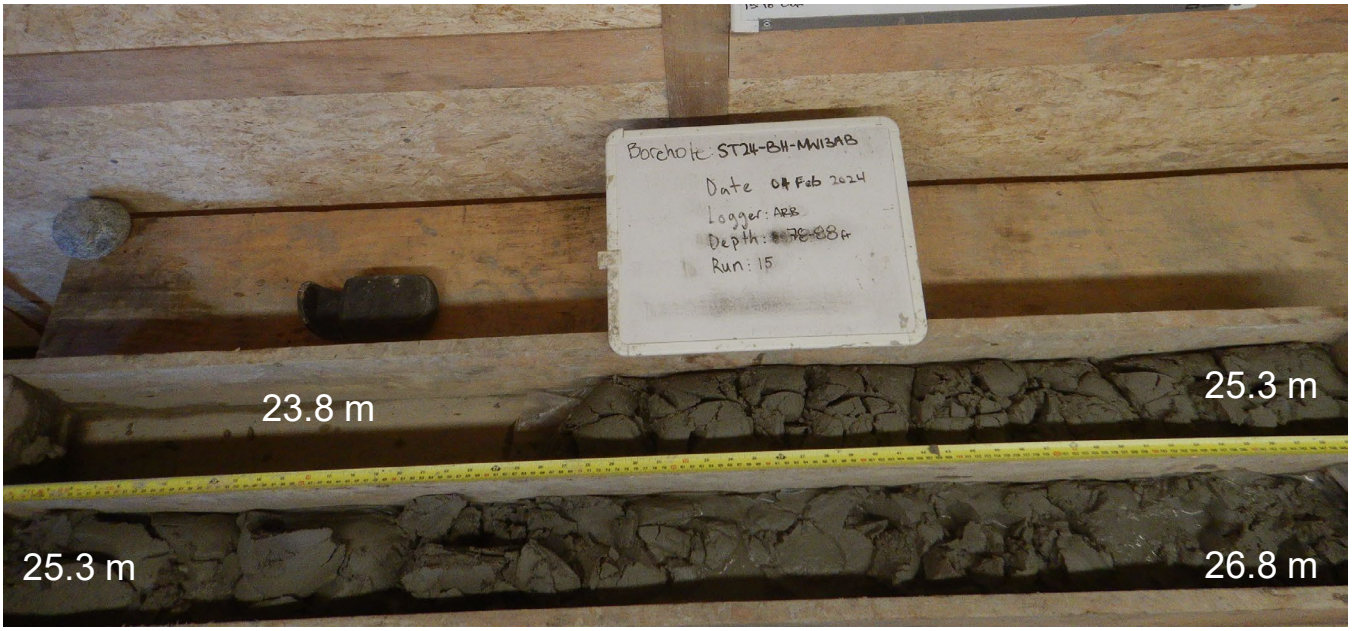
Depth (m): 17.7 – 20.7



Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 23.8 – 26.8



Depth (m): 26.8 – 31.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 23.8 – 31.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 31.4 – 36.0



Depth (m): 31.4 – 36.0

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 36.0 – 39.0



Depth (m): 39.0 – 42.1

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 36.0 – 42.1**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 42.1 – 45.1



Depth (m): 45.1 – 48.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 42.1 – 48.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 48.2 – 51.2



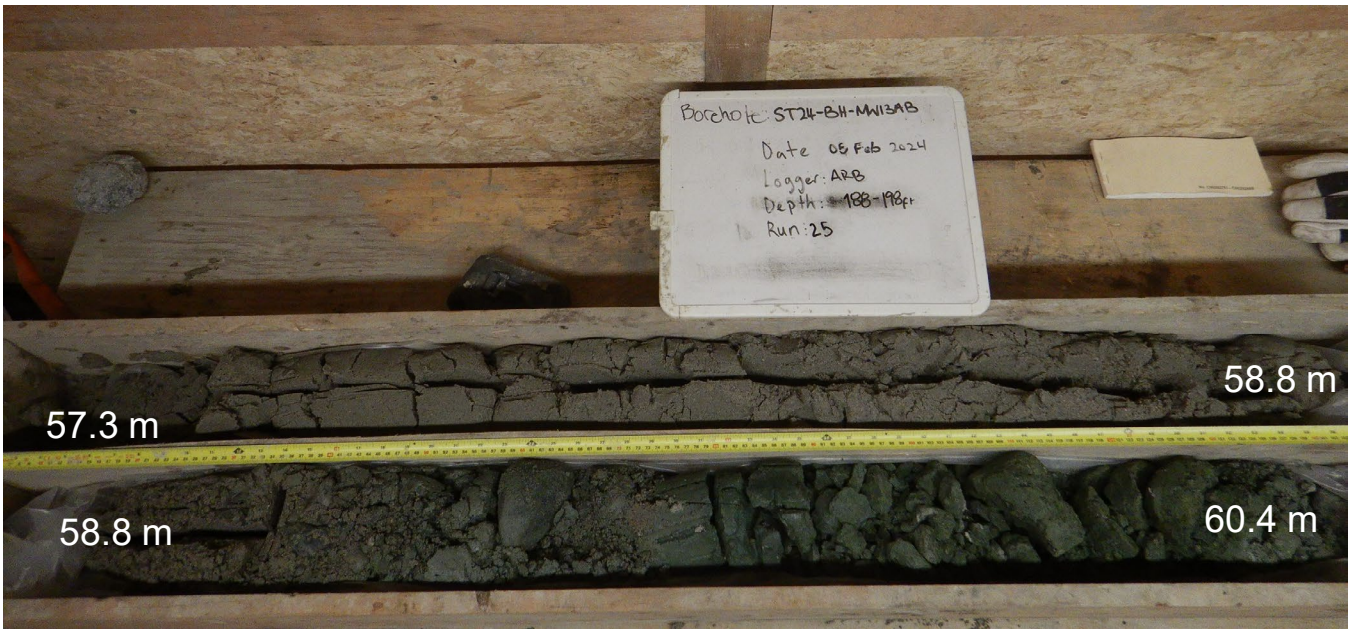
Depth (m): 51.2 – 54.3

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 48.2 – 54.3**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **12 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 54.3 – 57.3



Depth (m): 57.3 – 60.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 54.3 – 60.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **13 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 60.4 – 63.4



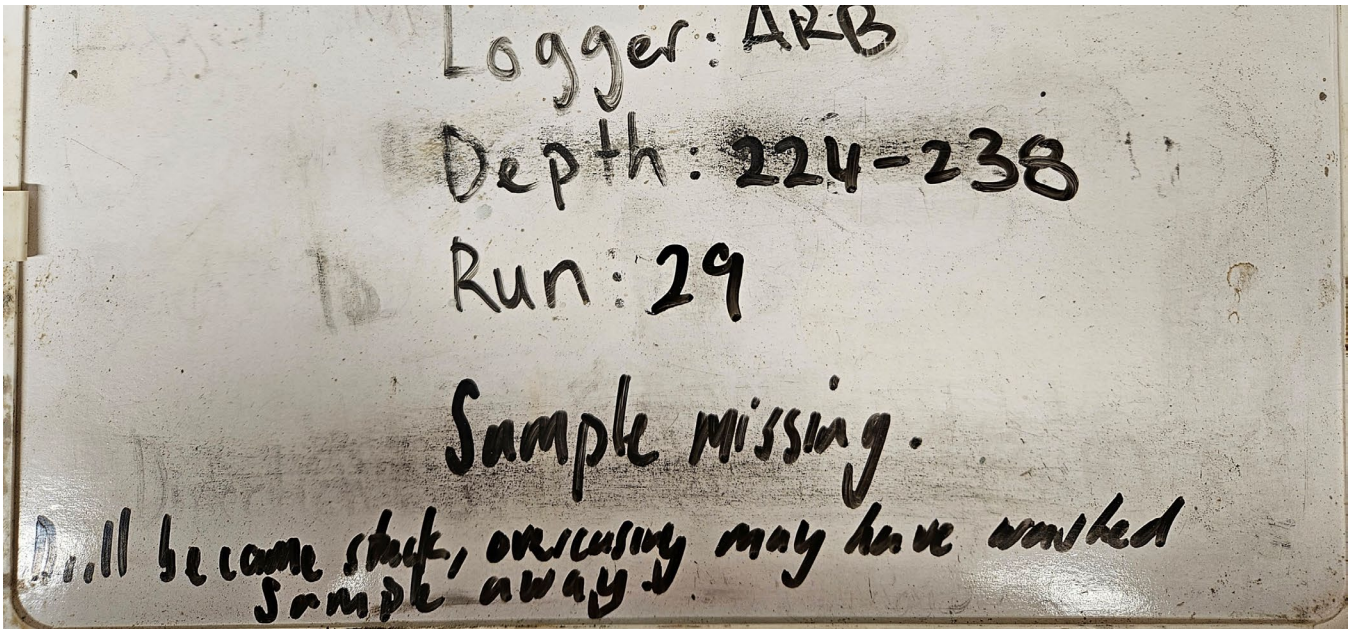
Depth (m): 63.4 – 66.4

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 60.4 – 66.4**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **14 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



Depth (m): 66.4 – 68.3



Depth (m): 68.3 – 72.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 66.4 – 72.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **15 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



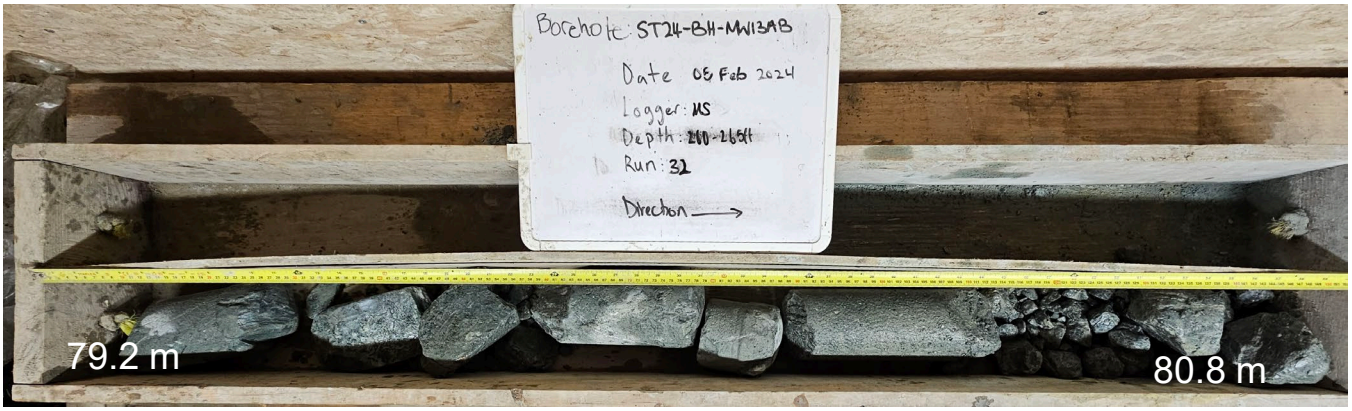
Depth (m): 72.5 – 73.5



Depth (m): 73.5 – 79.2

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 72.5 – 79.2**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **16 of 17**

Borehole ID: ST24-BH-MW-13AB
Location: Monitoring Wells



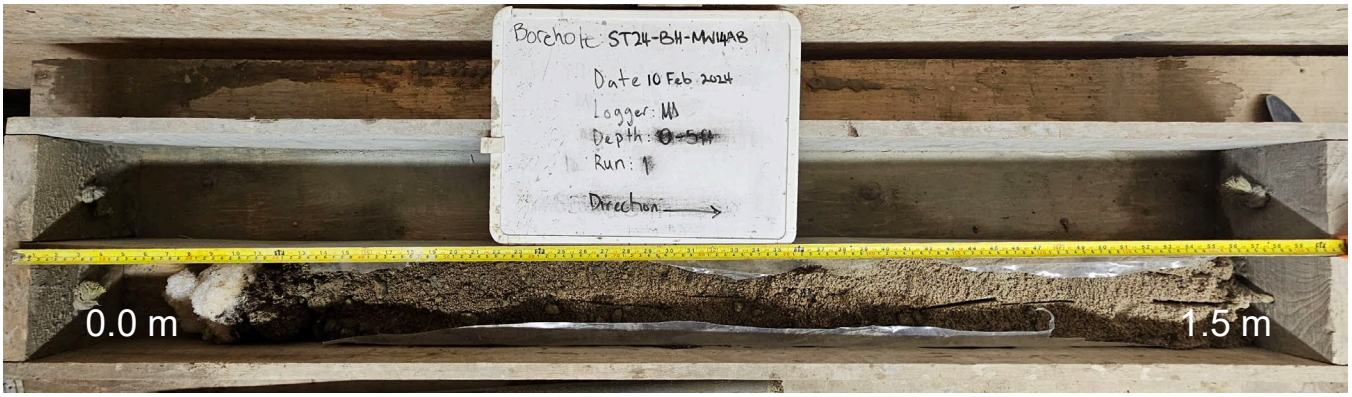
Depth (m): 79.2 – 80.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **SR24-BH-MW-13AB** **Depth (m): 79.2 – 80.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **17 of 17**

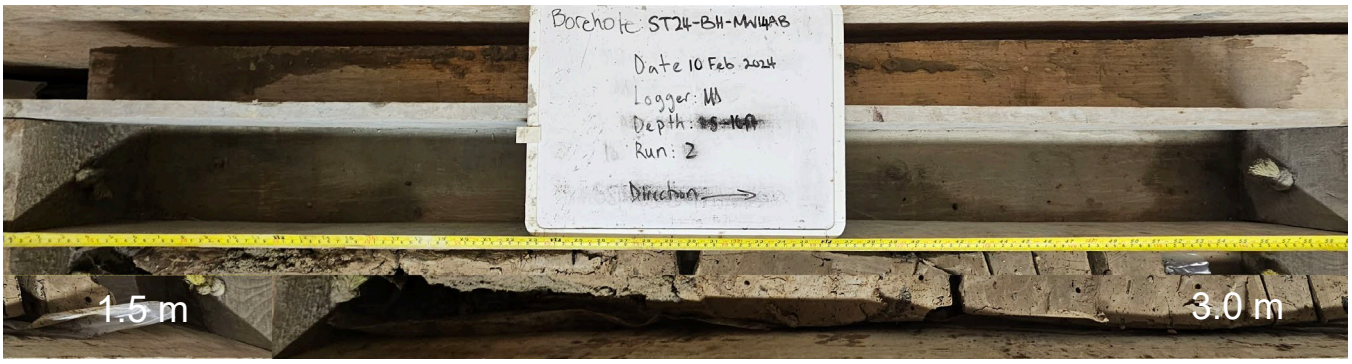
ST24-BH-MW-14AB

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



Depth (m): 0.0 – 1.5



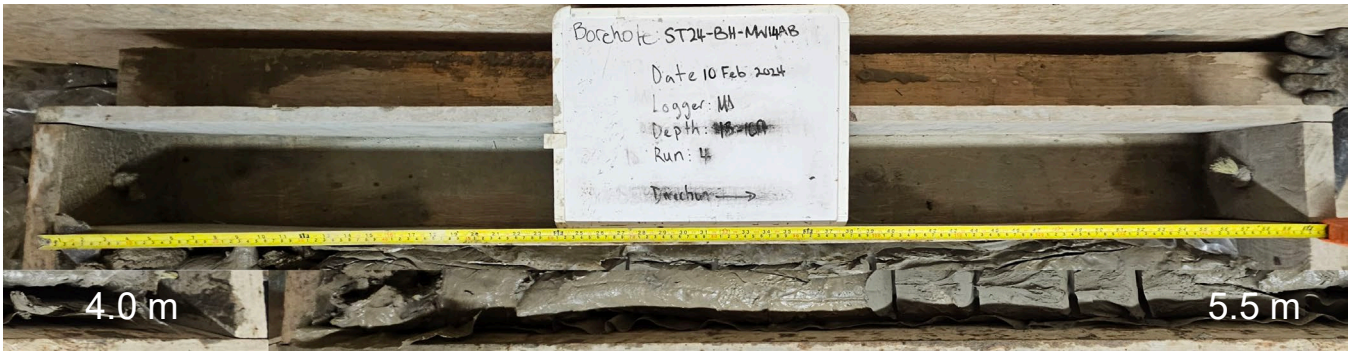
Depth (m): 1.5 – 3.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
		ST24-BH-MW-14AB		
		Depth (m): 0.0 – 3.0		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells

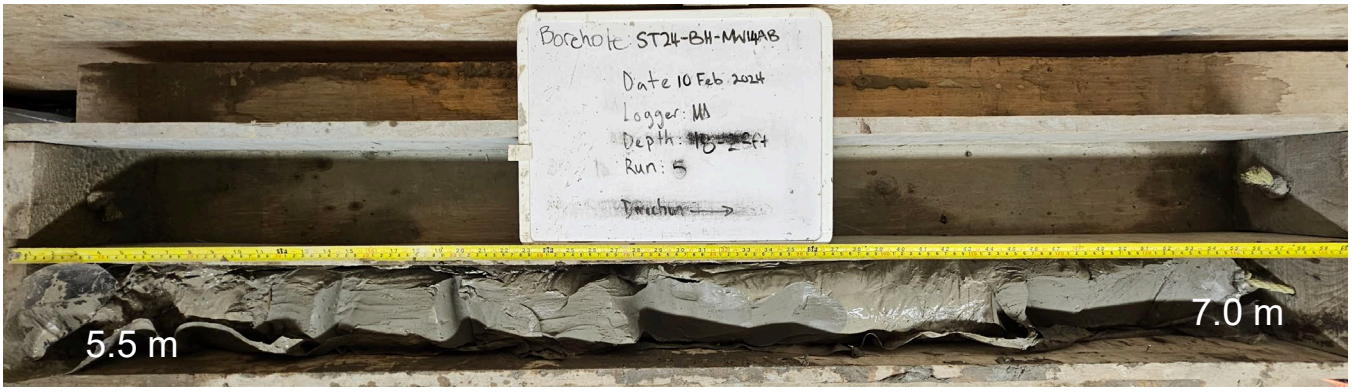


Depth (m): 3.0 – 4.0



Depth (m): 4.0 – 5.5

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



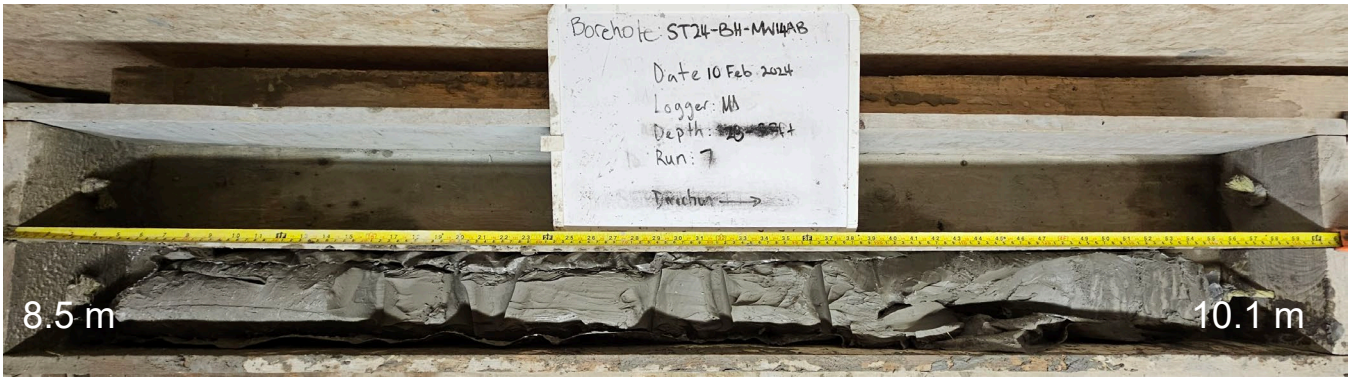
Depth (m): 5.5 – 7.0



Depth (m): 7.0 – 8.5

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 5.5 – 8.5**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **3 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



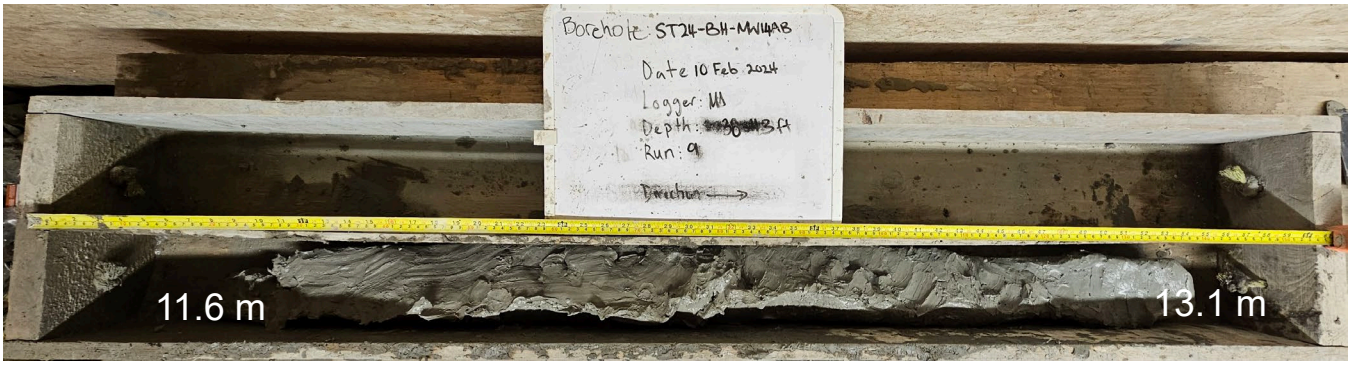
Depth (m): 8.5 – 10.1



Depth (m): 10.1 – 11.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 8.5 – 11.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **4 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



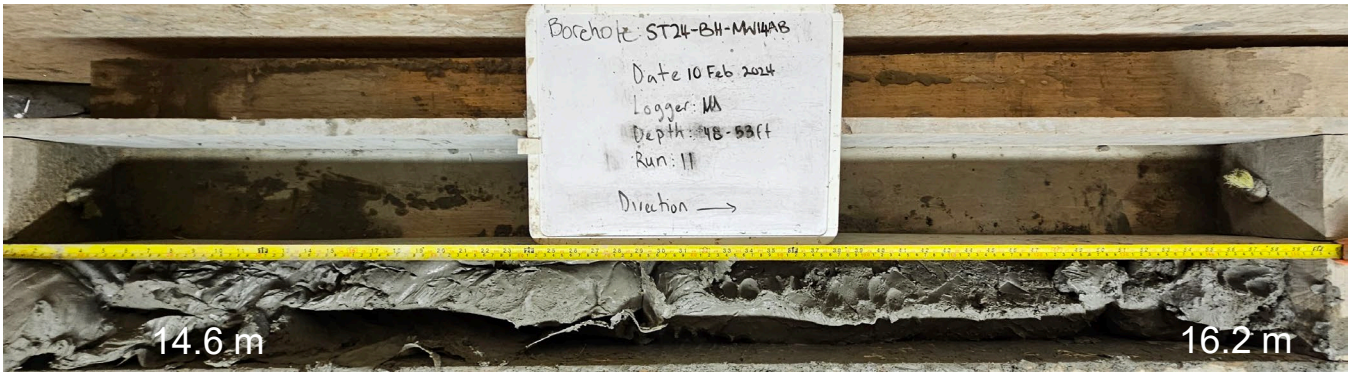
Depth (m): 11.6 – 13.1



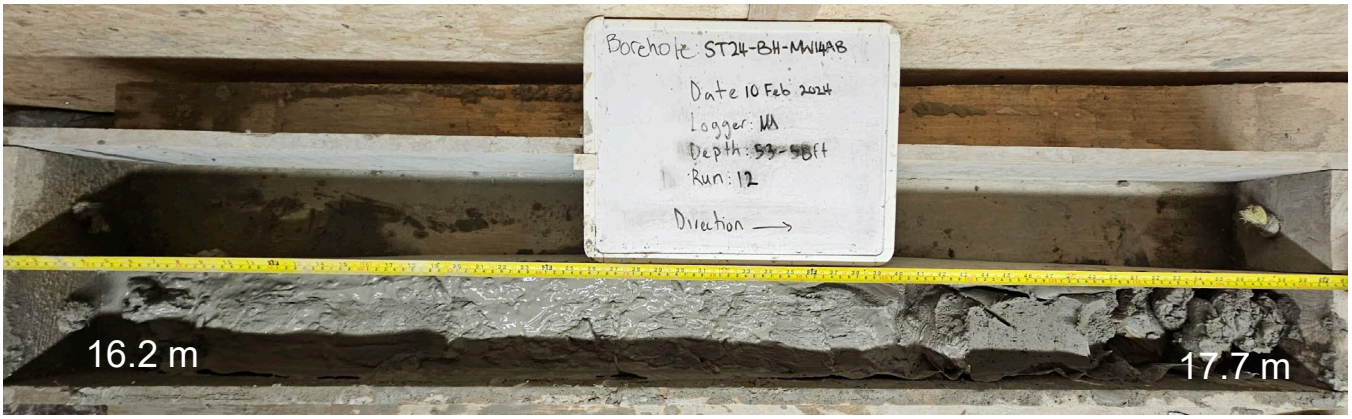
Depth (m): 13.1 – 14.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 11.6 – 14.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **5 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



Depth (m): 14.6 – 16.2



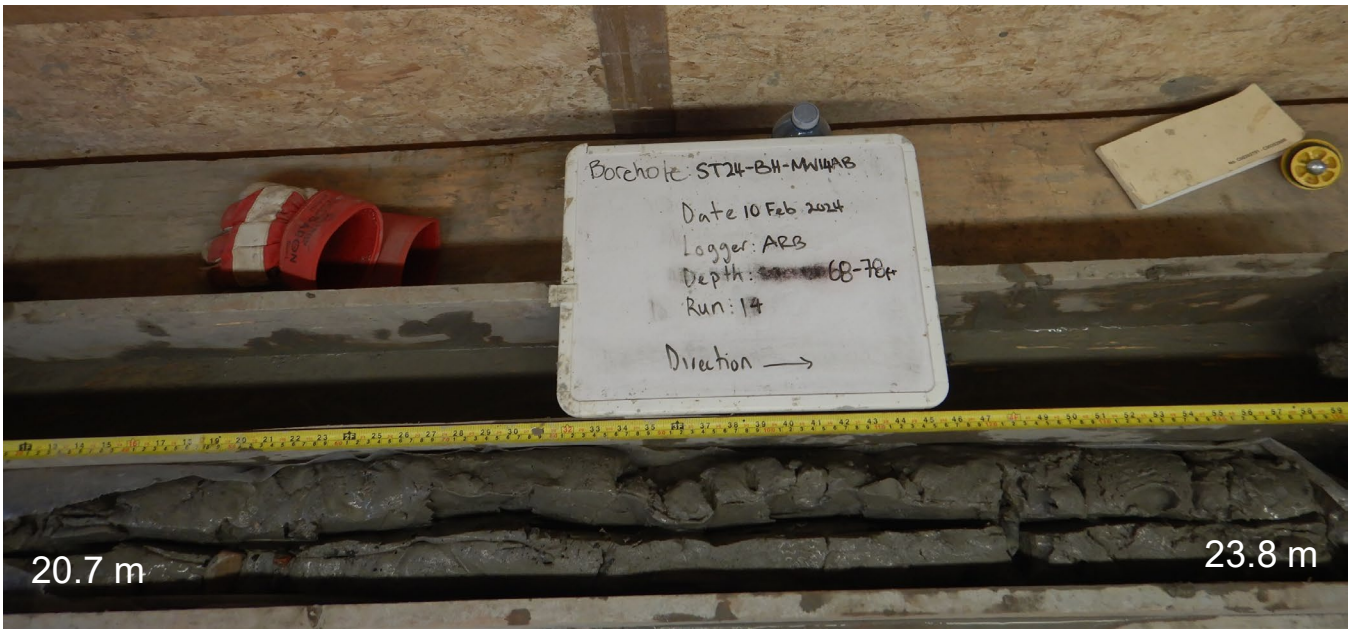
Depth (m): 16.2 – 17.7

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 14.6 – 17.7**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **6 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



Depth (m): 17.7 – 20.7



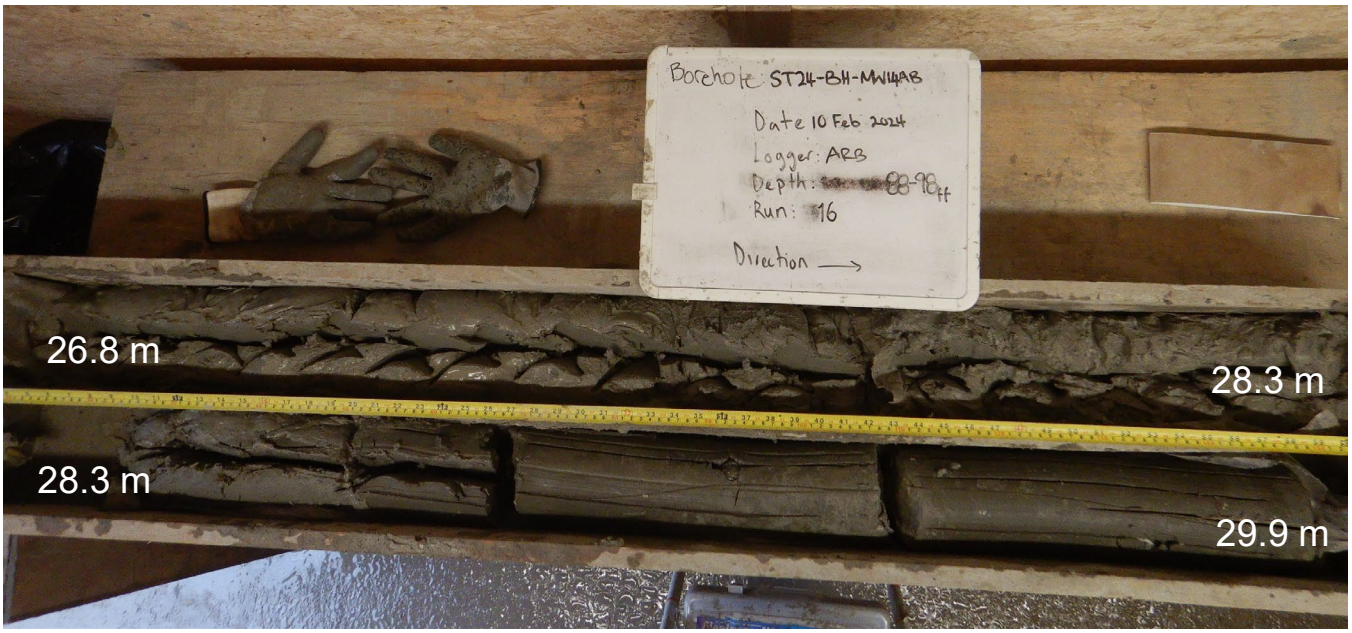
Depth (m): 20.7 – 23.8

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 17.7 – 23.8**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **7 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



Depth (m): 23.8 – 26.8



Depth (m): 26.8 – 29.9

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 23.8 – 29.9**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **8 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



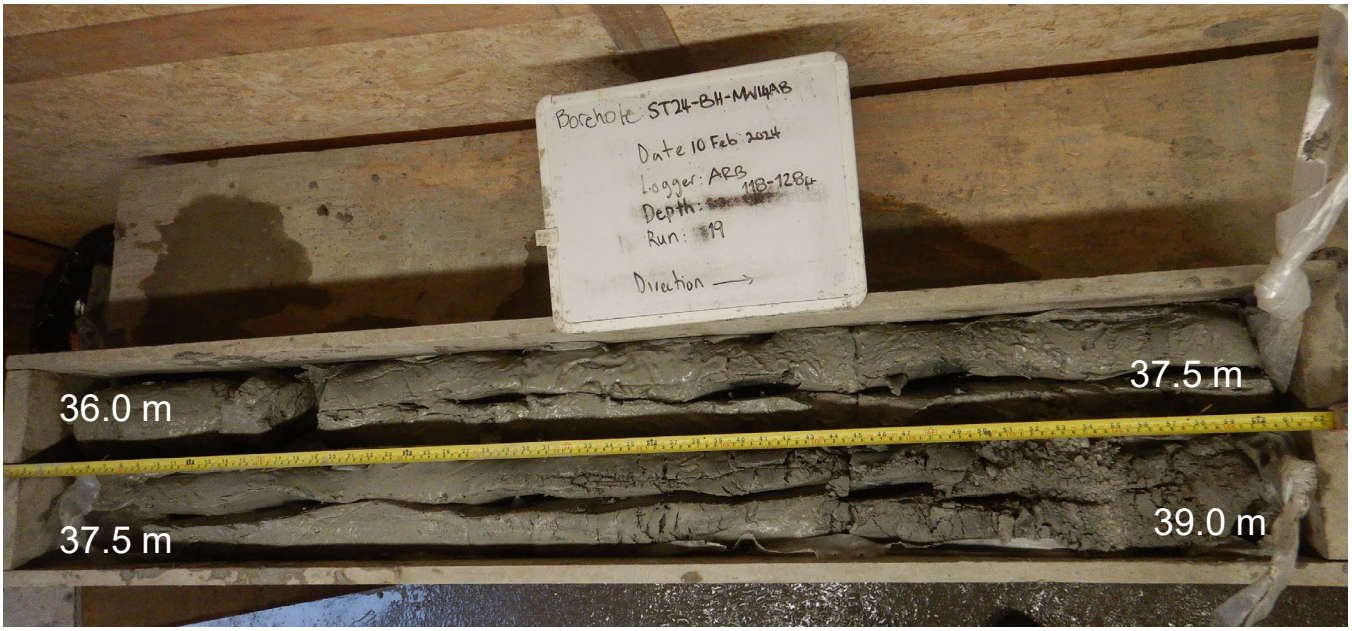
Depth (m): 29.9 – 32.9



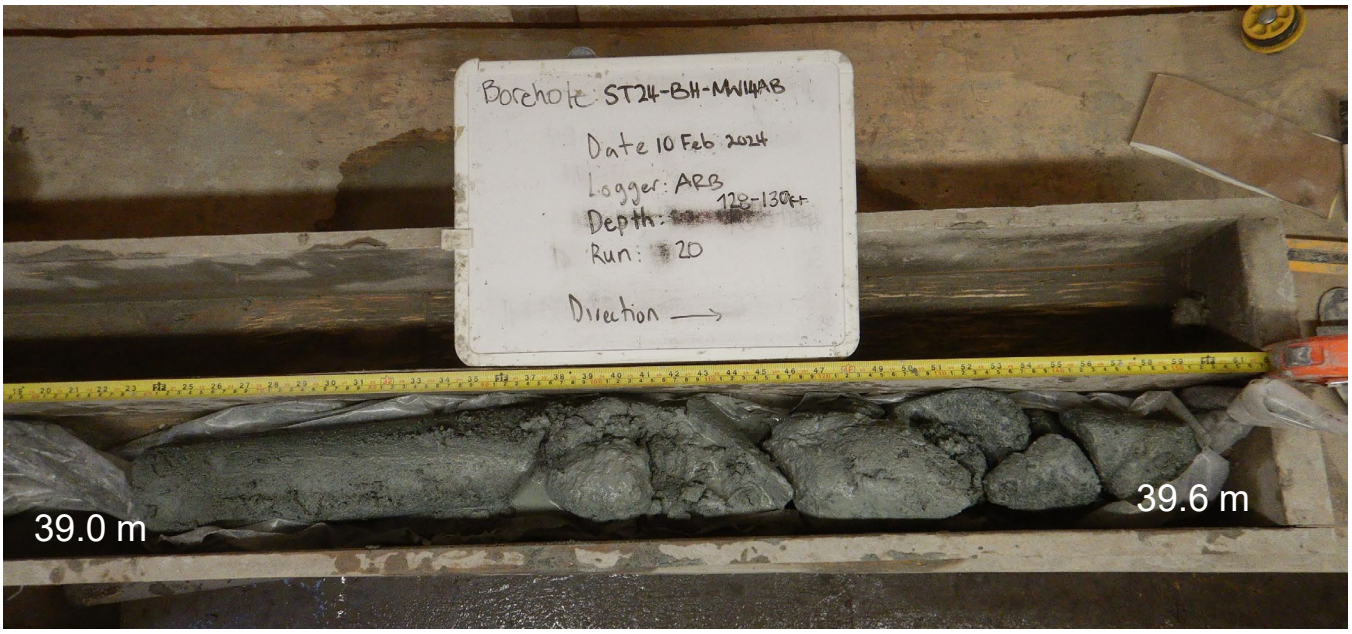
Depth (m): 32.9 – 36.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 29.9 – 36.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **9 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



Depth (m): 36.0 – 39.0



Depth (m): 39.0 – 39.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 36.0 – 39.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **10 of 11**

Borehole ID: ST24-BH-MW-14AB
Location: Monitoring Wells



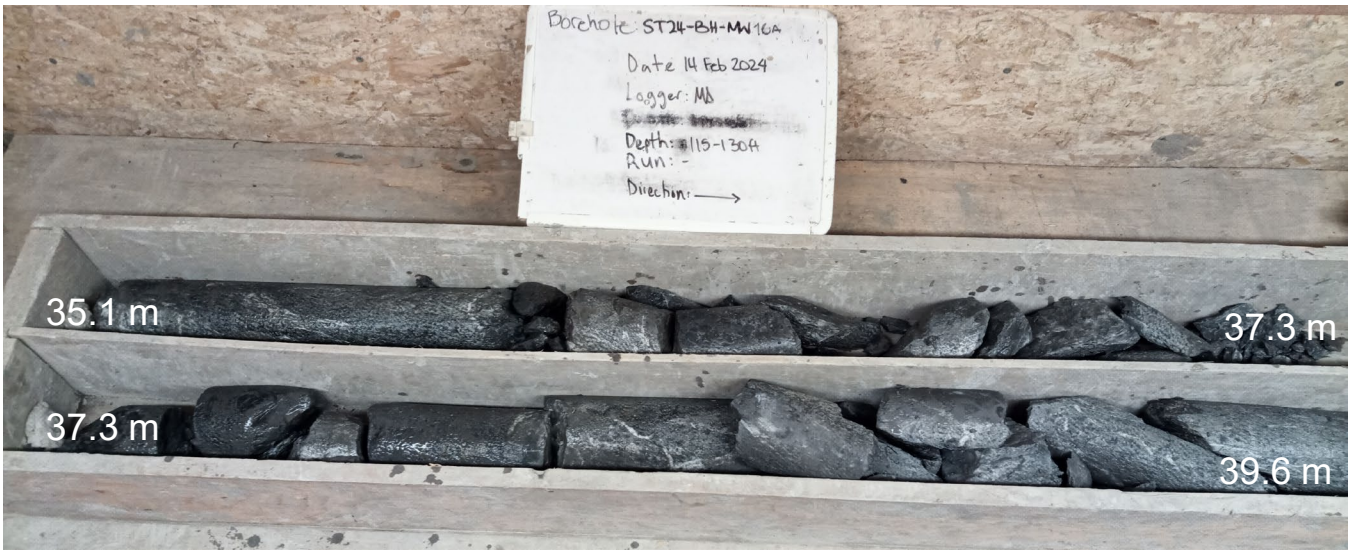
Depth (m): 39.6 – 42.0

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-14AB** **Depth (m): 39.6 – 42.0**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **11 of 11**

ST24-BH-MW-16A

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1		
Job No: CAPR000801	Crawford	Date: February 2024	Approved:	Figure:

Borehole ID: ST24-BH-MW-16A
Location: Monitoring Wells



Depth (m): 35.1 – 39.6

srk consulting	CANADA NICKEL COMPANY	Crawford Overburden Geotechnical Investigation Factual Report 2024-Q1 **ST24-BH-MW-16A** **Depth (m): 35.1 – 39.6**		
Job No: CAPR000801	Crawford	Date: February 2024	Approved: ARB	Figure: **1 of 1**

Appendix D: CPT Report

PRESENTATION OF SITE INVESTIGATION RESULTS

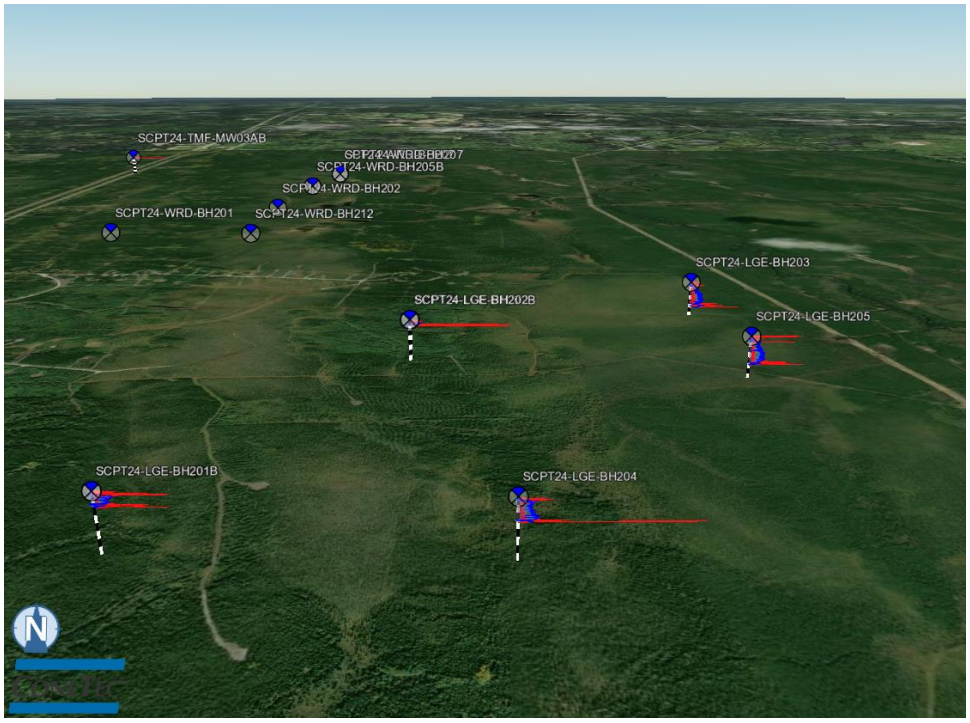
Crawford Mine - SRK

Prepared for:

Canada Nickel Company

ConeTec Job No: 24-05-27159

Project Start Date: 2024-02-15
Project End Date: 2024-03-22
Report Date: 2024-04-09



Prepared by:

ConeTec Investigations Ltd.
9033 Leslie Street, Unit 15
Richmond Hill, ON L4B 4K3

Tel: (905) 886-2663
Fax: (905) 886-2664

ConeTecON@conetec.com
www.conetec.com
www.conetecdataservices.com

© 2024 ConeTec Group of Companies. All Rights Reserved.

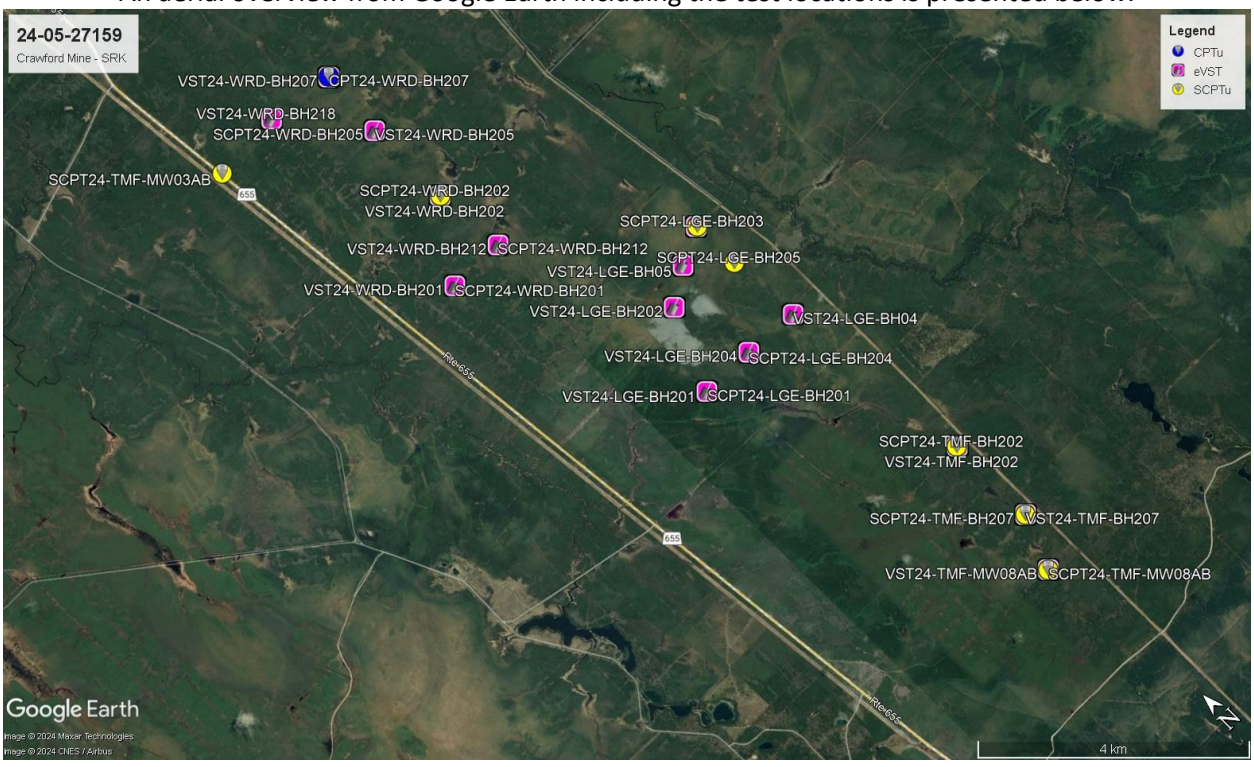
Introduction

The enclosed report presents the results of the site investigation program conducted by ConeTec Investigations Ltd. for Canada Nickel Company at Crawford Mine, north of Timmins, ON. The program consisted of 1 cone penetration test (CPTu), 17 seismic cone penetration tests (SCPTu) and 15 electric field vane shear test (eVST) locations. Please note that this report, which also includes all accompanying data, are subject to the 3rd Party Disclaimer and Client Disclaimer that follow in the 'Limitations' section of this report.

Project Information

Project	
Client	Canada Nickel Company
Project	Crawford Mine - SRK
ConeTec project number	24-05-27159

An aerial overview from Google Earth including the test locations is presented below.



Rig Description	Deployment System	Test Type
CPT track rig (M5TII)	14 ton rig cylinder	CPTu, SCPTu
Track mounted drill rig (Choice)	Portable	SCPTu, eVST

Coordinates		
Test Type	Collection Method	EPSG Number
CPTu, SCPTu, eVST	Consumer grade GPS	32617

Cone Penetrometers Used for this Project						
Cone Description	Cone Number	Cross Sectional Area (cm^2)	Sleeve Area (cm^2)	Tip Capacity (bar)	Sleeve Capacity (bar)	Pore Pressure Capacity (bar)
762:T1500F15U35	762	15	225	1500	15	35
958:T1500F15U35	958	15	225	1500	15	35
The CPTu summary indicates which cone was used for each sounding.						

Cone Penetration Test (CPTu)	
Depth reference	Depths are referenced to the existing ground surface at the time of each test.
Tip and sleeve data offset	0.1 meter This has been accounted for in the CPT data files.
Seismic calculations	Poisson's ratio (ν) was calculated from the shear wave (V_s) and compression wave (V_p) velocities using the following equation: $$\nu = \frac{(V_p/V_s)^2 - 2}{2\left((V_p/V_s)^2 - 1\right)}$$
Additional plots	• Standard plots with expanded range • Advanced plots with Ic, Su(Nkt), phi and N1(60)Ic • CPT Seismic plots with Vs, Vp and Poisson's Ratio • Soil Behaviour Type (SBT) scatter plots

Calculated Geotechnical Parameter Tables	
Additional information	The Non-Normalized Soil Behaviour Type Chart (Robertson, 2010) was used to classify the soil for this project. A detailed set of calculated CPTu parameters have been generated and are provided in Excel format files in the release folder. The CPTu parameter calculations are based on values of corrected tip resistance (q_t) sleeve friction (f_s) and pore pressure (u_2). Effective stresses are calculated based on unit weights that have been assigned to the individual soil behaviour type zones and the assumed equilibrium pore pressure profile. Soils were classified as either drained or undrained based on the Non-Normalized Soil Behaviour Type Chart (Robertson, 2010). Calculations for both drained and undrained parameters were included for materials that classified as silt mixtures and sand mixtures (zones 4 and 5). Equilibrium pore pressure profiles generated from the pore pressure dissipation data and assumed equilibrium points were used for the calculated parameters. Based on the dynamic pore pressure response, hydrostatic conditions were assumed after the last equilibrium pore pressure point. The equilibrium pore pressure profile points and profile line, as well as the hydrostatic line are plotted on the dynamic pore pressure for comparison.

Electric Field Vane Shear Test (eVST)	
Depth reference	Depths are referenced to the existing surface at the time of each test.
Load Cell Capacity	100 N.m
Load Cell Location	Surface
Additional Information	Peak undrained shear strength values (Su) are over-plotted on the CPTu Su profile for comparison.

Limitations

3rd Party Disclaimer

This report titled “Crawford Mine - SRK”, referred to as the (“Report”), was prepared by ConeTec for Canada Nickel Company. The Report is confidential and may not be distributed to or relied upon by any third parties without the express written consent of ConeTec. Any third parties gaining access to the Report do not acquire any rights as a result of such access. Any use which a third party makes of the Report, or any reliance on or decisions made based on it, are the responsibility of such third parties. ConeTec accepts no responsibility for loss, damage and/or expense, if any, suffered by any third parties as a result of decisions made, or actions taken or not taken, which are in any way based on, or related to, the Report or any portion(s) thereof.

Client Disclaimer

ConeTec was retained by Canada Nickel Company to collect and provide the raw data (“Data”) which is included in this report titled “Crawford Mine - SRK”, which is referred to as the (“Report”). ConeTec has collected and reported the Data in accordance with current industry standards. No other warranty, express or implied, with respect to the Data is made by ConeTec. In order to properly understand the Data included in the Report, reference must be made to the documents accompanying and other sources referenced in the Report in their entirety. Any analysis, interpretation, judgment, calculations and/or geotechnical parameters (collectively “Interpretations”) included in the Report, including those based on the Data, are outside the scope of ConeTec’s retainer and are included in the Report as a courtesy only. Other than the Data, the contents of the Report (including any Interpretations) should not be relied upon in any fashion without independent verification and ConeTec is in no way responsible for any loss, damage or expense resulting from the use of, and/or reliance on, such material by any party.

Cone penetration tests (CPTu) are conducted using an integrated electronic piezocone penetrometer and data acquisition system manufactured by Adara Systems Ltd., a subsidiary of ConeTec.

ConeTec's piezocone penetrometers are compression type designs in which the tip and friction sleeve load cells are independent and have separate load capacities. The piezocones use strain gauged load cells for tip and sleeve friction and a strain gauged diaphragm type transducer for recording pore pressure. The piezocones also have a platinum resistive temperature device (RTD) for monitoring the temperature of the sensors, an accelerometer type dual axis inclinometer and two geophone sensors for recording seismic signals. All signals are amplified and measured with minimum sixteen-bit resolution down hole within the cone body, and the signals are sent to the surface using a high bandwidth, error corrected digital interface through a shielded cable.

ConeTec penetrometers are manufactured with various tip, friction and pore pressure capacities in both 10 cm^2 and 15 cm^2 tip base area configurations in order to maximize signal resolution for various soil conditions. The specific piezocone used for each test is described in the CPT summary table presented in the first appendix. The 15 cm^2 penetrometers do not require friction reducers as they have a diameter larger than the deployment rods. The 10 cm^2 piezocones use a friction reducer consisting of a rod adapter extension behind the main cone body with an enlarged cross sectional area (typically 44 millimeters diameter over a length of 32 millimeters with tapered leading and trailing edges) located at a distance of 585 millimeters above the cone tip.

The penetrometers are designed with equal end area friction sleeves, a net end area ratio of 0.8 and cone tips with a 60 degree apex angle.

All ConeTec piezocones can record pore pressure at various locations. Unless otherwise noted, the pore pressure filter is located directly behind the cone tip in the "u_2" position (ASTM Type 2). The filter is six millimeters thick, made of porous plastic (polyethylene) having an average pore size of 125 microns (90-160 microns). The function of the filter is to allow rapid movements of extremely small volumes of water needed to activate the pressure transducer while preventing soil ingress or blockage.

The piezocone penetrometers are manufactured with dimensions, tolerances and sensor characteristics that are in general accordance with the current ASTM D5778 standard. ConeTec's calibration criteria also meets or exceeds those of the current ASTM D5778 standard. An illustration of the piezocone penetrometer is presented in Figure CPTu.

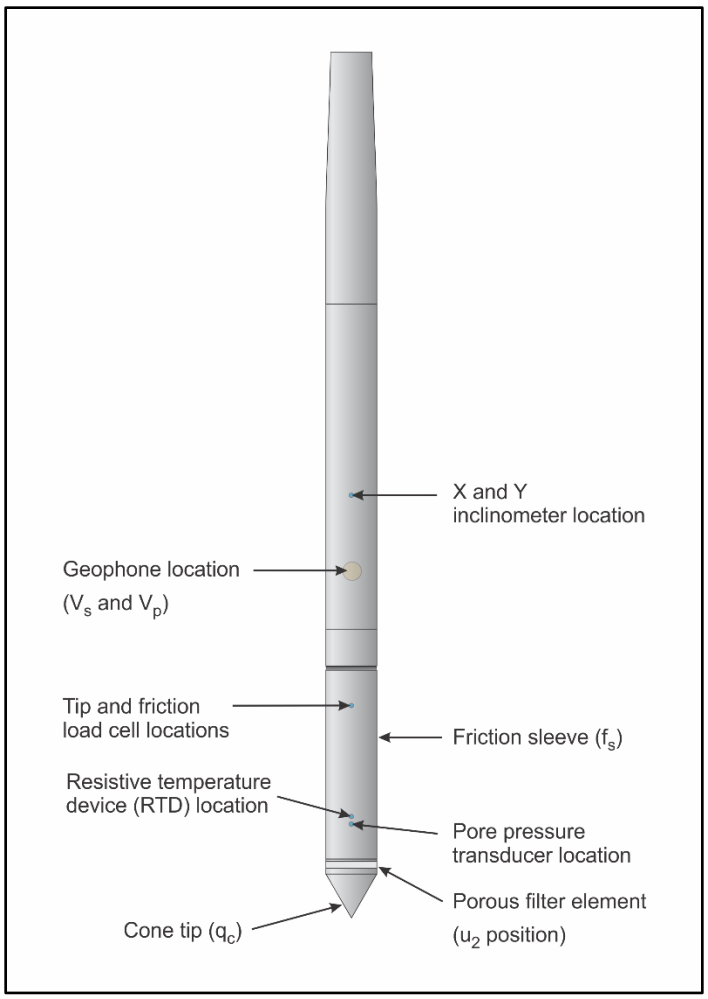


Figure CPTu. Piezocone Penetrometer (15 cm^2)

The ConeTec data acquisition systems consist of a Windows based computer and a signal interface box and power supply. The signal interface combines depth increment signals, seismic trigger signals and the downhole digital data. This combined data is then sent to the Windows based computer for collection and presentation. The data is recorded at fixed depth increments using a depth wheel attached to the push cylinders or by using a spring loaded rubber depth wheel that is held against the cone rods. The typical recording interval is 2.5 centimeters; custom recording intervals are possible.

The system displays the CPTu data in real time and records the following parameters to a storage media during penetration:

- Depth
- Uncorrected tip resistance (q_c)
- Sleeve friction (f_s)
- Dynamic pore pressure (u)
- Additional sensors such as resistivity, passive gamma, ultra violet induced fluorescence, if applicable

All testing is performed in accordance to ConeTec's CPTu operating procedures which are in general accordance with the current ASTM D5778 standard.

Prior to the start of a CPTu sounding a suitable cone is selected, the cone and data acquisition system are powered on, the pore pressure system is saturated with silicone oil and the baseline readings are recorded with the cone hanging freely in a vertical position.

The CPTu is conducted at a steady rate of two centimeters per second, within acceptable tolerances. Typically one meter length rods with an outer diameter of 38.1 millimeters are added to advance the cone to the sounding termination depth. After cone retraction final baselines are recorded.

Additional information pertaining to ConeTec's cone penetration testing procedures:

- Each filter is saturated in silicone oil under vacuum pressure prior to use
- Baseline readings are compared to previous readings
- Soundings are terminated at the client's target depth or at a depth where an obstruction is encountered, excessive rod flex occurs, excessive inclination occurs, equipment damage is likely to take place, or a dangerous working environment arises
- Differences between initial and final baselines are calculated to ensure zero load offsets have not occurred and to ensure compliance with ASTM standards

The interpretation of piezocone data for this report is based on the corrected tip resistance (q_t), sleeve friction (f_s) and pore water pressure (u). The interpretation of soil type is based on the correlations developed by Robertson et al. (1986) and Robertson (1990, 2009). It should be noted that it is not always possible to accurately identify a soil behaviour type based on these parameters. In these situations, experience, judgment and an assessment of other parameters may be used to infer soil behaviour type.

The recorded tip resistance (q_c) is the total force acting on the piezocone tip divided by its base area. The tip resistance is corrected for pore pressure effects and termed corrected tip resistance (q_t) according to the following expression presented in Robertson et al. (1986):

$$q_t = q_c + (1\text{-}a) \bullet u_2$$

where: q_t is the corrected tip resistance
q_c is the recorded tip resistance
u_2 is the recorded dynamic pore pressure behind the tip (u_2 position)
a is the Net Area Ratio for the piezocone (0.8 for ConeTec probes)

The sleeve friction (f_s) is the frictional force on the sleeve divided by its surface area. As all ConeTec piezocones have equal end area friction sleeves, pore pressure corrections to the sleeve data are not required.

The dynamic pore pressure (u) is a measure of the pore pressures generated during cone penetration. To record equilibrium pore pressure, the penetration must be stopped to allow the dynamic pore pressures to stabilize. The rate at which this occurs is predominantly a function of the permeability of the soil and the diameter of the cone.

The friction ratio (Rf) is a calculated parameter. It is defined as the ratio of sleeve friction to the tip resistance expressed as a percentage. Generally, saturated cohesive soils have low tip resistance, high friction ratios and generate large excess pore water pressures. Cohesionless soils have higher tip resistances, lower friction ratios and do not generate significant excess pore water pressure.

A summary of the CPTu soundings along with test details and individual plots are provided in the appendices. A set of files with calculated geotechnical parameters were generated for each sounding based on published correlations and are provided in Excel format in the data release folder. Information regarding the methods used is also included in the data release folder.

For additional information on CPTu interpretations and calculated geotechnical parameters, refer to Robertson et al. (1986), Lunne et al. (1997), Robertson (2009), Mayne (2013, 2014) and Mayne and Peuchen (2012).

References

ASTM D5778-20, 2020, "Standard Test Method for Performing Electronic Friction Cone and Piezocone Penetration Testing of Soils", ASTM International, West Conshohocken, PA. DOI: 10.1520/D5778-20.

Lunne, T., Robertson, P.K. and Powell, J. J. M., 1997, “Cone Penetration Testing in Geotechnical Practice”, Blackie Academic and Professional.

Mayne, P.W., 2013, “Evaluating yield stress of soils from laboratory consolidation and in-situ cone penetration tests”, Sound Geotechnical Research to Practice (Holtz Volume) GSP 230, ASCE, Reston/VA: 406-420. DOI: 10.1061/9780784412770.027.

Mayne, P.W. and Peuchen, J., 2012, “Unit weight trends with cone resistance in soft to firm clays”, Geotechnical and Geophysical Site Characterization *4,* Vol. 1 (Proc. ISC-4, Pernambuco), CRC Press, London: 903-910.

Mayne, P.W., 2014, “Interpretation of geotechnical parameters from seismic piezocone tests”, CPT’14 Keynote Address, Las Vegas, NV, May 2014.

Robertson, P.K., Campanella, R.G., Gillespie, D. and Greig, J., 1986, “Use of Piezometer Cone Data”, Proceedings of InSitu 86, ASCE Specialty Conference, Blacksburg, Virginia.

Robertson, P.K., 1990, “Soil Classification Using the Cone Penetration Test”, Canadian Geotechnical Journal, Volume 27: 151-158. DOI: 10.1139/T90-014.

Robertson, P.K., 2009, “Interpretation of cone penetration tests – a unified approach”, Canadian Geotechnical Journal, Volume 46: 1337-1355. DOI: 10.1139/T09-065.

Shear wave velocity (Vs) testing is performed in conjunction with the piezocone penetration test (SCPTu) in order to collect interval velocities. For some projects seismic compression wave velocity (Vp) testing is also performed.

ConeTec's 15 cm^2 piezocone penetrometers are manufactured with one horizontally active geophone (28 hertz) and one vertically active geophone (28 hertz). Both geophones are rigidly mounted in the body of the cone penetrometer, 0.2 meters behind the cone tip. The vertically mounted geophone is more sensitive to compression waves; however, it is often affected by the compression wave travelling through the cone rods.

Shear waves are typically generated by using an impact hammer horizontally striking a beam that is held in place by a normal load. In some instances, an auger source or an imbedded impulsive source may be used for both shear waves and compression waves. The hammer and beam act as a contact trigger that initiates the recording of the seismic wave traces. For impulsive devices an accelerometer trigger may be used. The traces are recorded in the memory of the cone using a fast analog to digital converter. The seismic trace is then transmitted digitally uphole to a Windows based computer through a signal interface box for recording and analysis. An illustration of the shear wave testing configuration is presented in Figure SCPTu-1.

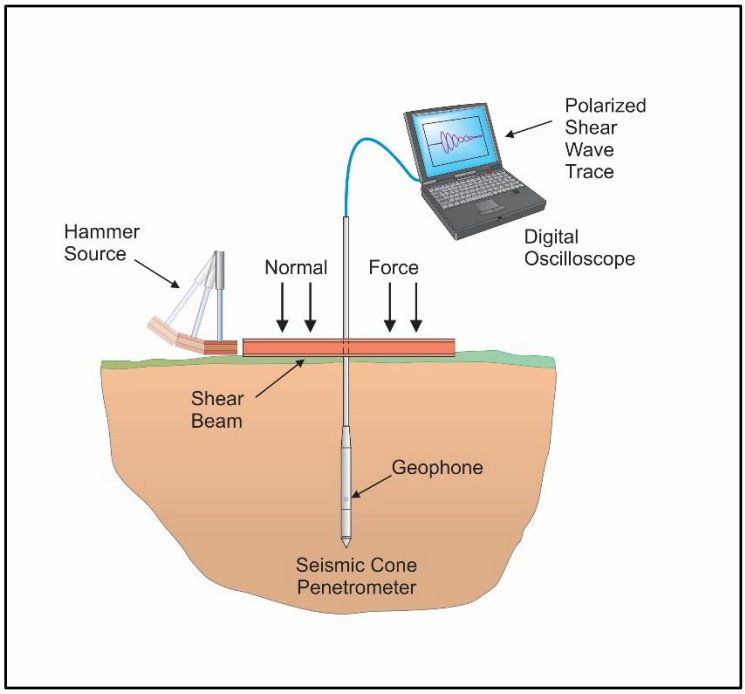


Figure SCPTu-1. Illustration of the SCPTu system

All testing is performed in accordance to ConeTec's SCPTu operating procedures which are in general accordance with the current ASTM D5778 and ASTM D7400 standards.

Prior to the start of a SCPTu sounding, the procedures described in the Cone Penetration Test section are followed. In addition, the active axis of the geophone is aligned parallel to the beam (or source) and the horizontal offset between the cone and the source is measured and recorded.

Prior to recording seismic waves at each test depth, cone penetration is stopped and the rods are decoupled from the rig to avoid transmission of rig energy down the rods. Typically, five wave traces for each orientation are recorded for quality control and uncertainty analysis purposes. After reviewing wave traces for consistency the cone is pushed to the next test depth (typically one meter intervals or as requested by the client). Figure SCPTu-2 presents an illustration of a SCPTu test.

For additional information on seismic cone penetration testing refer to Robertson et al. (1986).

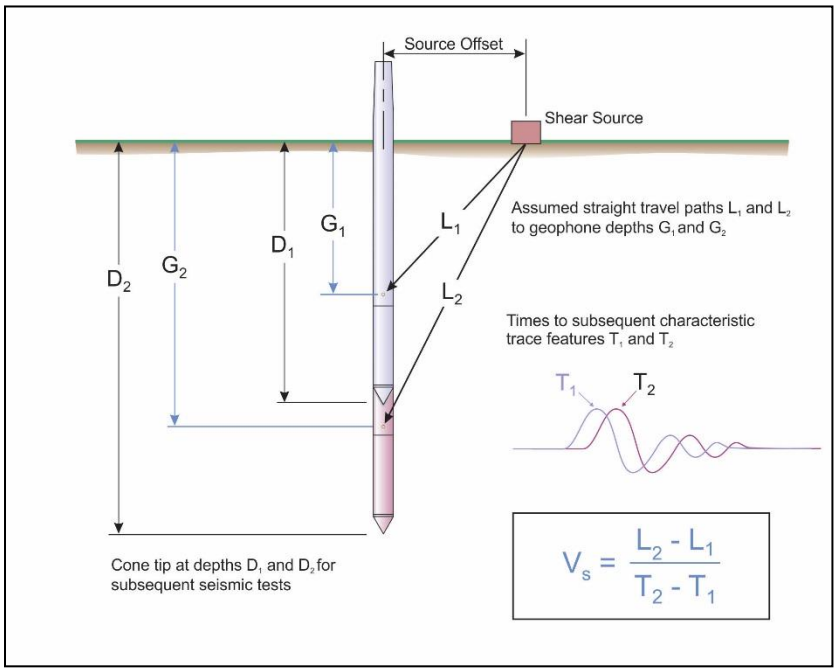


Figure SCPTu-2. Illustration of a seismic cone penetration test

For the determination of interval travel times the wave traces from all depths are displayed in analysis software. The results of the interval picks are supplied in the relevant appendix of this report. Standard practice for ConeTec is to record five wave traces for each source direction at each test depth. Outlier impacts are identified in the field and the impacts are repeated. For the final wave trace profile, the traces are stacked in the time domain to display a single average trace.

Determination of the shear wave interval velocities are performed by visually picking a common feature (e.g. the first characteristic peak, trough, or crossover) on all of the trace depths and taking the difference in ray path divided by the time difference between features at subsequent depths. The same process is used for compression waves, however the first break is most commonly used for selecting an arrival time. For velocity calculation, the ray path is defined as the straight-line distance from the seismic source to the geophone, accounting for beam offset, source depth and geophone offset from the cone tip.

In some cases, usually for shear wave velocity testing, more than one characteristic marker may be used. If there is an overlap between different sets of characteristic markers, then the average time value for those sets of interval times is applied to the determination of velocity.

Ideally, all depths are used for the determination of the velocity profile. However, an interval may be skipped if there is some ambiguity or quality concern with a particular depth, resulting in a larger interval.

Tabular results and SCPTu plots are presented in the relevant appendix.

The average shear wave velocity to a depth of thirty meters (V_{s30}) has been calculated and provided for all applicable soundings using an equation presented in Crow et al. (2012).

$$V_{s30} = \frac{\text{total thickness of all layers (30m)}}{\sum(\text{layer traveltimes})}$$

The layer travel times refers to the travel times propagating in the vertical direction, not the measured travel times from an offset source.

References

ASTM D5778-20, 2020, "Standard Test Method for Performing Electronic Friction Cone and Piezocone Penetration Testing of Soils", ASTM International, West Conshohocken, PA. DOI: 10.1520/D5778-20.

ASTM D7400/D7400M-19, 2019, "Standard Test Methods for Downhole Seismic Testing", ASTM International, West Conshohocken, PA. DOI: 10.1520/D7400_D7400M-19.

Crow, H.L., Hunter, J.A., Bobrowsky, P.T., 2012, “National shear wave measurement guidelines for Canadian seismic site assessment”, GeoManitoba 2012, Sept 30 to Oct 2, Winnipeg, Manitoba.

Robertson, P.K., Campanella, R.G., Gillespie D and Rice, A., 1986, “Seismic CPT to Measure In-Situ Shear Wave Velocity”, Journal of Geotechnical Engineering ASCE, Vol. 112, No. 8: 791-803. DOI: 10.1061/(ASCE)0733-9410(1986)112:8(791).

The cone penetration test is halted at specific depths to carry out pore pressure dissipation (PPD) tests, shown in Figure PPD-1. For each dissipation test the cone and rods are decoupled from the rig and the data acquisition system measures and records the variation of the pore pressure (u) with time (t).

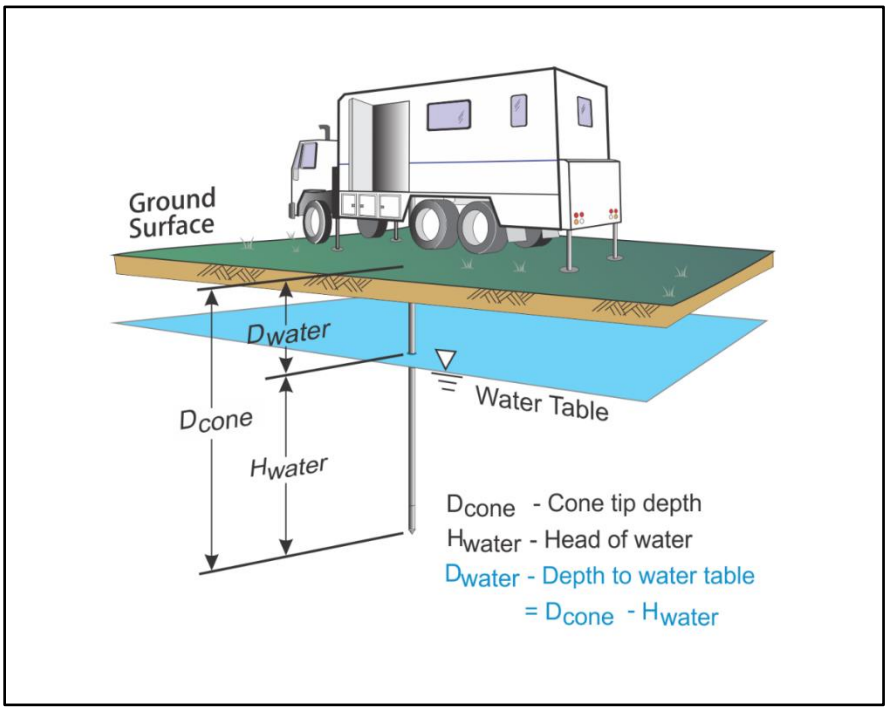


Figure PPD-1. Pore pressure dissipation test setup

Pore pressure dissipation data can be interpreted to provide estimates of ground water conditions, permeability, consolidation characteristics and soil behaviour.

The typical shapes of dissipation curves shown in Figure PPD-2 are very useful in assessing soil type, drainage, in situ pore pressure and soil properties. A flat curve that stabilizes quickly is typical of a freely draining sand. Undrained soils such as clays will typically show positive excess pore pressure and have long dissipation times. Dilative soils will often exhibit dynamic pore pressures below equilibrium that then rise over time. Overconsolidated fine-grained soils will often exhibit an initial dilatory response where there is an initial rise in pore pressure before reaching a peak and dissipating.

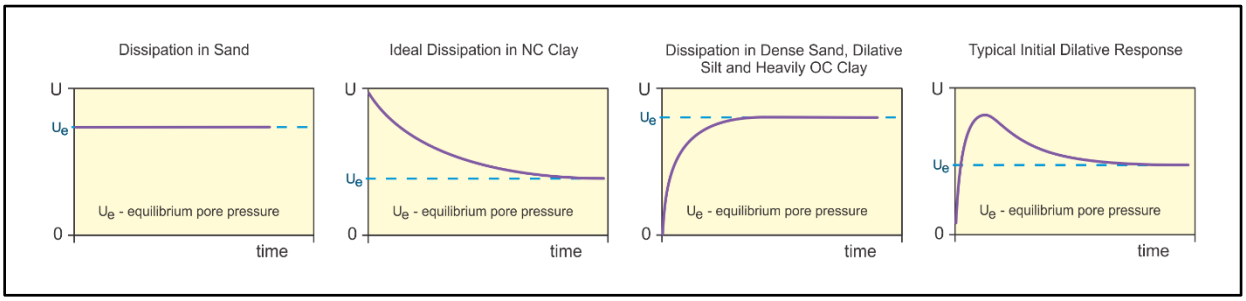


Figure PPD-2. Pore pressure dissipation curve examples

In order to interpret the equilibrium pore pressure (u_{eq}) and the apparent phreatic surface, the pore pressure should be monitored until such time as there is no variation in pore pressure with time as shown for each curve in Figure PPD-2.

In fine grained deposits the point at which 100% of the excess pore pressure has dissipated is known as t_{100}. In some cases this can take an excessive amount of time and it may be impractical to take the dissipation to t_{100}. A theoretical analysis of pore pressure dissipations by Teh and Houlsby, 1991 showed that a single curve relating degree of dissipation versus theoretical time factor (T*) may be used to calculate the coefficient of consolidation (c_h) at various degrees of dissipation resulting in the expression for c_h shown below.

$$c_h = \frac{T^* \cdot a^2 \cdot \sqrt{I_r}}{t}$$

Where:

T* is the dimensionless time factor (Table Time Factor)
a is the radius of the cone
I_r is the rigidity index
t is the time at the degree of consolidation

Table Time Factor. T* versus degree of dissipation (Teh and Houlsby, 1991)

Degree of Dissipation (%)	20	30	40	50	60	70	80
T* (u_2)	0.038	0.078	0.142	0.245	0.439	0.804	1.60

The coefficient of consolidation is typically analyzed using the time (t_{50}) corresponding to a degree of dissipation of 50% (u_{50}). In order to determine t_{50}, dissipation tests must be taken to a pressure less than u_{50}. The u_{50} value is half way between the initial maximum pore pressure and the equilibrium pore pressure value, known as u_{100}. To estimate u_{50}, both the initial maximum pore pressure and u_{100} must be known or estimated. Other degrees of dissipations may be considered, particularly for extremely long dissipations.

At any specific degree of dissipation the equilibrium pore pressure (u at t_{100}) must be estimated at the depth of interest. The equilibrium value may be determined from one or more sources such as measuring the value directly (u_{100}), estimating it from other dissipations in the same profile, estimating the phreatic surface and assuming hydrostatic conditions, from nearby soundings, from client provided information, from site observations and/or past experience, or from other site instrumentation.

For calculations of c_h (Teh and Houlsby, 1991), t_{50} values are estimated from the corresponding pore pressure dissipation curve and a rigidity index (I_r) is assumed. For curves having an initial dilatory response in which an initial rise in pore pressure occurs before reaching a peak, the relative time from the peak value is used in determining t_{50}. In cases where the time to peak is excessive, t_{50} values are not calculated.

A summary of the pore pressure dissipation tests and dissipation plots are presented in the relevant appendix.

References

Teh, C.I., and Houlsby, G.T., 1991, “An analytical study of the cone penetration test in clay”, Geotechnique, 41(1): 17-34. DOI: 10.1680/geot.1991.41.1.17.

The electric field vane system is manufactured by Adara Systems Ltd., a subsidiary of ConeTec. An illustration of the uphole vane system configuration is presented in Figure eVST.

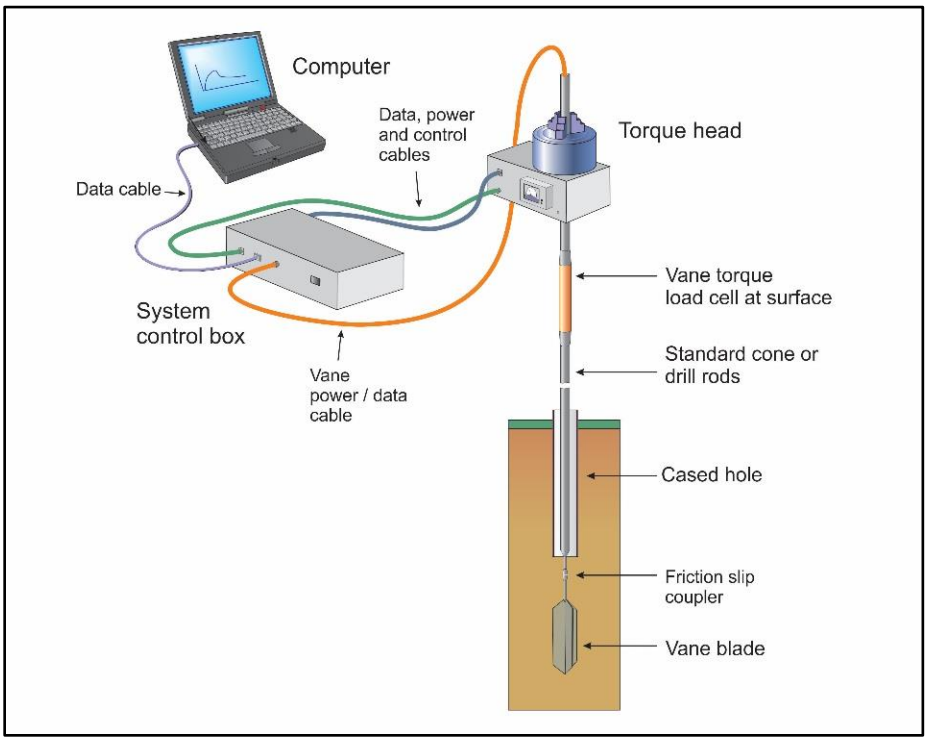


Figure eVST. Illustration of the uphole electric field vane system configuration

The vane system is designed with an array of strain gauges in a load cell that measure the applied torque. The torque signal is amplified and converted to digital data within the tool and transmitted to the data acquisition system through a shielded cable. The system uses a friction slip coupler to permit the free slip or play of approximately fifteen degrees between the rods and the vane blade in order to isolate and record rod friction from the soil before rotation of the vane blade starts. The system is designed to use vane blades of various sizes and configurations that connect to the friction slip coupler. The vane blades manufactured by Adara have dimensions and tolerances that are in general accordance with the current ASTM D2573 standards. In very soft soil conditions and at the request of the client, ConeTec may use a large diameter vane blade that exceeds the ASTM D2573 maximum size specifications in order to maximize torque resolution. In very stiff soil conditions and at the request of the client, ConeTec may use a smaller diameter vane blade than the minimum size specified in ASTM D2573 in order to obtain a peak torque below the capacity of the load cell.

The electric motor (capable of 100 Newton-meters of torque) is designed to clamp onto and rotate the rods and vane blade at a constant rate.

ConeTec's calibration criteria of the load cells are in accordance with the current ASTM D2573 standard.

The data acquisition system consists of a computer that records the vane data every 0.2 degrees of rotation. The system records the following parameters and saves them to a file as the test is conducted:

- Torque in Newton-meters
- Rotation in degrees
- Elapsed time in seconds (from the start of the test)

All testing is performed in accordance to ConeTec's field vane testing operating procedures and in general accordance with the current ASTM D2573 standard. For additional information on vane shear testing refer to Greig et al. (1987).

Prior to the start of a vane shear test profile, a suitable sized vane blade is selected, the vane system is powered on and the vane load cell baseline reading is recorded with the load cell hanging freely in a vertical position.

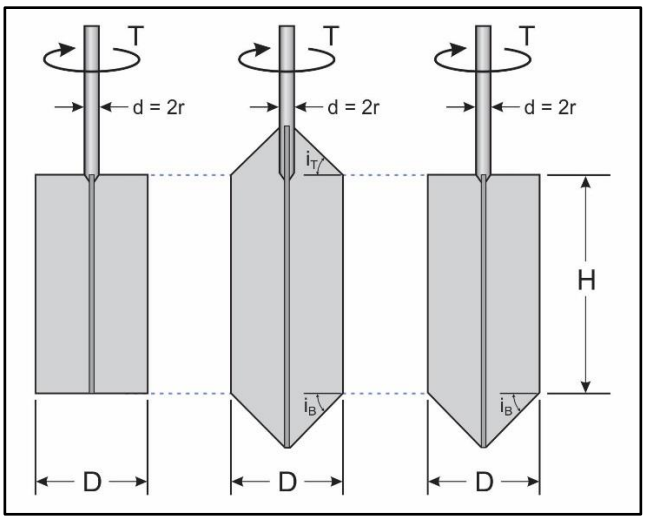
The vane blade, slip coupler and rods are advanced to the desired test depth through a cased hole, typically using AWJ drill rods or one-meter length rods with an outer diameter of 1.5 inches (38.1 millimeters). Test depths are referenced to the middle of the rectangular portion of the vane blade. The motor rotates the rods at a near constant rate up to and beyond the yield stress (peak) until the load remains near constant (post peak). Following post peak readings, the vane blade is then rapidly rotated clockwise ten times to completely remold the soil. The test procedure is repeated in order to record the remolded strength of the soil. The vane blade is then advanced to the next depth and the procedure is repeated or the vane blade is retracted to allow for drilling and vane blade size changes. Once the vane profile is complete, the final baseline of the load cell is recorded and compared to previous reading as a QA/QC check.

Undrained shear strength from the field vane, $(S_u)_{fv}$, is calculated from torque measurements using the following general equation (ASTM D2573) taking into consideration the case of rectangular or tapered ends at the top and/or bottom of the vane blade.

$$(S_u)_{fv} = \frac{12 \cdot T_{max}}{\pi D^2 \left(\frac{D}{\cos(i_T)} + \frac{D}{\cos(i_B)} + 6H \right)}$$

where:

$(S_u)_{fv}$	=	undrained shear strength from the field vane
T_{max}	=	maximum value of torque
D	=	vane diameter
H	=	height of the rectangular portion of the vane
i_T	=	angle of taper at vane top (with respect to horizontal)
i_B	=	angle of taper at vane bottom (with respect to horizontal)



For rectangular vane blades where H/D = 2, the above equation simplifies to:

$$(S_u)_{fv} = \frac{6 \cdot T_{max}}{7\pi D^3}$$

The recorded rod friction is subtracted from the peak and remolded torque. No correction factors are applied to the vane results to derive the mobilized shear strength ($\tau_{mobilized}$).

A summary of the vane shear tests, a table of results and individual VST plots are provided in the relevant appendices. Tabular data in Excel format is provided in the data release folder.

References

ASTM D2573 / D2573M-18, 2018, "Standard Test Method for Field Vane Shear Test in Saturated Fine-Grained Soils", ASTM International, West Conshohocken, PA. DOI: 10.1520/D2573_D2573M-18.

Greig, J.W., R.G. Campanella and P.K. Robertson, 1987, "Comparison of Field Vane Results With Other In-Situ Test Results", International Symposium on Laboratory and Field Vane Shear Strength Testing, ASTM, Tampa, FL, Proceedings.

The appendices listed below are included in the report:

- Cone Penetration Test Summary and Standard Cone Penetration Test Plots
- Standard Cone Penetration Test Plots with Expanded Range
- Advanced Cone Penetration Test Plots
- Seismic Cone Penetration Test Plots
- Seismic Cone Penetration Test Shear Wave (Vs) Tabular Results
- Seismic Cone Penetration Test Shear Wave (Vs) Traces
- Seismic Cone Penetration Test Compression Wave (Vp) Tabular Results
- Seismic Cone Penetration Test Compression Wave (Vp) Traces
- Seismic Cone Penetration Test Poisson's Ratio Tabular Results
- Soil Behaviour Type (SBT) Scatter Plots
- Pore Pressure Dissipation Summary and Pore Pressure Dissipation Plots
- Description of Methods for Calculated CPT Geotechnical Parameters
- Electric field Vane Shear Test Summary, Results and Timing
- Electric Field Vane Shear Test Plots

Cone Penetration Test Summary and Standard Cone Penetration Test Plots

CONETEC

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Start Date:	2024-02-14
End Date:	2024-03-22

CONE PENETRATION TEST SUMMARY

Sounding ID	File Name	Date From	Date To	Rig	Cone	Cone Area (cm^2)	Assumed Phreatic Surface[1] (m)	Final Depth (m)	Northing[2] (m)	Easting[2] (m)	Refer to Notation Number
SCPT24-LGE-BH201	24-05-27159_SP201	2024-02-19	2024-02-20	M5TII	958:T1500F15U35	15	2.9	10.025	5407391	474842	
SCPT24-LGE-BH201B	24-05-27159_SP201B	2024-02-20	2024-02-20	M5TII	958:T1500F15U35	15		3.000	5407392	474842	5, 6
SCPT24-LGE-BH202	24-05-27159_SP202	2024-02-16	2024-02-16	M5TII	958:T1500F15U35	15	1.2	4.900	5408601	475374	3
SCPT24-LGE-BH202B	24-05-27159_SP202B	2024-02-17	2024-02-17	M5TII	958:T1500F15U35	15	1.3	5.250	5408594	475372	3, 6
SCPT24-LGE-BH203	24-05-27159_SP203	2024-02-14	2024-02-16	M5TII	958:T1500F15U35	15	3.2	29.250	5409174	476455	3
SCPT24-LGE-BH204	24-05-27159_SP204	2024-02-18	2024-02-19	M5TII	958:T1500F15U35	15	2.7	15.525	5407351	475669	
SCPT24-LGE-BH205	24-05-27159_SP205	2024-02-26	2024-02-27	M5TII	958:T1500F15U35	15	3.2	26.725	5408416	476456	
SCPT24-TMF-MW03AB	24-05-27159_SPTMF03AB	2024-03-13	2024-03-13	M5TII	958:T1500F15U35	15	1.2	2.425	5414676	472128	
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	2024-03-20	2024-03-22	Portable	762:T1500F15U35	15	0.0	34.525	5401992	476468	
SCPT24-TMF-BH202	24-05-27159_SPTMF202	2024-03-15	2024-03-16	Portable	762:T1500F15U35	15	0.0	29.000	5404211	476818	7
SCPT24-TMF-BH207	24-05-27159_SPTMF207	2024-03-18	2024-03-20	Portable	762:T1500F15U35	15	0.0	24.200	5402798	476813	
SCPT24-WRD-BH201	24-05-27159_SPWRD201	2024-03-01	2024-03-02	M5TII	958:T1500F15U35	15	4.0	23.125	5411103	473341	3
SCPT24-WRD-BH202	24-05-27159_SPWRD202	2024-03-04	2024-03-05	M5TII	958:T1500F15U35	15	0.0	18.950	5412168	474136	
SCPT24-WRD-BH205	24-05-27159_SPWRD205	2024-03-08	2024-03-08	M5TII	958:T1500F15U35	15	0.0	7.725	5413526	474146	
SCPT24-WRD-BH205B	24-05-27159_SPWRD205B	2024-03-08	2024-03-08	M5TII	958:T1500F15U35	15	0.0	7.650	5413524	474147	8
CPT24-WRD-BH207	24-05-27159_CPWRD207	2024-03-12	2024-03-12	M5TII	958:T1500F15U35	15	0.4	6.425	5414555	474237	4
SCPT24-WRD-BH207	24-05-27159_SPWRD207	2024-03-11	2024-03-11	M5TII	958:T1500F15U35	15	0.4	6.250	5414553	474239	
SCPT24-WRD-BH212	24-05-27159_SPWRD212	2024-03-03	2024-03-03	M5TII	958:T1500F15U35	15	2.7	15.000	5411072	474212	

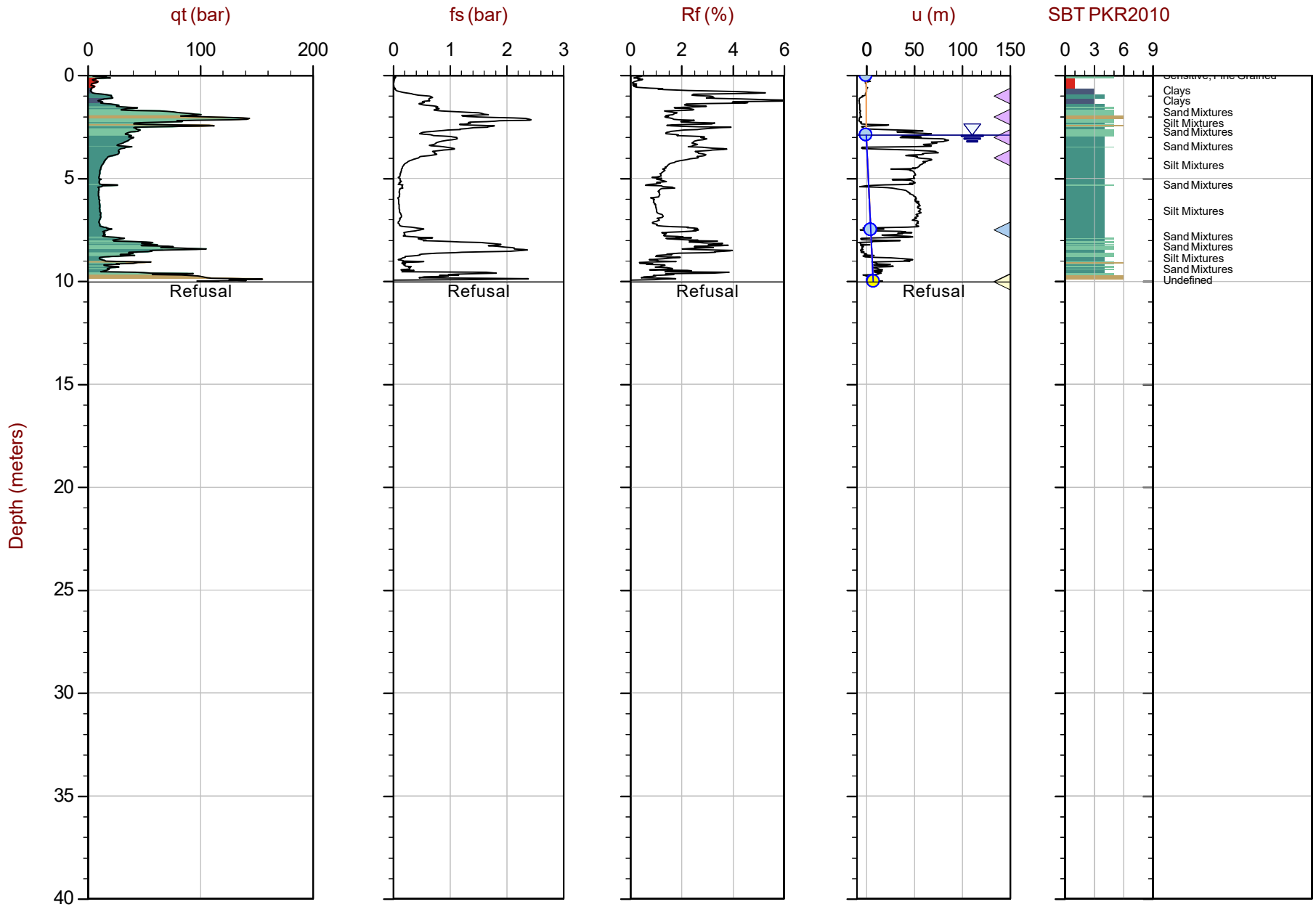
1. The assumed phreatic surface was based on pore pressure dissipation tests, unless otherwise noted. Equilibrium pore pressure profiles were used for the calculated parameters.
2. Coordinates were collected with a consumer grade GPS device with datum WGS84/UTM Zone 17 North.
3. The assumed phreatic surface was based on the dynamic pore pressure response.
4. The assumed phreatic surface was based on the adjacent CPT sounding.
5. No clear phreatic surface was detected.
6. No seismic data due to early refusal. Seismic data collected on the initial sounding.
7. No data recorded from 0.000 m to 0.400 m due to an equipment issue.
8. No p-wave data reported due to poor signal quality.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 10.025 m / 32.89 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT '10)
Coords: UTM 17N N: 5407391m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

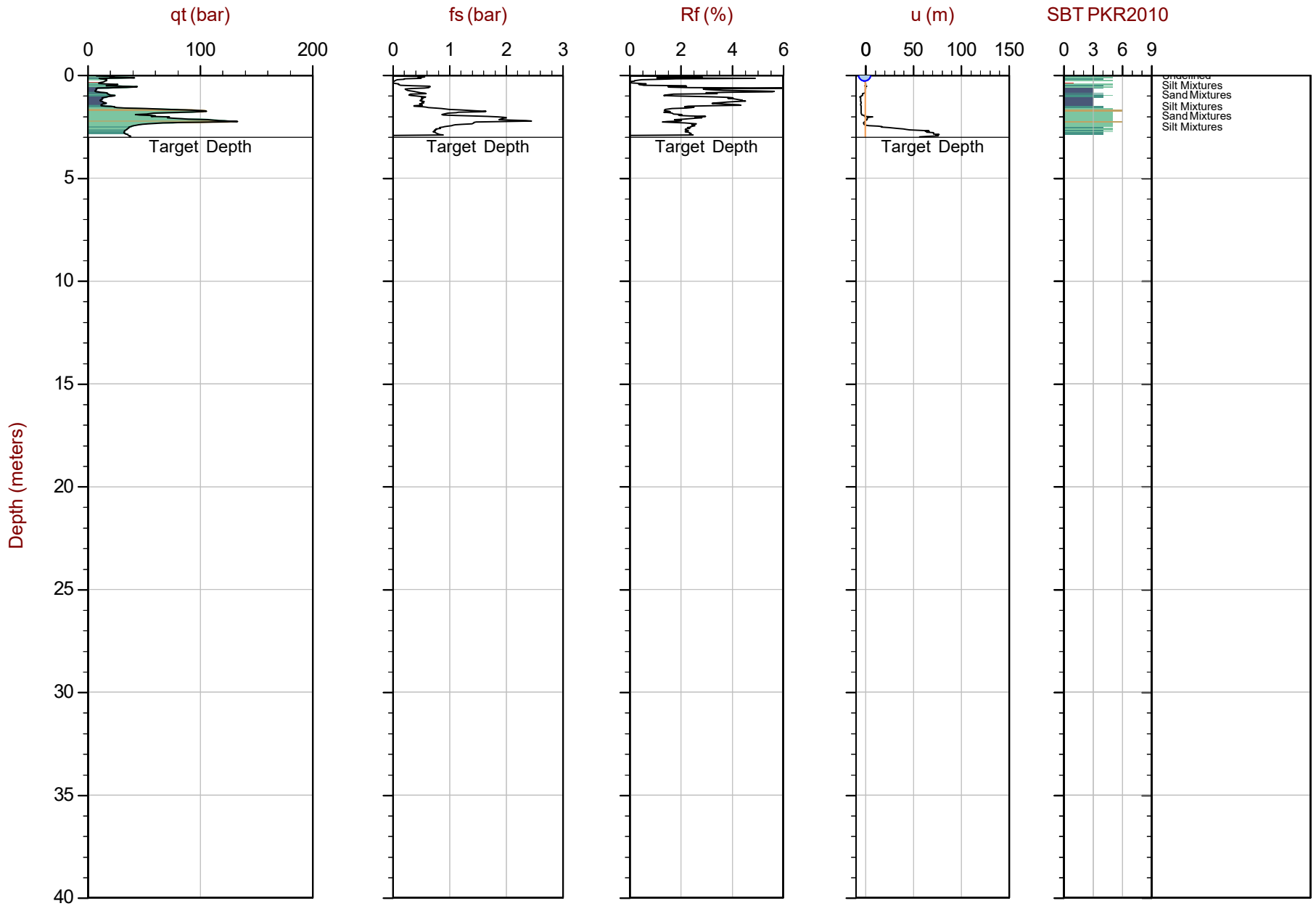
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-20 13:25
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 3.000 m / 9.84 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407392m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved Dissipation, Ueq assumed Ueq Line Hydrostatic Line

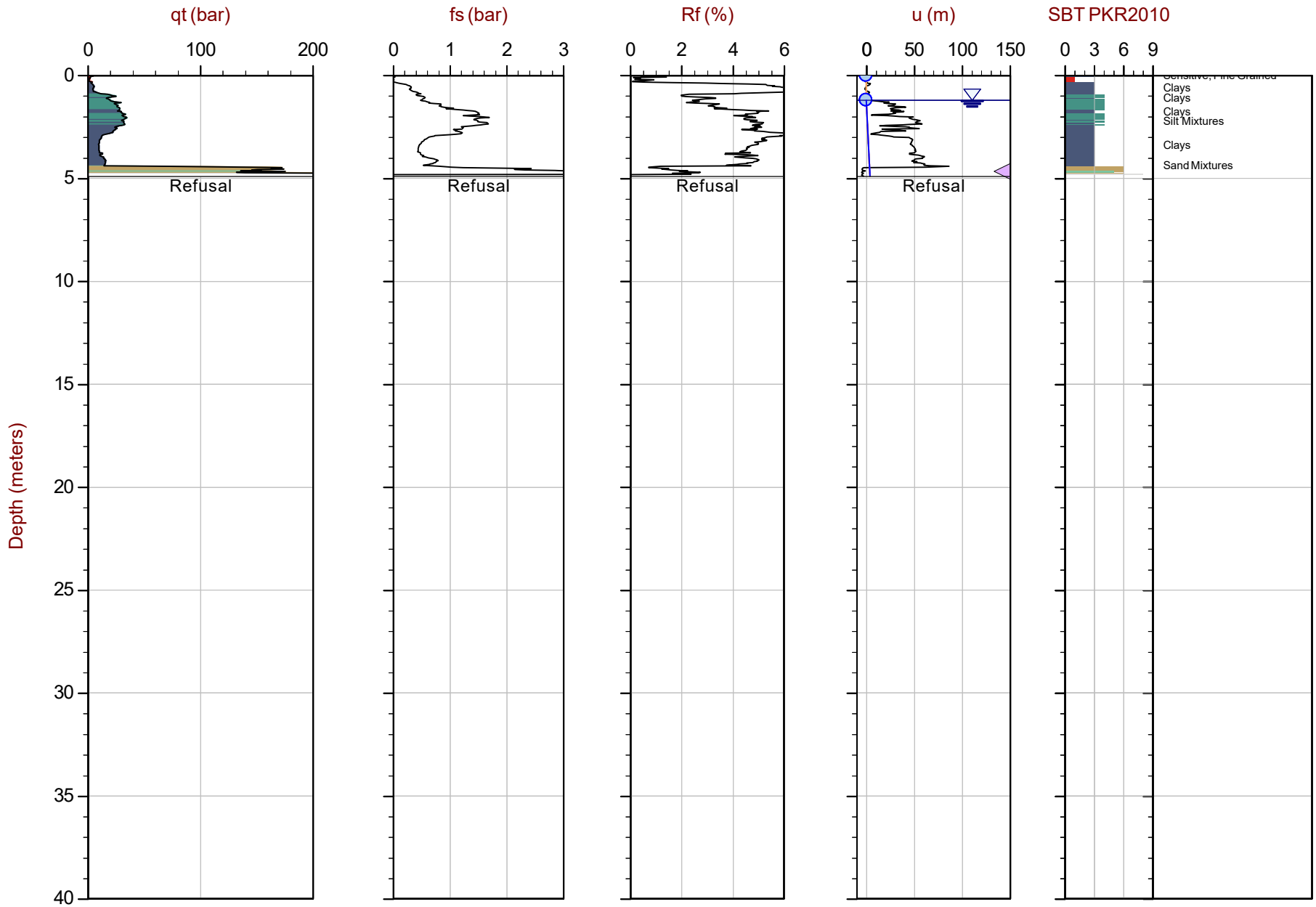
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-16 14:19
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 4.900 m / 16.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408601m E: 475374m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

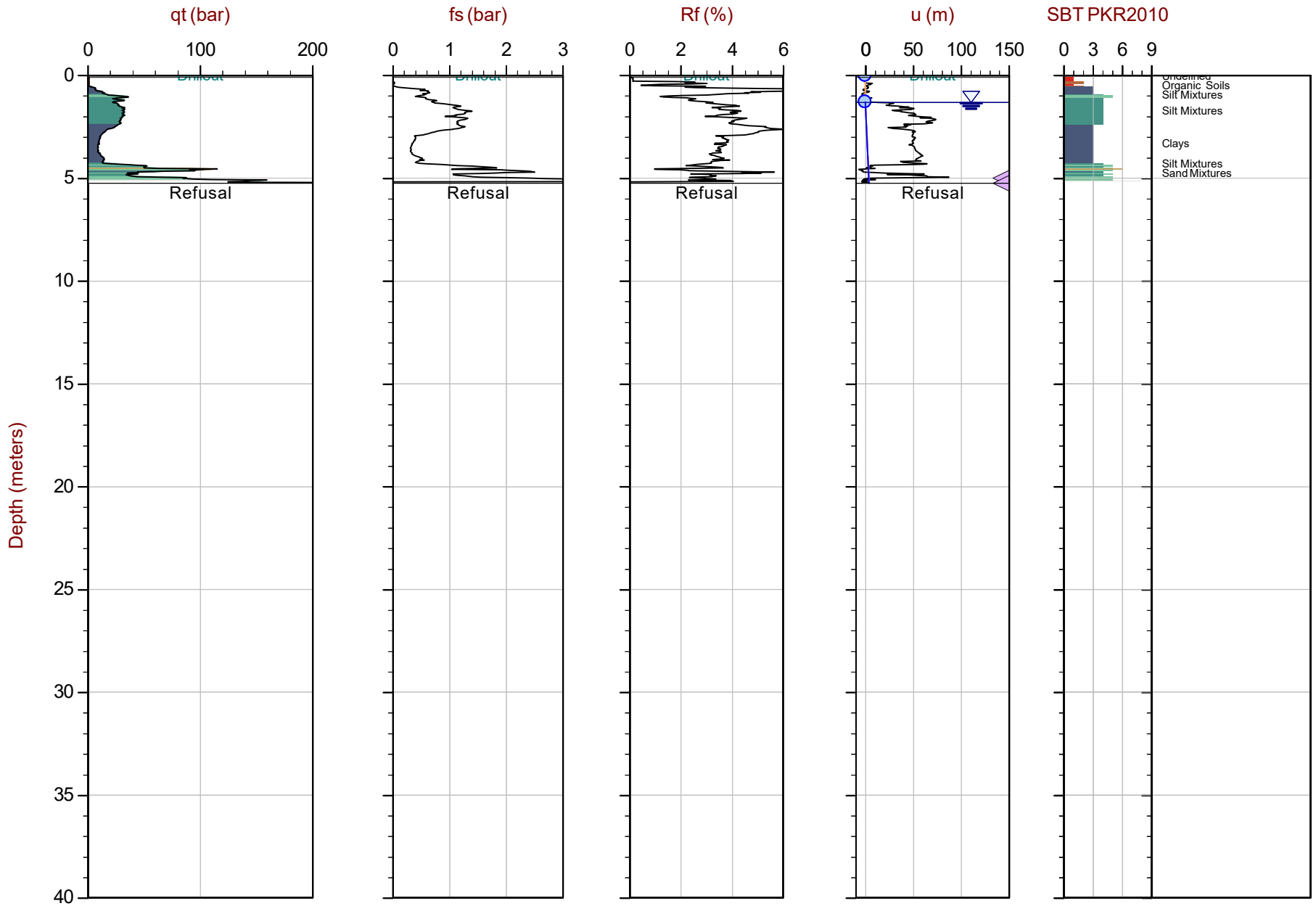
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-17 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 5.250 m / 17.22 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408594m E: 475372m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

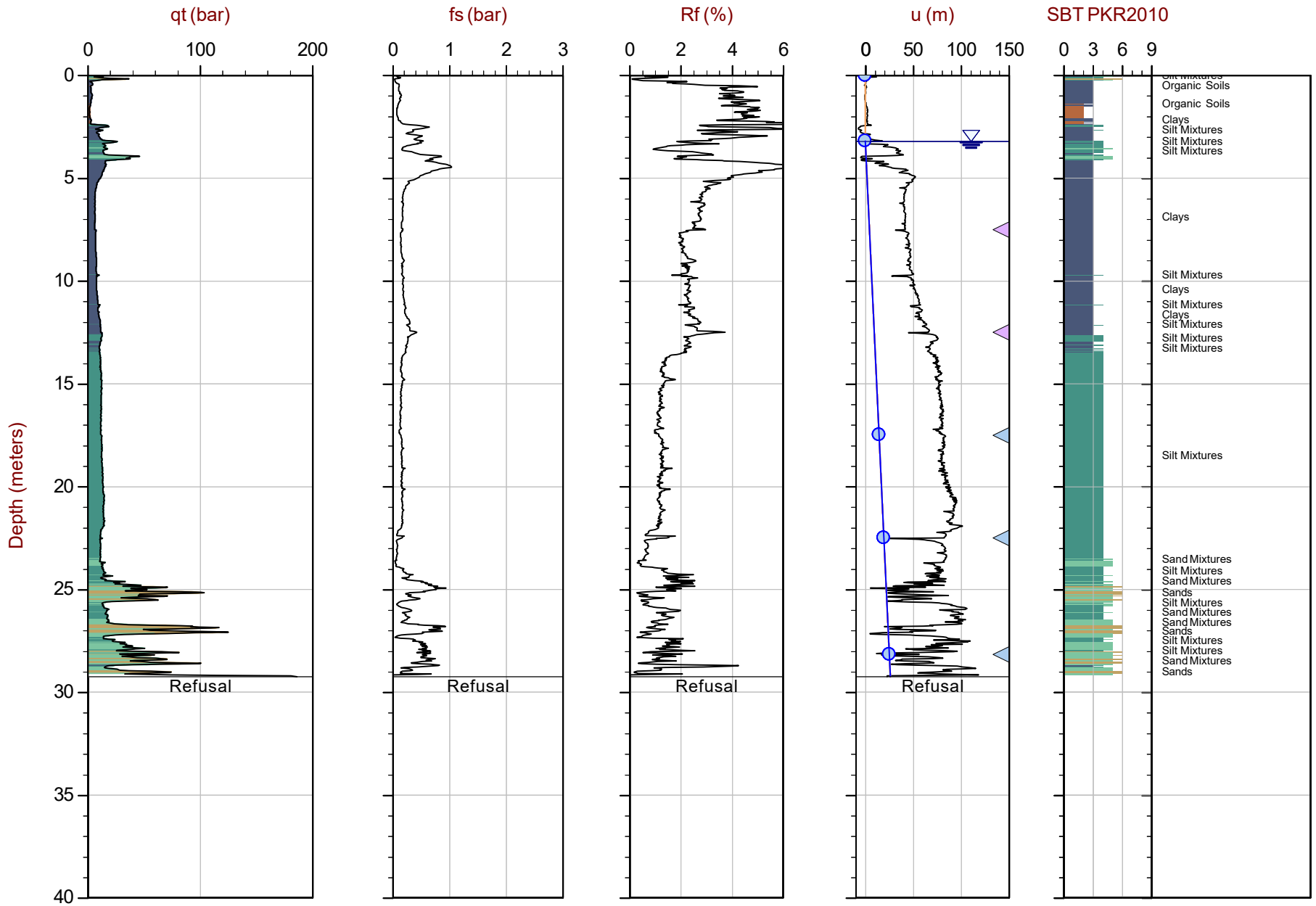
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 29.250 m / 95.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP203.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5409174m E: 476455m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

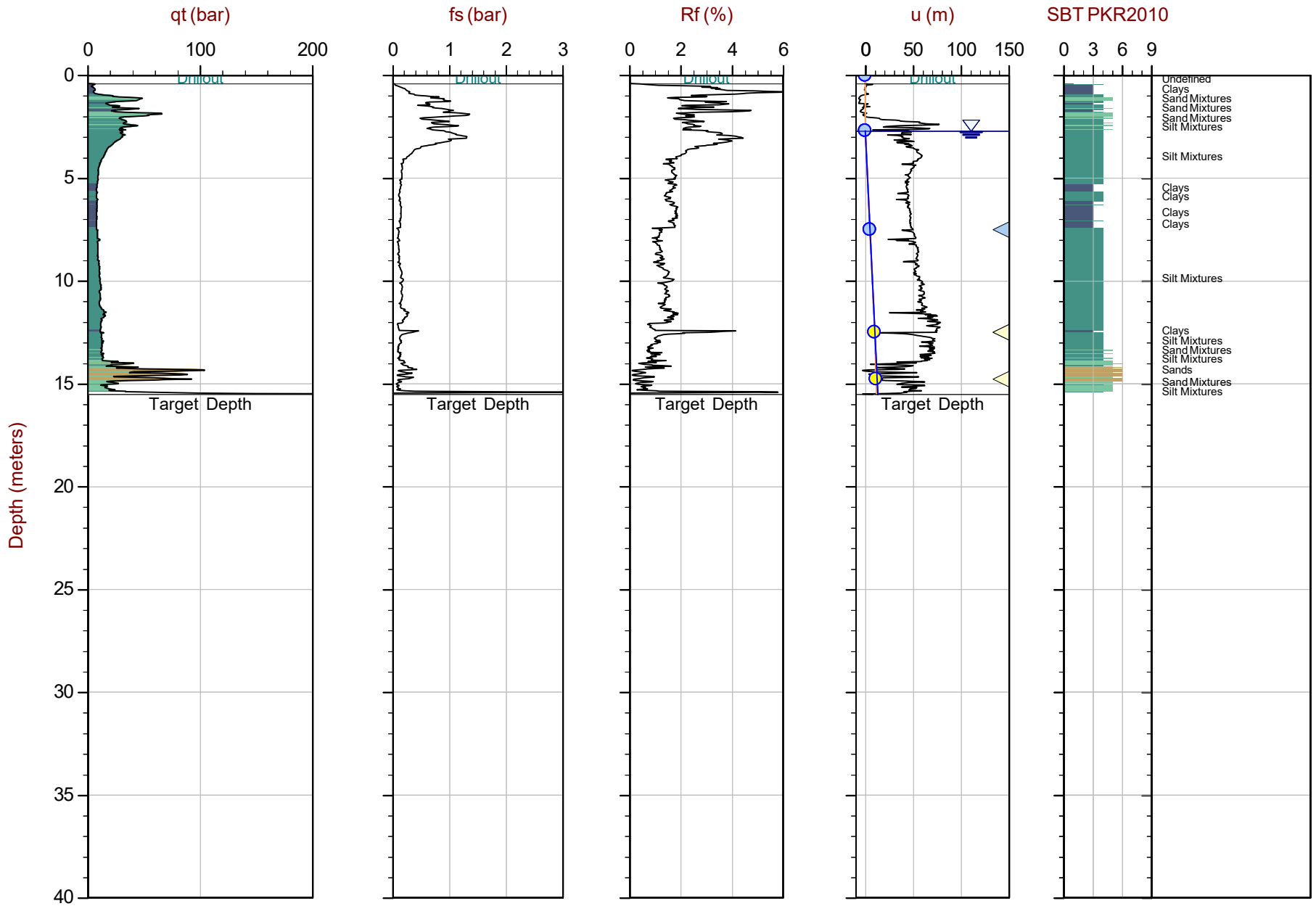
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.525 m / 50.93 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP204.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407351m E: 475669m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

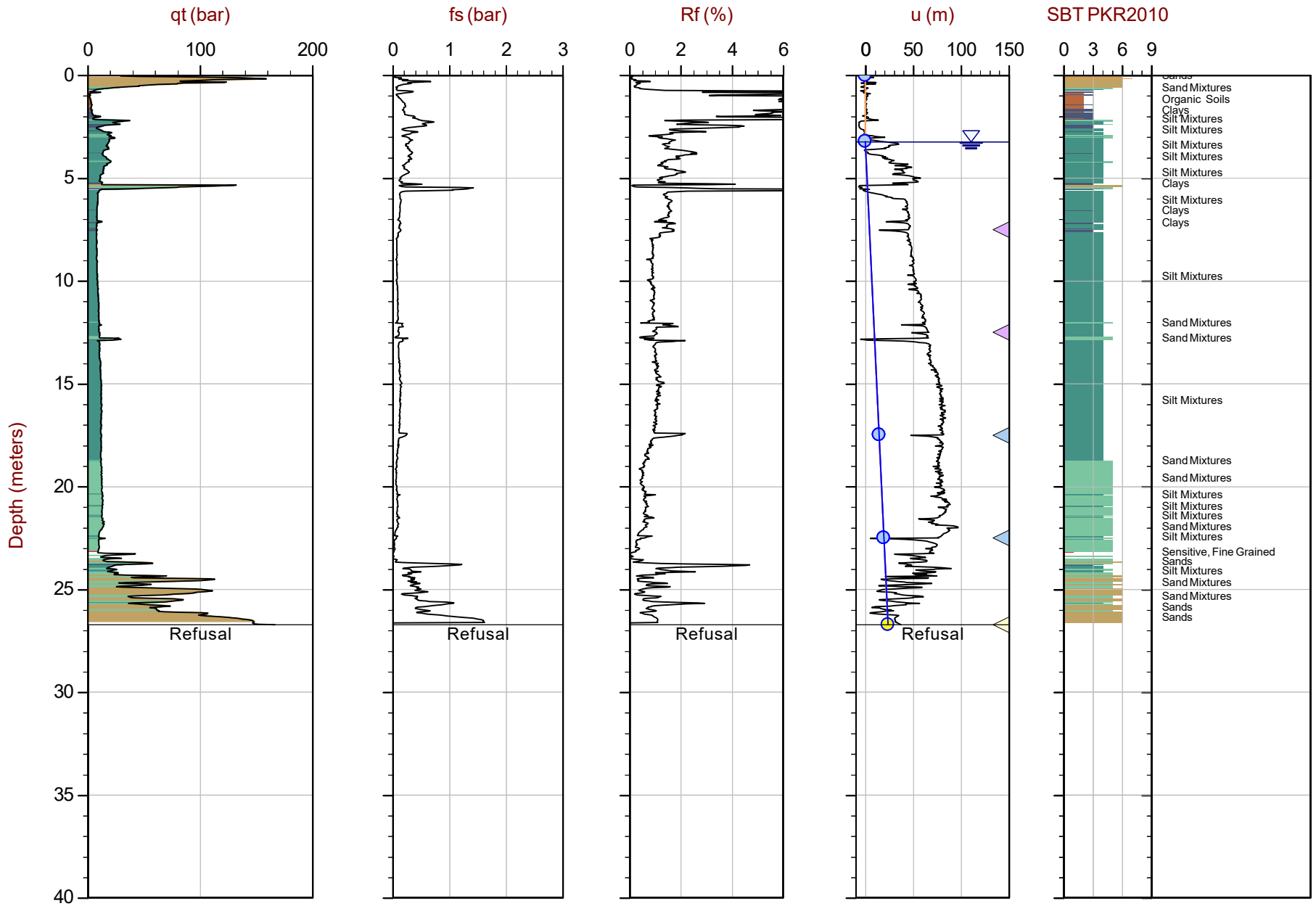
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 26.725 m / 87.68 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP205.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT '10)
Coords: UTM 17N N: 5408416m E: 476456m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

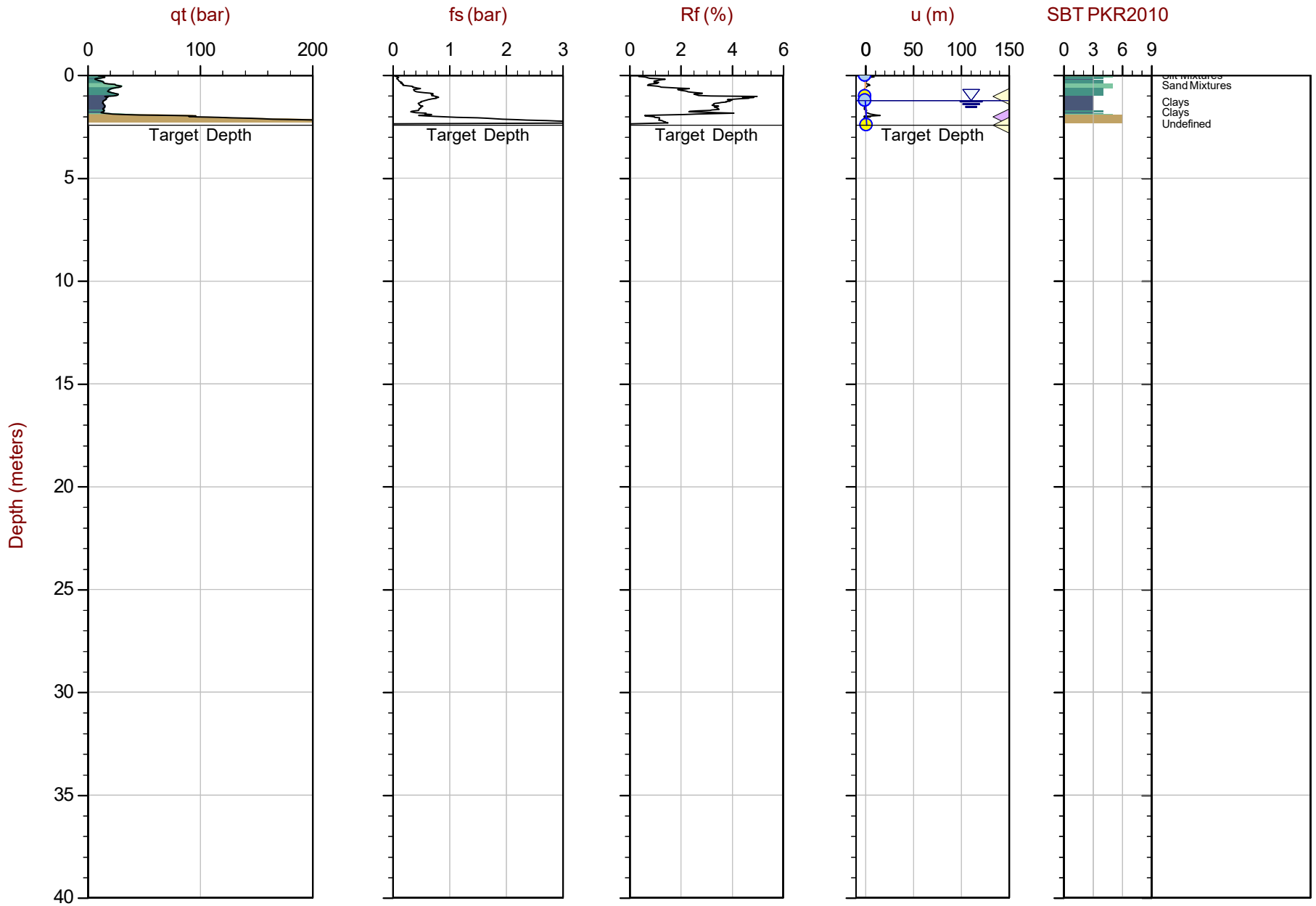
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 2.425 m / 7.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF03AB.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414676m E: 472128m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

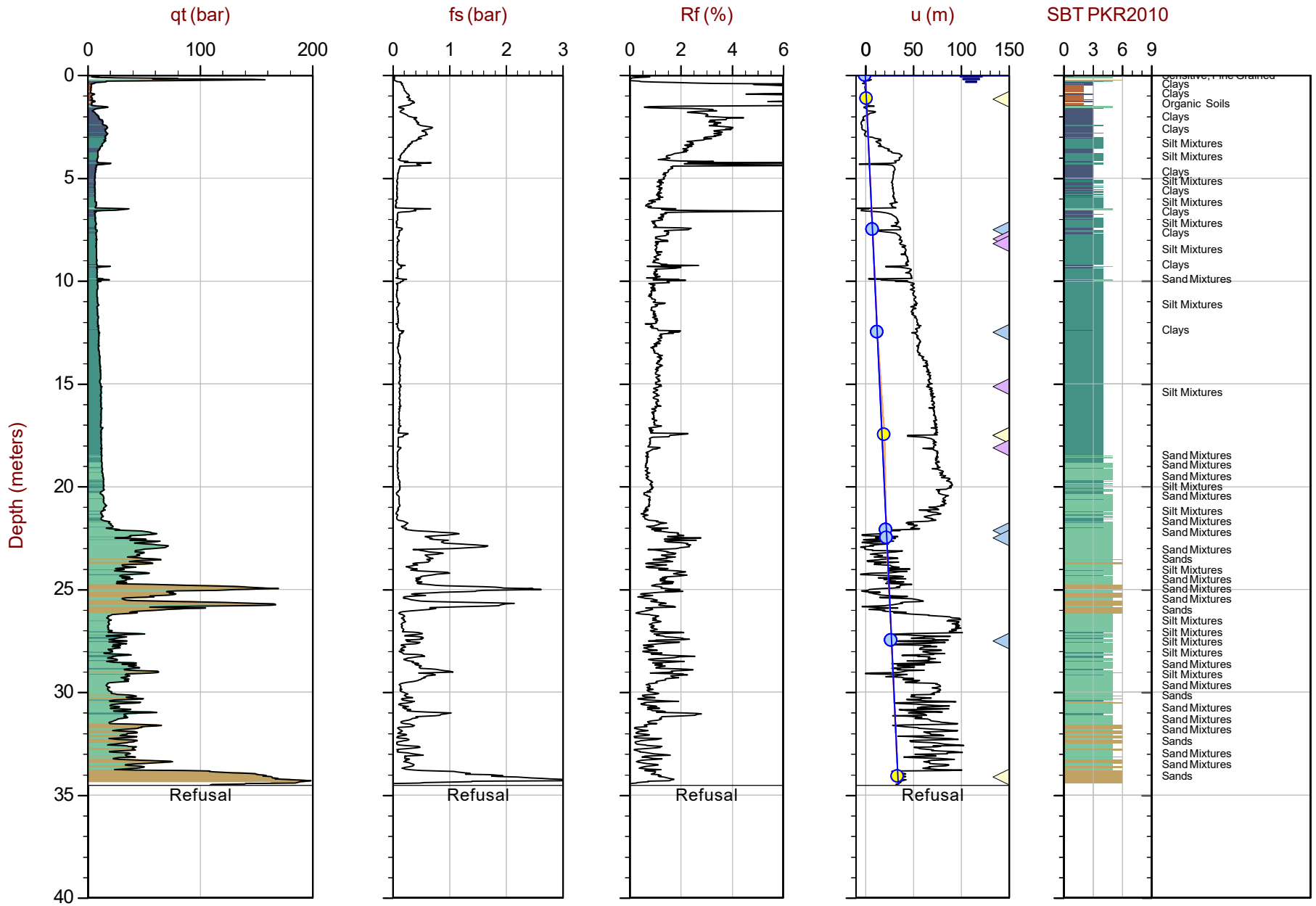
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 34.525 m / 113.27 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF08AB.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5401992m E: 476468m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

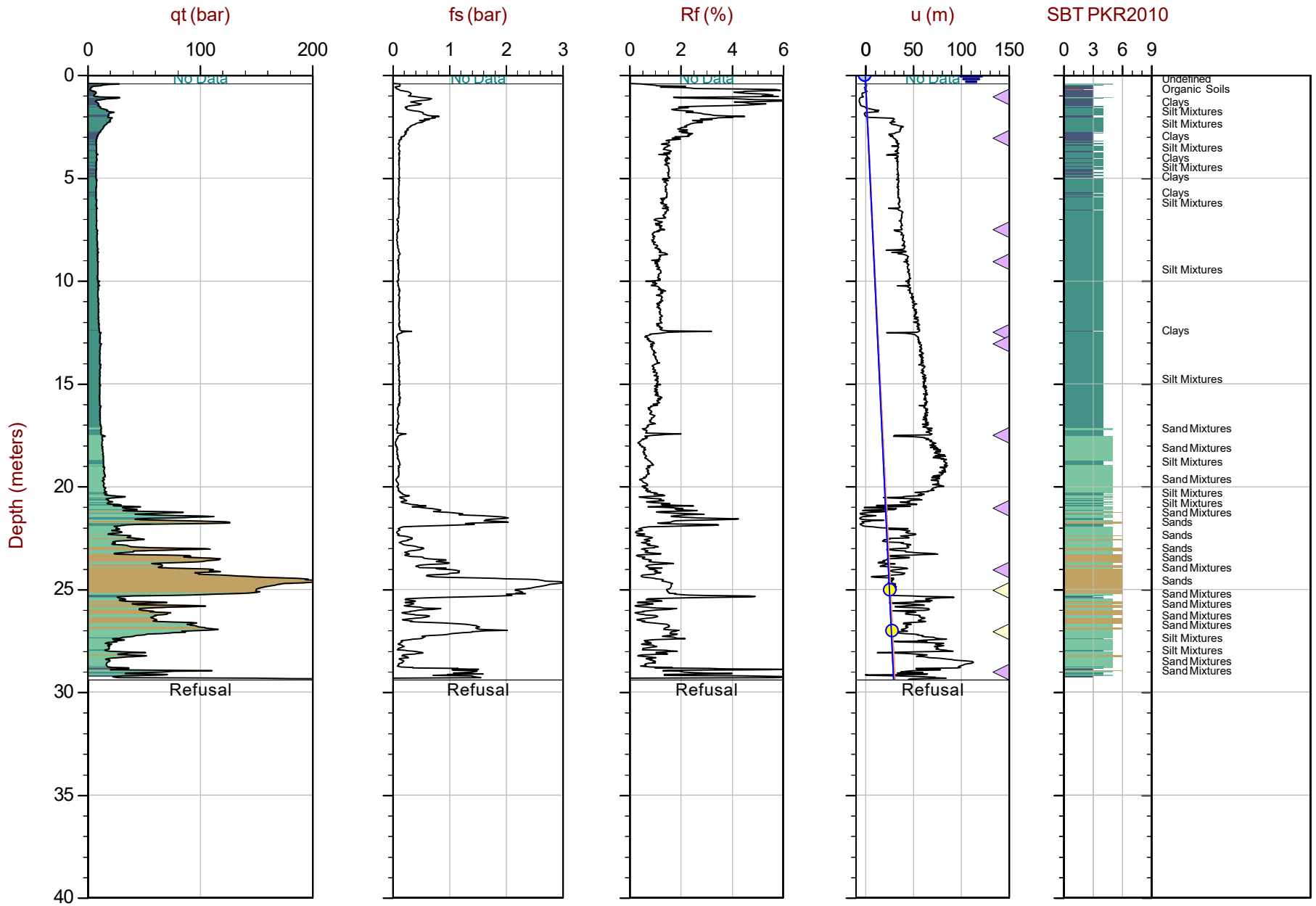
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 29.400 m / 96.46 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5404211m E: 476818m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

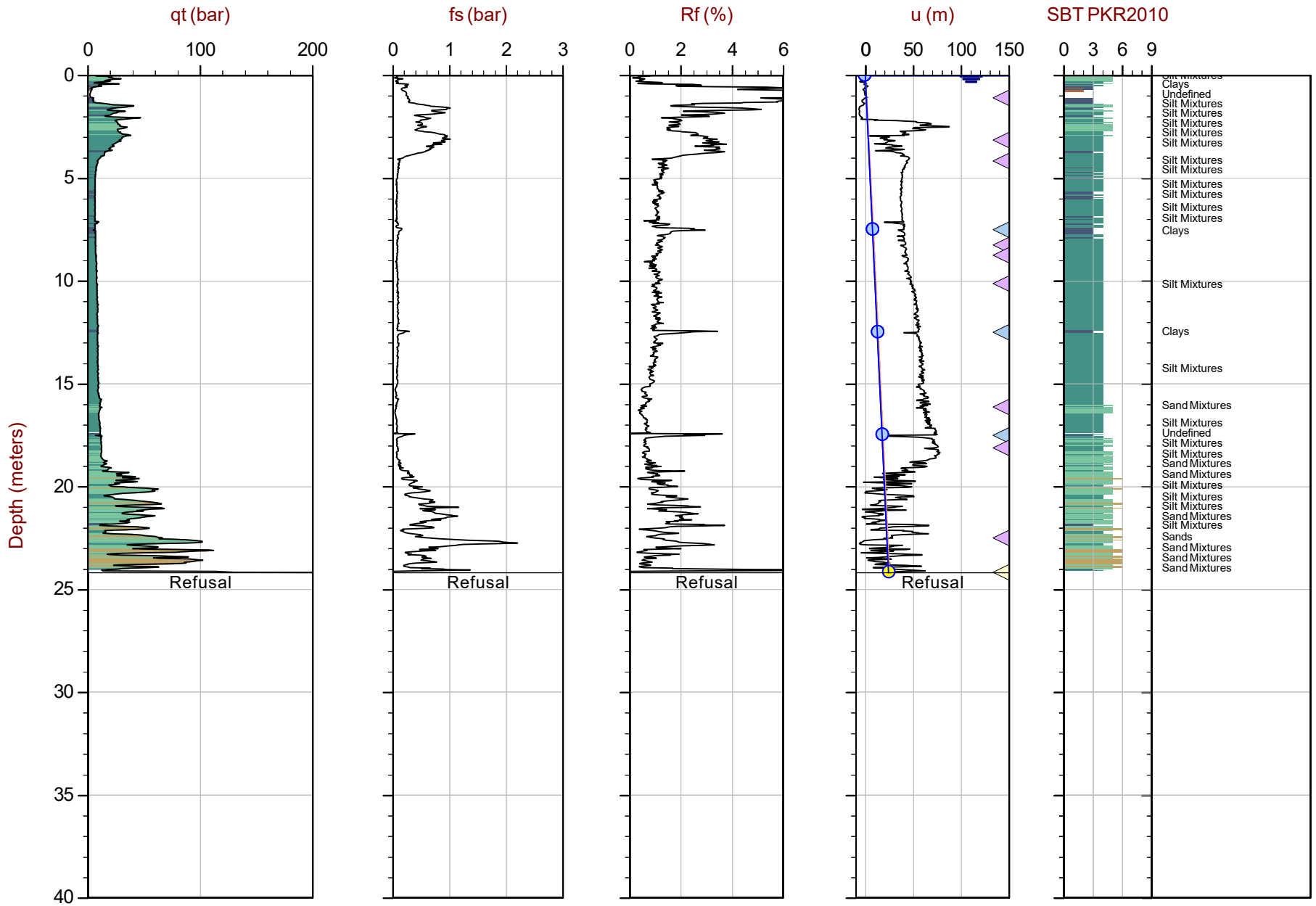
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 24.200 m / 79.40 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5402798m E: 476813m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

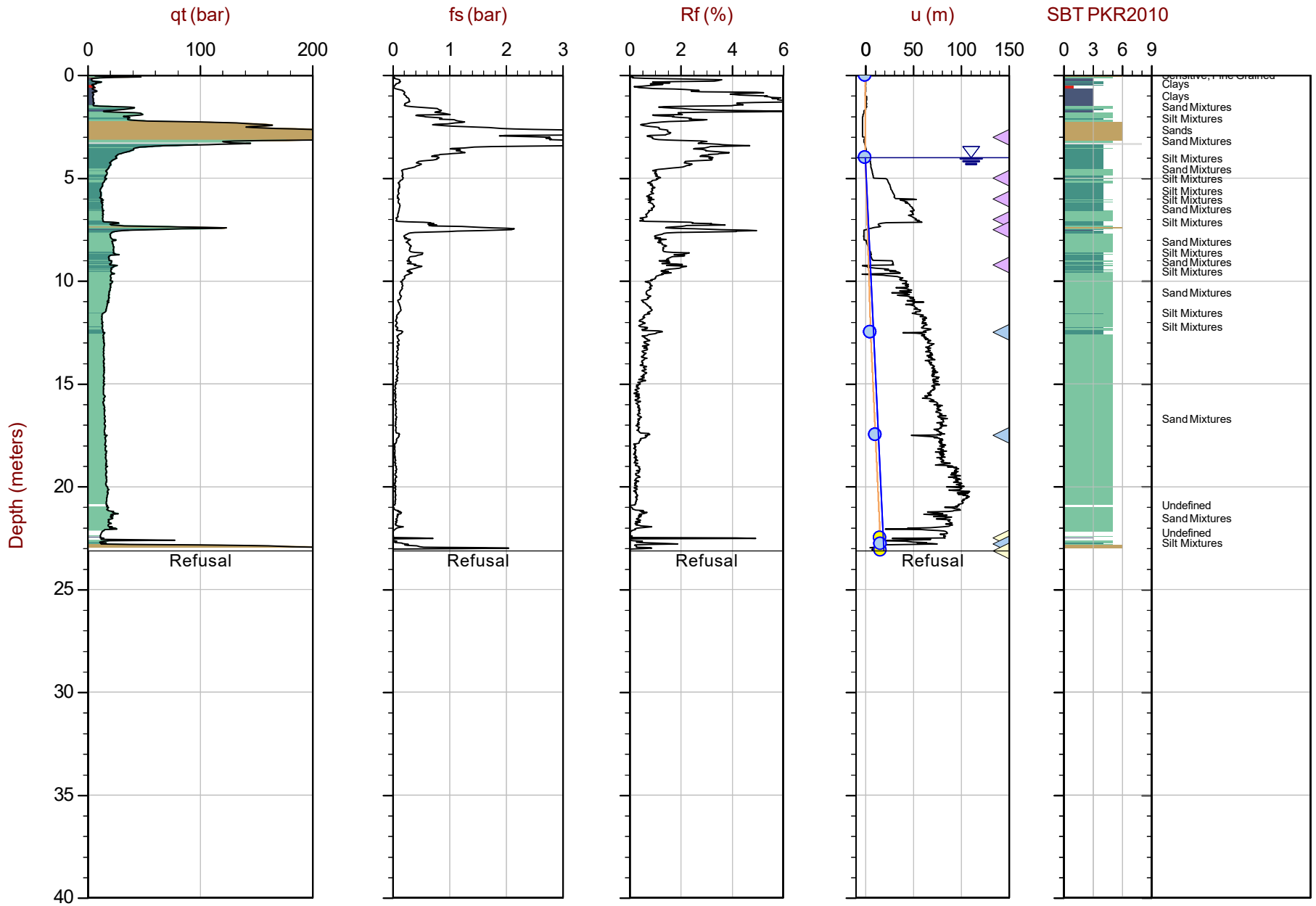
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 23.125 m / 75.87 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD201.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411103m E: 473341m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

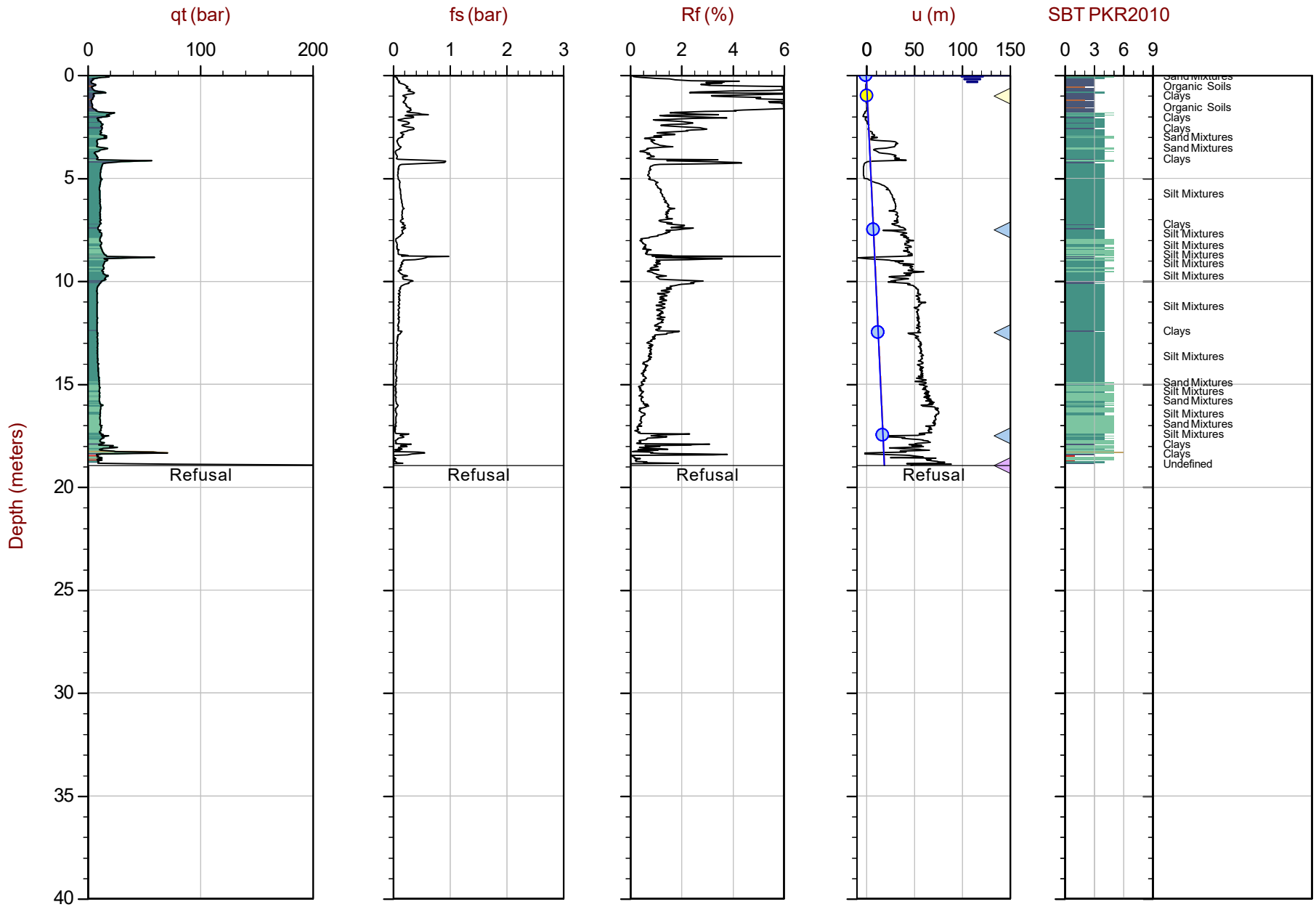
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 18.950 m / 62.17 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5412168m E: 474136m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

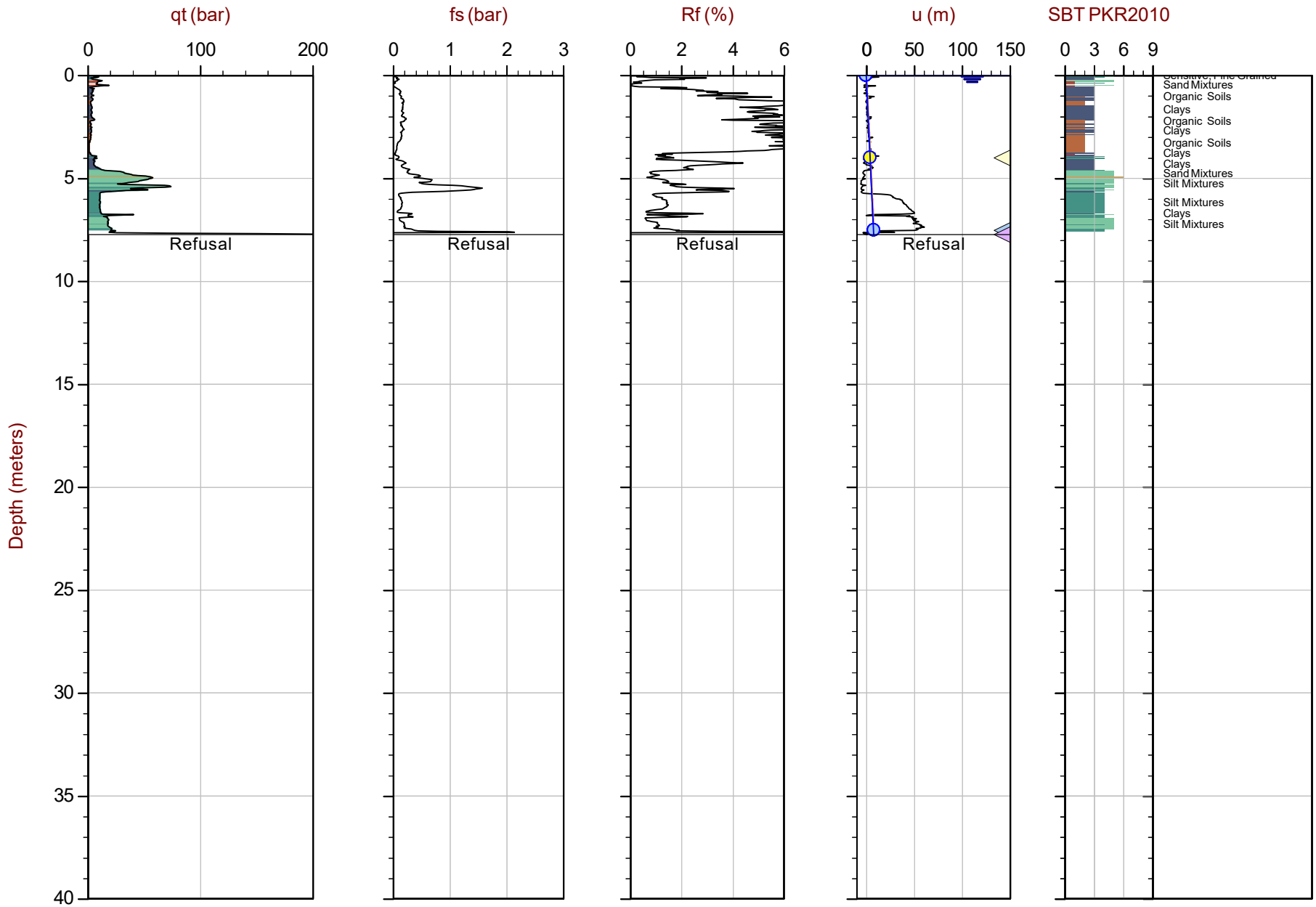
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.725 m / 25.34 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413526m E: 474146m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

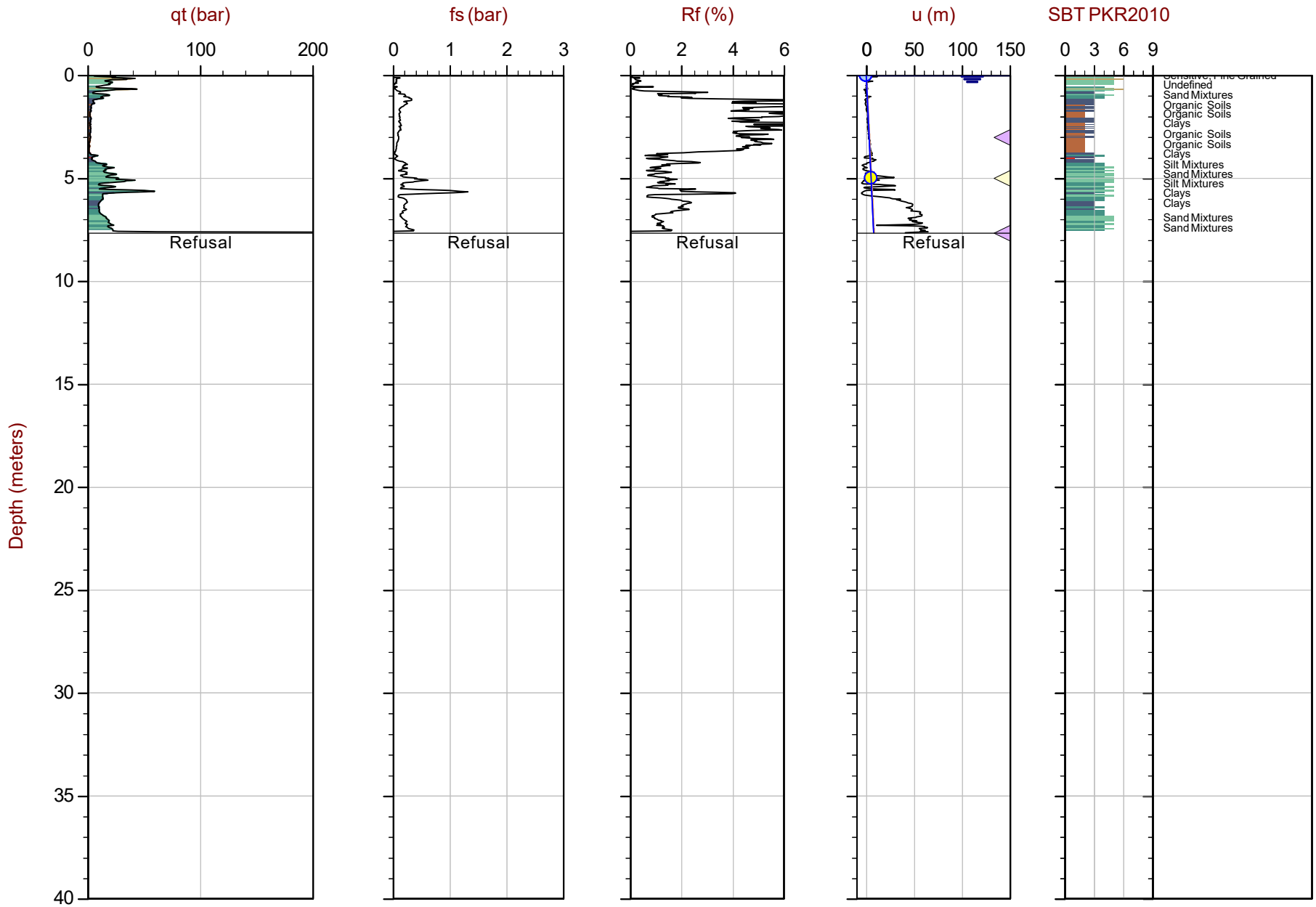
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.650 m / 25.10 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413524m E: 474147m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

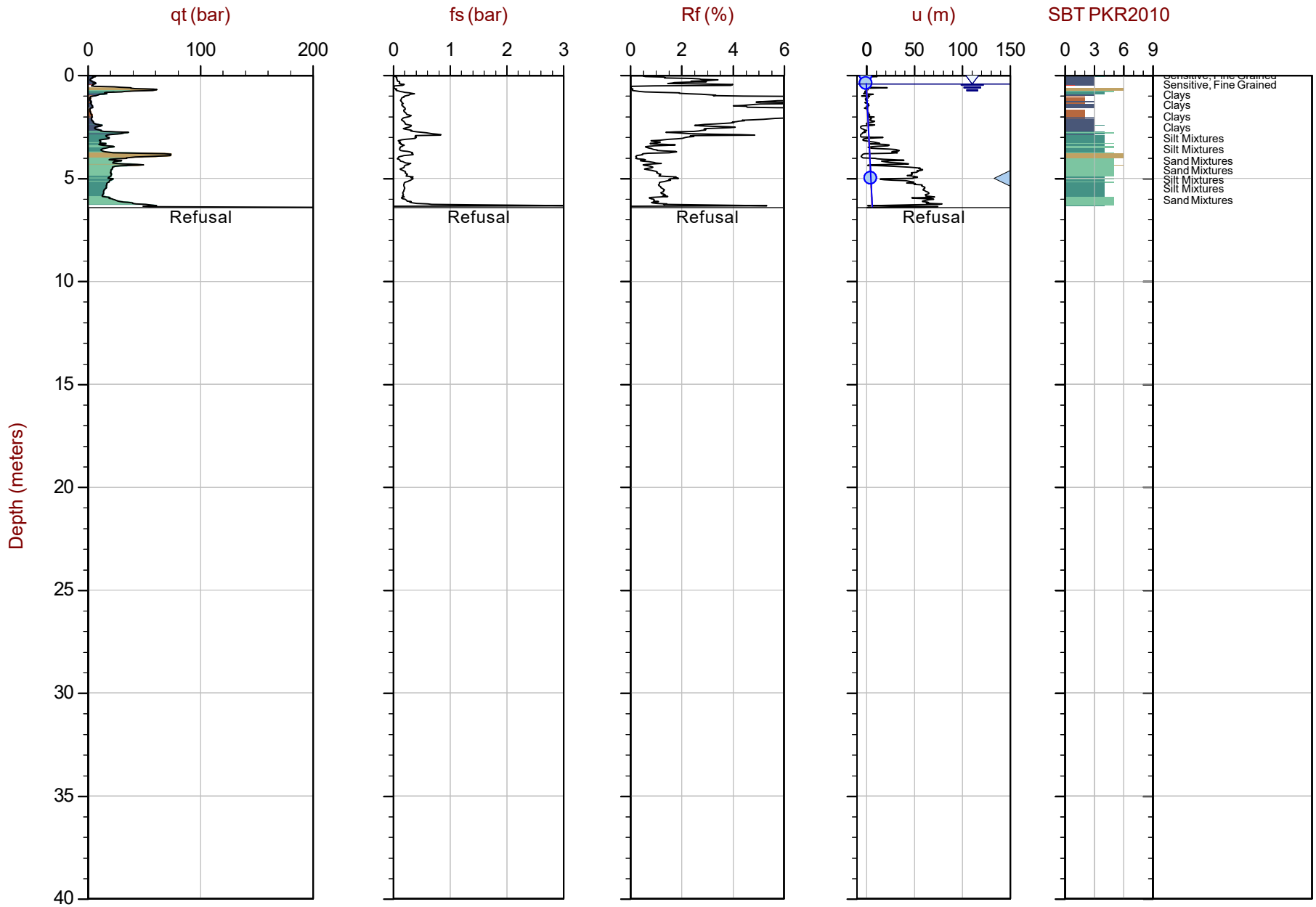
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-12 09:14
Site: Crawford Mine - SRK

Sounding: CPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.425 m / 21.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_CPWRD207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414555m E: 474237m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

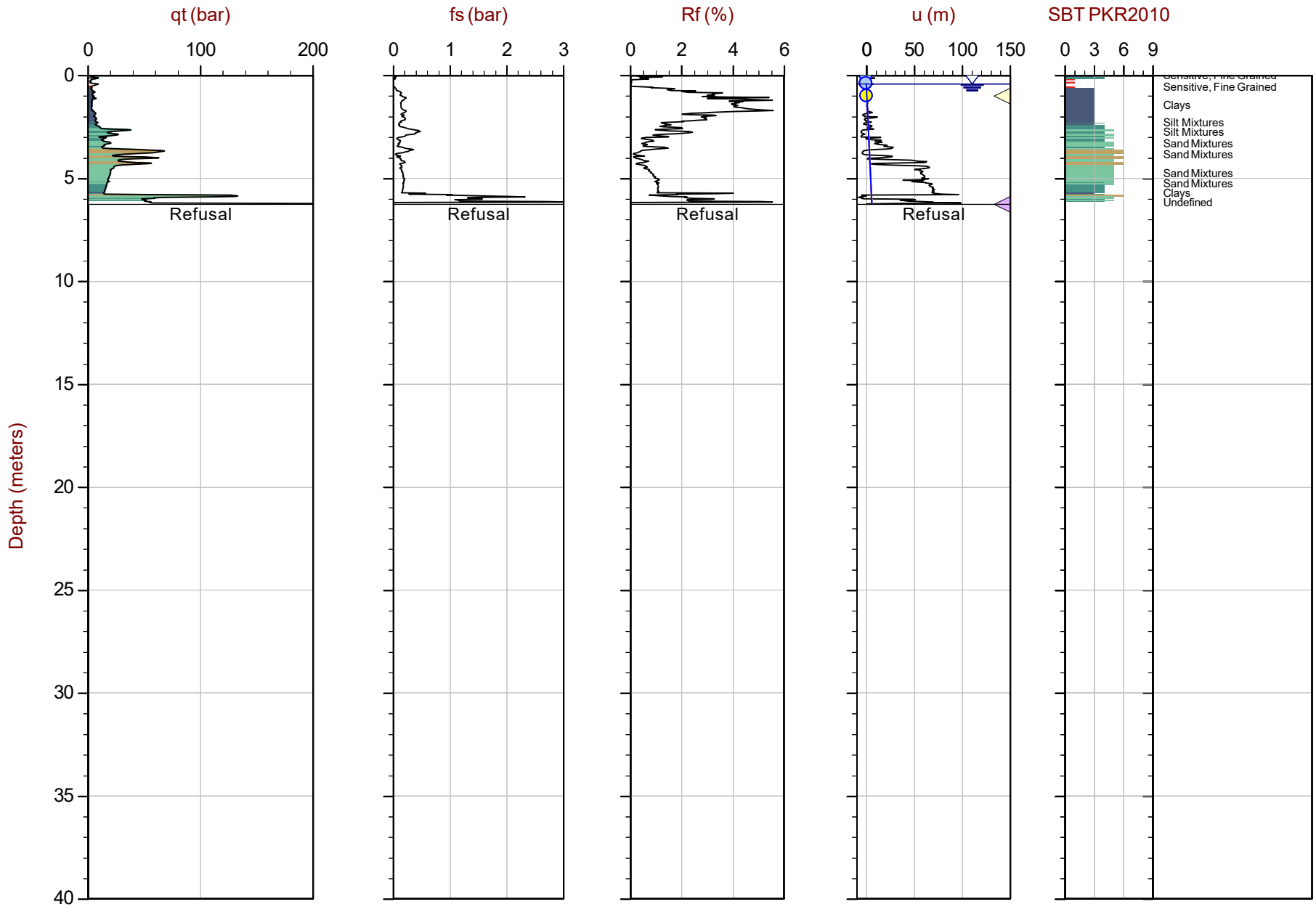
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.250 m / 20.51 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414553m E: 474239m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

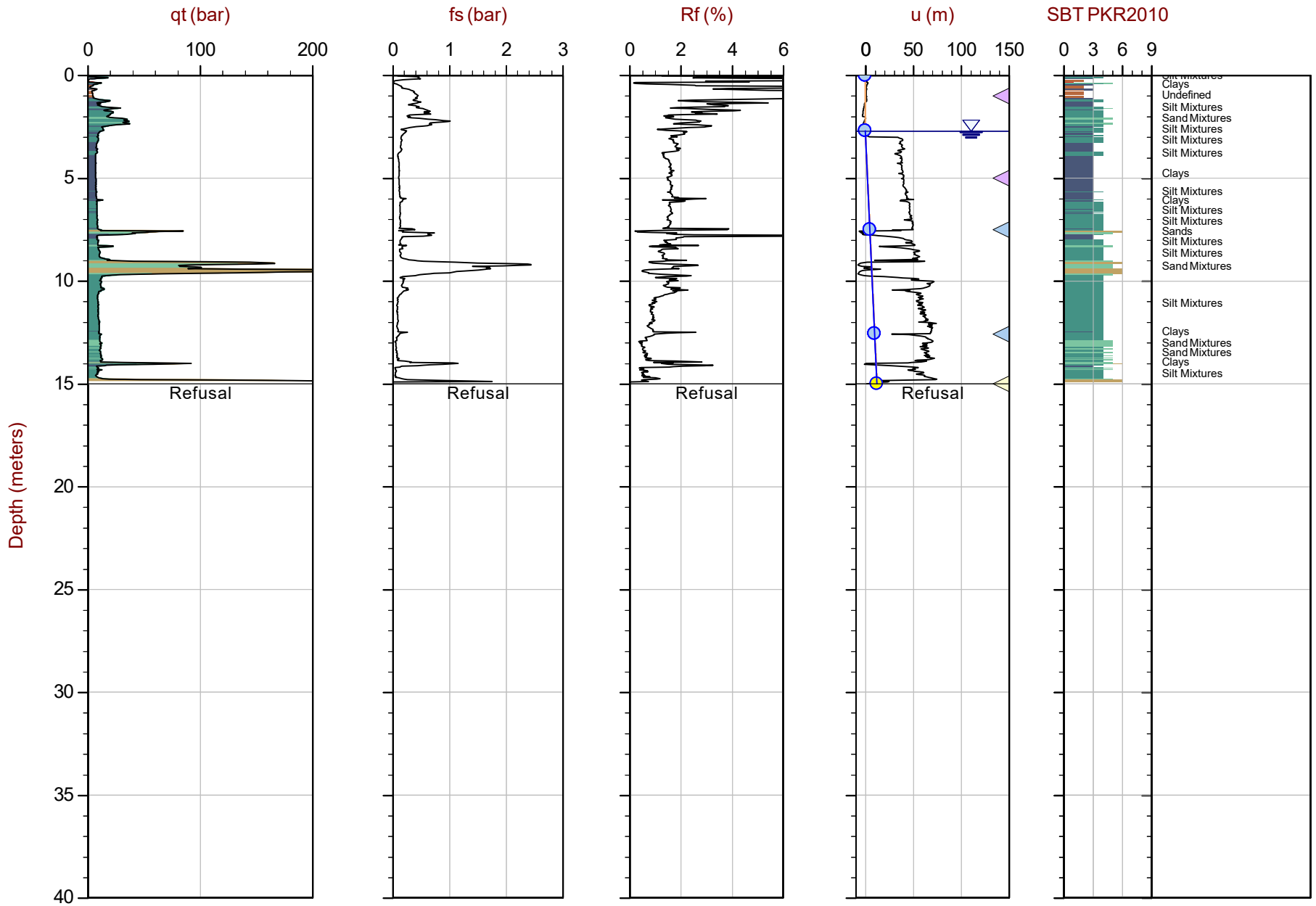
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.000 m / 49.21 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD212.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411072m E: 474212m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Standard Cone Penetration Test Plots with Expanded Range

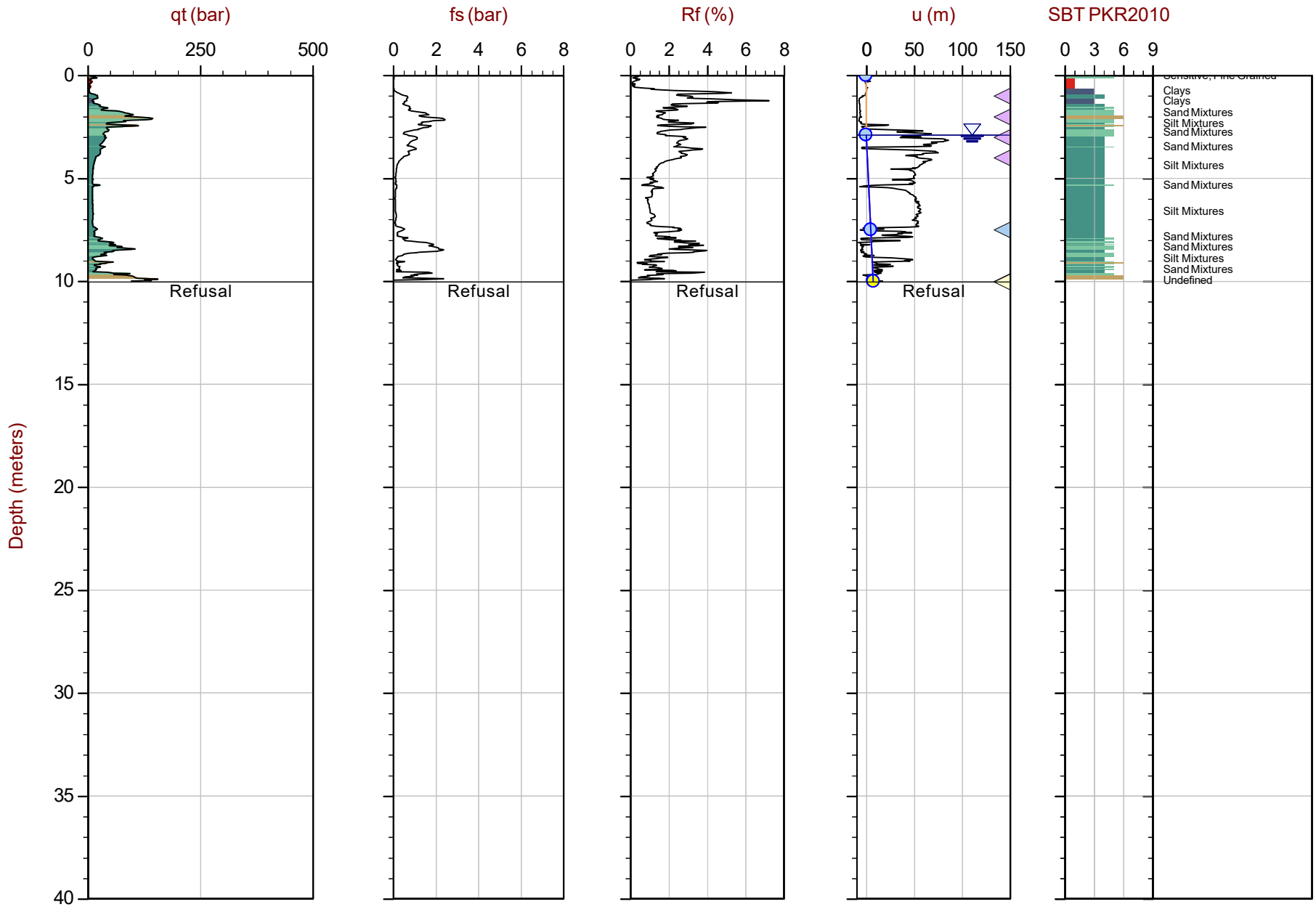
CONETEC

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 10.025 m / 32.89 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT '10)
Coords: UTM 17N N: 5407391m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

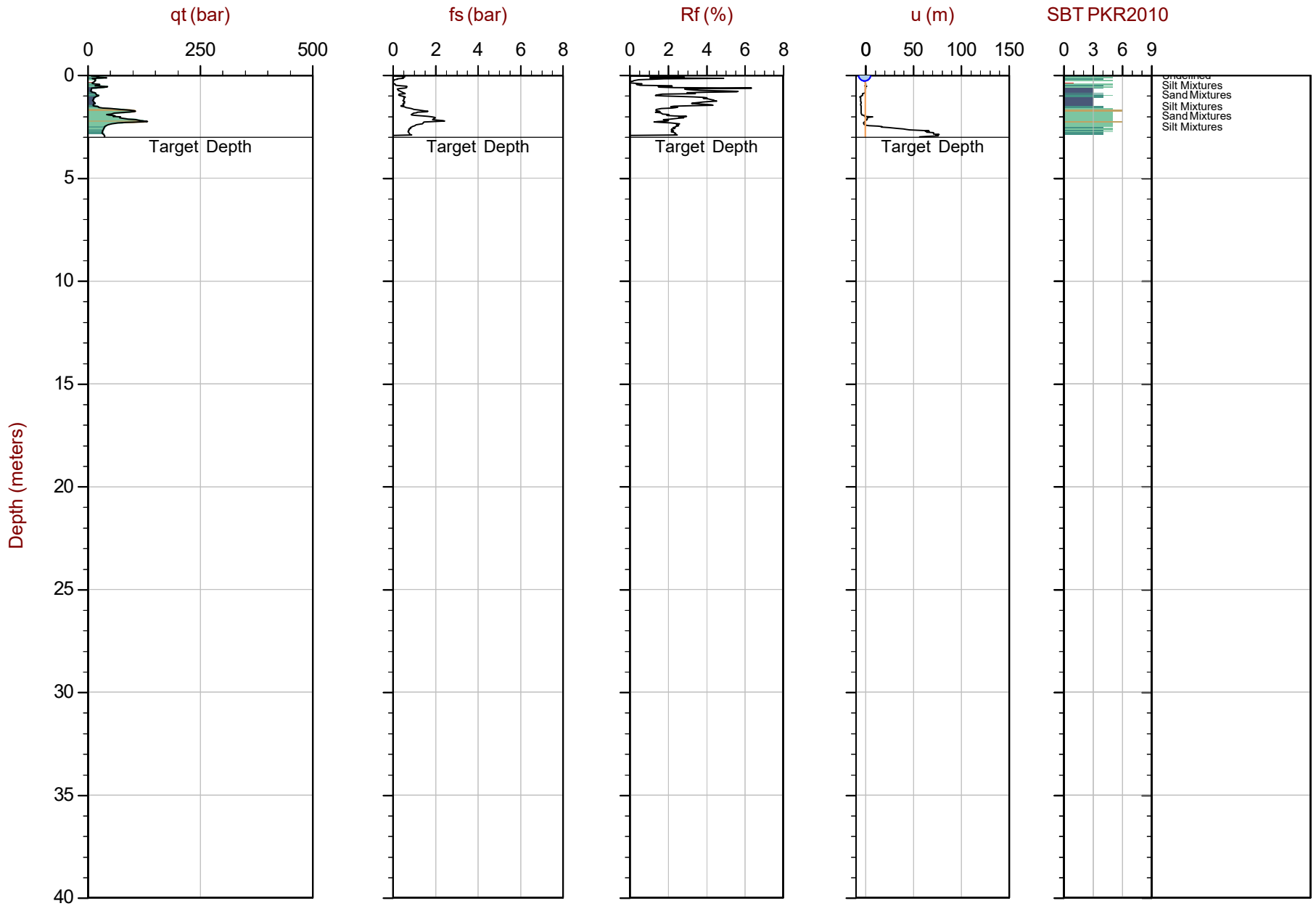
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-20 13:25
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 3.000 m / 9.84 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407392m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

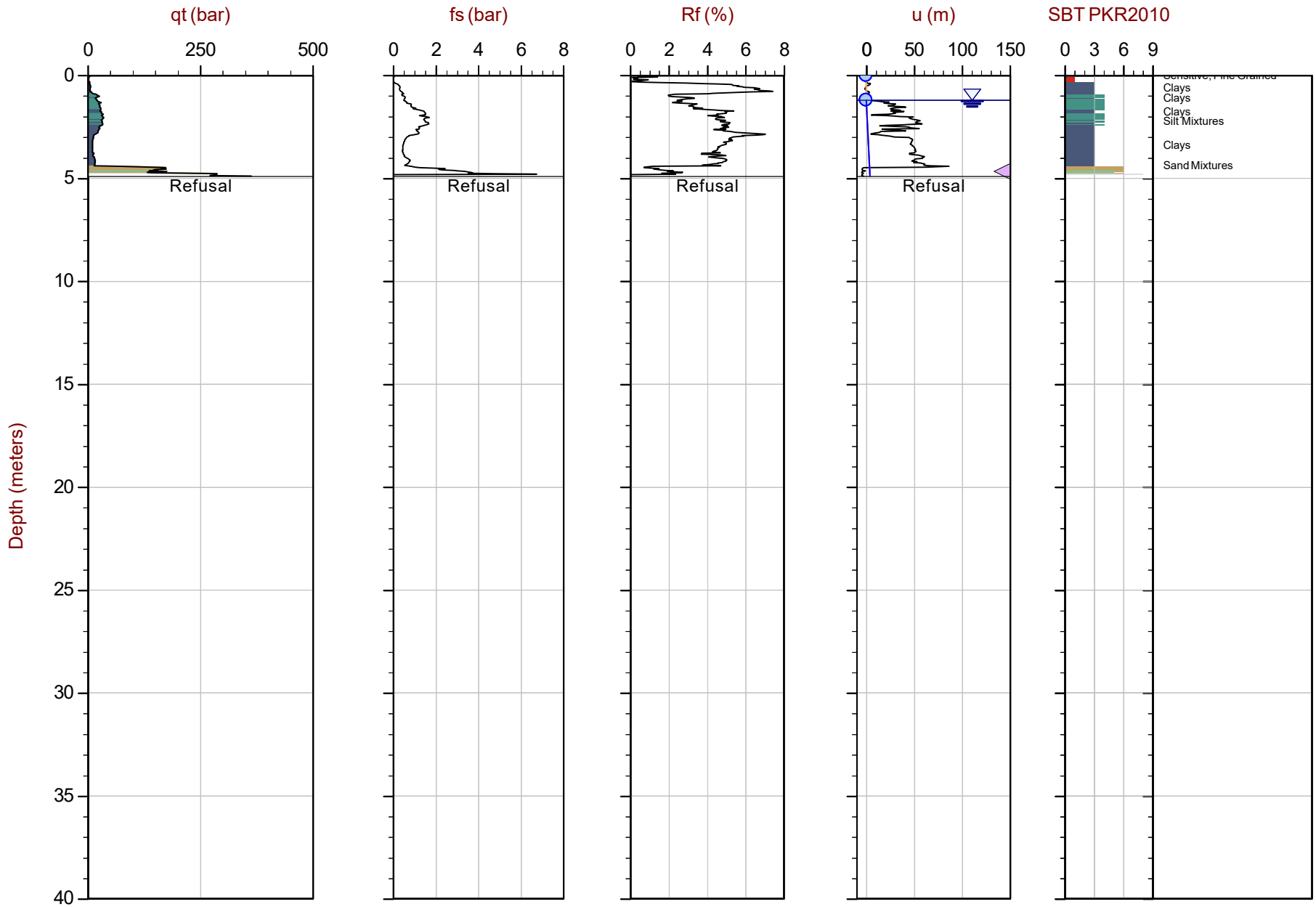
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-16 14:19
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 4.900 m / 16.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408601m E: 475374m
Sheet No: 1 of 1

Overplot Item: Ueq Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved Dissipation, Ueq assumed Ueq Line Hydrostatic Line

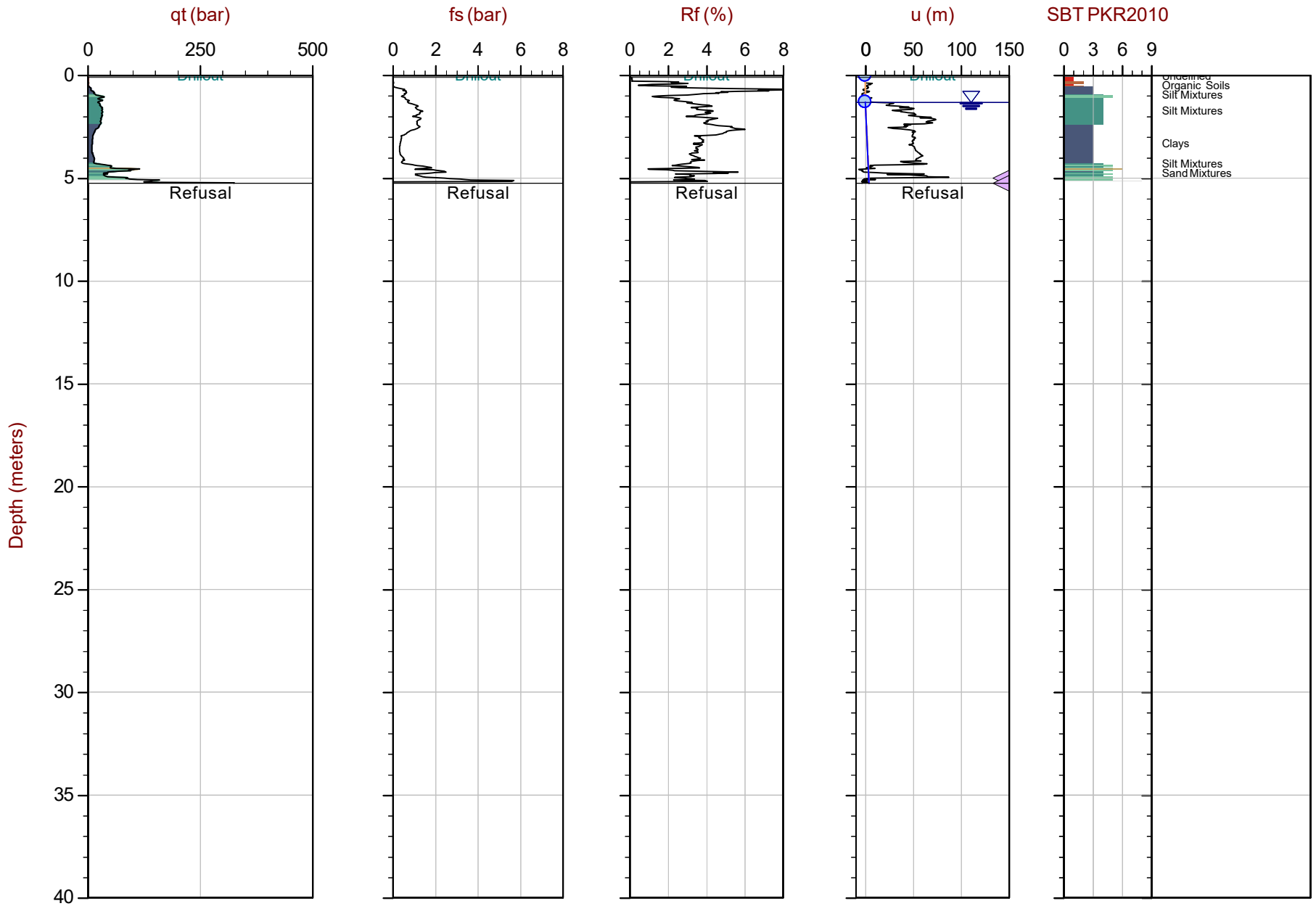
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-17 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 5.250 m / 17.22 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT '10)
Coords: UTM 17N N: 5408594m E: 475372m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

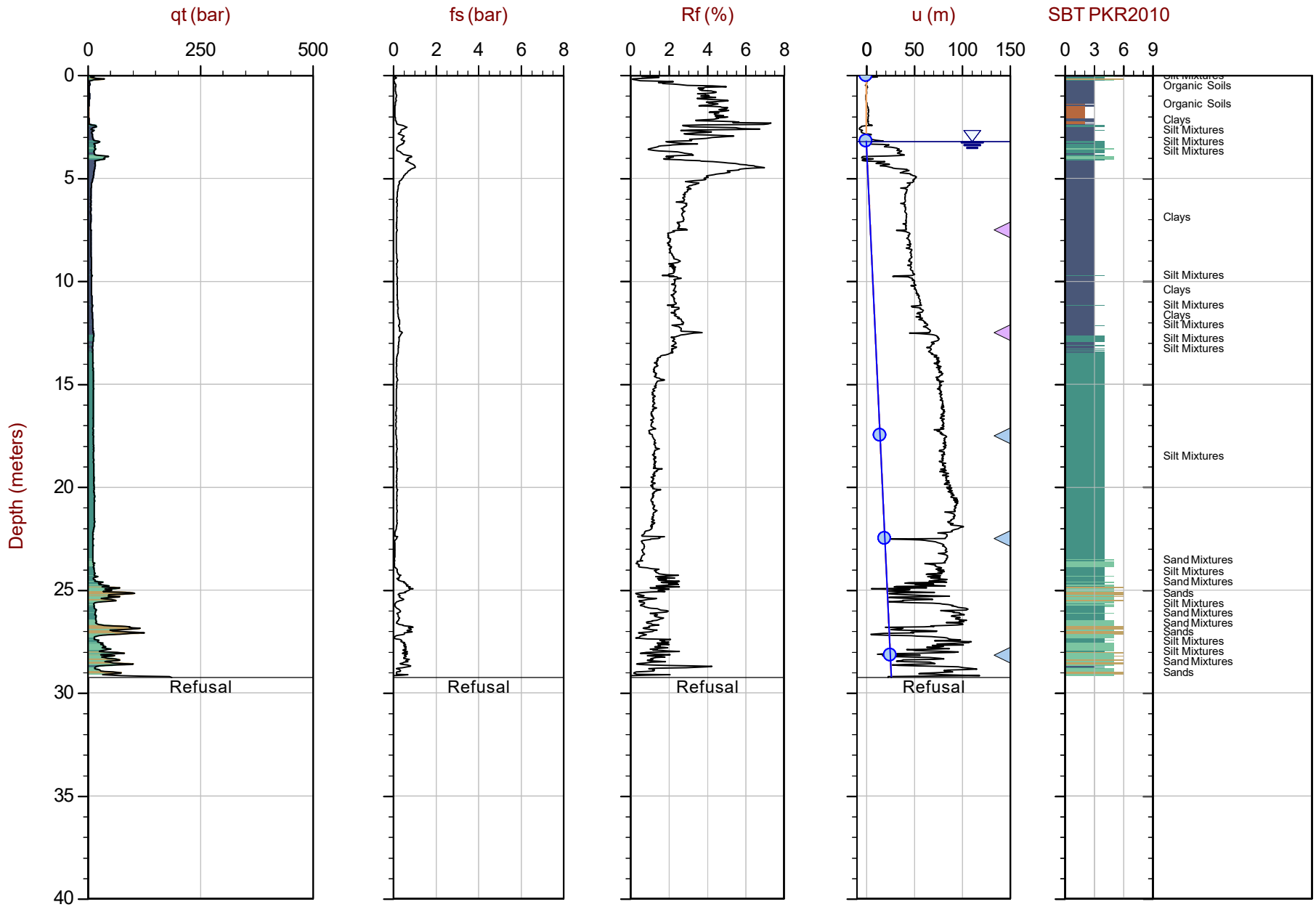
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 29.250 m / 95.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP203.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5409174m E: 476455m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

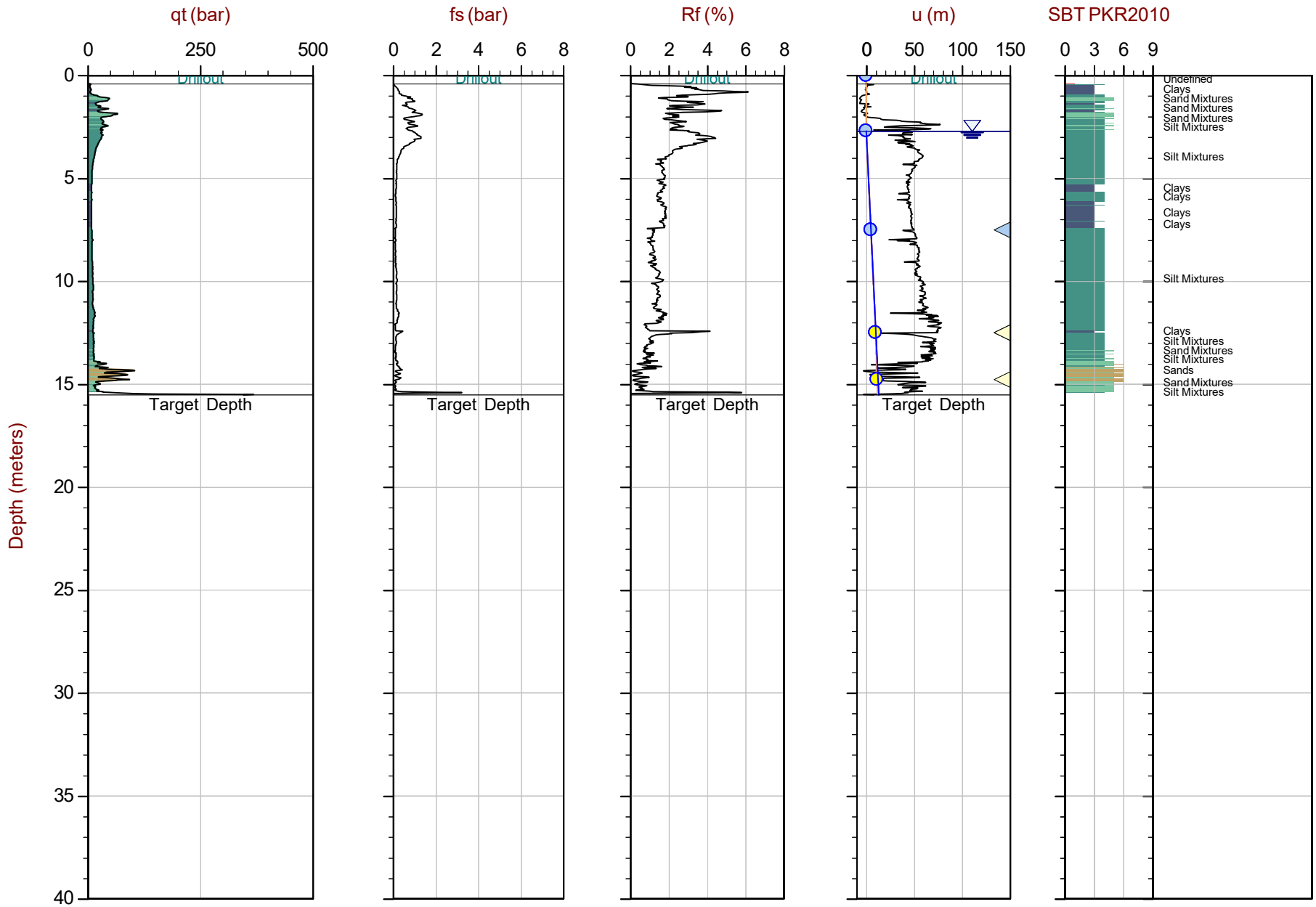
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.525 m / 50.93 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP204.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407351m E: 475669m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

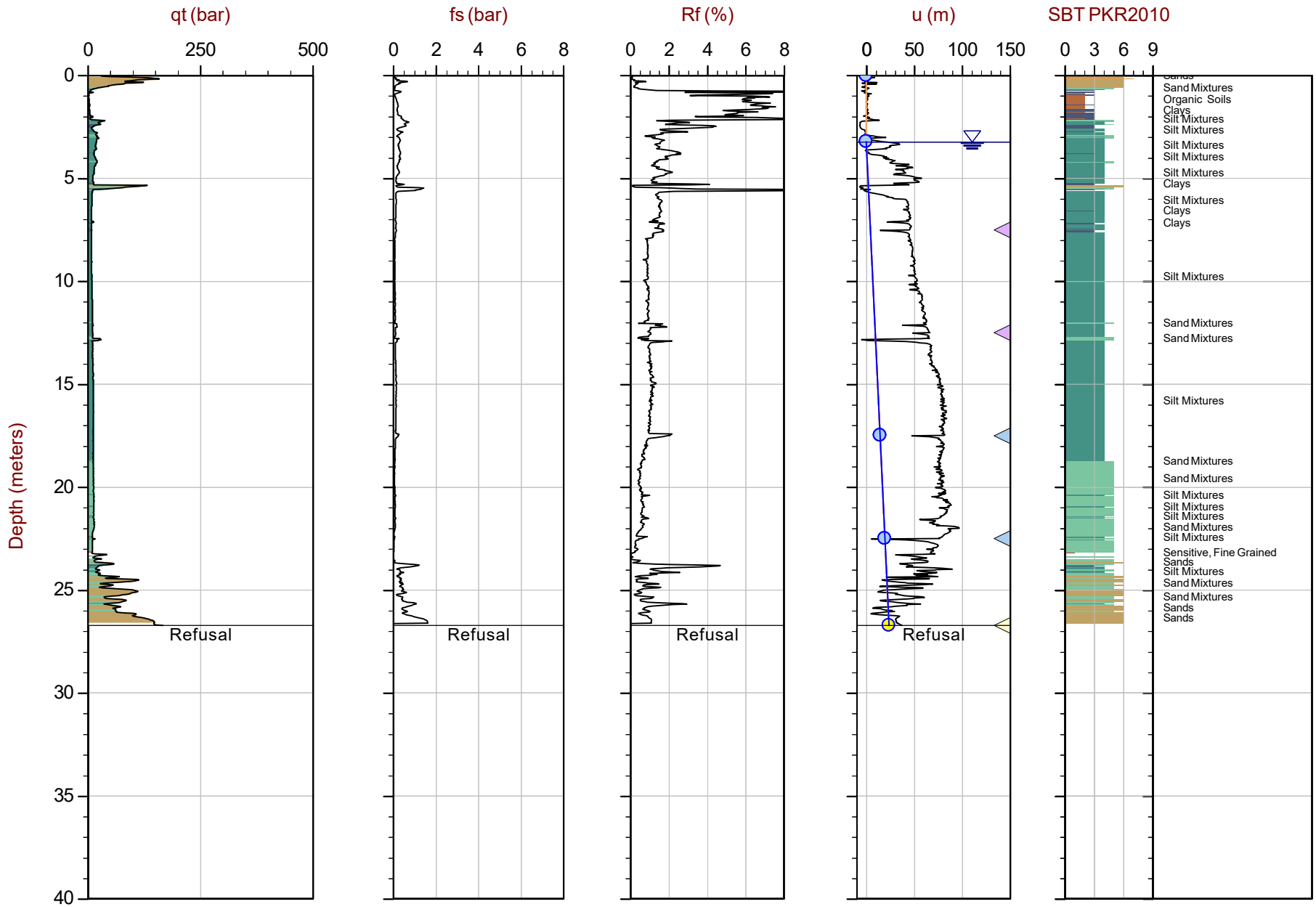
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 26.725 m / 87.68 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP205.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408416m E: 476456m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

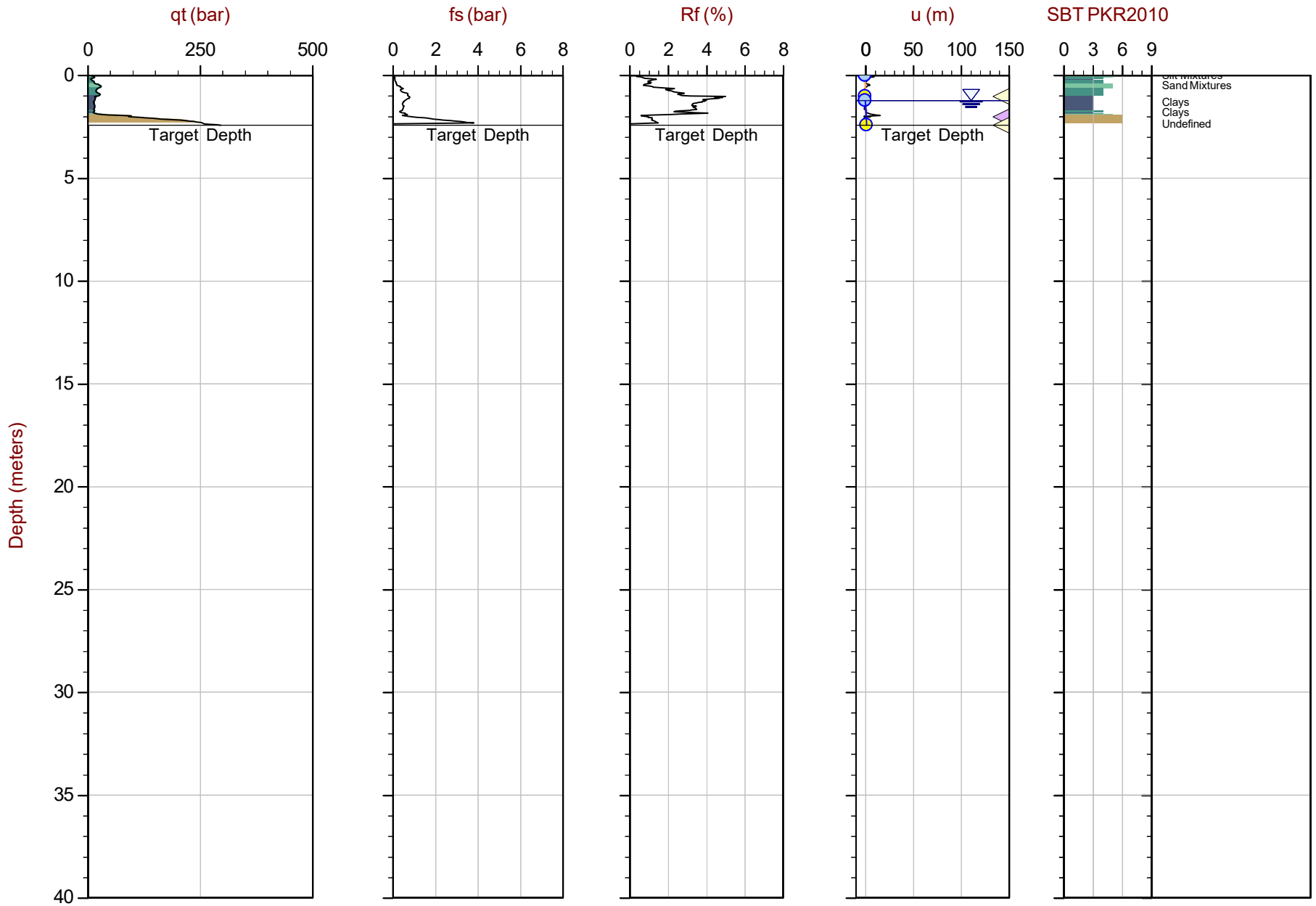
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 2.425 m / 7.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF03AB.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414676m E: 472128m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

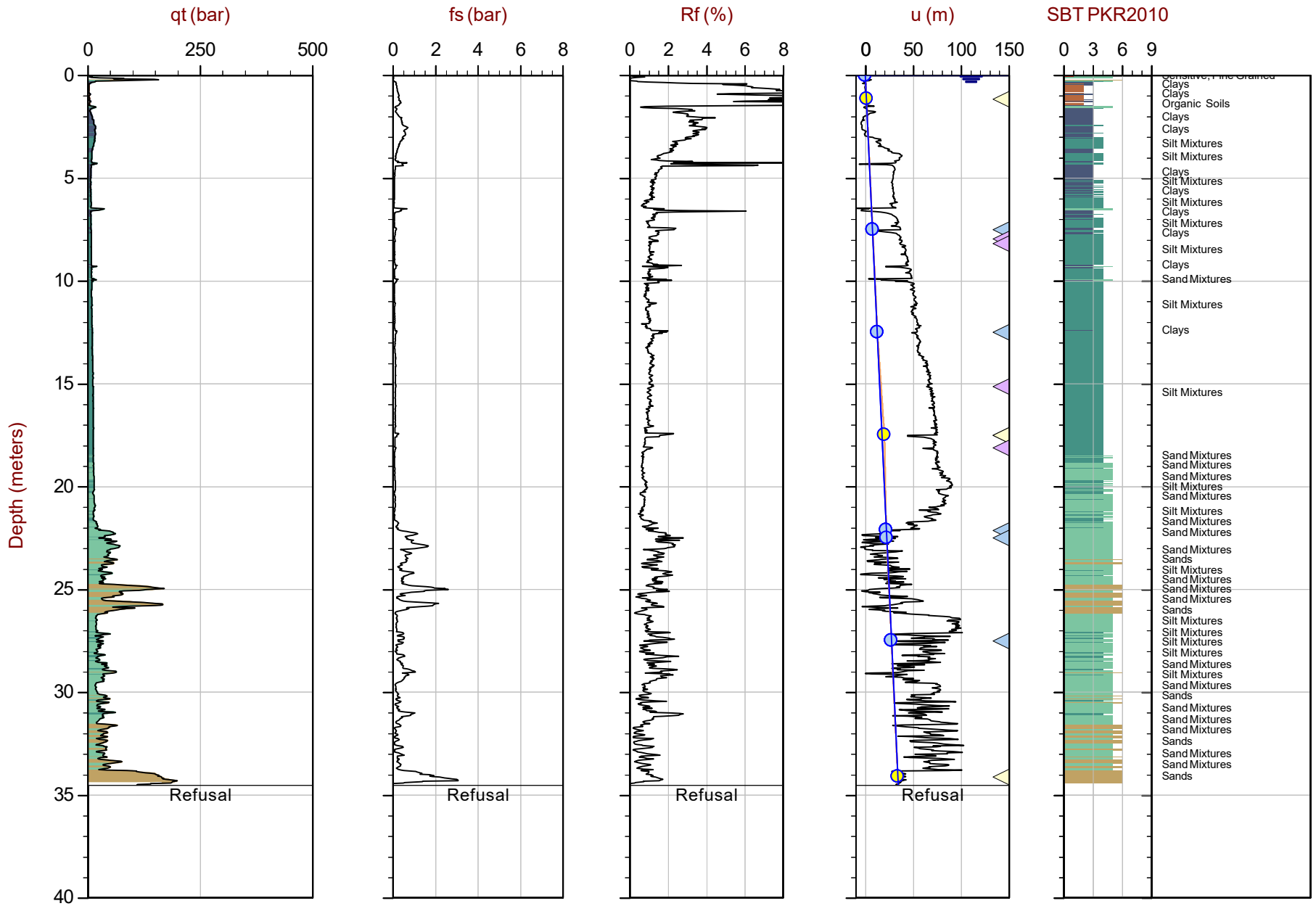
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 34.525 m / 113.27 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF08AB.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5401992m E: 476468m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

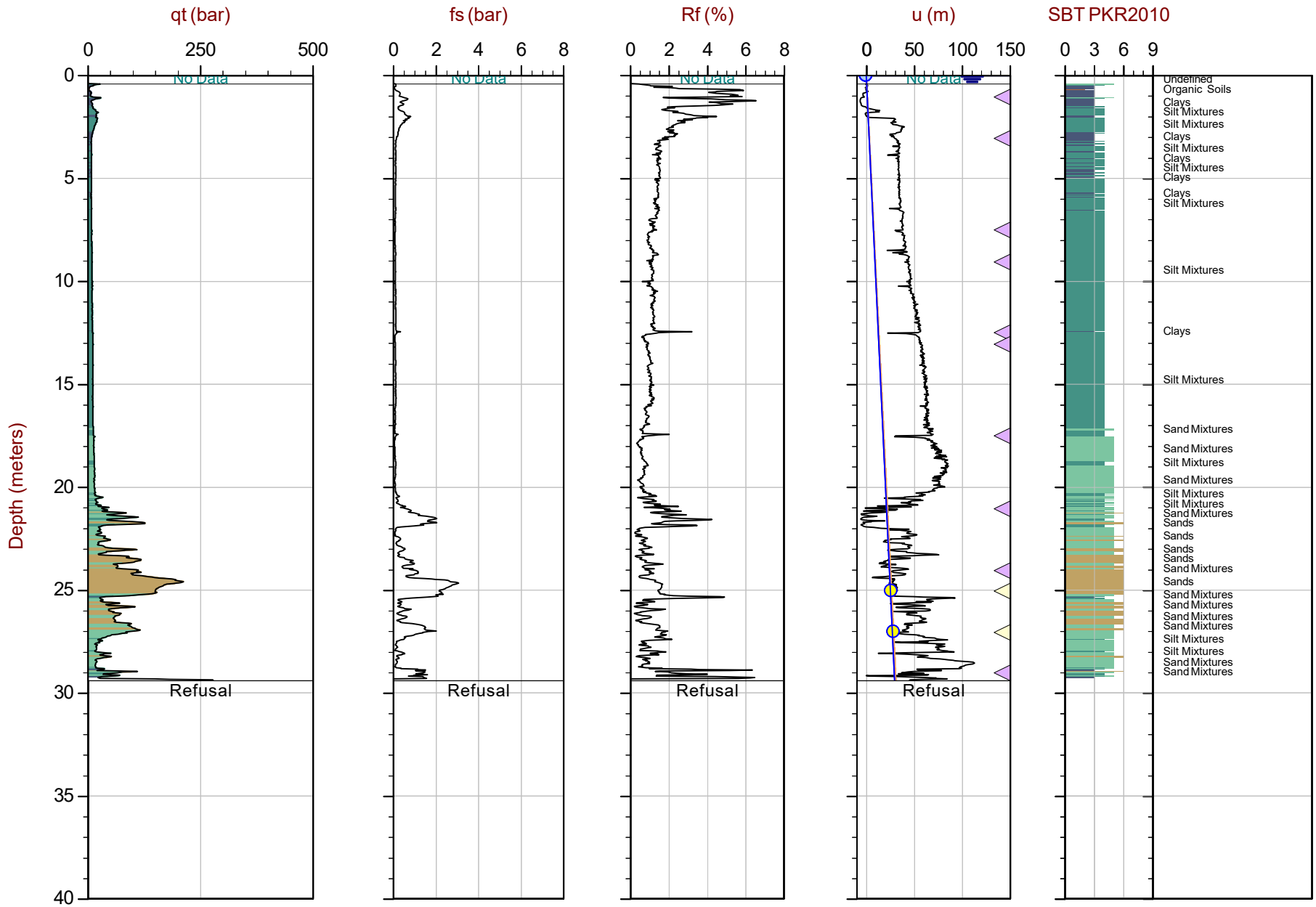
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 29.400 m / 96.46 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5404211m E: 476818m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

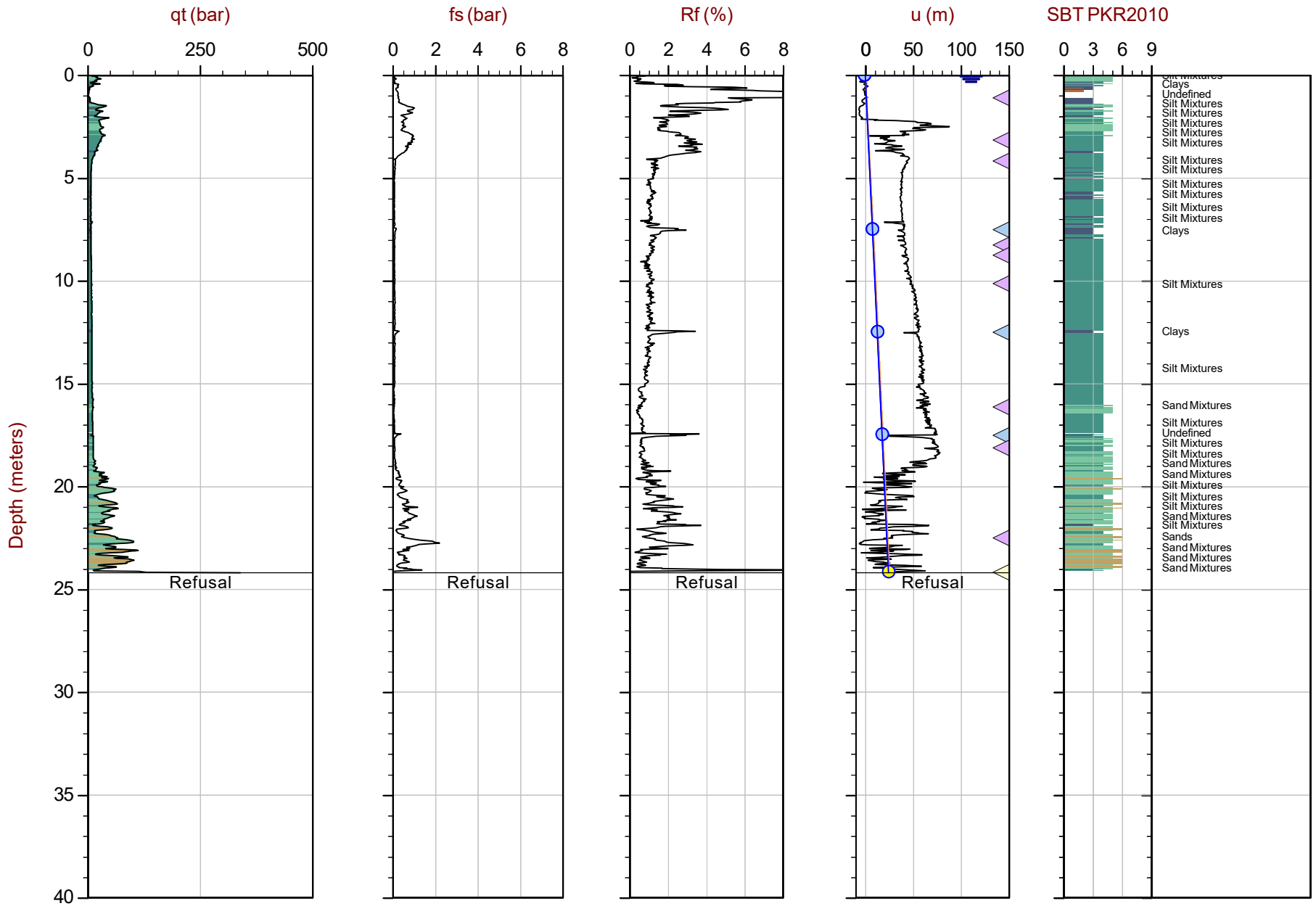
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 24.200 m / 79.40 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5402798m E: 476813m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

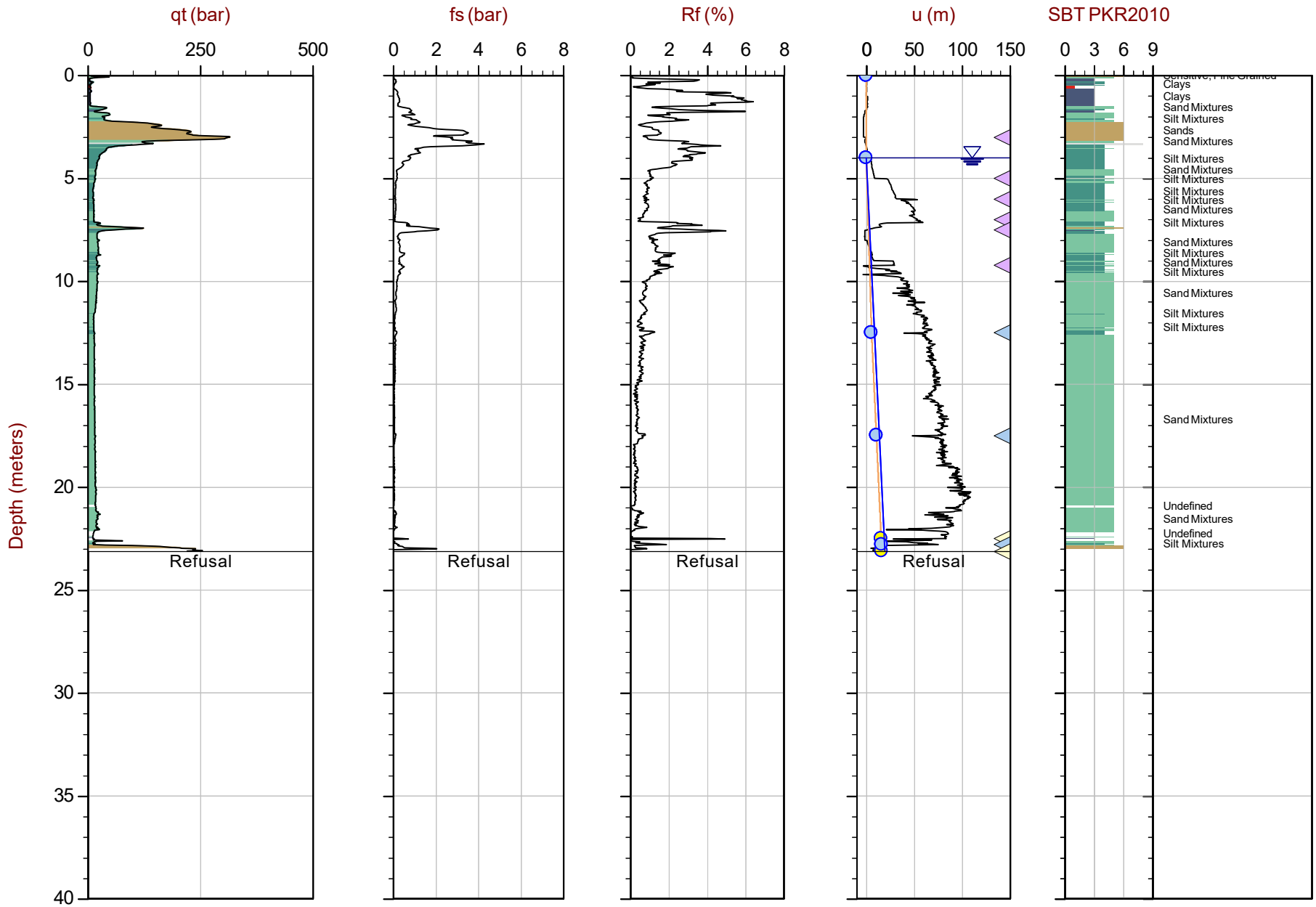
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 23.125 m / 75.87 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD201.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT '10)
Coords: UTM 17N N: 5411103m E: 473341m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

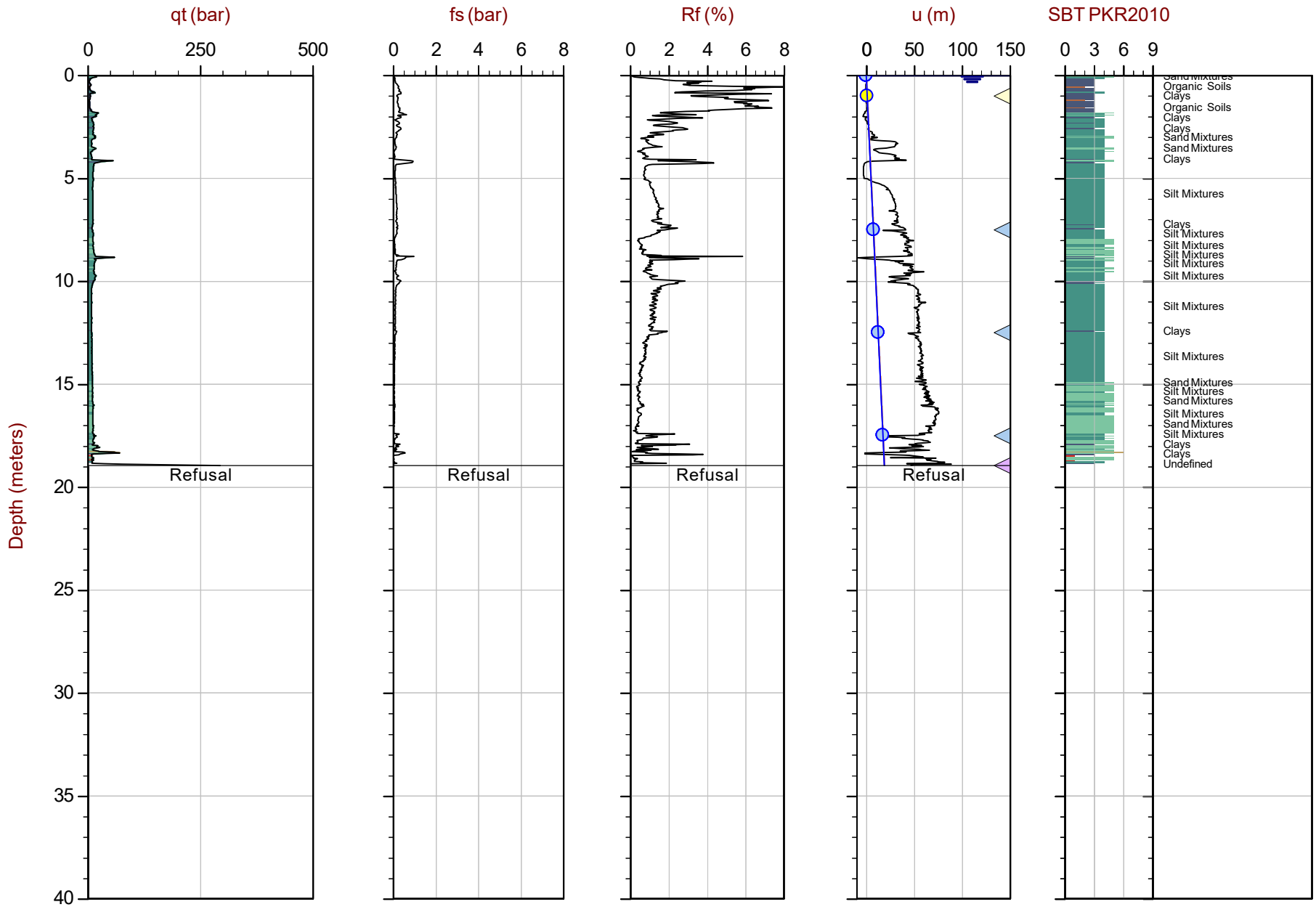
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 18.950 m / 62.17 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5412168m E: 474136m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

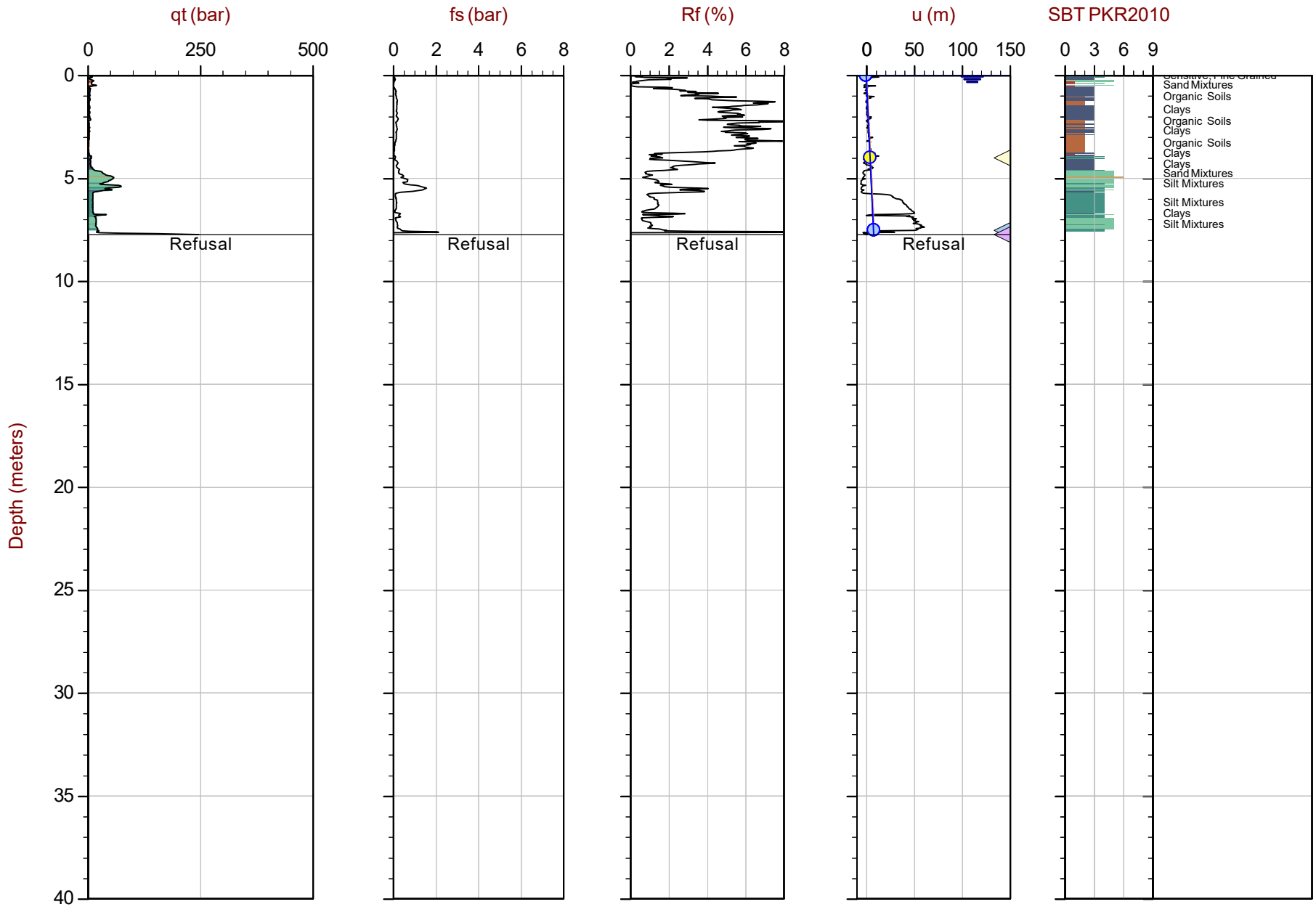
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.725 m / 25.34 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413526m E: 474146m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

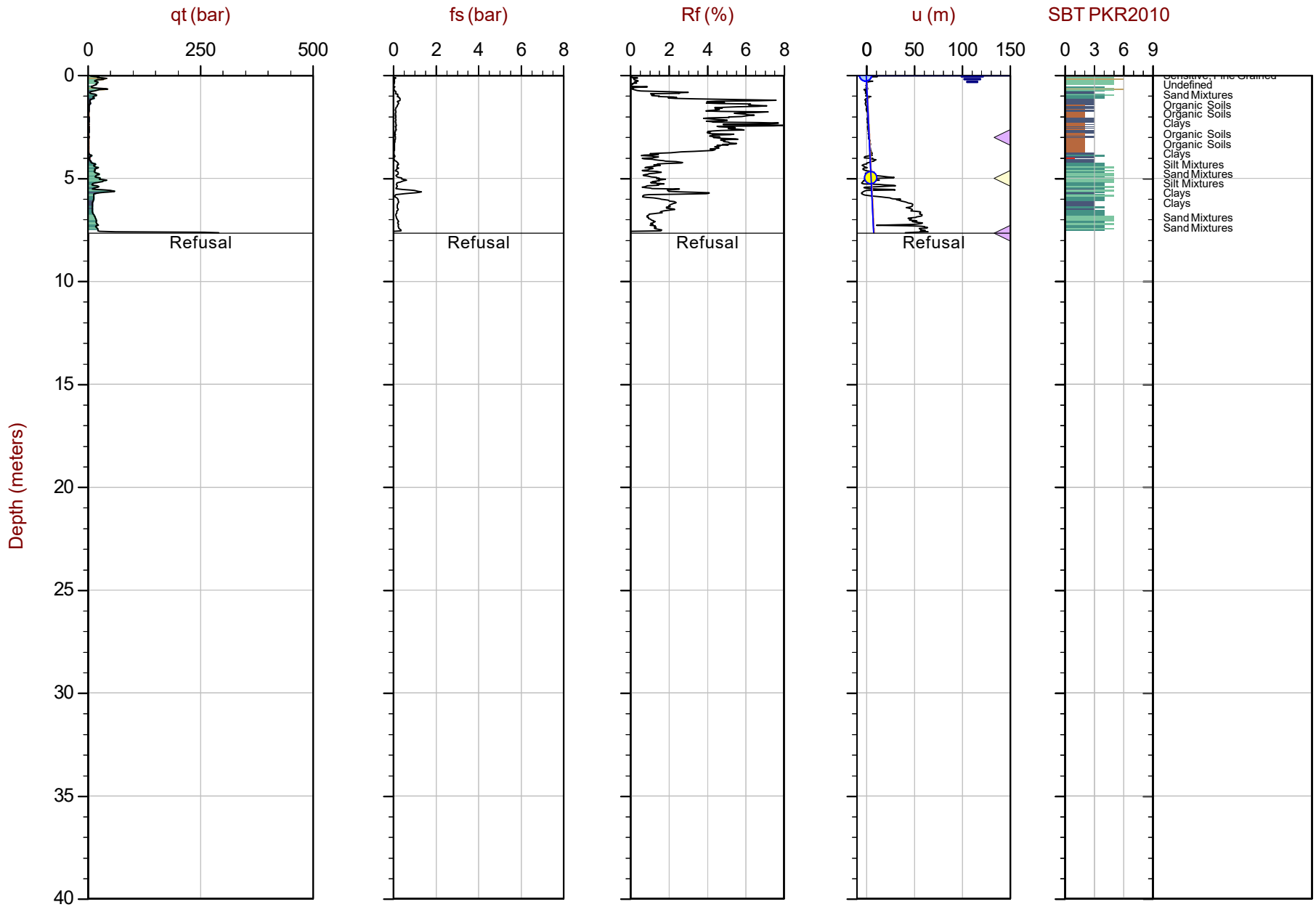
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.650 m / 25.10 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413524m E: 474147m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

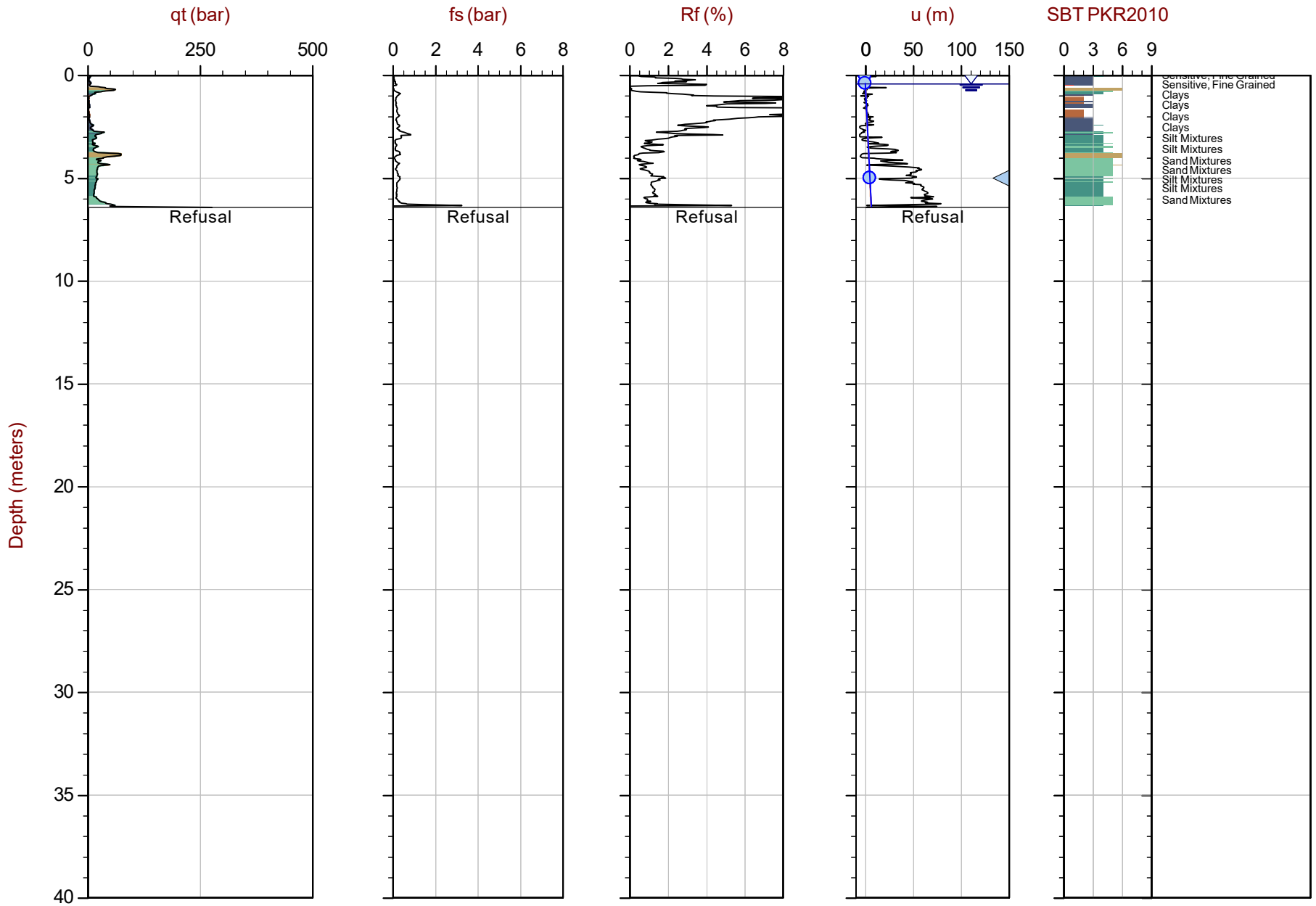
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-12 09:14
Site: Crawford Mine - SRK

Sounding: CPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.425 m / 21.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_CPWRD207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414555m E: 474237m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

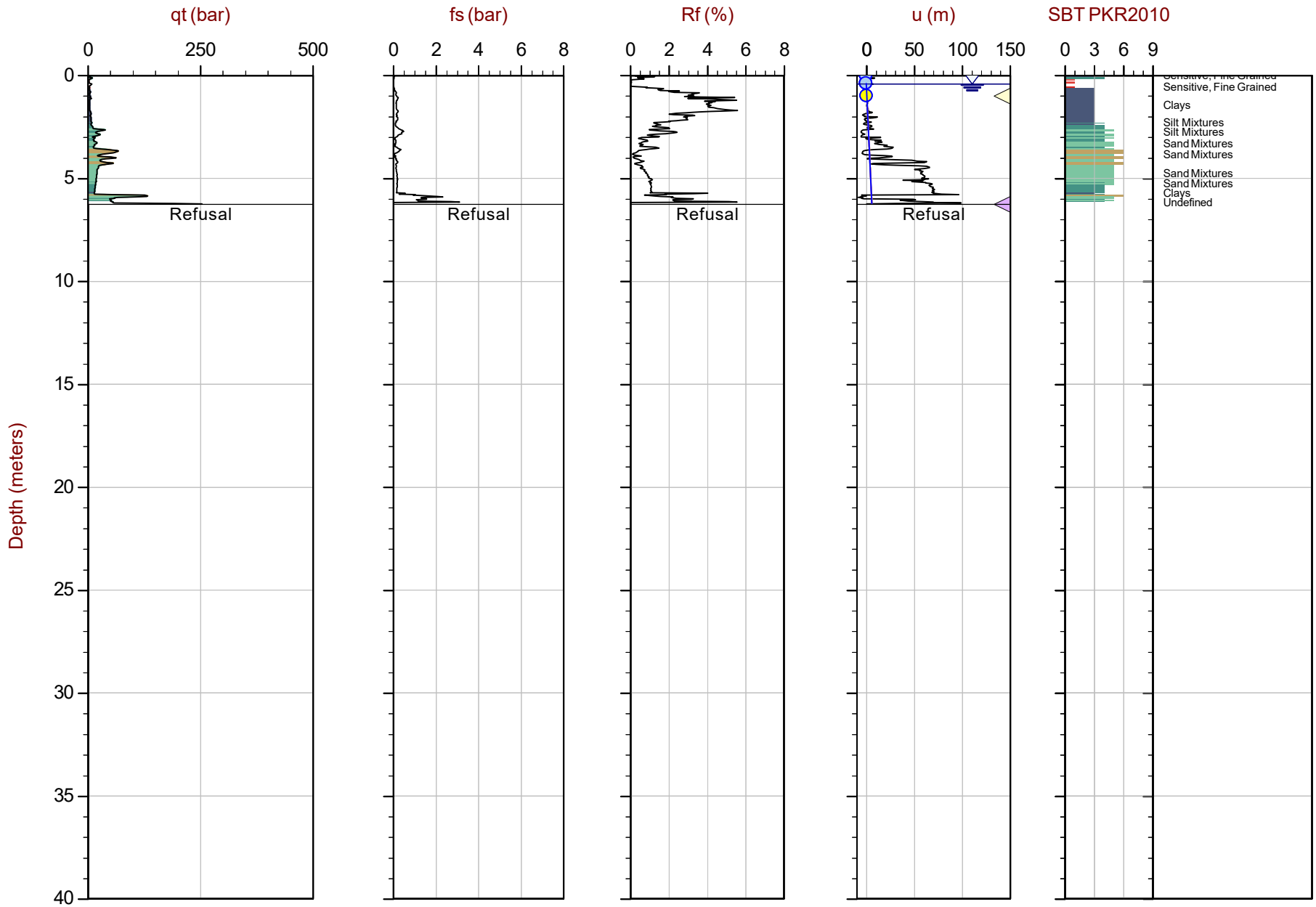
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.250 m / 20.51 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414553m E: 474239m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

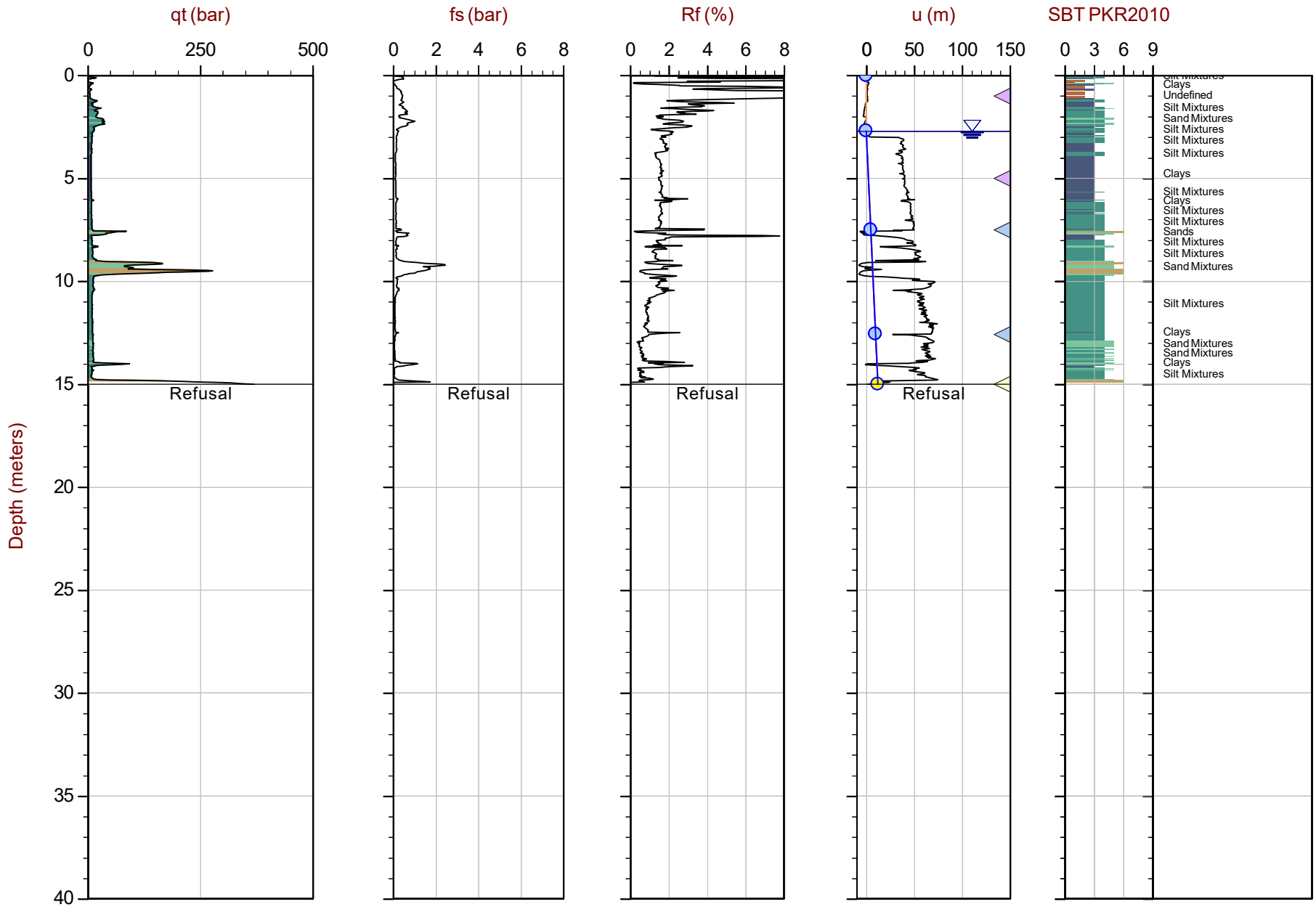
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.000 m / 49.21 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD212.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411072m E: 474212m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Advanced Cone Penetration Test Plots

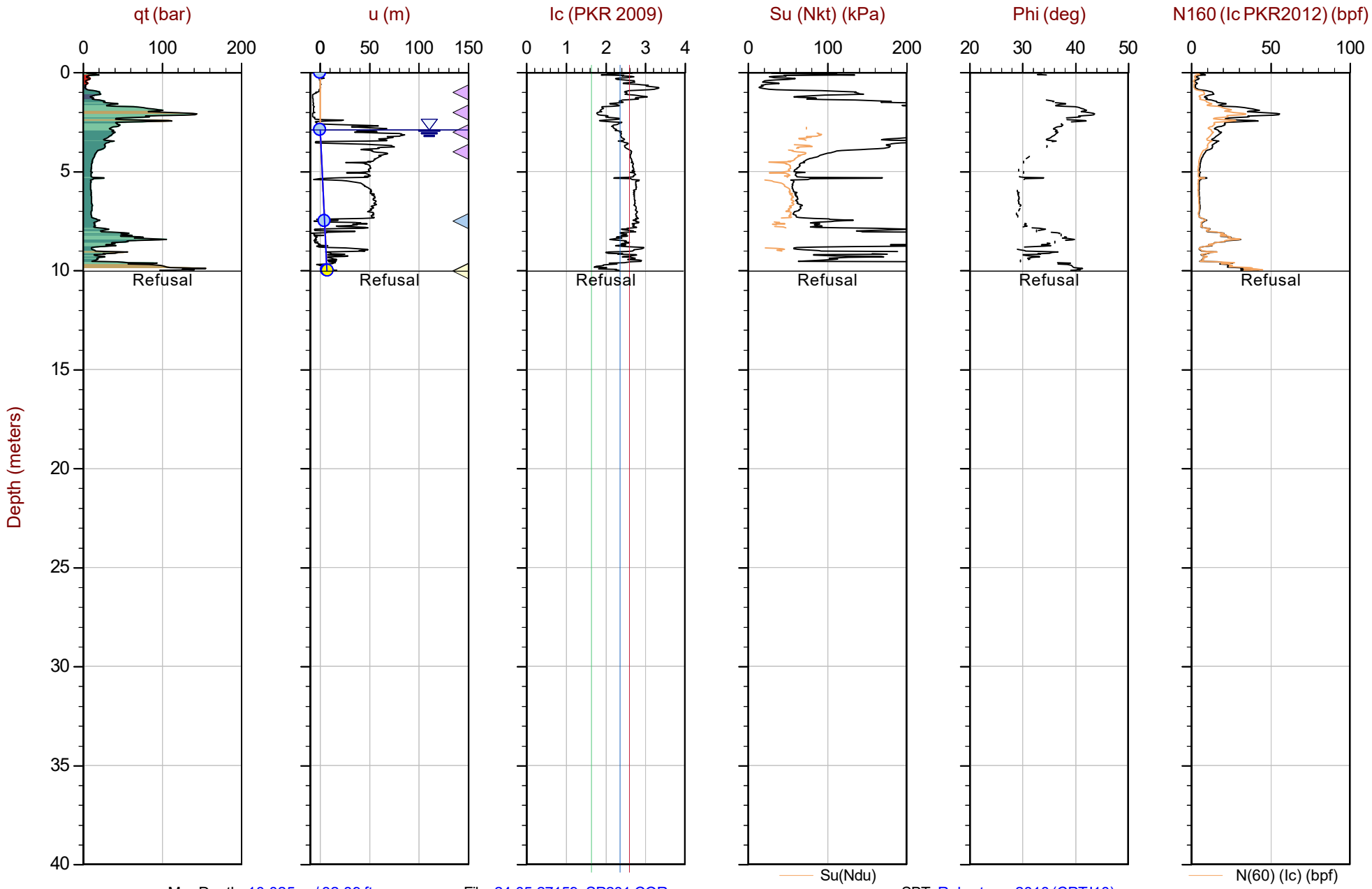
CONETEC

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 10.025 m / 32.89 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407391m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

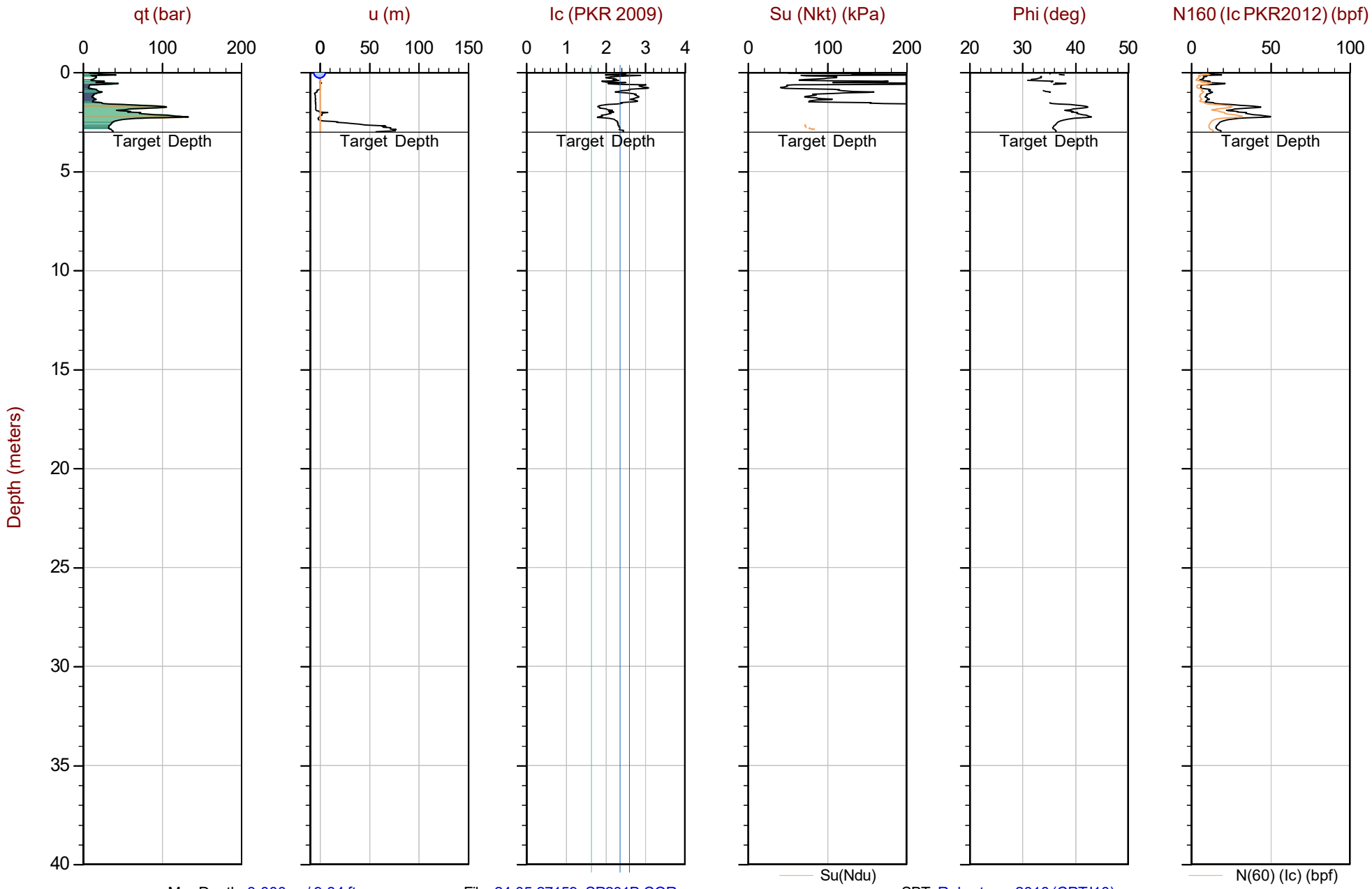
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-20 13:25
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 3.000 m / 9.84 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201B.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407392m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

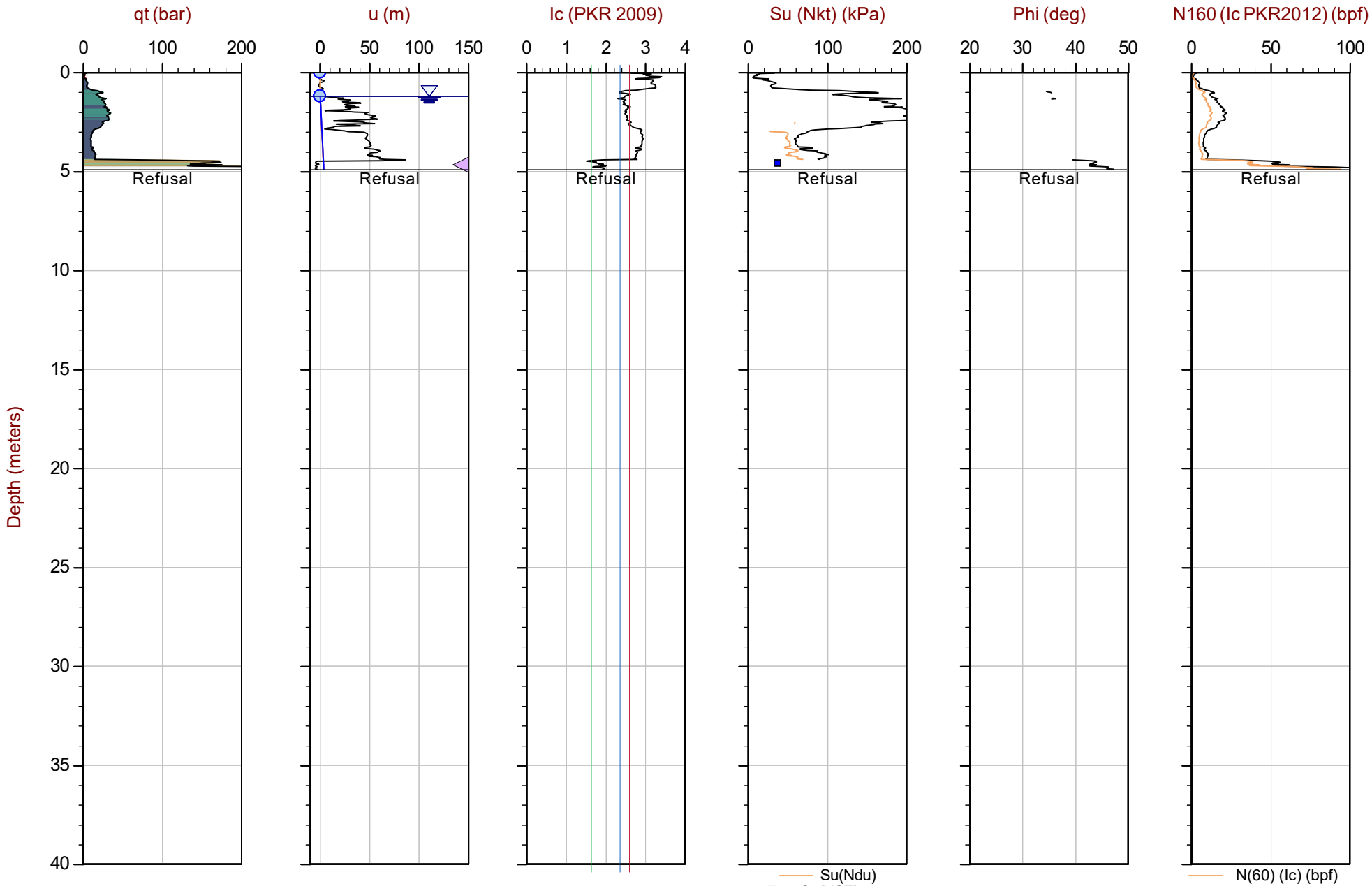
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-16 14:19
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 4.900 m / 16.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408601m E: 475374m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

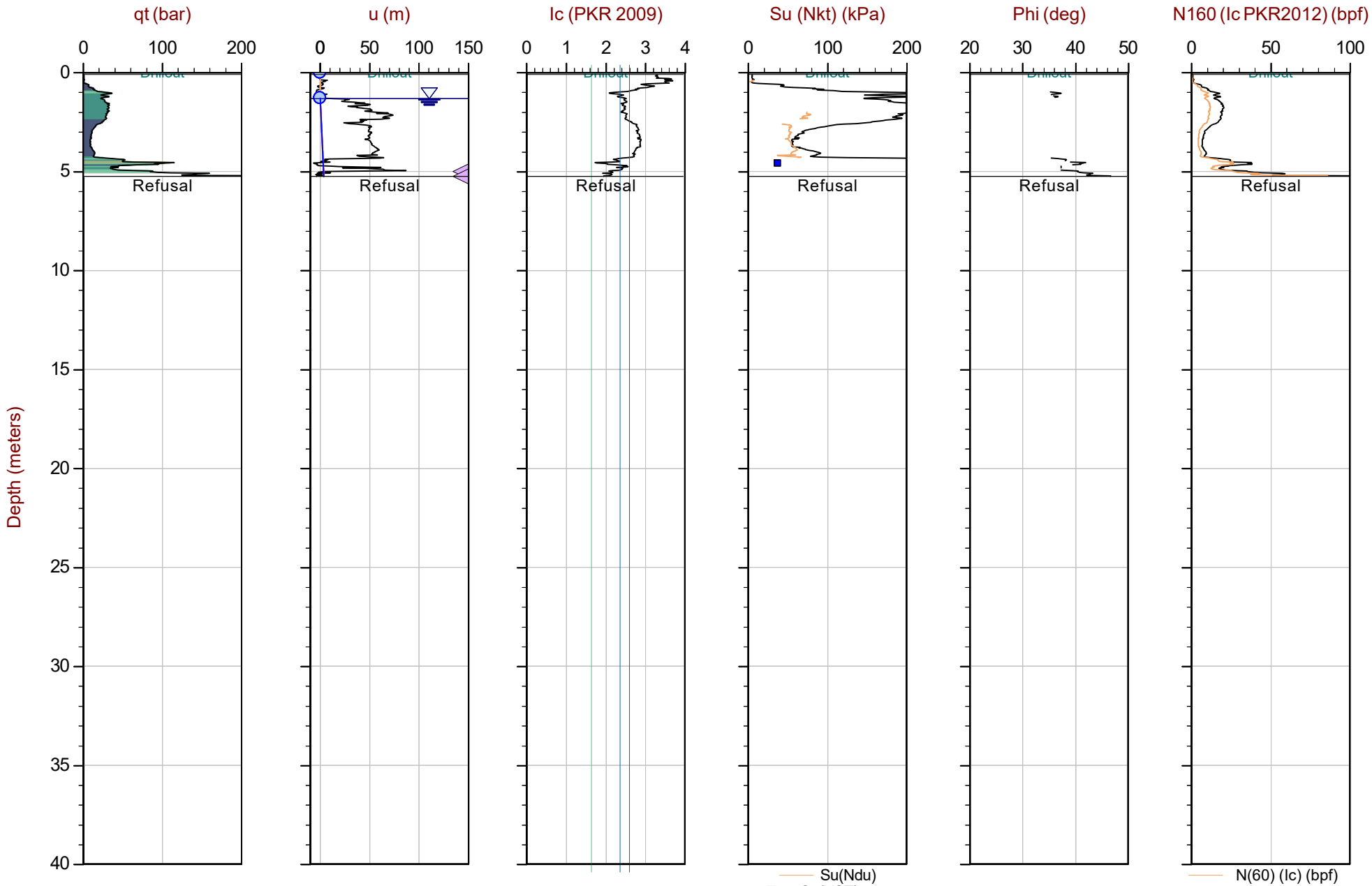
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-17 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 5.250 m / 17.22 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202B.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408594m E: 475372m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

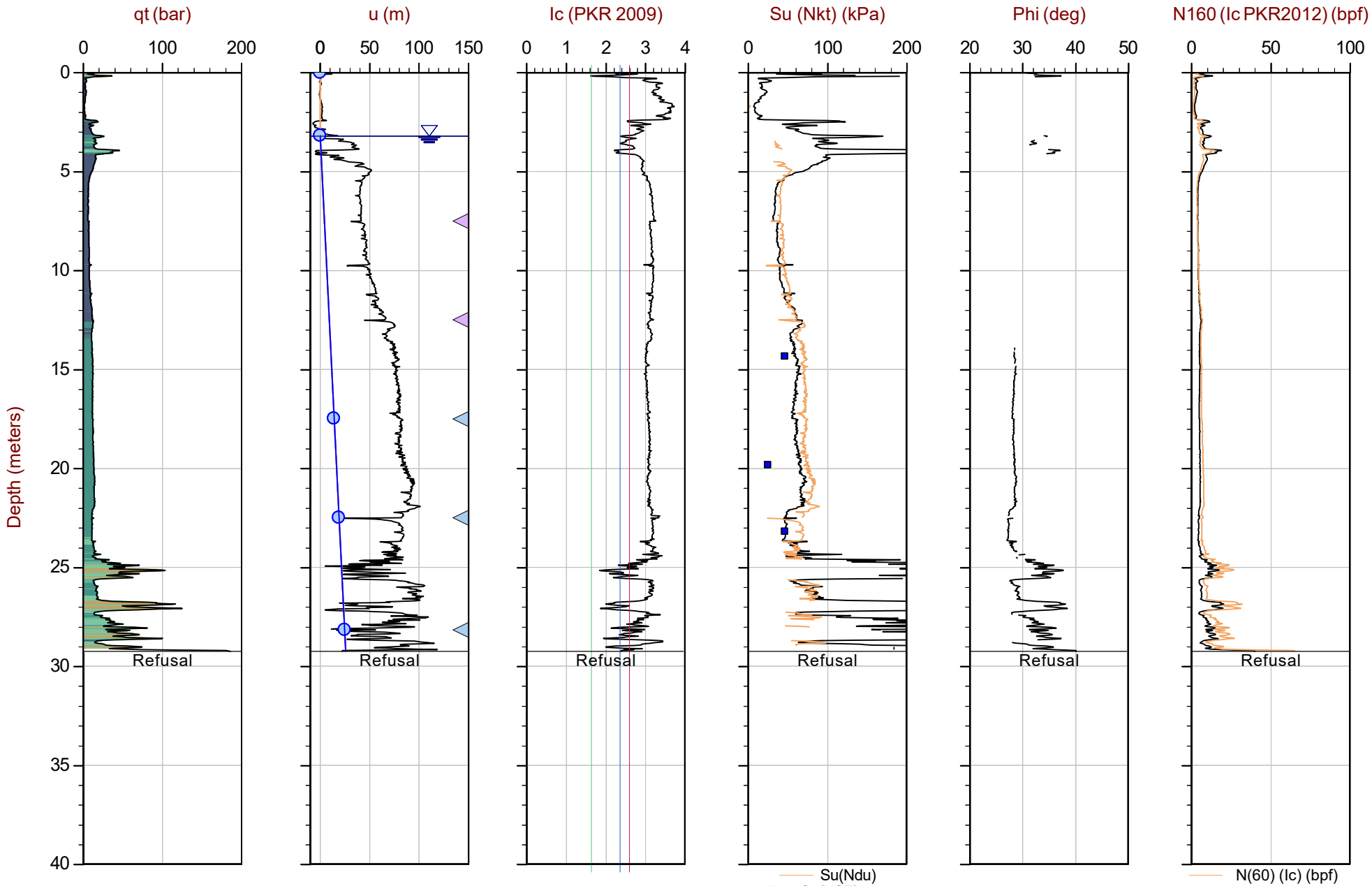
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 29.250 m / 95.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP203.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5409174m E: 476455m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

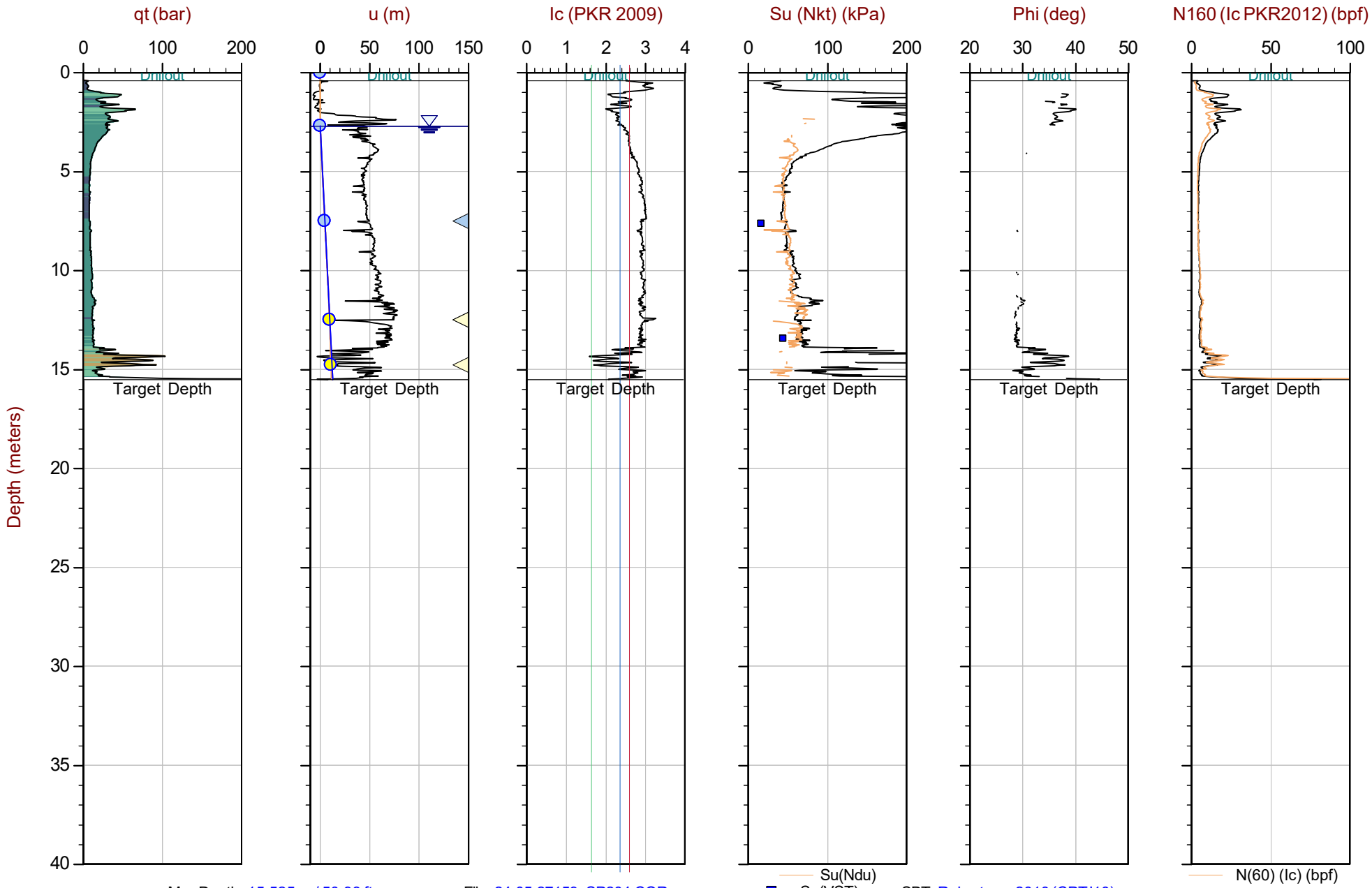
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.525 m / 50.93 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP204.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407351m E: 475669m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

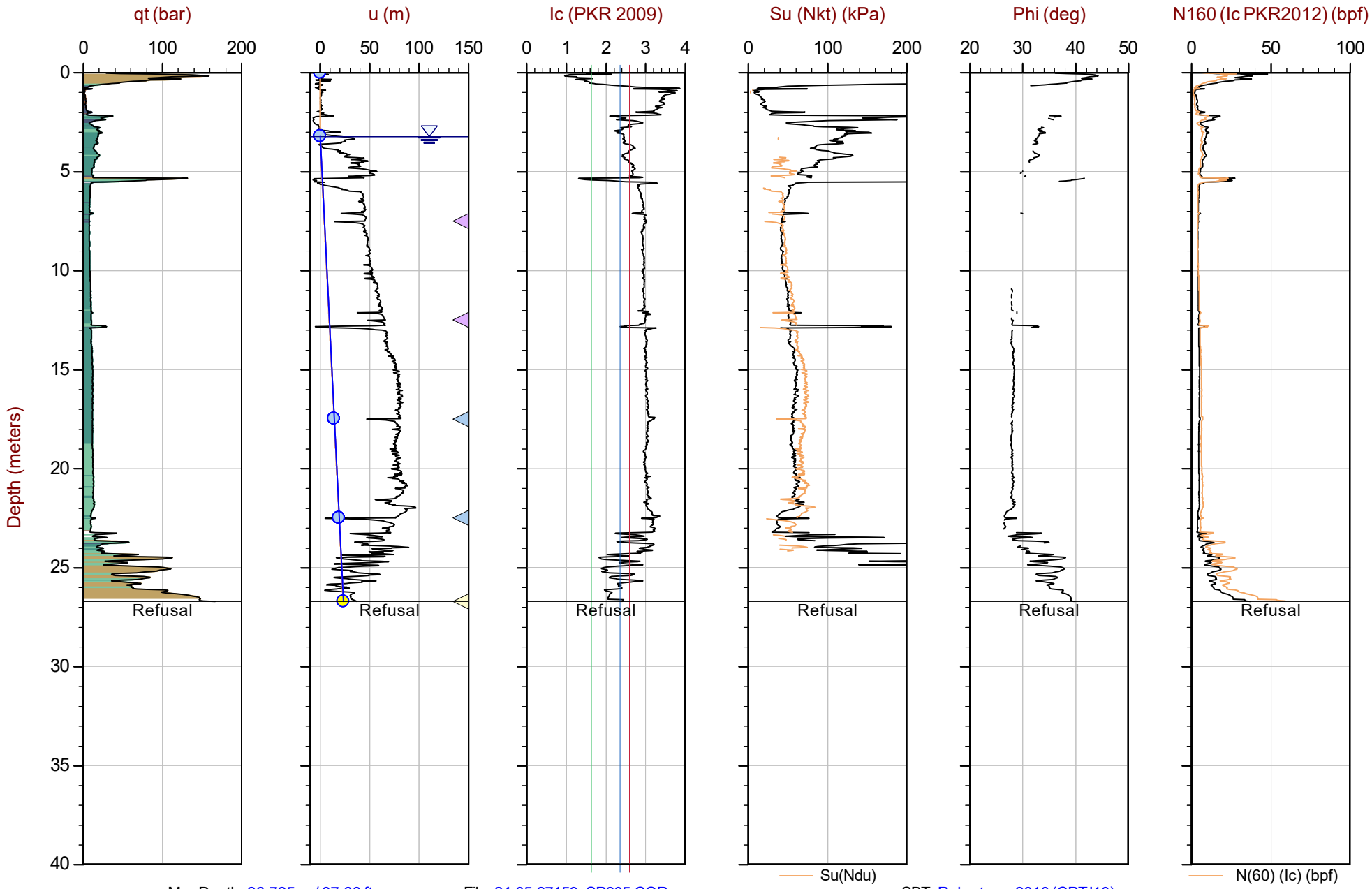
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 26.725 m / 87.68 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP205.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408416m E: 476456m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

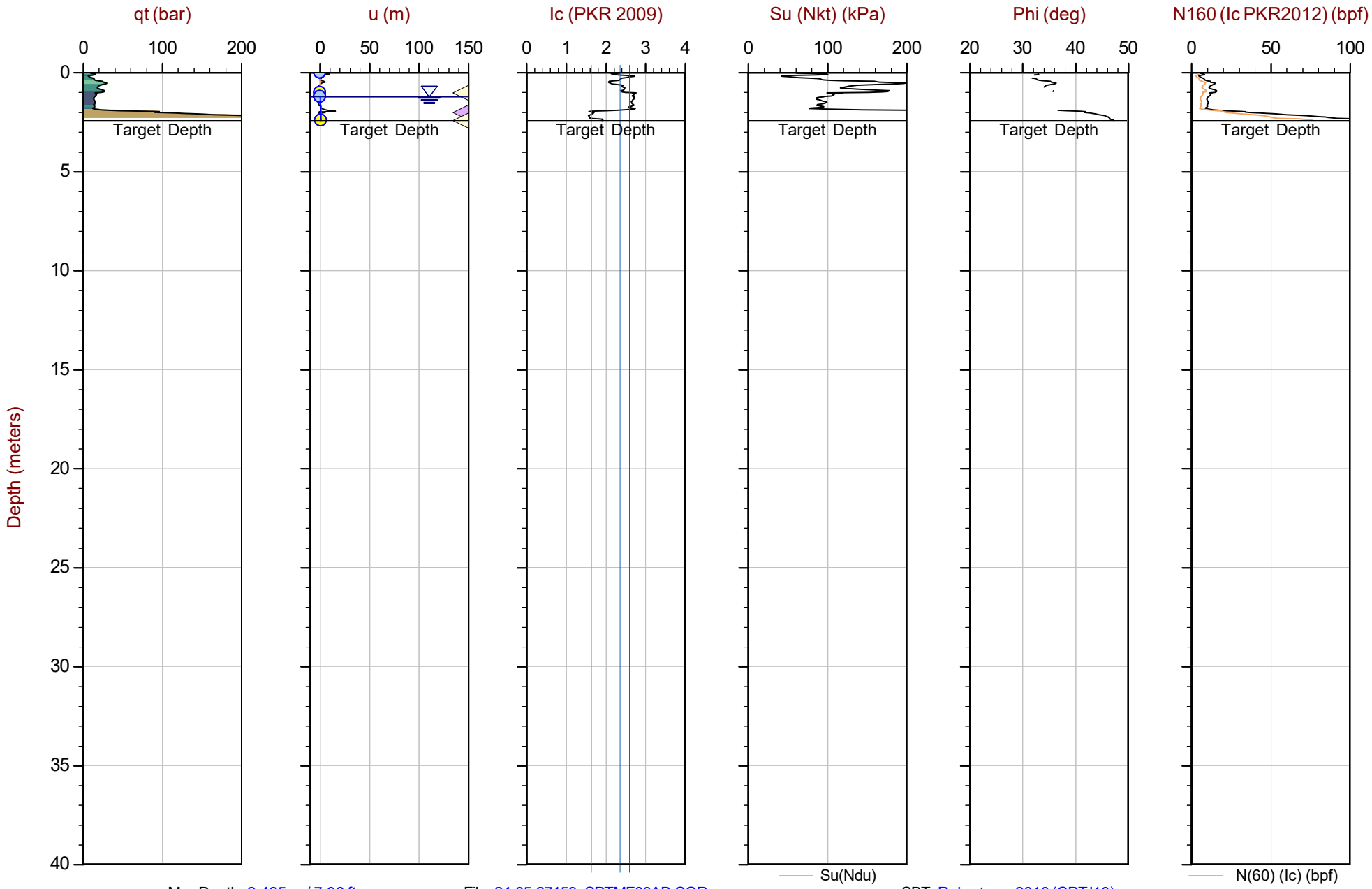
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 2.425 m / 7.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF03AB.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414676m E: 472128m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

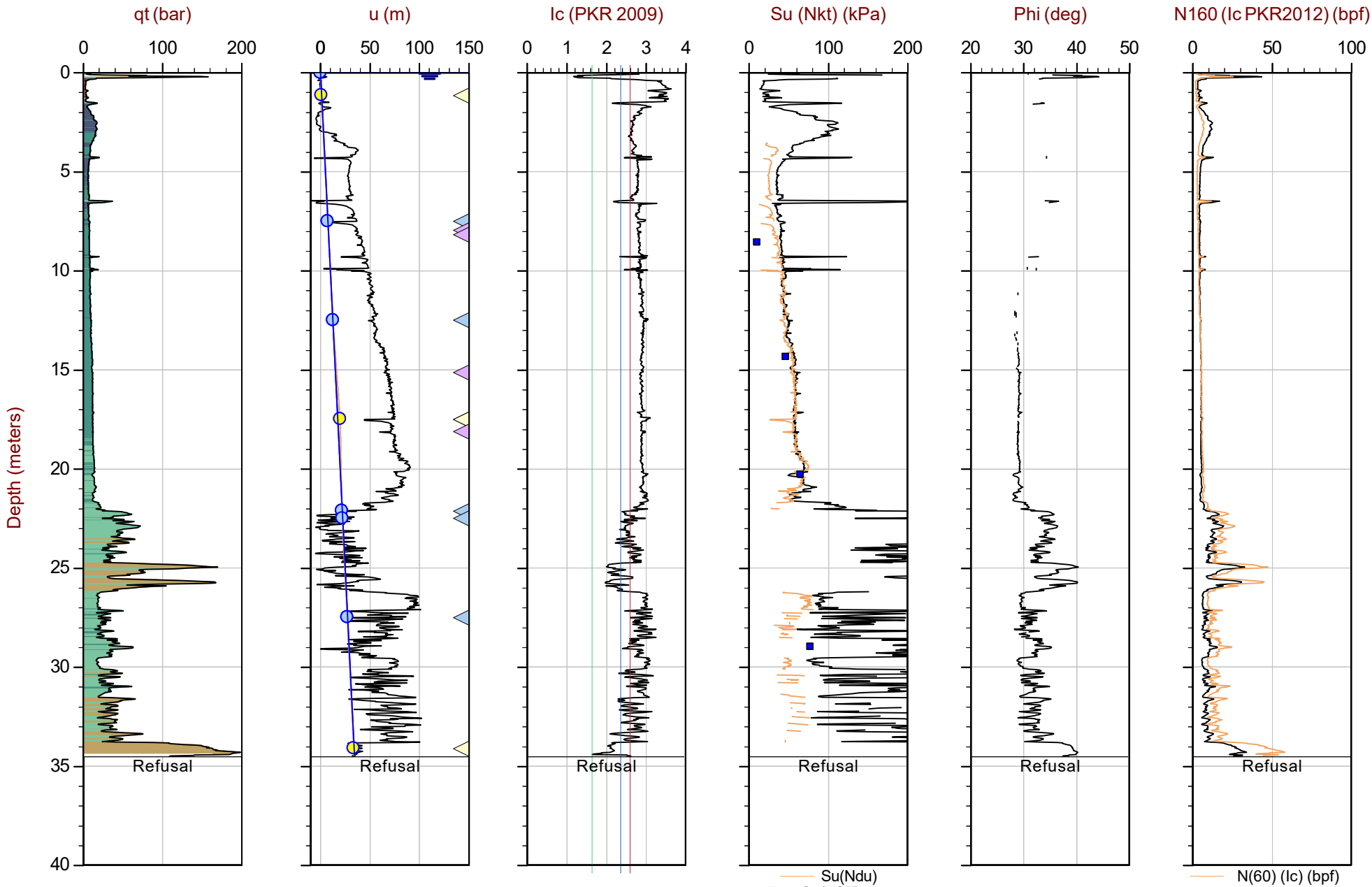
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 34.525 m / 113.27 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF08AB.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5401992m E: 476468m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

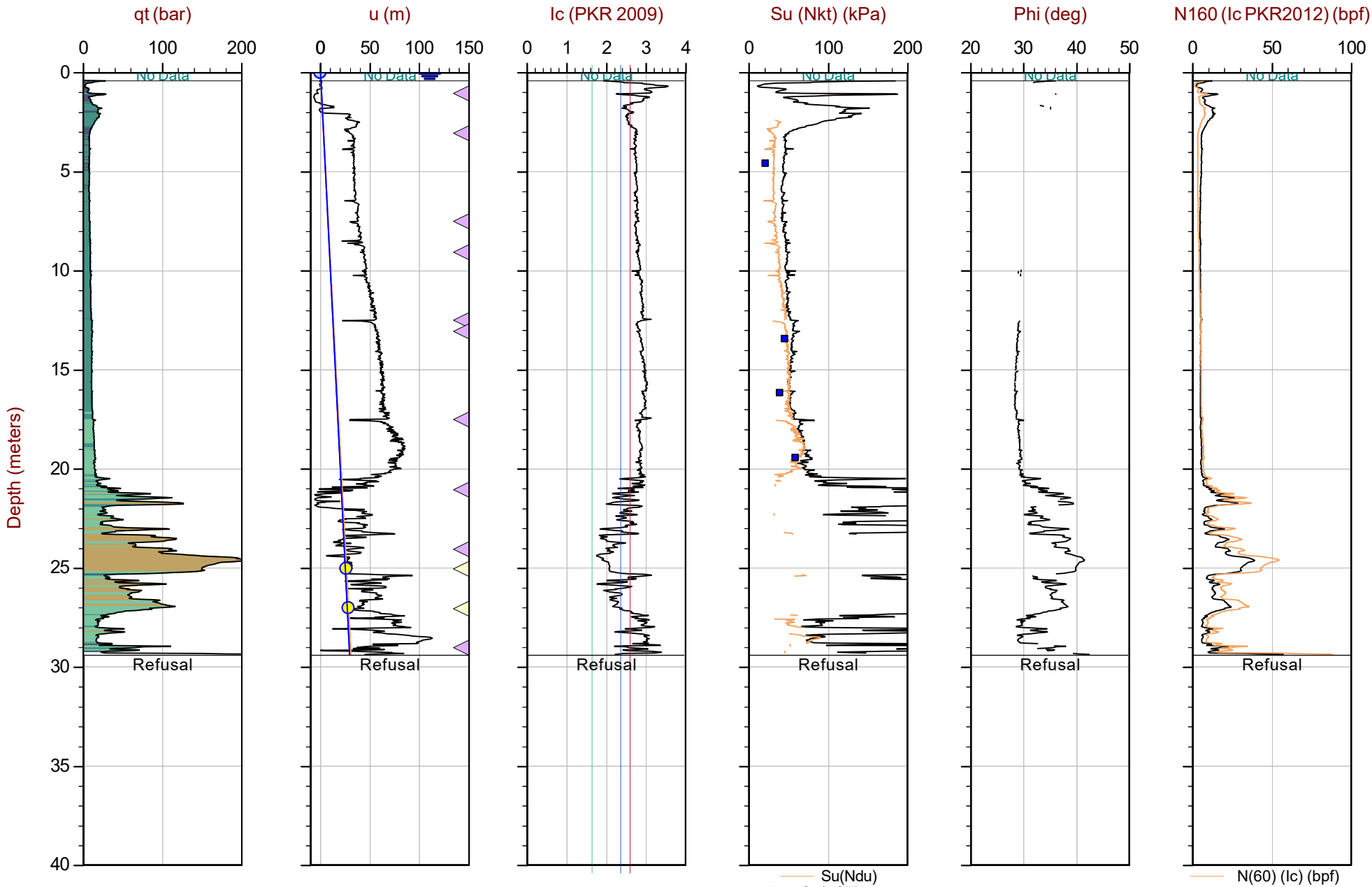
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 29.400 m / 96.46 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF202.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5404211m E: 476818m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

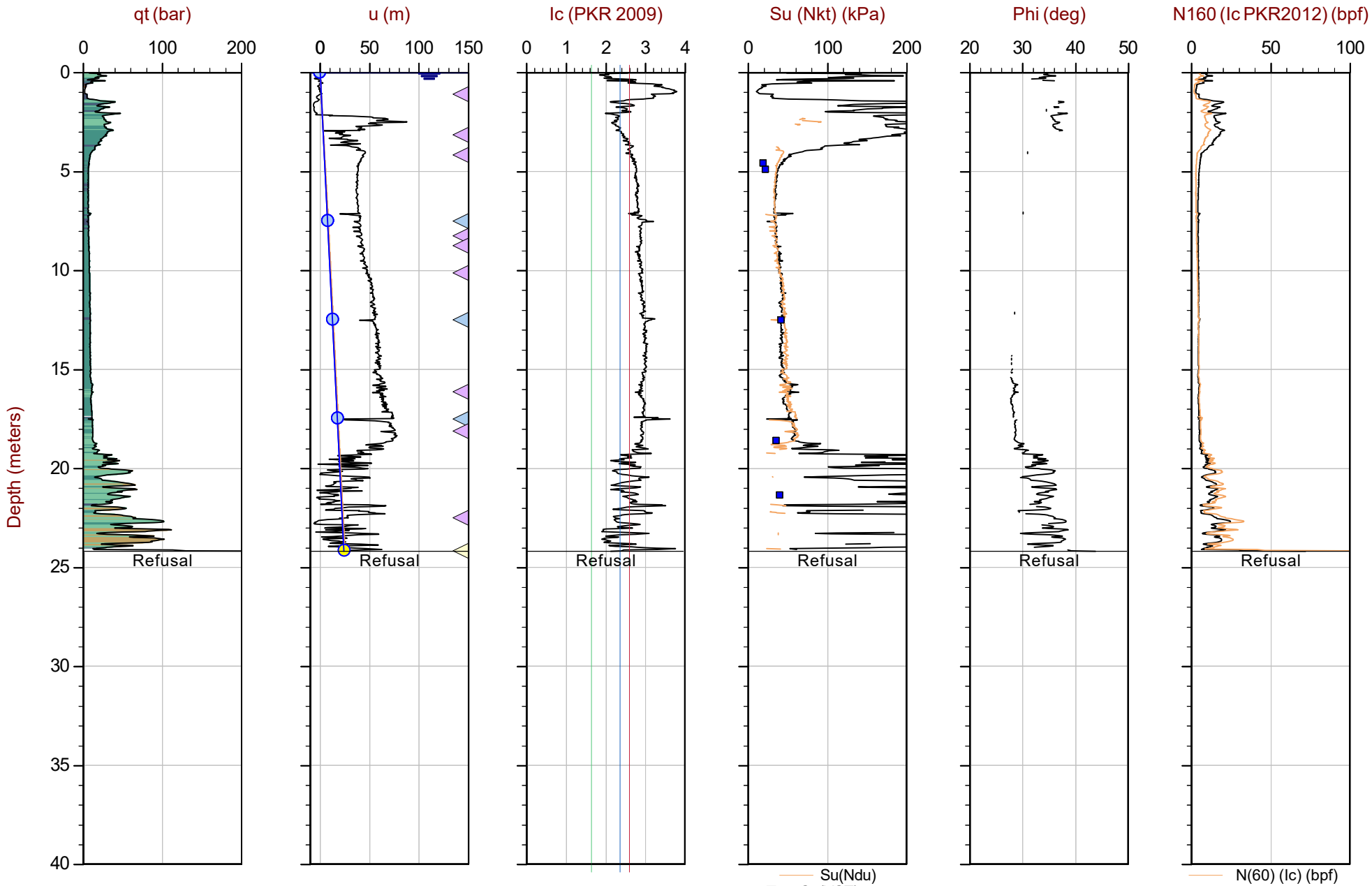
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 24.200 m / 79.40 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF207.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5402798m E: 476813m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

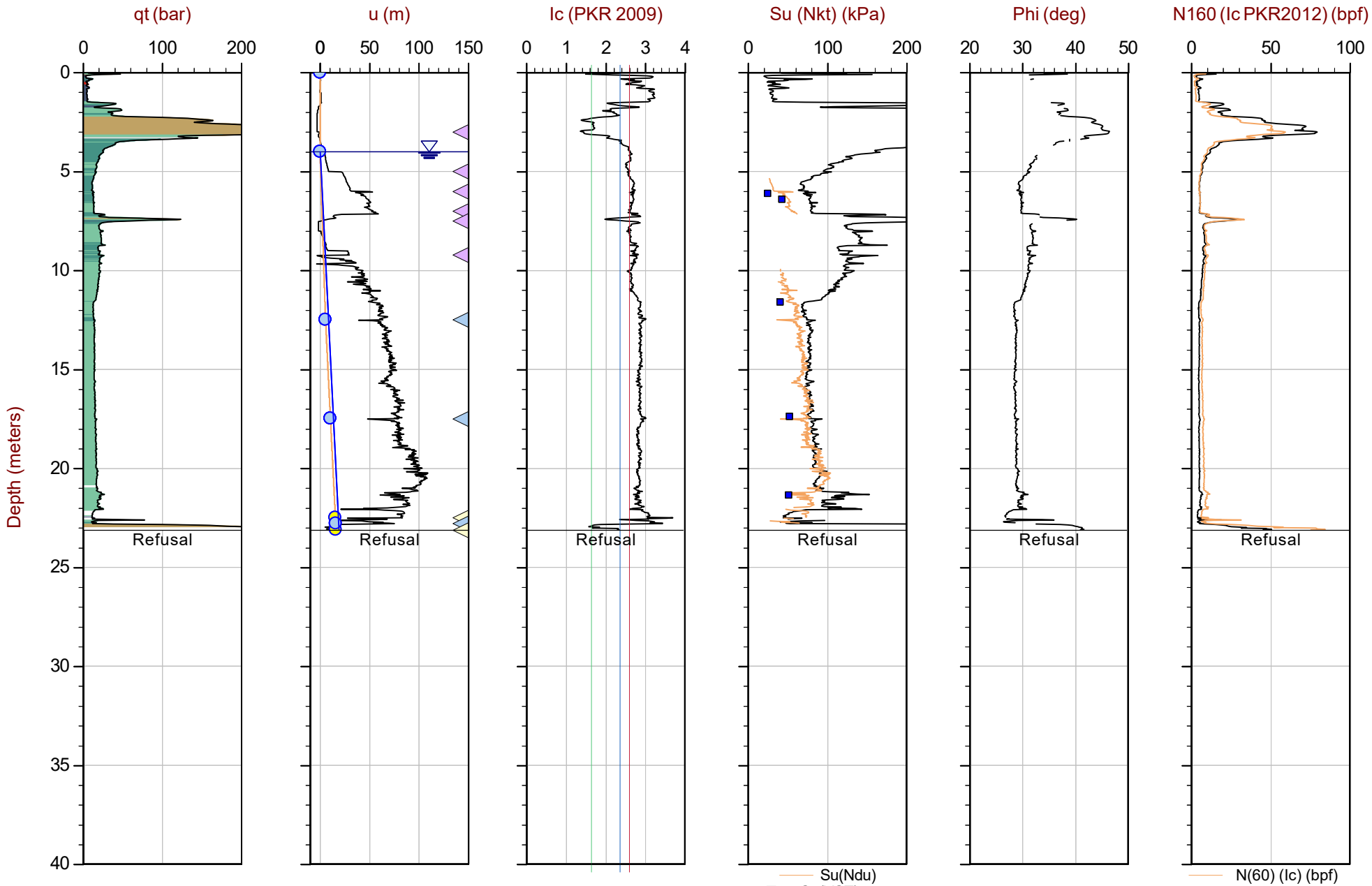
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 23.125 m / 75.87 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD201.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411103m E: 473341m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

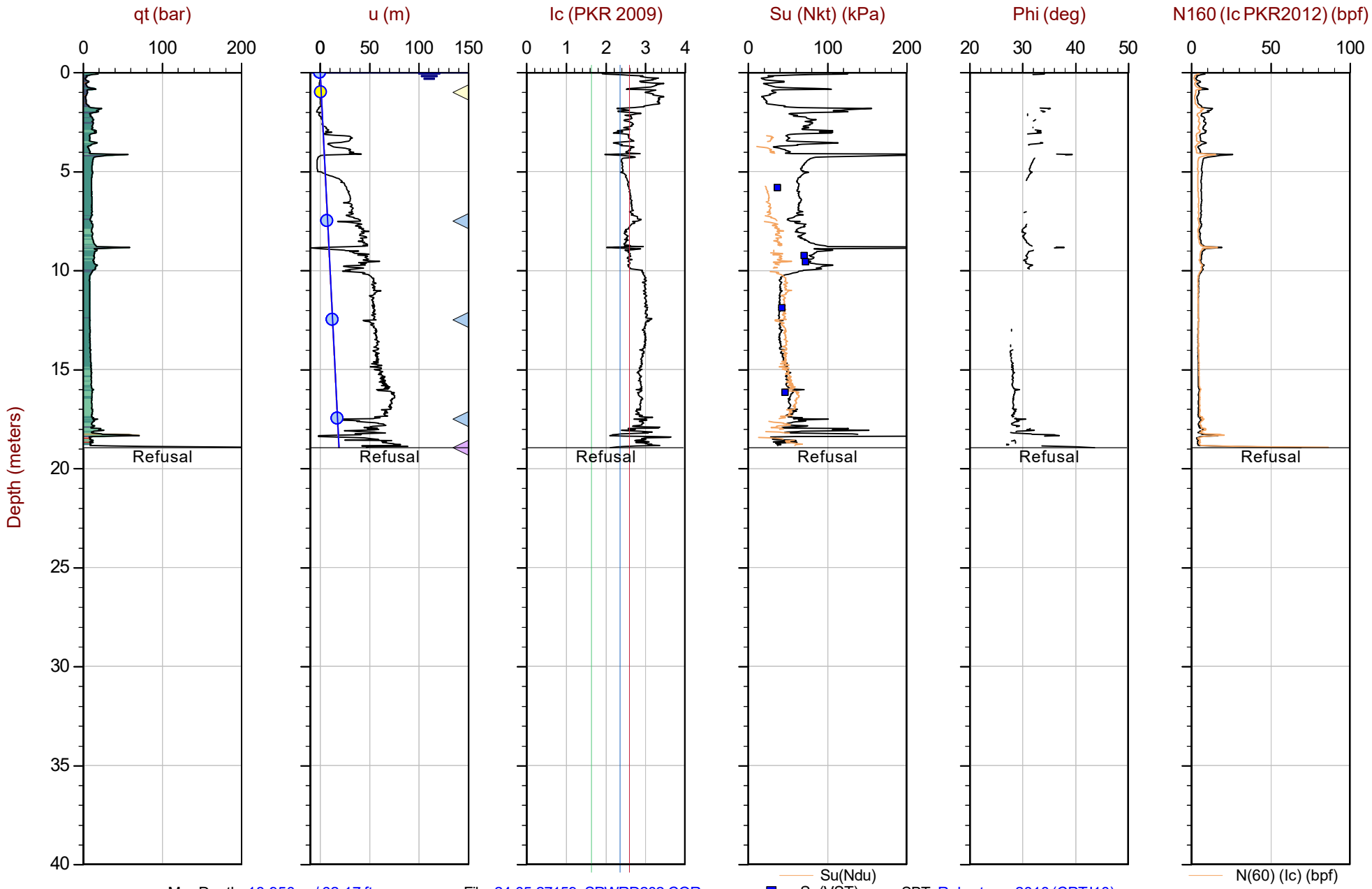
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 18.950 m / 62.17 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD202.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5412168m E: 474136m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

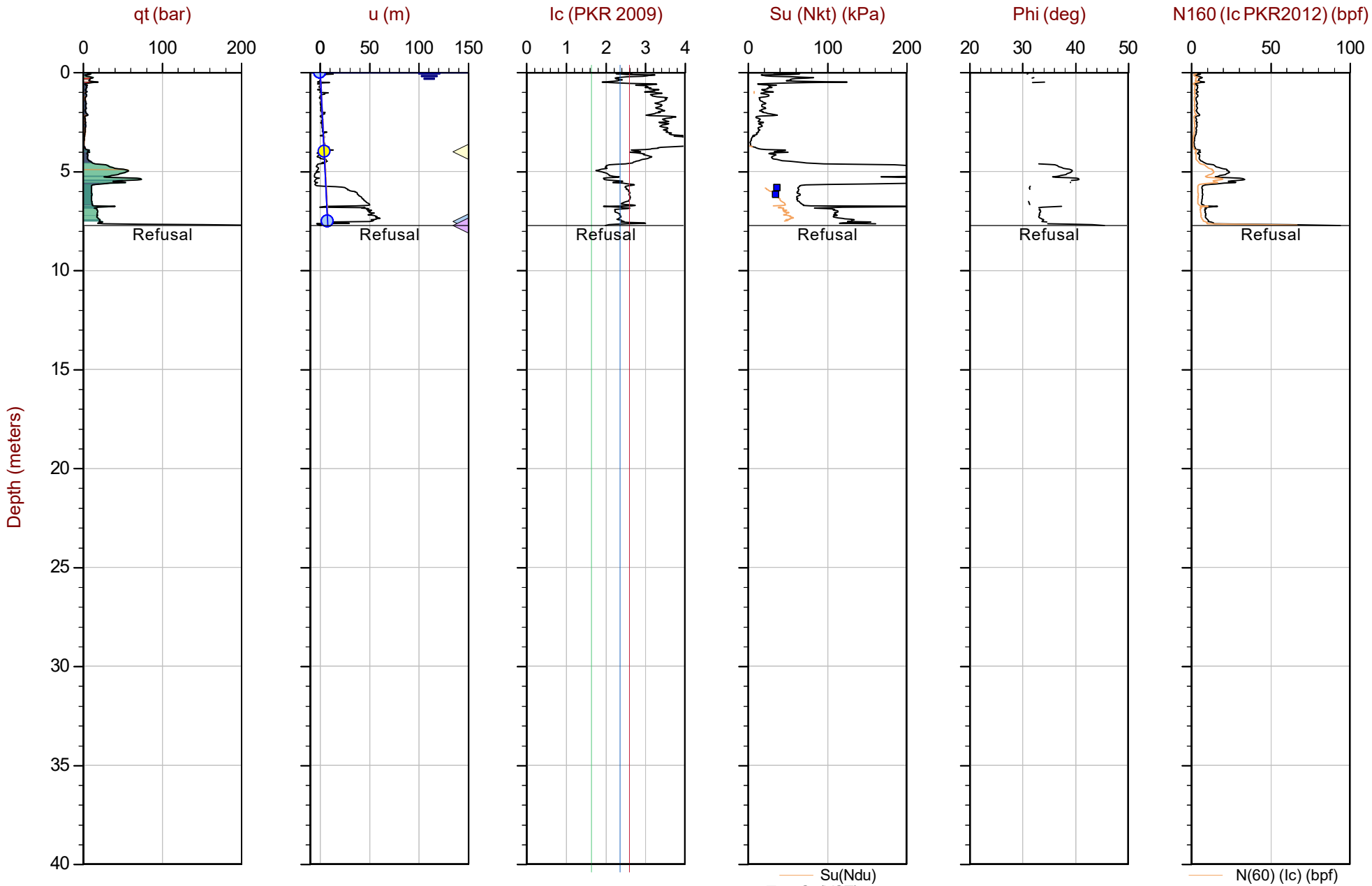
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.725 m / 25.34 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413526m E: 474146m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

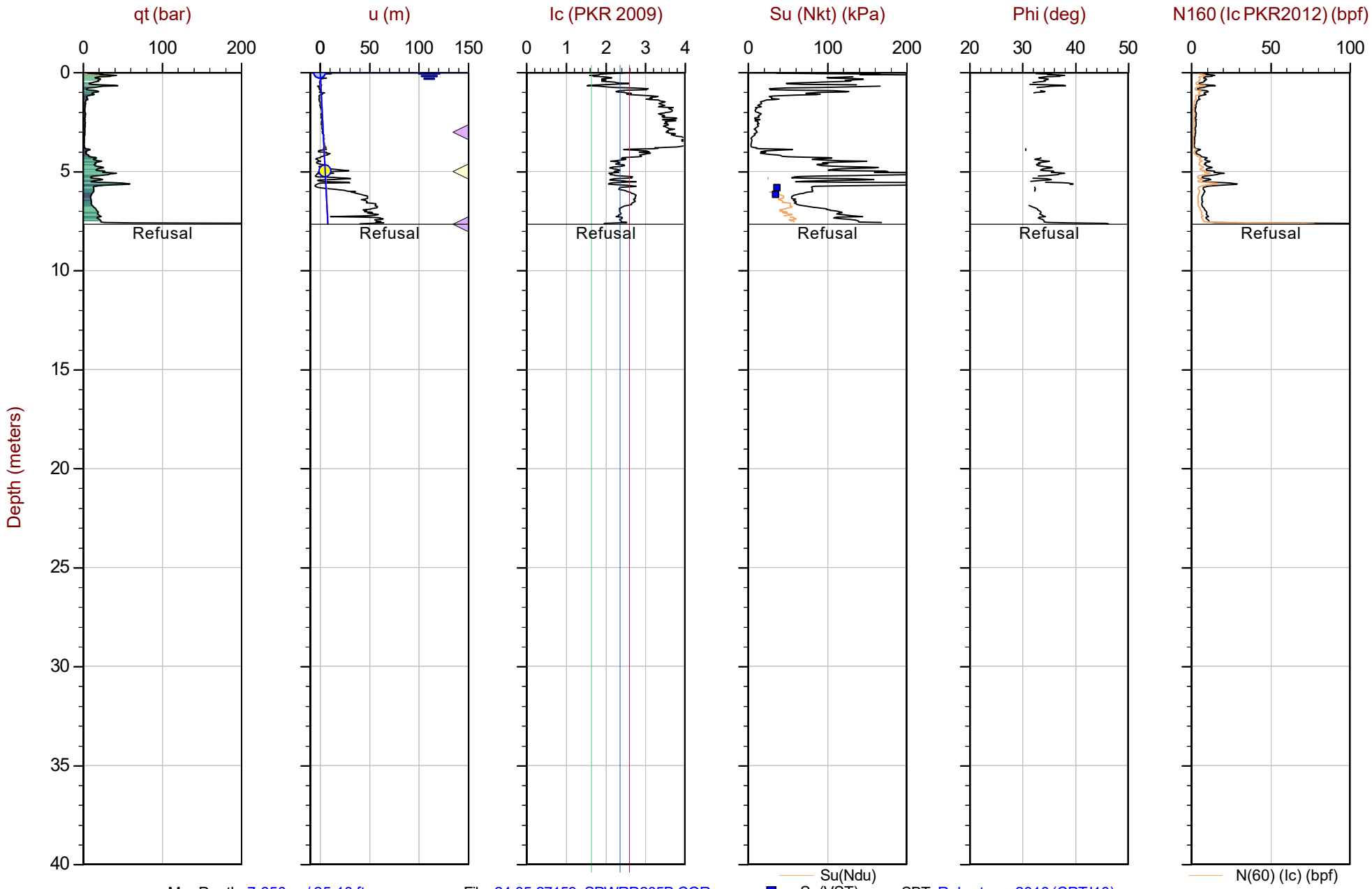
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.650 m / 25.10 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205B.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413524m E: 474147m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

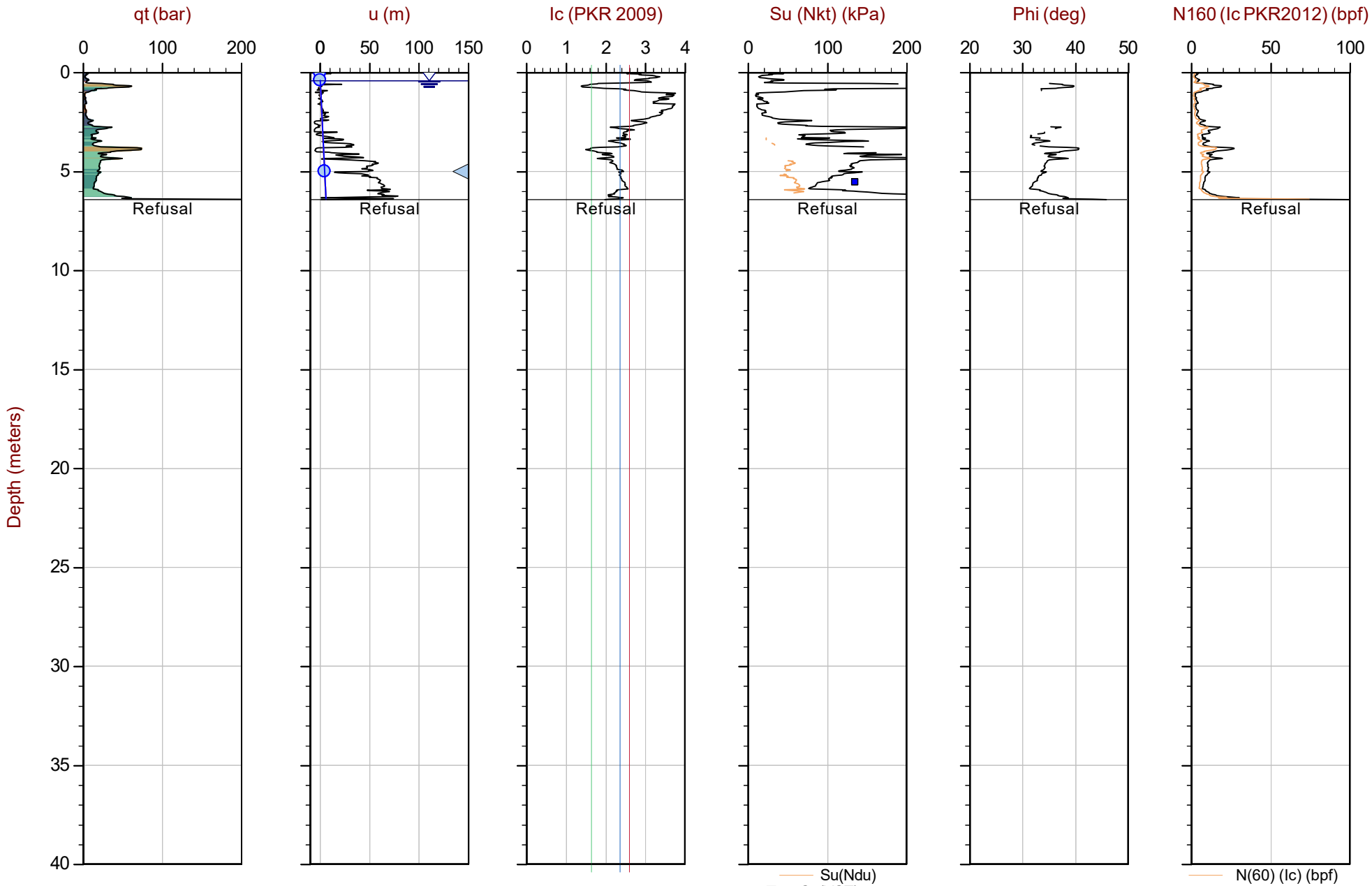
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-12 09:14
Site: Crawford Mine - SRK

Sounding: CPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.425 m / 21.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_CPWRD207.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414555m E: 474237m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

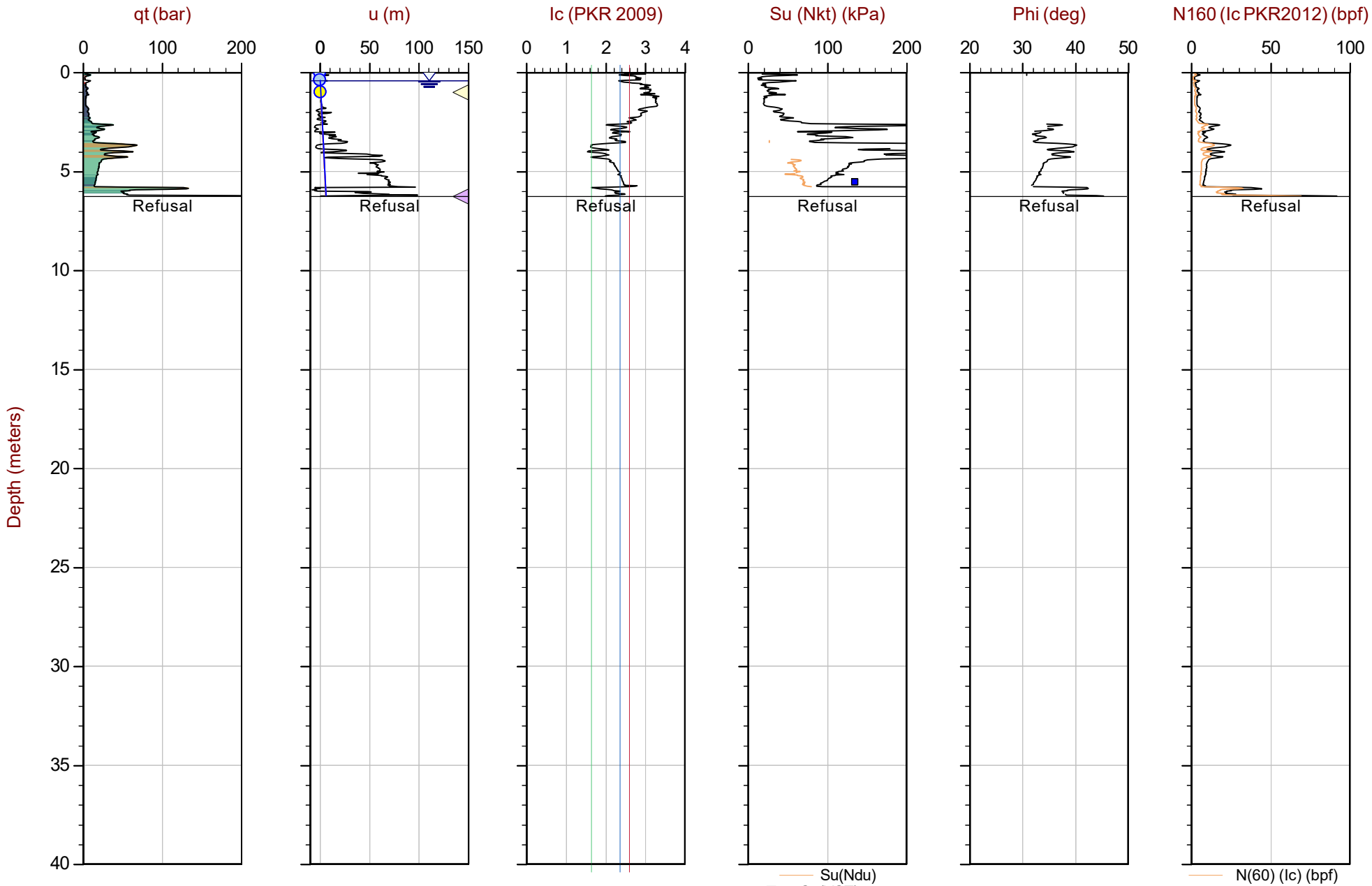
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.250 m / 20.51 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD207.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414553m E: 474239m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

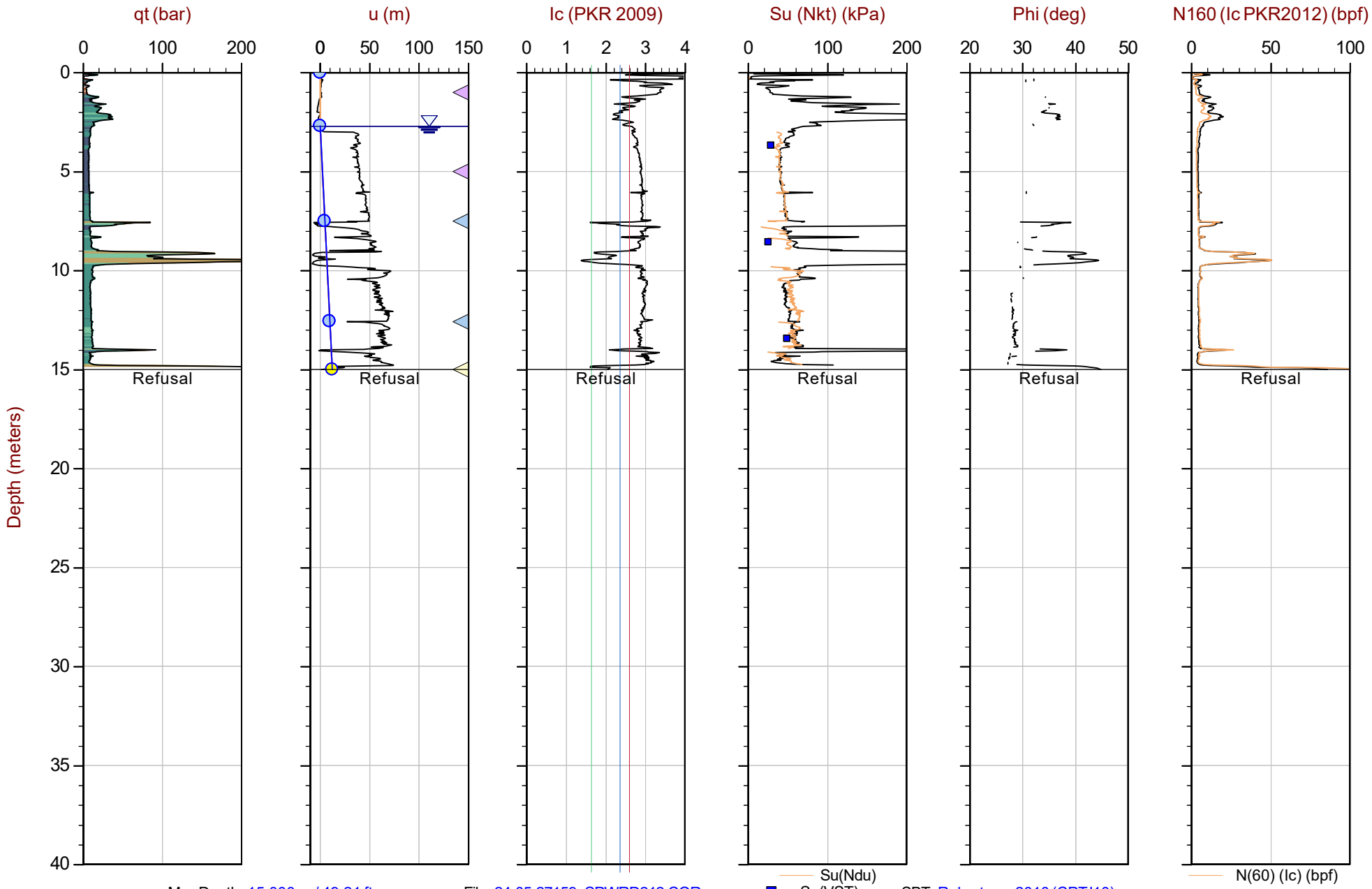
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.000 m / 49.21 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD212.COR
Unit Wt: Rev SBT (PKR2010)
Su Nkt/Ndu: 15.0 / 9.0

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411072m E: 474212m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Seismic Cone Penetration Test Plots

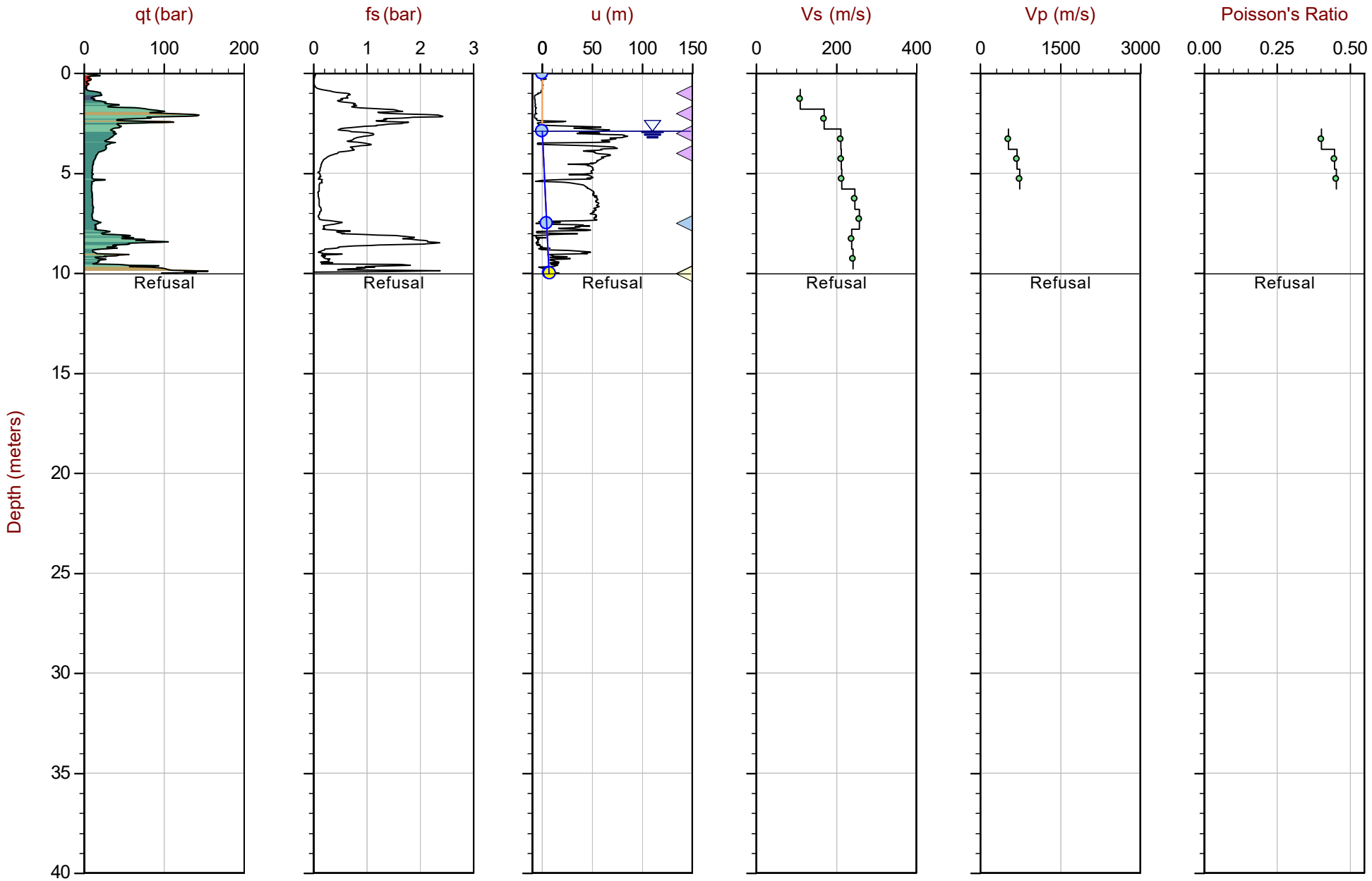
CONETEC

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 10.025 m / 32.89 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP201.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407391m E: 474842m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

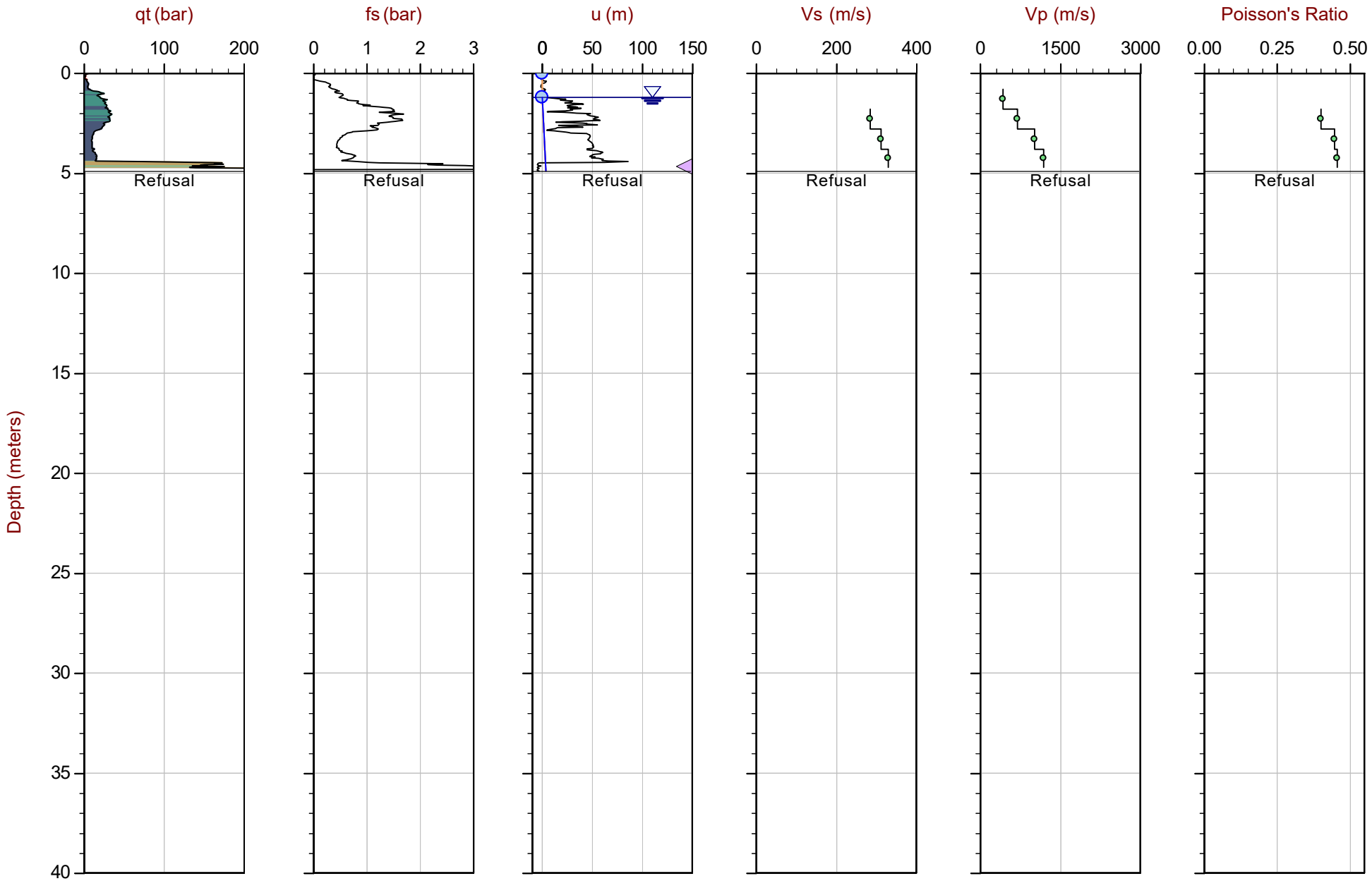
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-16 14:19
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 4.900 m / 16.08 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408601m E: 475374m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

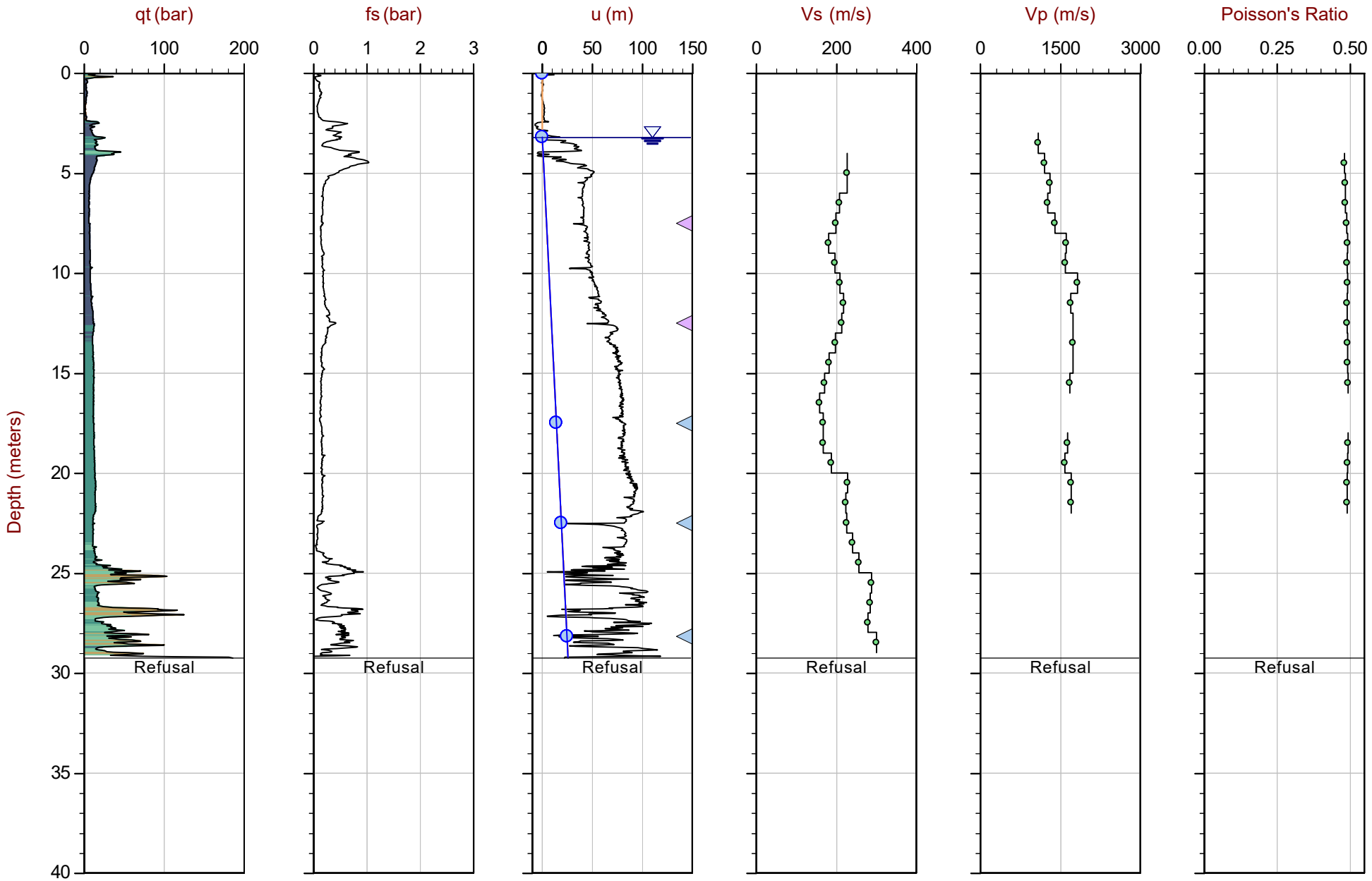
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 29.250 m / 95.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP203.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5409174m E: 476455m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

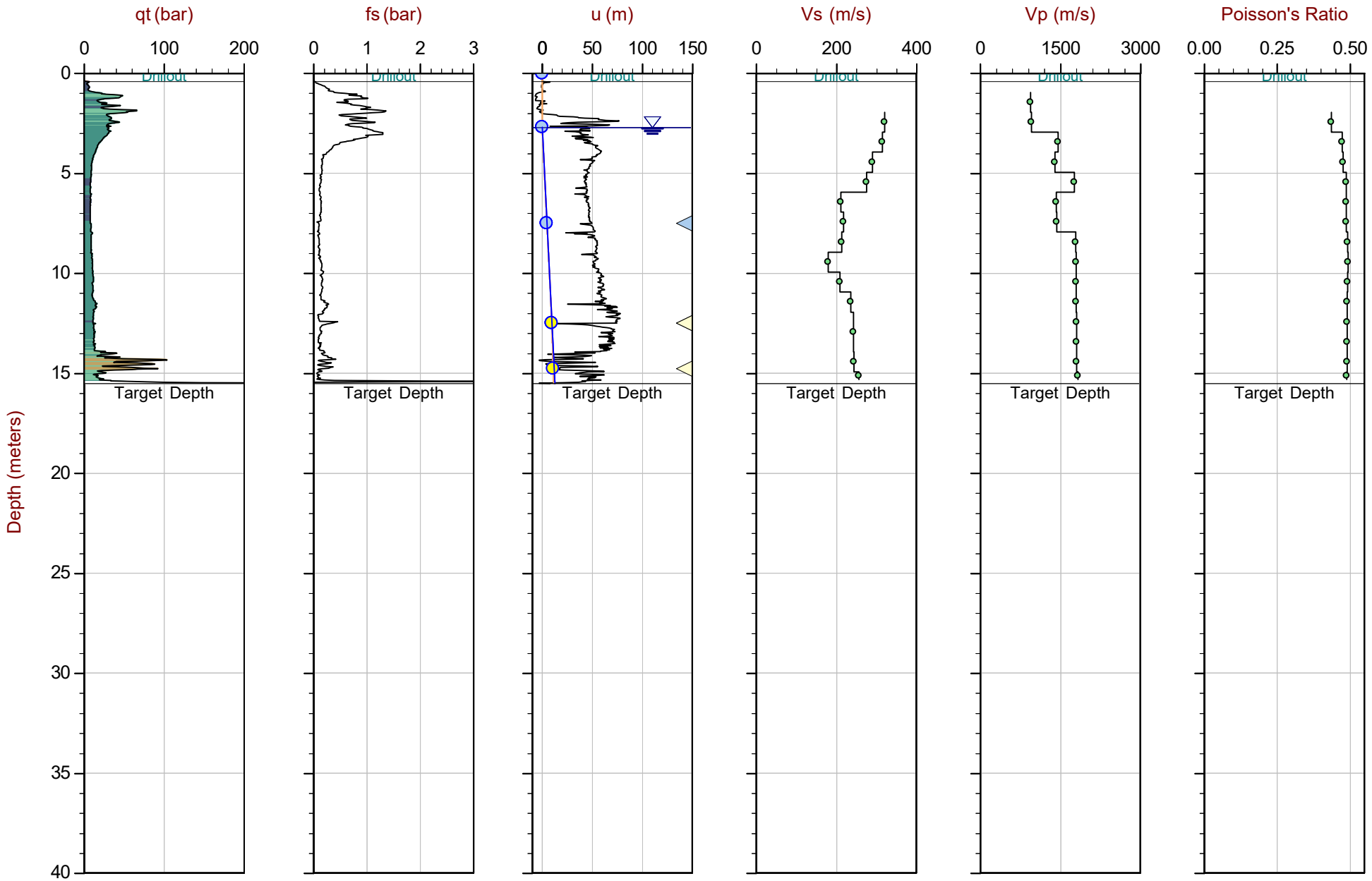
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.525 m / 50.93 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP204.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5407351m E: 475669m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

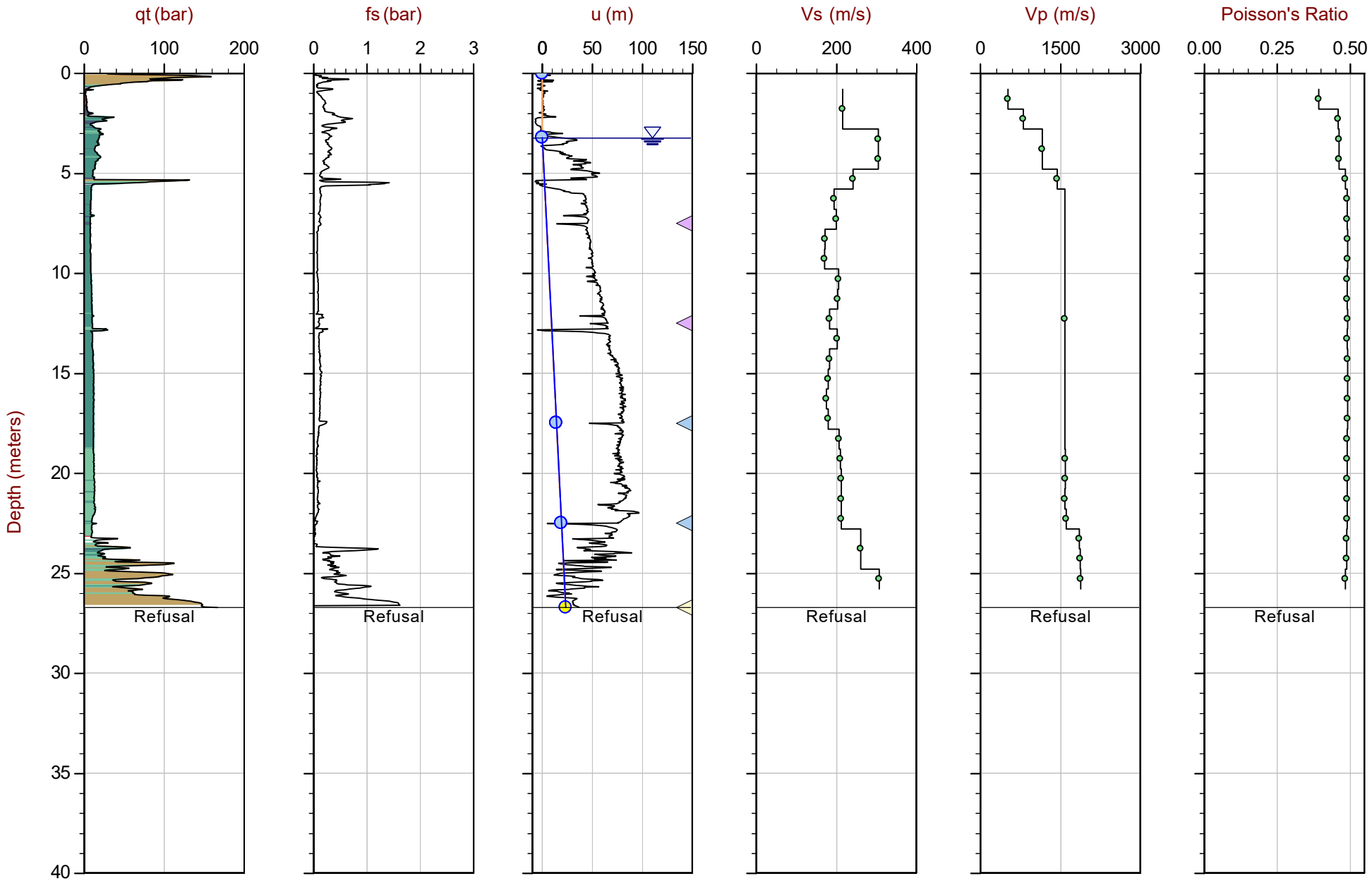
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 26.725 m / 87.68 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SP205.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5408416m E: 476456m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

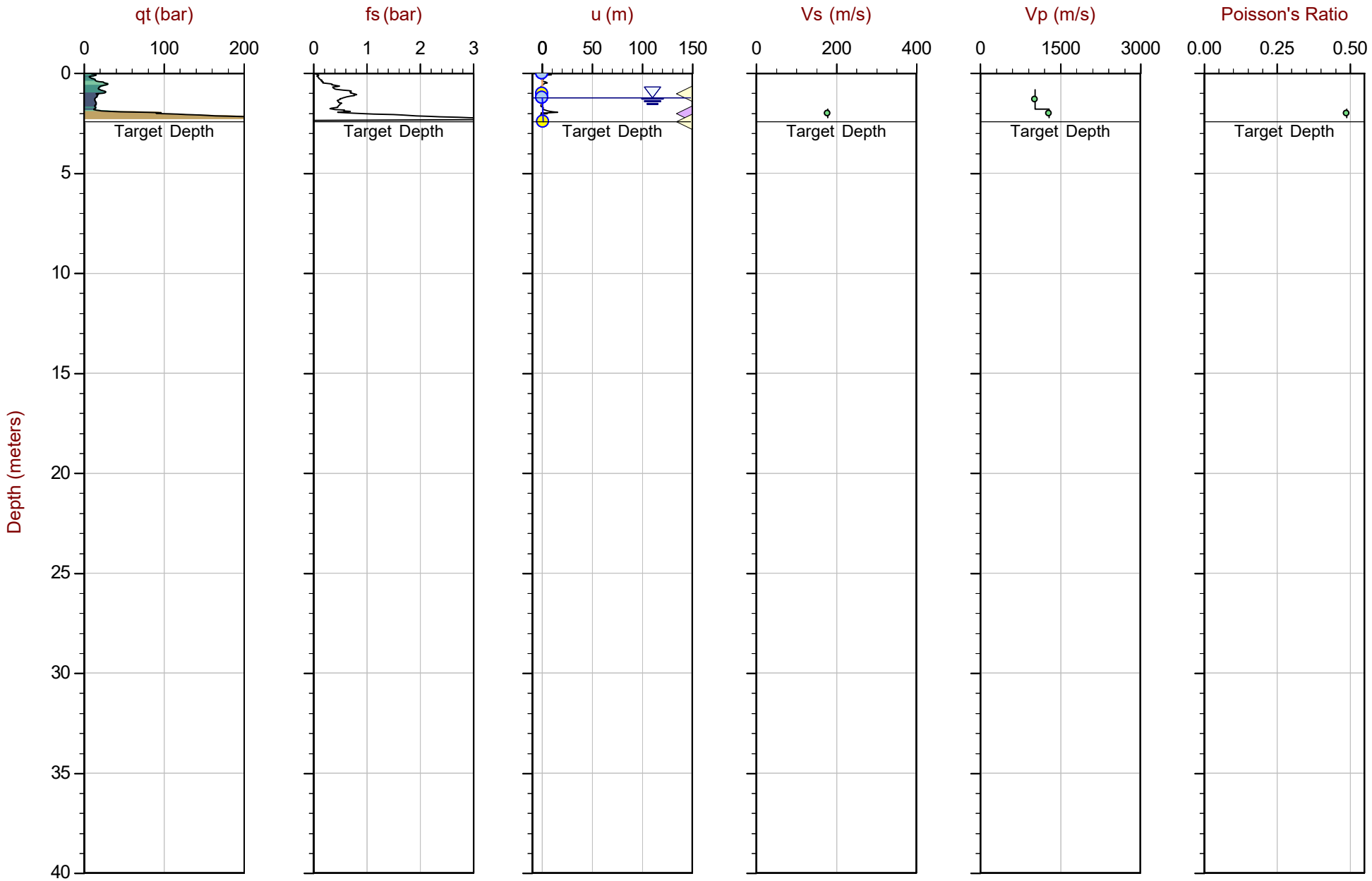
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 2.425 m / 7.96 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF03AB.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414676m E: 472128m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

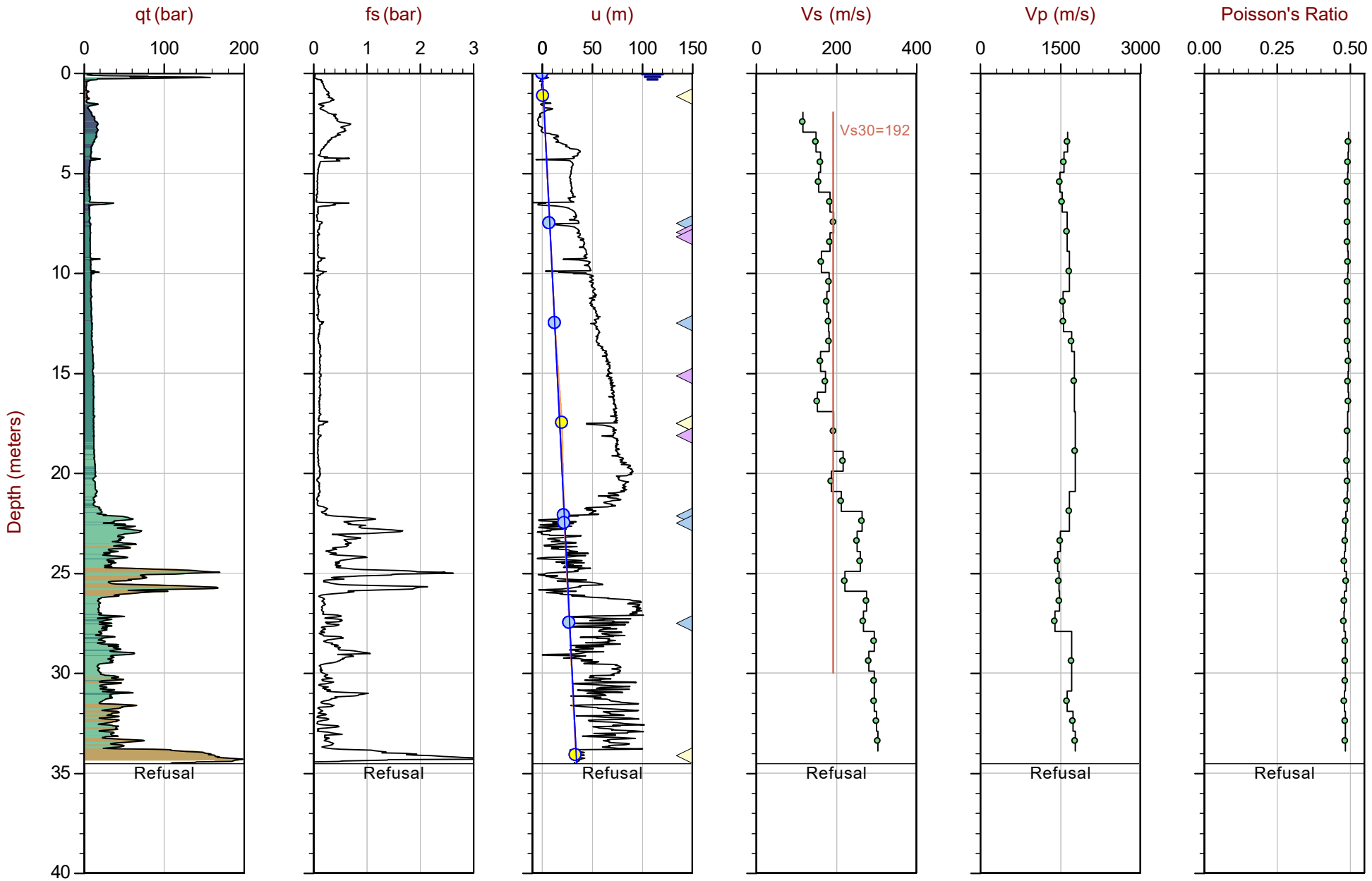
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 34.525 m / 113.27 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF08AB.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5401992m E: 476468m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

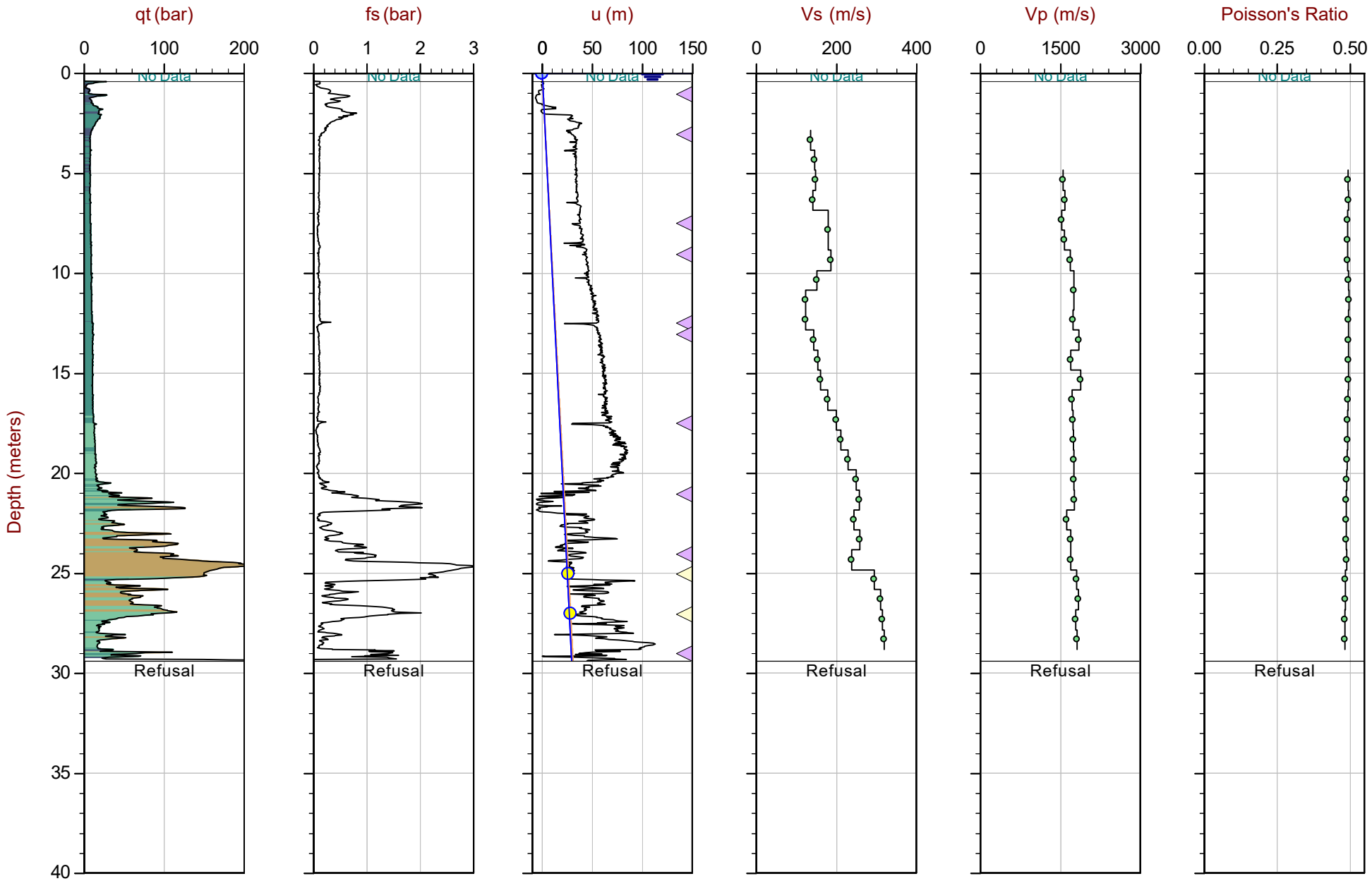
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 29.400 m / 96.46 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5404211m E: 476818m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

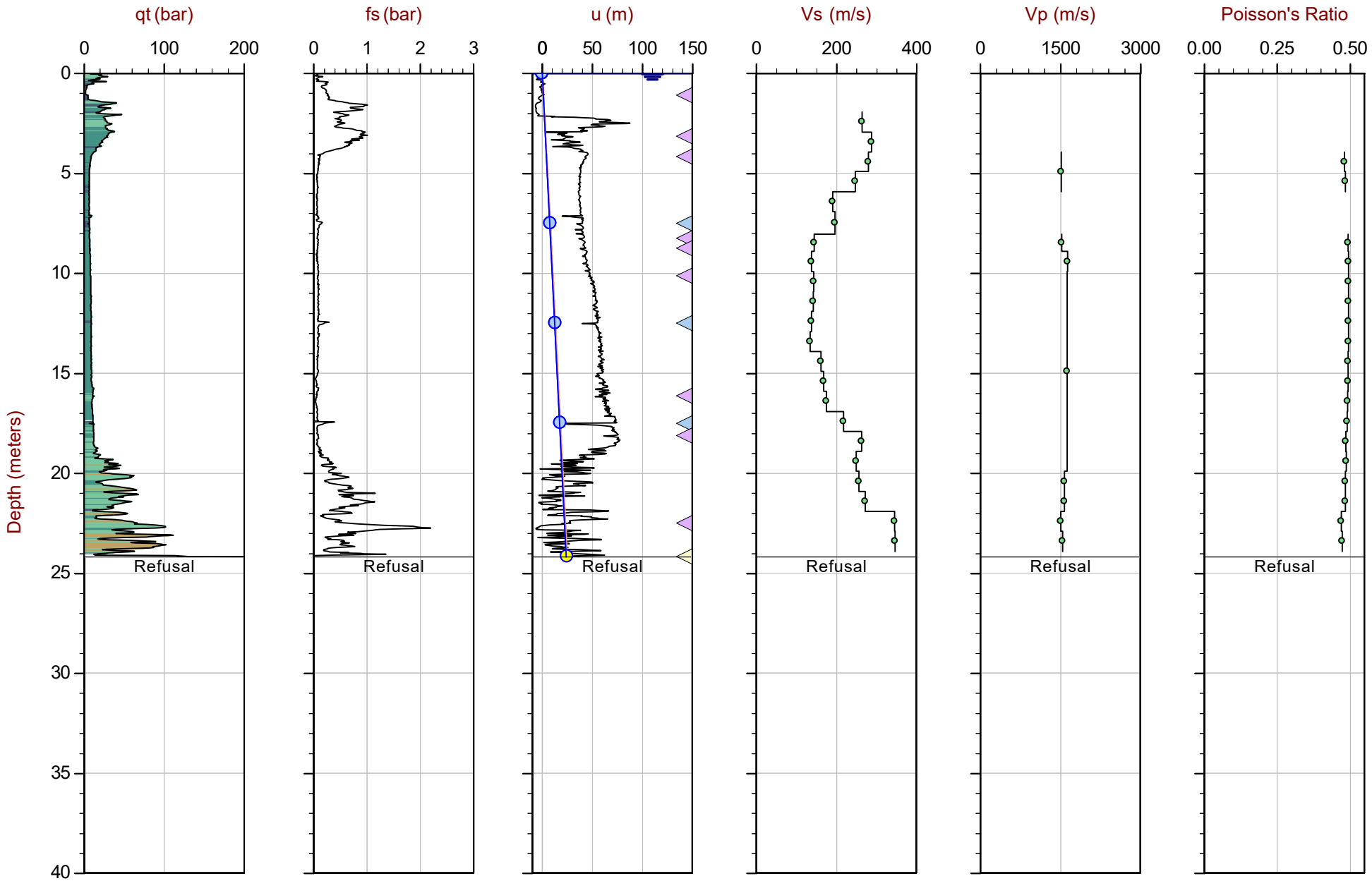
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Max Depth: 24.200 m / 79.40 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPTMF207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5402798m E: 476813m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

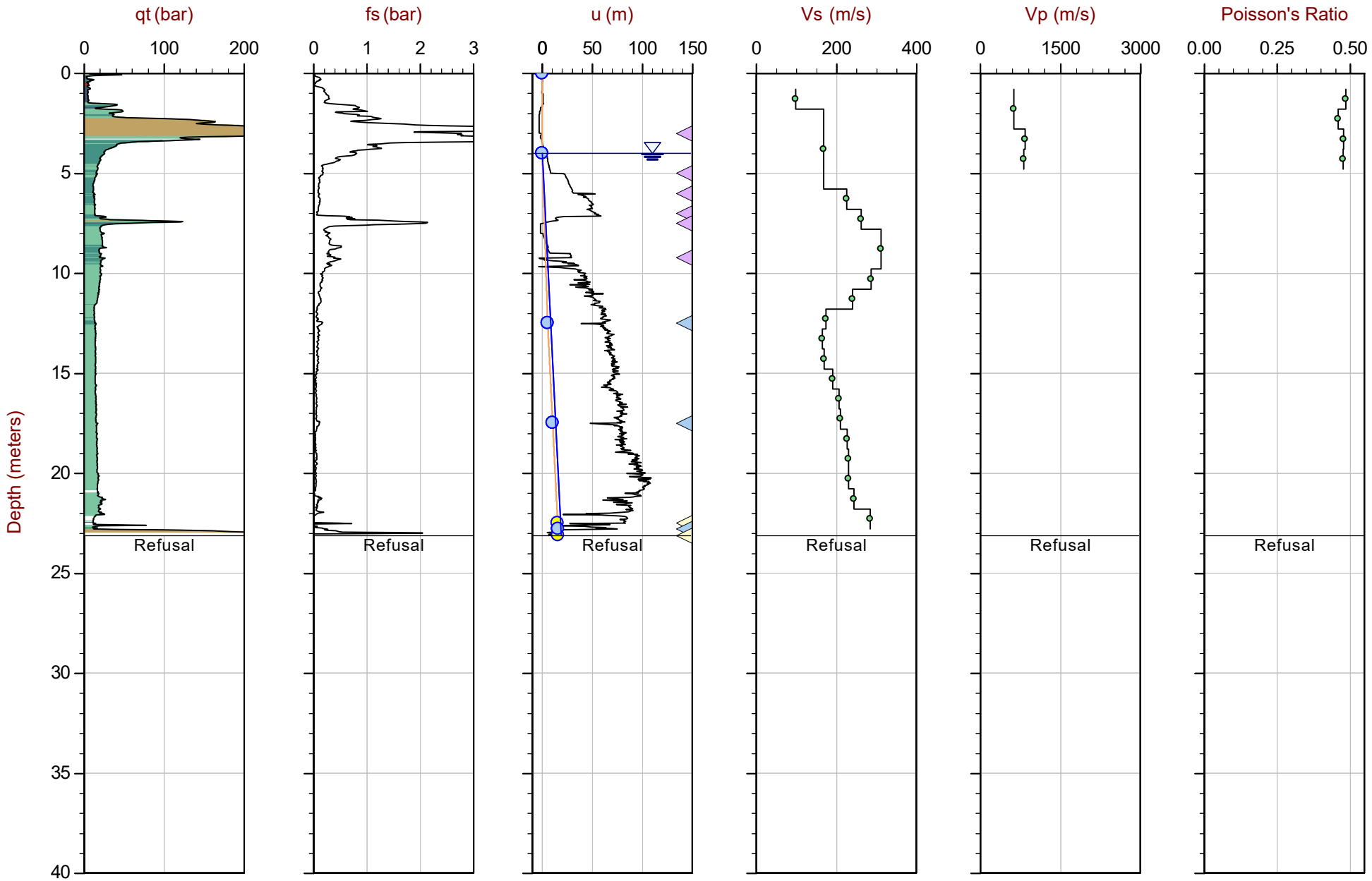
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 23.125 m / 75.87 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD201.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411103m E: 473341m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

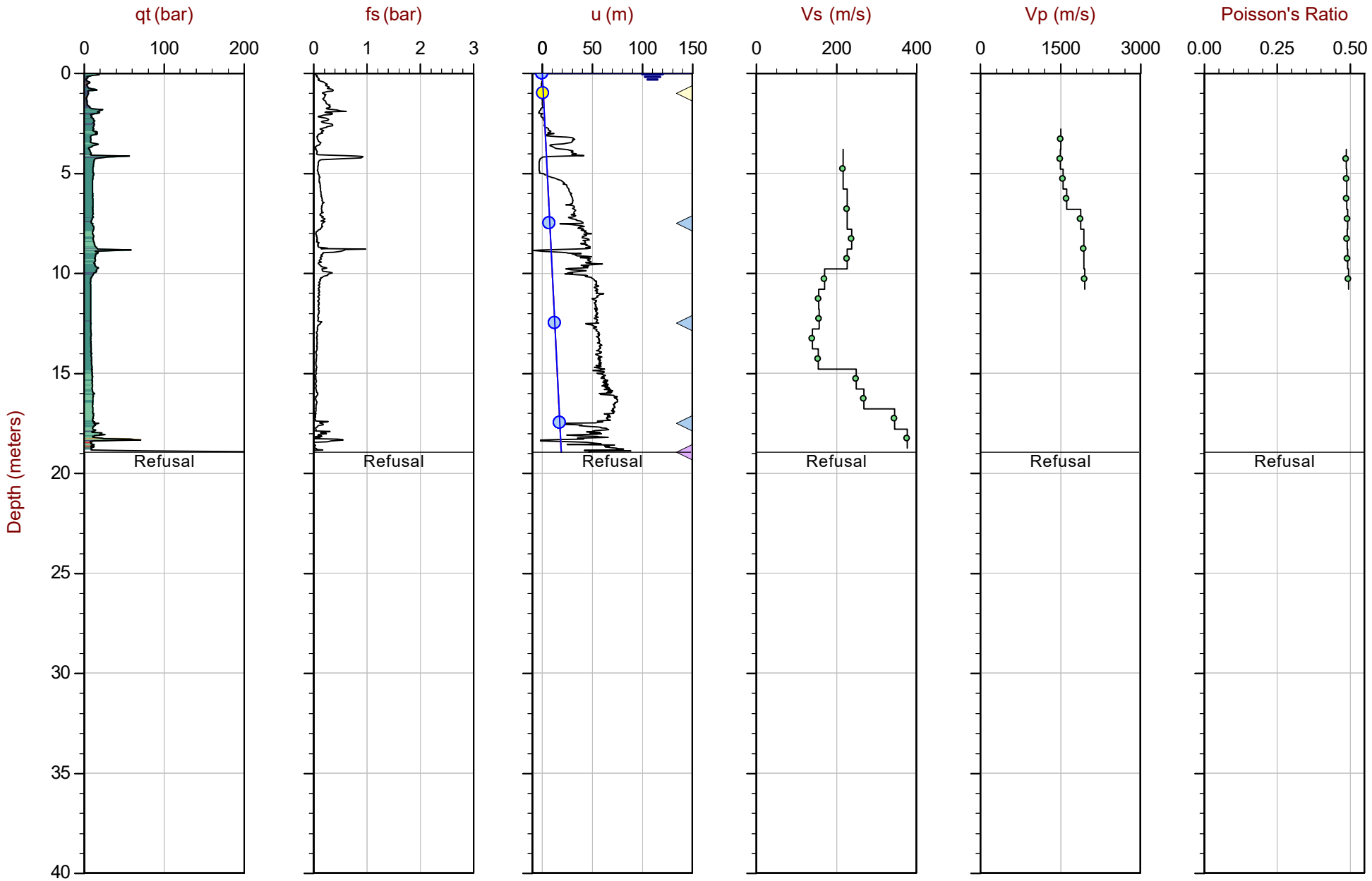
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 18.950 m / 62.17 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD202.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5412168m E: 474136m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

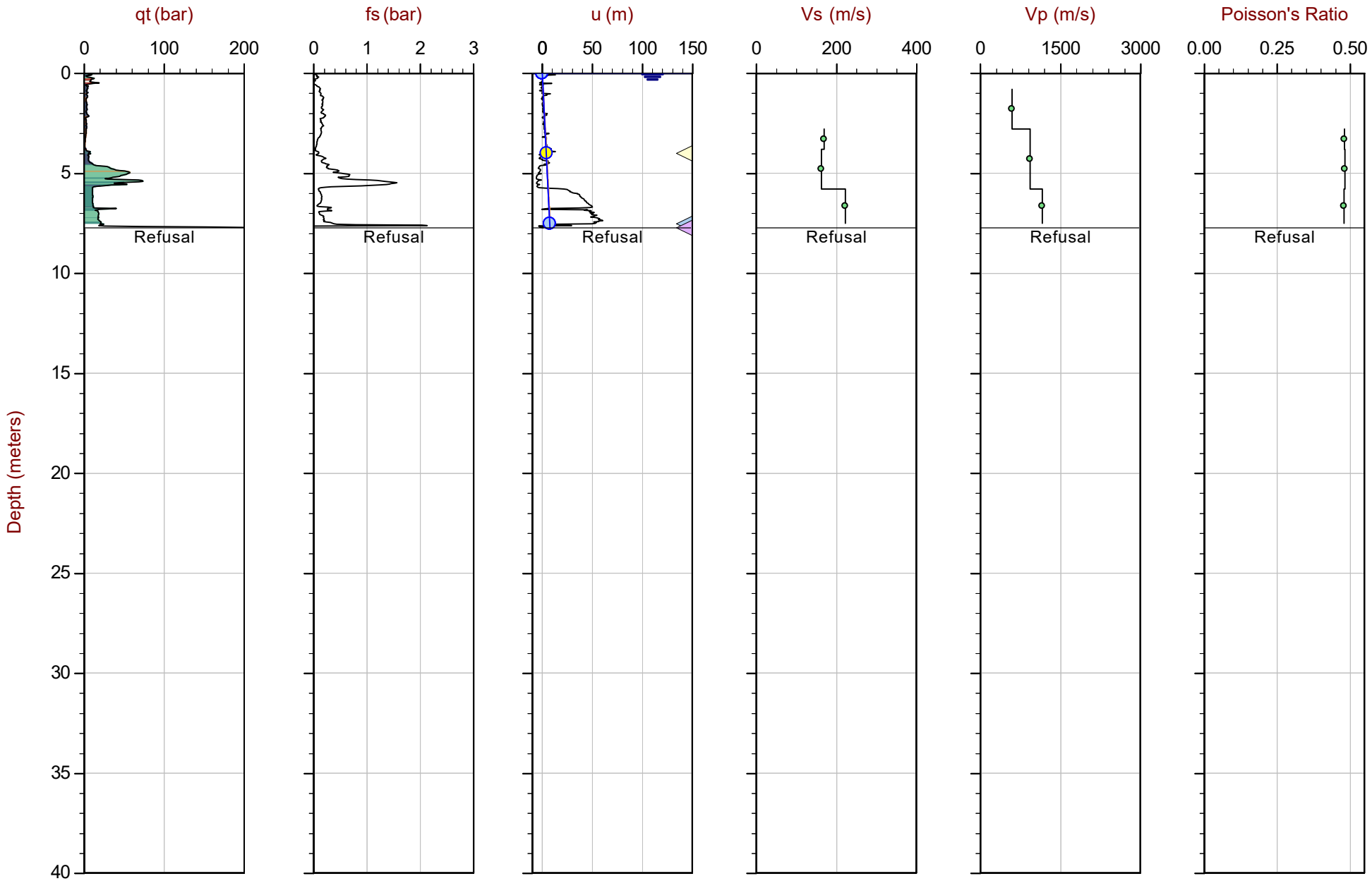
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.725 m / 25.34 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413526m E: 474146m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

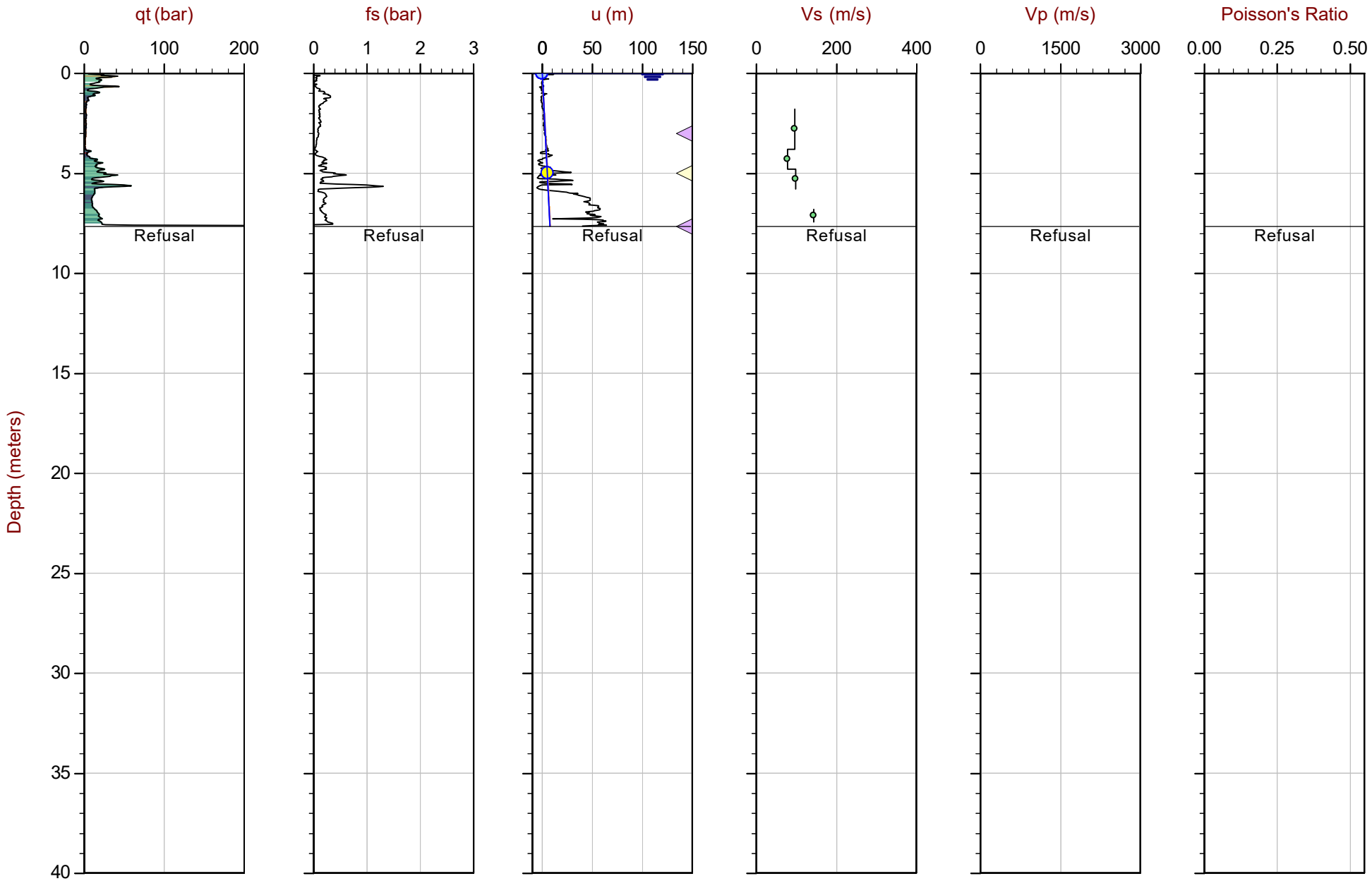
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 7.650 m / 25.10 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD205B.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5413524m E: 474147m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

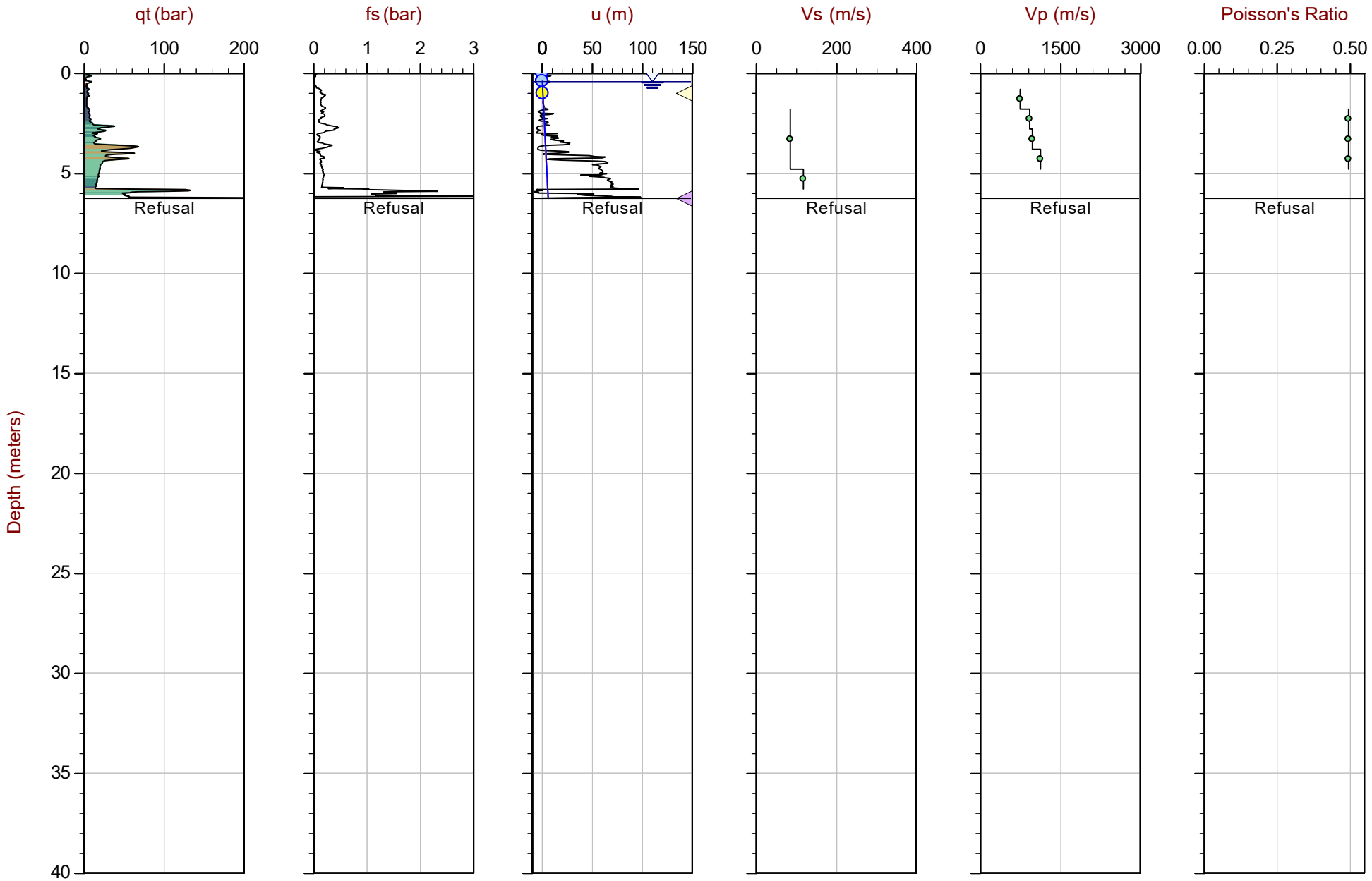
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 6.250 m / 20.51 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD207.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5414553m E: 474239m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

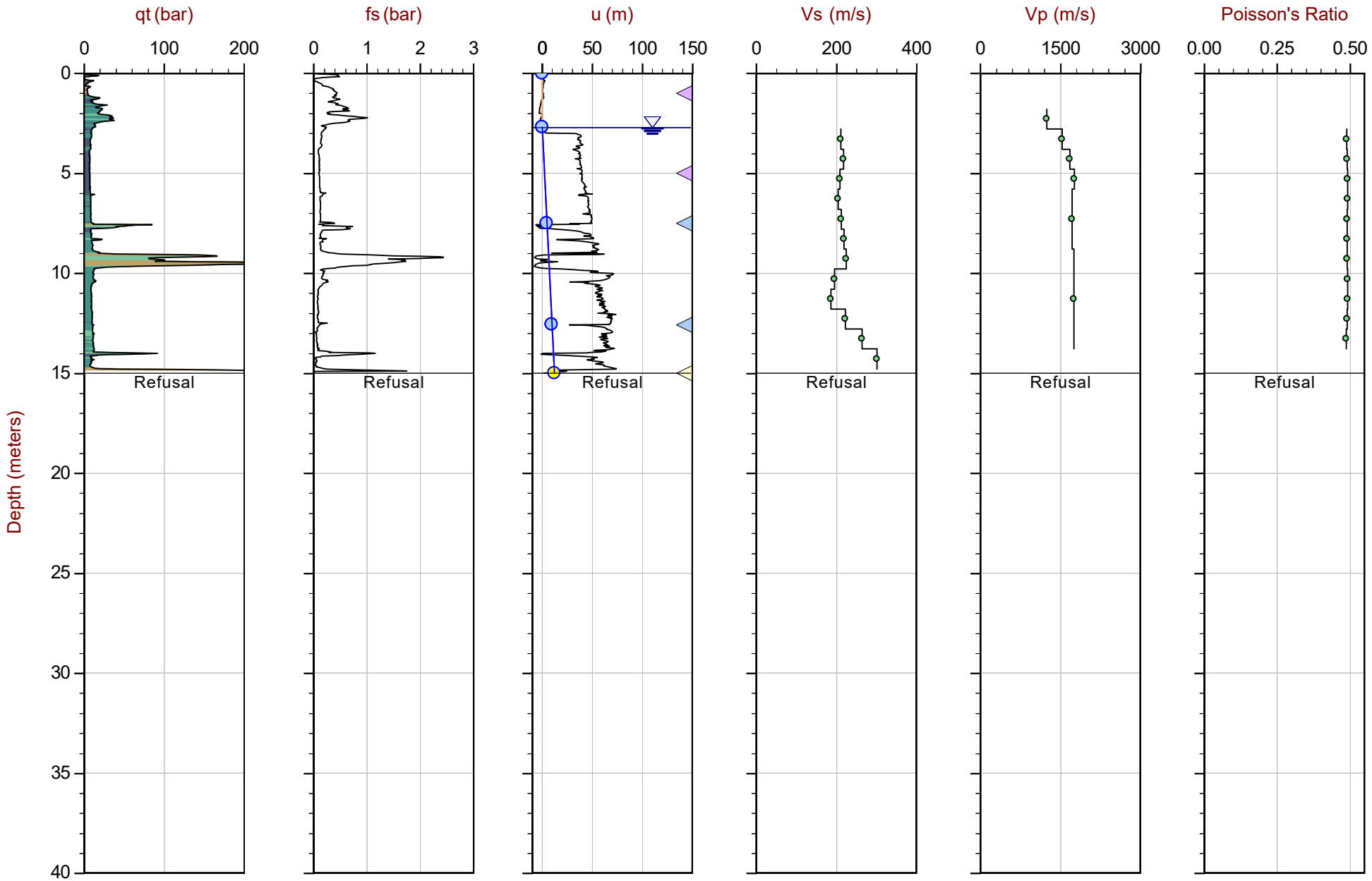
The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Max Depth: 15.000 m / 49.21 ft
Depth Inc: 0.025 m / 0.082 ft
Avg Int: Every Point

File: 24-05-27159_SPWRD212.COR
Unit Wt: Rev SBT (PKR2010)

SBT: Robertson, 2010 (CPT'10)
Coords: UTM 17N N: 5411072m E: 474212m
Sheet No: 1 of 1

Overplot Item: Ueq, Assumed Ueq, Dissipation, Ueq achieved, Dissipation, Ueq not achieved, Dissipation, Ueq assumed, Ueq Line, Hydrostatic Line

The reported coordinates were acquired from consumer grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Seismic Cone Penetration Test Shear Wave (Vs) Tabular Results

CONETEC

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH201
Date:	2024-02-19
Seismic Source:	Wedge
Seismic Offset (m):	1.20
Source Depth (m):	0.10
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.39			
2.00	1.80	2.08	0.69	6.31	110
3.00	2.80	2.96	0.87	5.15	170
4.00	3.80	3.89	0.94	4.42	212
5.00	4.80	4.85	0.96	4.51	213
6.00	5.80	5.83	0.97	4.55	214
7.00	6.80	6.81	0.98	3.99	246
8.00	7.80	7.79	0.99	3.82	258
9.00	8.80	8.78	0.99	4.15	239
10.00	9.80	9.77	0.99	4.09	243

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH202
Date:	2024-02-16
Seismic Source:	Wedge
Seismic Offset (m):	0.95
Source Depth (m):	0.30
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.00	1.80	1.78			
3.00	2.80	2.67	0.90	3.15	285
4.00	3.80	3.63	0.95	3.06	312
4.90	4.70	4.50	0.87	2.64	331

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH203
Date:	2024-02-14
Seismic Source:	Wedge
Seismic Offset (m):	1.00
Source Depth (m):	0.30
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
4.20	4.00	3.83			
6.20	6.00	5.79	1.95	8.60	227
7.20	7.00	6.77	0.99	4.75	208
8.20	8.00	7.77	0.99	4.98	199
9.20	9.00	8.76	0.99	5.47	182
10.20	10.00	9.75	0.99	5.04	197
11.20	11.00	10.75	1.00	4.75	210
12.20	12.00	11.74	1.00	4.56	218
13.20	13.00	12.74	1.00	4.65	214
14.20	14.00	13.74	1.00	5.04	198
15.20	15.00	14.73	1.00	5.47	182
16.20	16.00	15.73	1.00	5.82	172
17.20	17.00	16.73	1.00	6.29	159
18.20	18.00	17.73	1.00	5.96	168
19.20	19.00	18.73	1.00	5.96	168
20.20	20.00	19.73	1.00	5.29	189
21.20	21.00	20.72	1.00	4.37	229
22.20	22.00	21.72	1.00	4.46	224
23.20	23.00	22.72	1.00	4.40	227
24.20	24.00	23.72	1.00	4.14	242
25.20	25.00	24.72	1.00	3.88	257
26.20	26.00	25.72	1.00	3.45	289
27.20	27.00	26.72	1.00	3.51	285
28.18	27.98	27.70	0.98	3.50	279
29.20	29.00	28.72	1.02	3.38	302

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH204
Date:	2024-02-18
Seismic Source:	Wedge
Seismic Offset (m):	1.20
Source Depth (m):	0.10
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.15	1.95	2.21			
3.15	2.95	3.09	0.89	2.76	322
4.15	3.95	4.03	0.94	2.98	316
5.15	4.95	5.00	0.96	3.31	291
6.15	5.95	5.97	0.98	3.53	276
7.15	6.95	6.95	0.98	4.63	212
8.15	7.95	7.94	0.99	4.52	218
9.15	8.95	8.93	0.99	4.64	214
10.15	9.95	9.92	0.99	5.52	180
11.15	10.95	10.92	0.99	4.74	209
12.15	11.95	11.91	1.00	4.20	237
14.15	13.95	13.90	1.99	8.16	244
15.15	14.95	14.90	1.00	4.08	244
15.52	15.32	15.27	0.37	1.43	257

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH205
Date:	2024-02-26
Seismic Source:	Wedge
Seismic Offset (m):	1.65
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.70			
3.00	2.80	2.91	1.21	5.61	217
4.00	3.80	3.78	0.87	2.84	305
5.00	4.80	4.70	0.92	3.01	306
6.00	5.80	5.65	0.95	3.91	243
7.00	6.80	6.61	0.96	4.94	195
8.00	7.80	7.58	0.97	4.85	201
9.00	8.80	8.56	0.98	5.68	172
10.00	9.80	9.54	0.98	5.74	171
11.00	10.80	10.53	0.99	4.77	207
12.00	11.80	11.52	0.99	4.84	204
13.00	12.80	12.51	0.99	5.41	183
14.00	13.80	13.50	0.99	4.89	203
15.00	14.80	14.49	0.99	5.39	184
16.00	15.80	15.49	0.99	5.51	180
17.00	16.80	16.48	1.00	5.68	175
18.00	17.80	17.48	1.00	5.51	181
19.00	18.80	18.47	1.00	4.79	208
20.00	19.80	19.47	1.00	4.72	211
21.00	20.80	20.47	1.00	4.68	213
22.00	21.80	21.46	1.00	4.67	213
23.00	22.80	22.46	1.00	4.67	213
25.00	24.80	24.46	2.00	7.61	262
26.00	25.80	25.45	1.00	3.24	308

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW03AB
Date:	2024-03-13
Seismic Source:	Wedge
Seismic Offset (m):	1.70
Source Depth (m):	0.30
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.00	1.80	2.27			
2.43	2.23	2.57	0.31	1.70	179

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW08AB
Date:	2024-03-20
Seismic Source:	Plate
Seismic Offset (m):	2.40
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.15	1.95	3.09			
3.15	2.95	3.80	0.71	6.08	117
4.15	3.95	4.62	0.82	5.47	150
5.15	4.95	5.50	0.88	5.46	161
6.15	5.95	6.42	0.92	5.84	157
7.15	6.95	7.35	0.94	5.06	185
8.18	7.98	8.33	0.98	5.06	194
9.12	8.92	9.24	0.90	4.89	185
10.18	9.98	10.27	1.03	6.28	164
11.12	10.92	11.18	0.92	5.03	182
12.15	11.95	12.19	1.01	5.70	177
13.12	12.92	13.14	0.95	5.26	181
14.12	13.92	14.13	0.98	5.40	182
15.12	14.92	15.11	0.99	6.15	161
16.15	15.95	16.13	1.02	5.87	173
17.12	16.92	17.09	0.96	6.27	153
19.12	18.92	19.07	1.98	10.23	194
20.12	19.92	20.06	0.99	4.55	218
21.12	20.92	21.06	0.99	5.26	189
22.12	21.92	22.05	0.99	4.66	213
23.12	22.92	23.05	0.99	3.74	266
24.12	23.92	24.04	1.00	3.95	252
25.12	24.92	25.04	1.00	3.81	261
26.12	25.92	26.03	1.00	4.49	222
27.12	26.92	27.03	1.00	3.61	276
28.12	27.92	28.02	1.00	3.71	268
29.12	28.92	29.02	1.00	3.37	295
30.12	29.92	30.02	1.00	3.54	281
31.12	30.92	31.01	1.00	3.37	296
32.12	31.92	32.01	1.00	3.37	296
33.12	32.92	33.01	1.00	3.31	302

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW08AB
Date:	2024-03-20
Seismic Source:	Plate
Seismic Offset (m):	2.40
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
34.12	33.92	34.01	1.00	3.27	305

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-BH202
Date:	2024-03-15
Seismic Source:	Plate
Seismic Offset (m):	5.60
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.05	2.85	6.28			
4.05	3.85	6.80	0.51	3.75	137
5.05	4.85	7.41	0.61	4.18	146
6.05	5.85	8.10	0.69	4.63	149
7.05	6.85	8.85	0.75	5.29	142
9.05	8.85	10.47	1.63	9.03	180
10.08	9.88	11.36	0.88	4.74	187
11.05	10.85	12.21	0.85	5.62	152
12.05	11.85	13.11	0.90	7.28	123
13.05	12.85	14.02	0.91	7.38	123
14.05	13.85	14.94	0.92	6.39	144
15.05	14.85	15.87	0.93	6.06	154
16.05	15.85	16.81	0.94	5.84	161
17.05	16.85	17.76	0.95	5.29	179
18.05	17.85	18.71	0.95	4.74	201
19.05	18.85	19.66	0.96	4.52	212
20.05	19.85	20.63	0.96	4.19	229
21.05	20.85	21.59	0.96	3.86	250
22.05	21.85	22.56	0.97	3.75	258
23.05	22.85	23.53	0.97	3.97	245
24.05	23.85	24.50	0.97	3.75	260
25.05	24.85	25.47	0.97	4.08	239
26.02	25.82	26.42	0.95	3.20	296
27.05	26.85	27.43	1.01	3.24	311
28.05	27.85	28.41	0.98	3.10	316
29.02	28.82	29.36	0.95	2.97	321

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-BH207
Date:	2024-03-18
Seismic Source:	Plate
Seismic Offset (m):	2.60
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.12	1.92	3.23			
3.15	2.95	3.93	0.70	2.64	265
4.15	3.95	4.73	0.80	2.76	289
5.12	4.92	5.57	0.84	2.98	281
6.12	5.92	6.47	0.90	3.64	248
7.12	6.92	7.39	0.93	4.85	191
8.25	8.05	8.46	1.07	5.40	198
9.12	8.92	9.29	0.83	5.73	145
10.12	9.92	10.26	0.96	6.95	139
11.12	10.92	11.23	0.97	6.72	144
12.12	11.92	12.20	0.98	6.83	143
13.12	12.92	13.18	0.98	7.05	139
14.12	13.92	14.16	0.98	7.27	135
15.12	14.92	15.15	0.98	6.06	162
16.12	15.92	16.13	0.99	5.84	169
17.12	16.92	17.12	0.99	5.62	176
18.12	17.92	18.11	0.99	4.52	219
19.12	18.92	19.10	0.99	3.75	264
20.12	19.92	20.09	0.99	3.97	250
21.12	20.92	21.08	0.99	3.86	257
22.12	21.92	22.07	0.99	3.64	273
23.12	22.92	23.07	0.99	2.86	347
24.12	23.92	24.06	0.99	2.87	347

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH201
Date:	2024-03-01
Seismic Source:	Wedge
Seismic Offset (m):	1.65
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.70			
2.00	1.80	2.16	0.47	4.72	99
6.00	5.80	5.65	3.48	20.63	169
7.00	6.80	6.61	0.96	4.26	226
8.00	7.80	7.58	0.97	3.71	263
10.00	9.80	9.54	1.96	6.28	313
11.00	10.80	10.53	0.99	3.43	287
12.00	11.80	11.52	0.99	4.11	241
13.00	12.80	12.51	0.99	5.66	175
14.00	13.80	13.50	0.99	6.01	165
15.00	14.80	14.49	0.99	5.85	170
16.00	15.80	15.49	0.99	5.19	192
17.00	16.80	16.48	1.00	4.79	208
18.00	17.80	17.48	1.00	4.73	210
19.00	18.80	18.47	1.00	4.37	228
20.00	19.80	19.47	1.00	4.30	232
21.00	20.80	20.47	1.00	4.31	232
22.00	21.80	21.46	1.00	4.08	244
23.00	22.80	22.46	1.00	3.50	285

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH202
Date:	2024-03-04
Seismic Source:	Wedge
Seismic Offset (m):	2.00
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
4.00	3.80	3.94			
6.00	5.80	5.76	1.81	8.34	217
8.00	7.80	7.67	1.91	8.39	227
9.00	8.80	8.64	0.97	4.06	239
10.00	9.80	9.61	0.98	4.28	228
11.00	10.80	10.59	0.98	5.74	171
12.00	11.80	11.57	0.98	6.28	157
13.00	12.80	12.56	0.99	6.27	157
14.00	13.80	13.55	0.99	7.01	141
15.00	14.80	14.54	0.99	6.38	155
16.00	15.80	15.53	0.99	3.96	250
17.00	16.80	16.52	0.99	3.69	269
18.00	17.80	17.52	0.99	2.87	346
18.95	18.75	18.46	0.94	2.50	378

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH205
Date:	2024-03-08
Seismic Source:	Wedge
Seismic Offset (m):	1.40
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.00	2.80	2.78			
4.00	3.80	3.68	0.90	5.30	170
6.00	5.80	5.58	1.90	11.63	164
7.72	7.52	7.26	1.68	7.52	223

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH05B
Date:	2024-03-08
Seismic Source:	Wedge
Seismic Offset (m):	1.50
Source Depth (m):	0.20
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.00	1.80	2.19			
4.00	3.80	3.90	1.71	17.74	96
5.00	4.80	4.84	0.94	11.95	79
6.00	5.80	5.80	0.96	9.73	99
7.65	7.45	7.40	0.64	4.43	144

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH207
Date:	2024-03-11
Seismic Source:	Wedge
Seismic Offset (m):	1.30
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.00	1.80	1.91			
5.00	4.80	4.59	2.68	31.58	85
6.00	5.80	5.55	0.97	8.19	118

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH212
Date:	2024-03-03
Seismic Source:	Wedge
Seismic Offset (m):	2.20
Source Depth (m):	0.40
Geophone Offset (m):	0.20

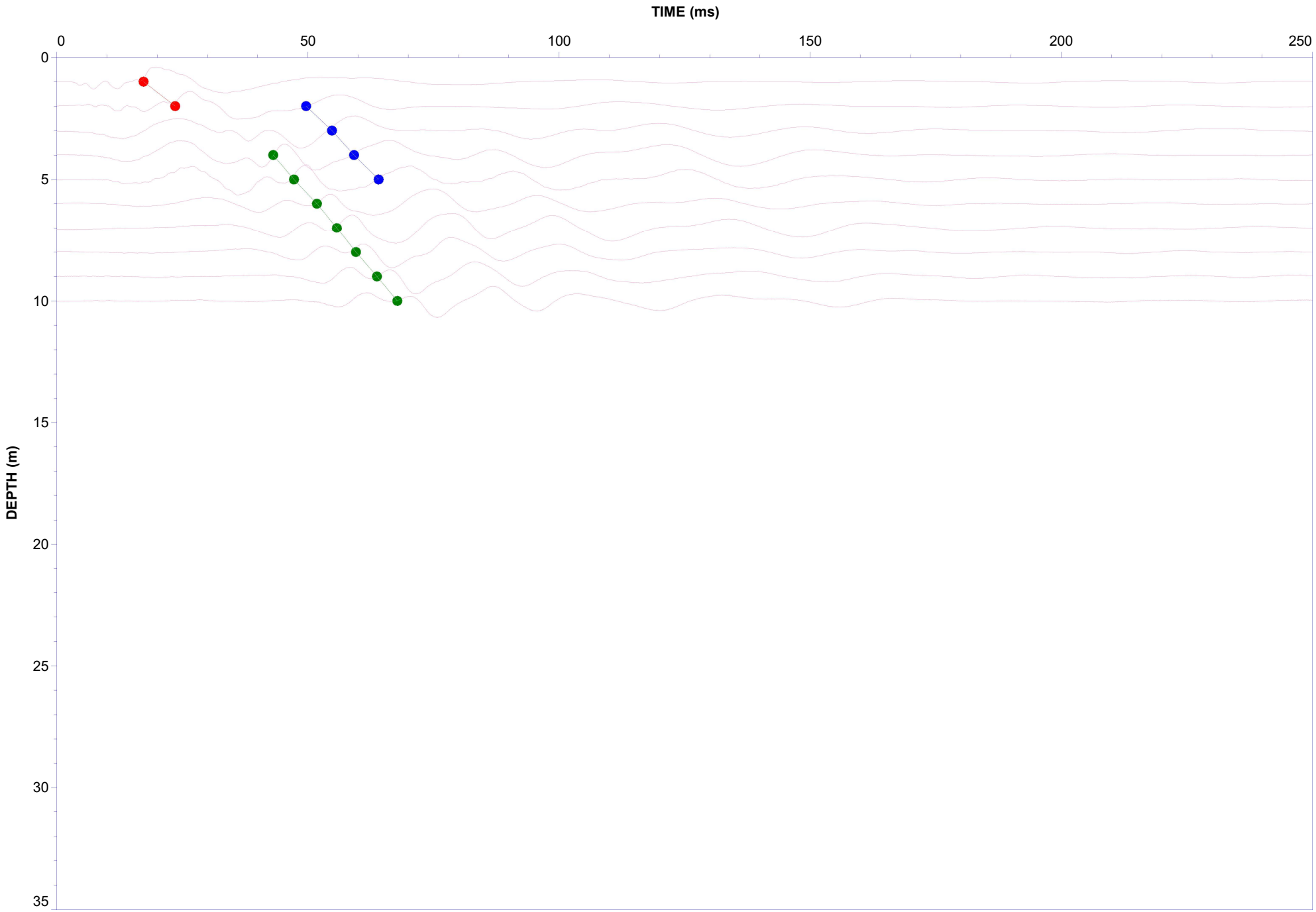
SCPTu SHEAR WAVE VELOCITY TEST RESULTS - Vs

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.00	2.80	3.26			
4.00	3.80	4.05	0.79	3.74	212
5.00	4.80	4.92	0.87	3.97	219
6.00	5.80	5.83	0.91	4.34	210
7.00	6.80	6.77	0.94	4.58	205
8.00	7.80	7.72	0.95	4.47	213
9.00	8.80	8.68	0.96	4.38	220
10.00	9.80	9.65	0.97	4.31	226
11.00	10.80	10.63	0.98	4.97	196
12.00	11.80	11.61	0.98	5.25	187
13.00	12.80	12.59	0.98	4.42	223
14.00	13.80	13.58	0.99	3.72	265
15.00	14.80	14.57	0.99	3.27	302

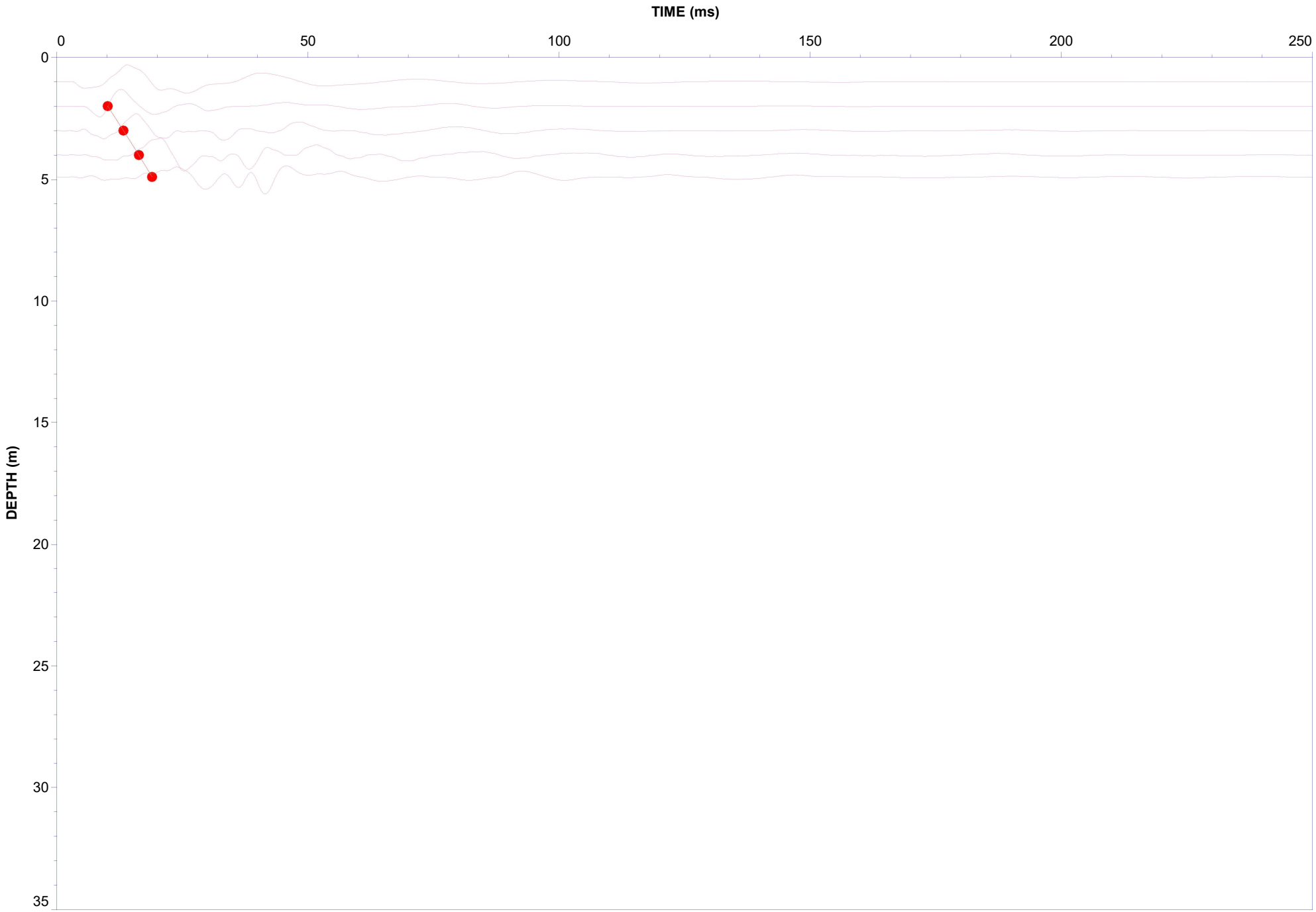
Seismic Cone Penetration Test Shear Wave (Vs) Traces

CONETEC

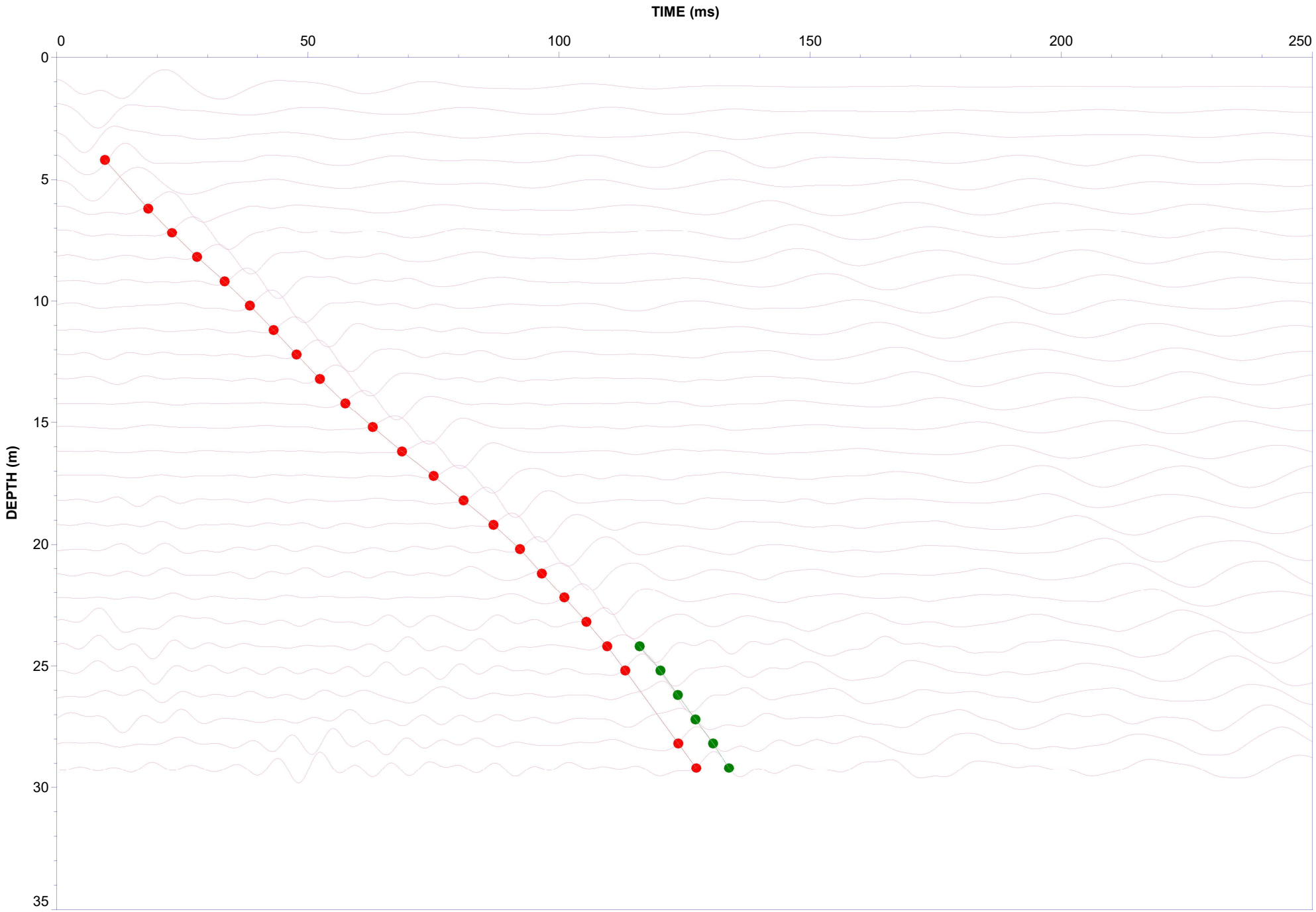
Job No: 24-05-27159 Client: Canada Nickel Company Project: Crawford Mine - SRK Filter: No Filter Sounding ID: SCPT24-LGE-BH201
Analysis: S wave-Geo X Date: 2024-02-19



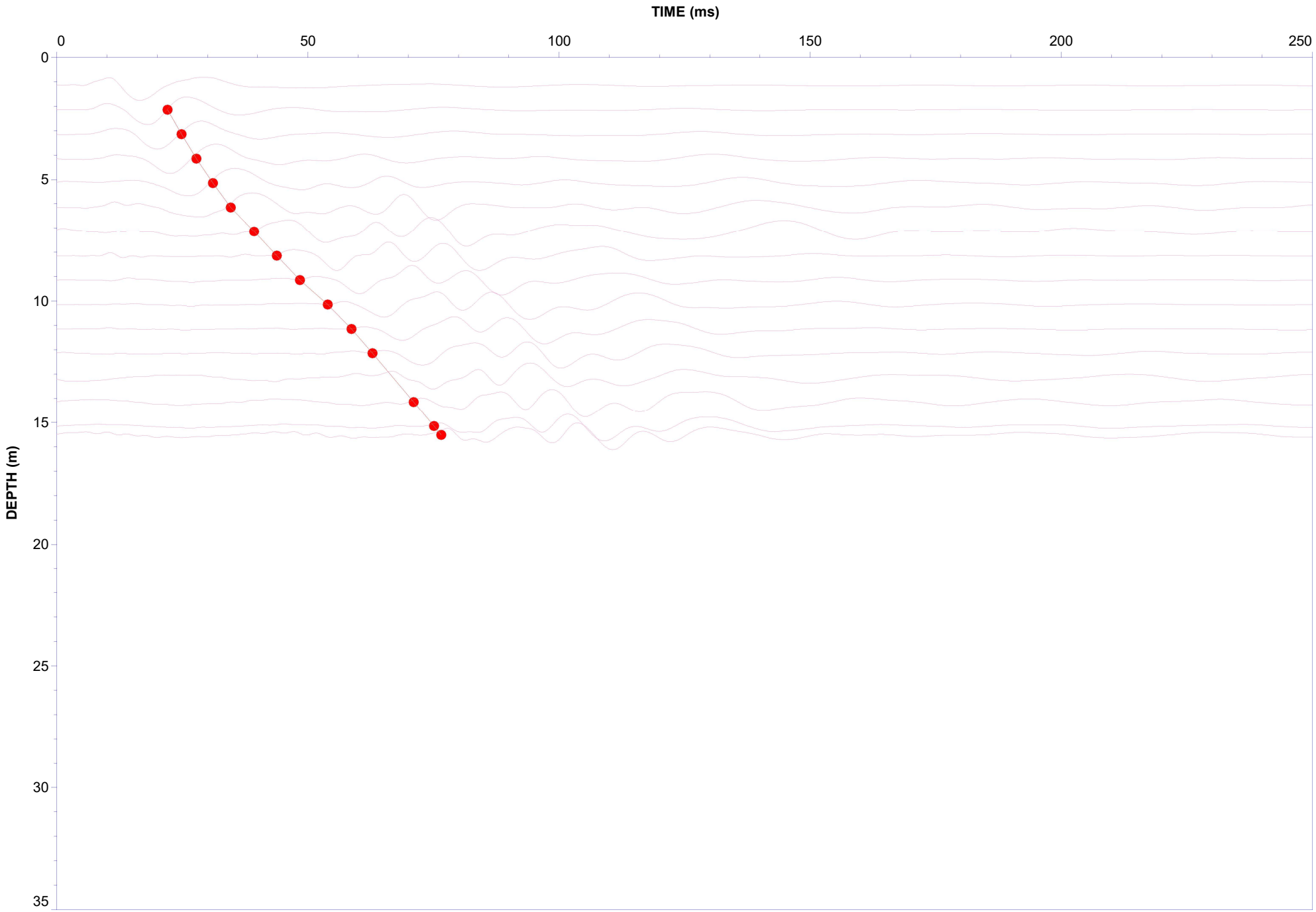
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-400 Hz | Sounding ID: SCPT24-LGE-BH202
Analysis: S wave-Geo X | Date: 2024-02-16



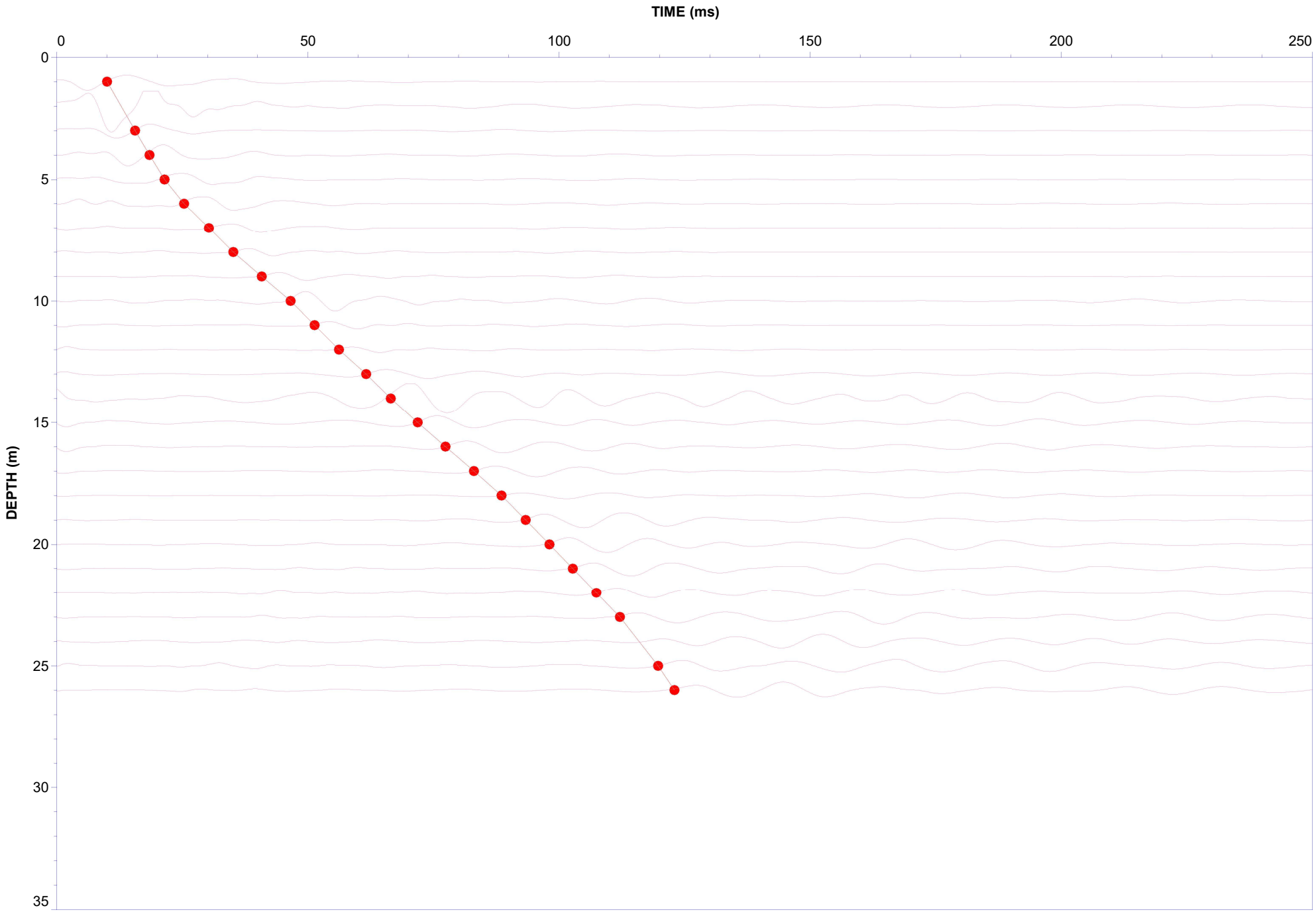
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 30-150 Hz | Sounding ID: SCPT24-LGE-BH203
Analysis: S wave-Geo X | Date: 2024-02-14



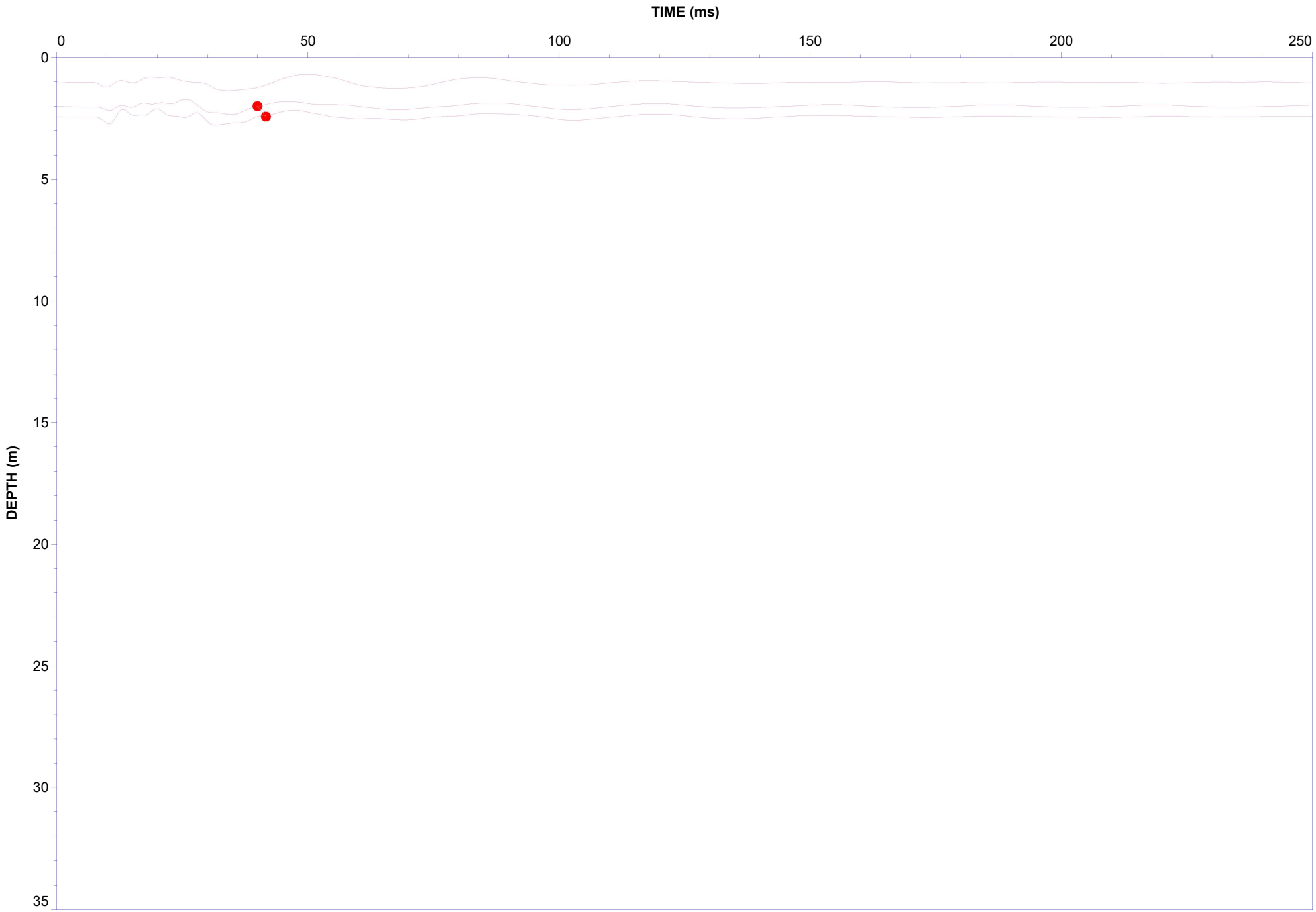
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-300Hz | Sounding ID: SCPT24-LGE-BH204
Analysis: S wave-Geo X | Date: 2024-02-18



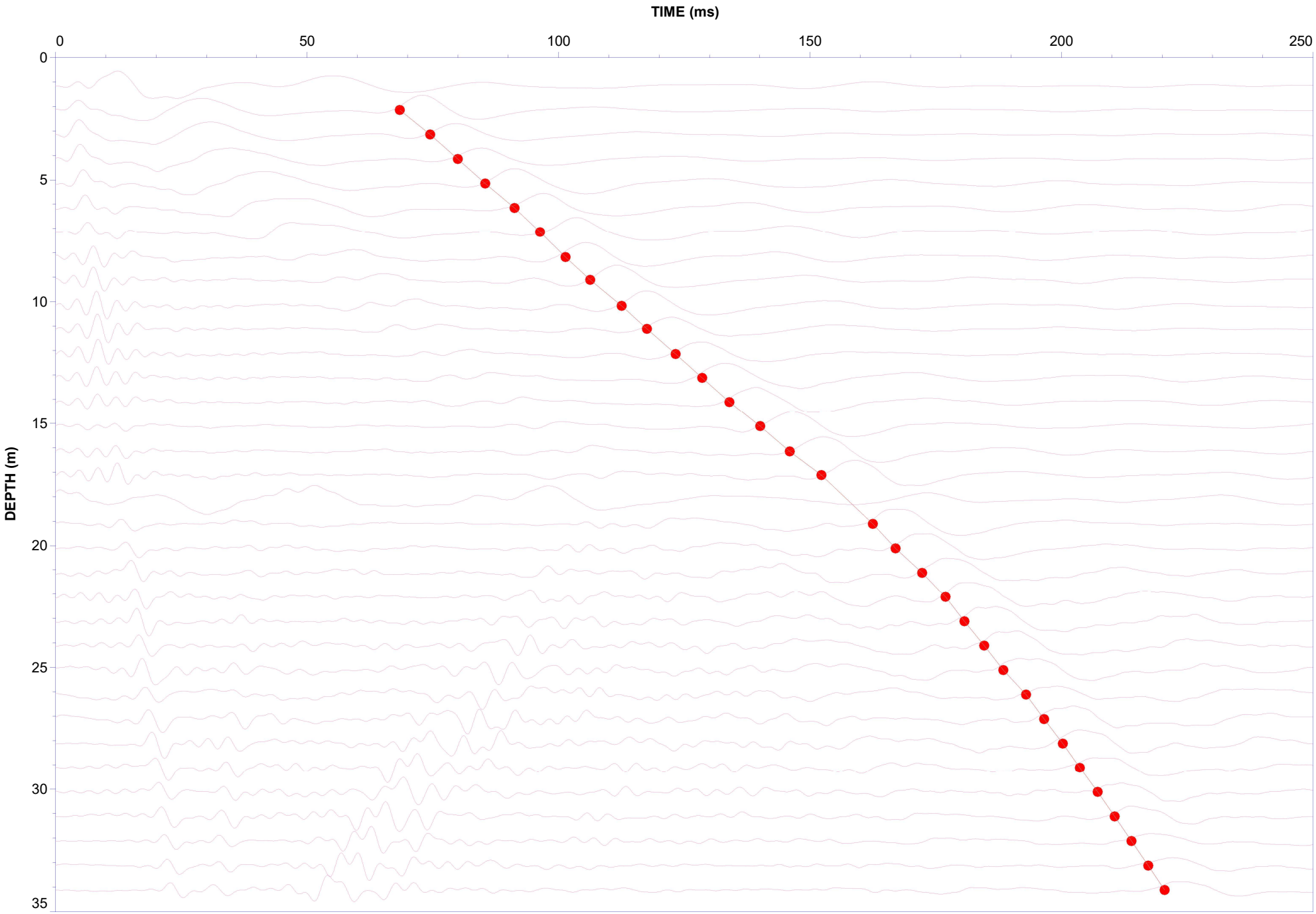
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 40-200Hz | Sounding ID: SCPT24-LGE-BH205
Analysis: S wave-Geo X | Date: 2024-02-26



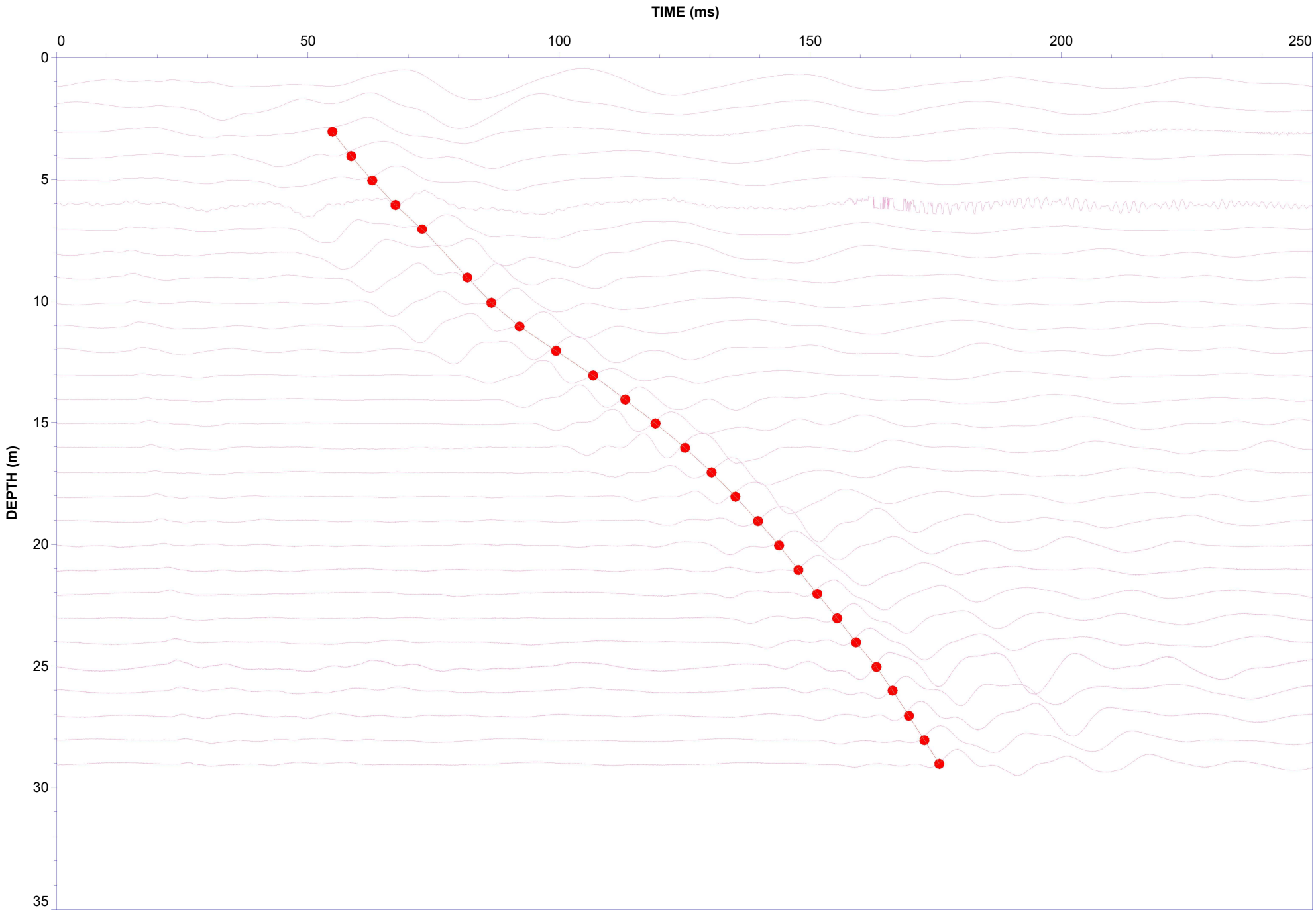
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-400 Hz | Sounding ID: SCPT24-TMF-MW03AB
Analysis: S wave-Geo X | Date: 2024-03-13



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-300Hz | Sounding ID: SCPT24-TMF-MW08AB
Analysis: S wave-Geo X | Date: 2024-03-20

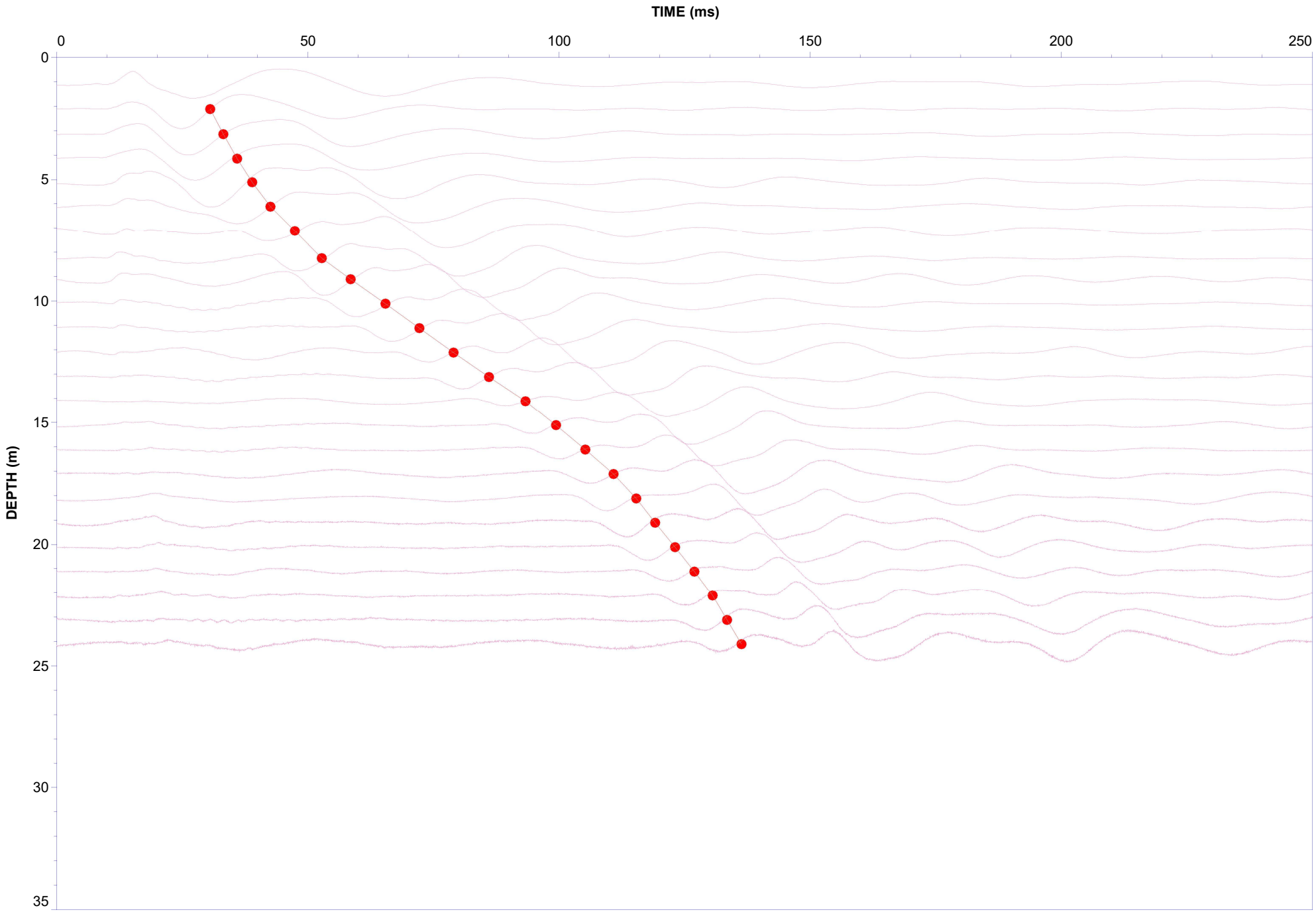


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: No Filter | Sounding ID: SCPT24-TMF-BH202
Analysis: S wave-Geo X | Date: 2024-03-15

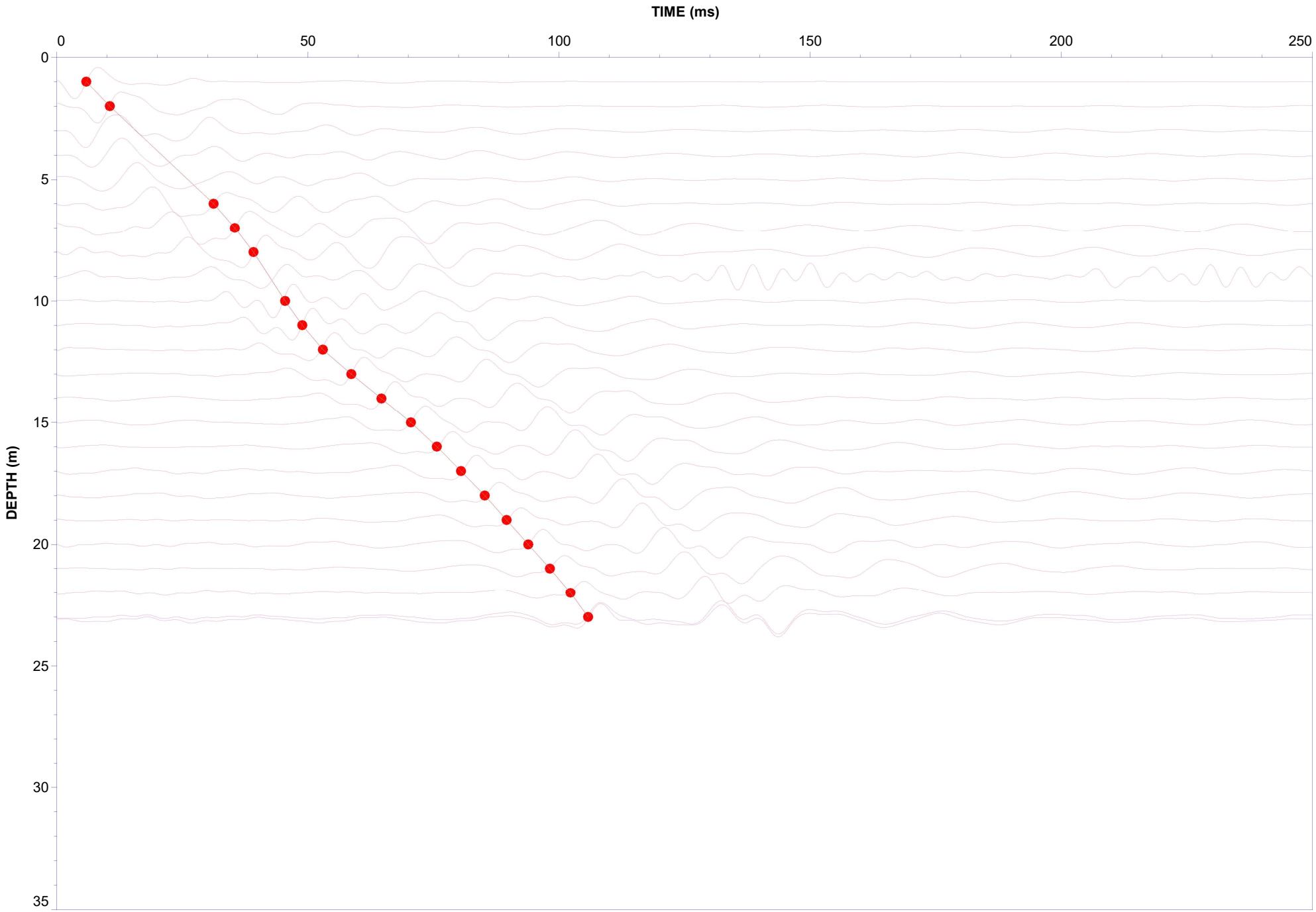


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: No Filter | Sounding ID: SCPT24-TMF-BH207

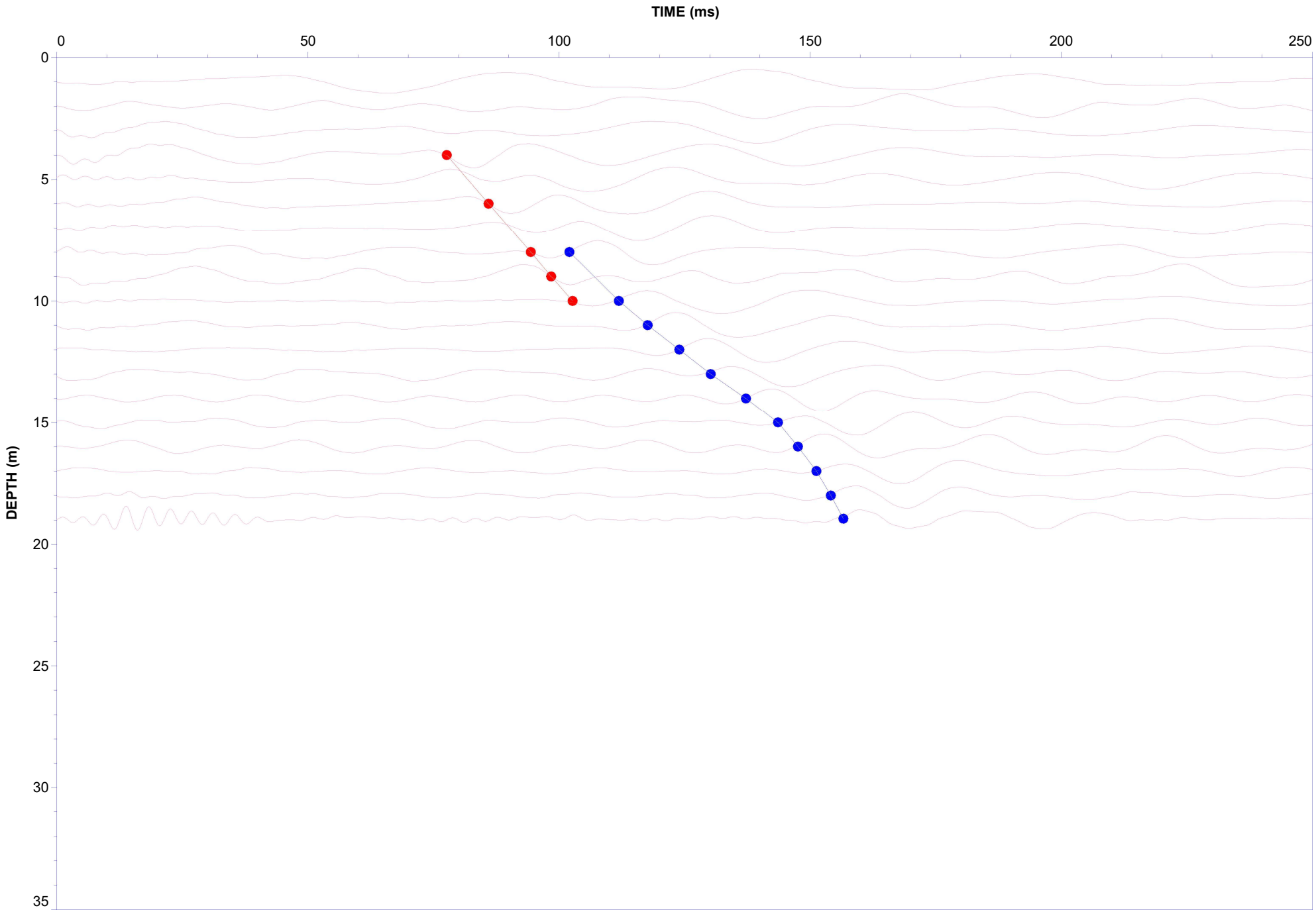
Analysis: S wave-Geo X | Date: 2024-03-18



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 40-200 Hz | Sounding ID: SCPT24-WRD-BH201
Analysis: S wave-Geo X | Date: 2024-03-01

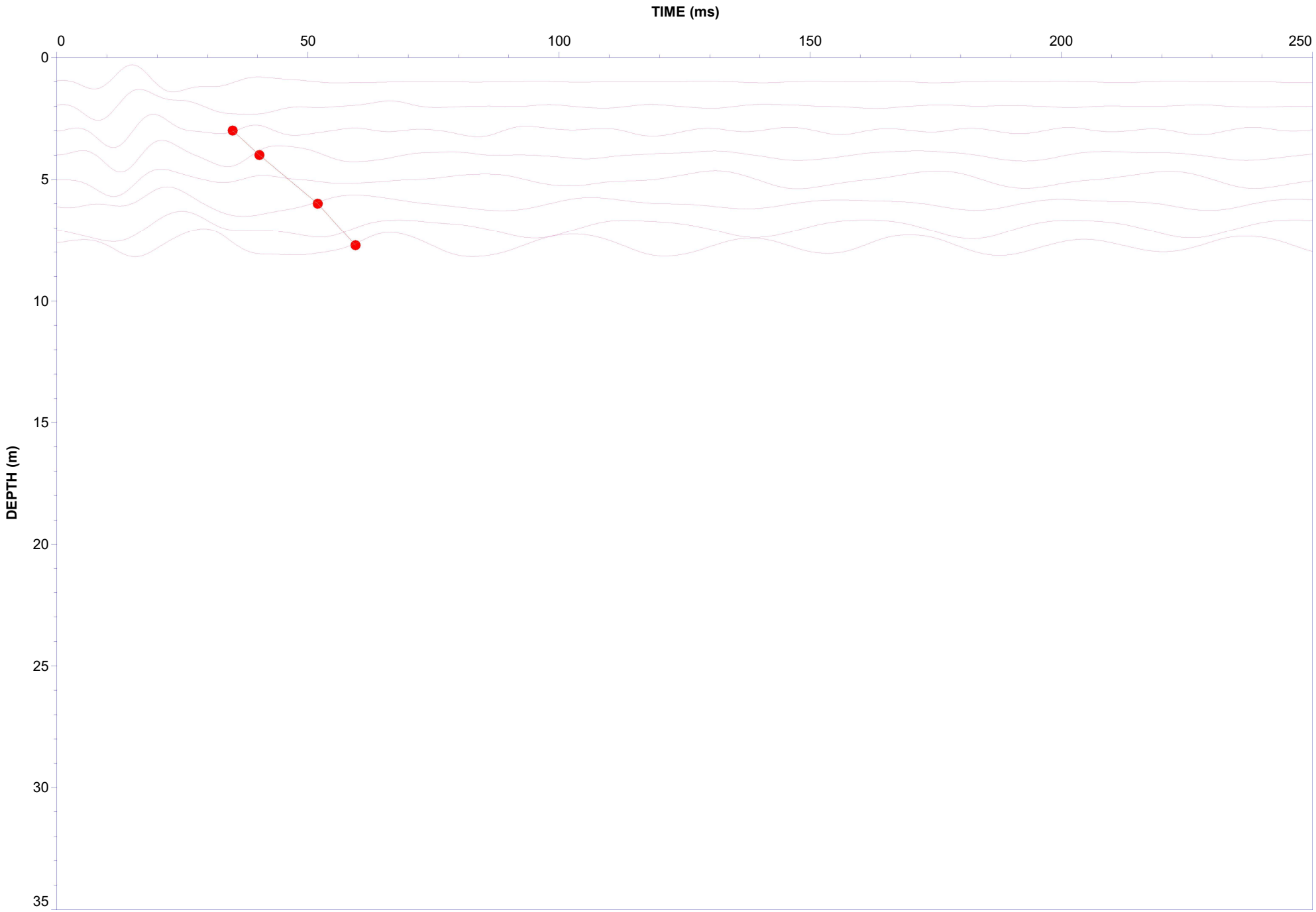


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-250 Hz | Sounding ID: SCPT24-WRD-BH202
Analysis: S wave-Geo X | Date: 2024-03-04

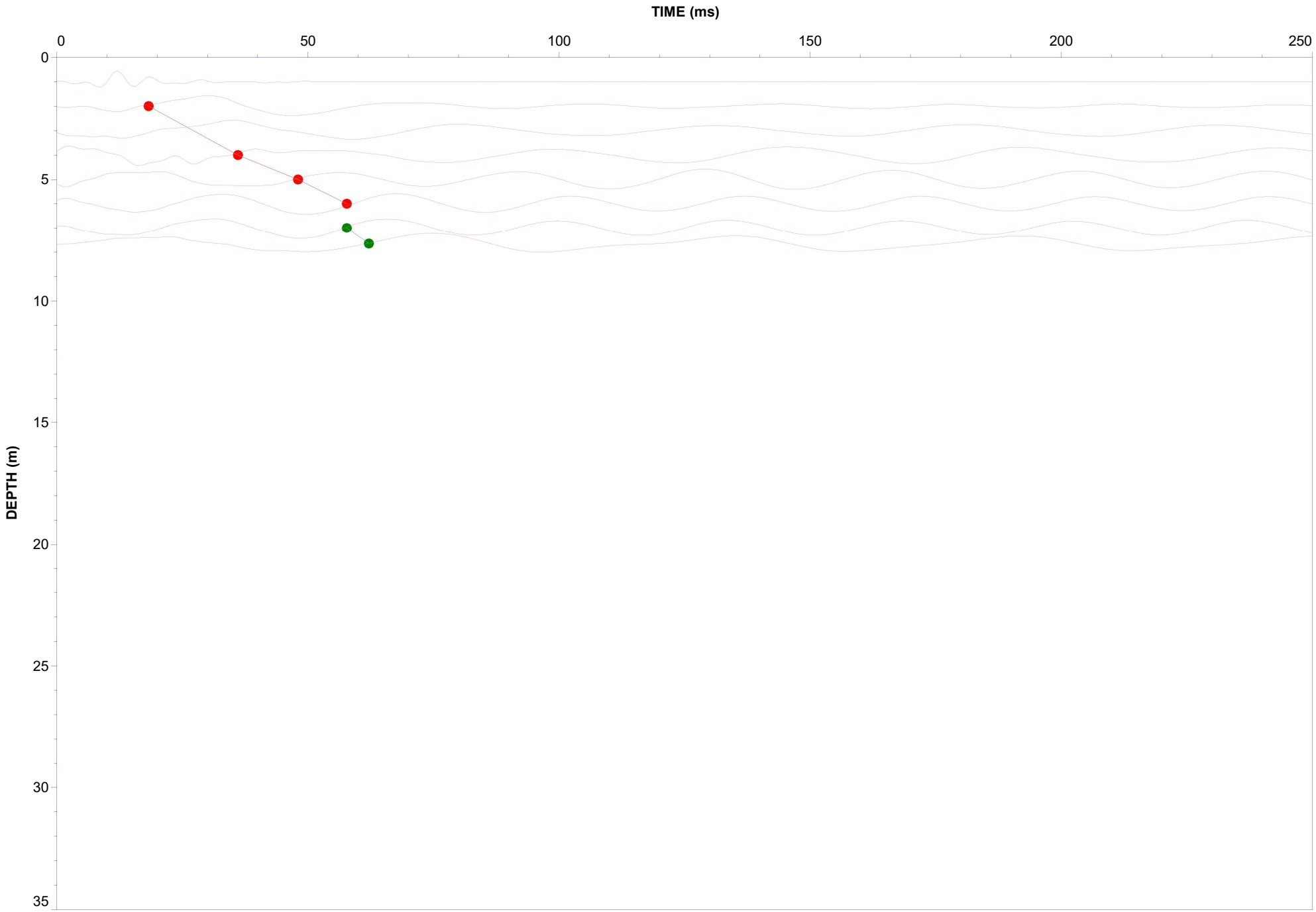


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-100 Hz | Sounding ID: SCPT24-WRD-BH205

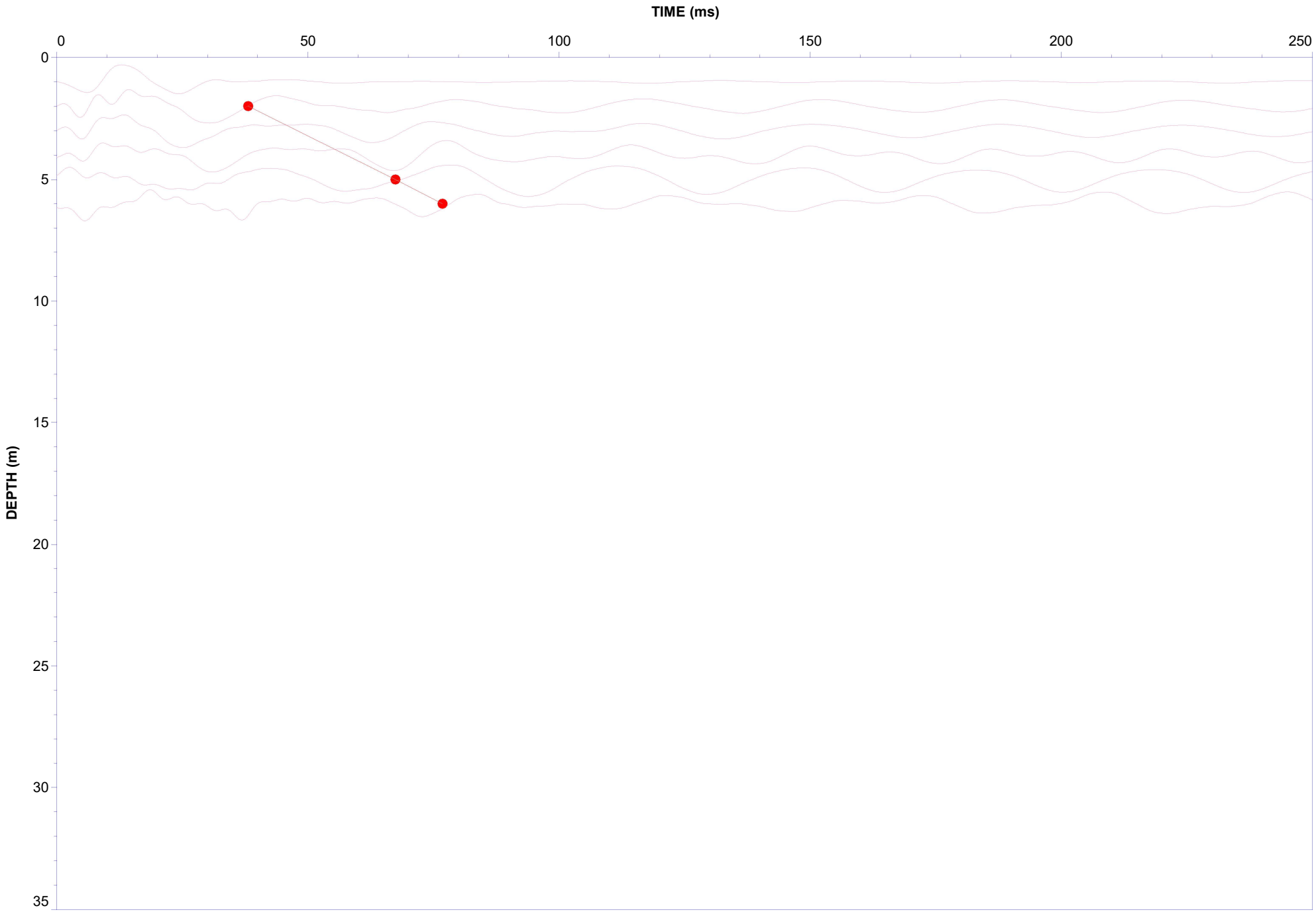
Analysis: S wave-Geo X | Date: 2024-03-08



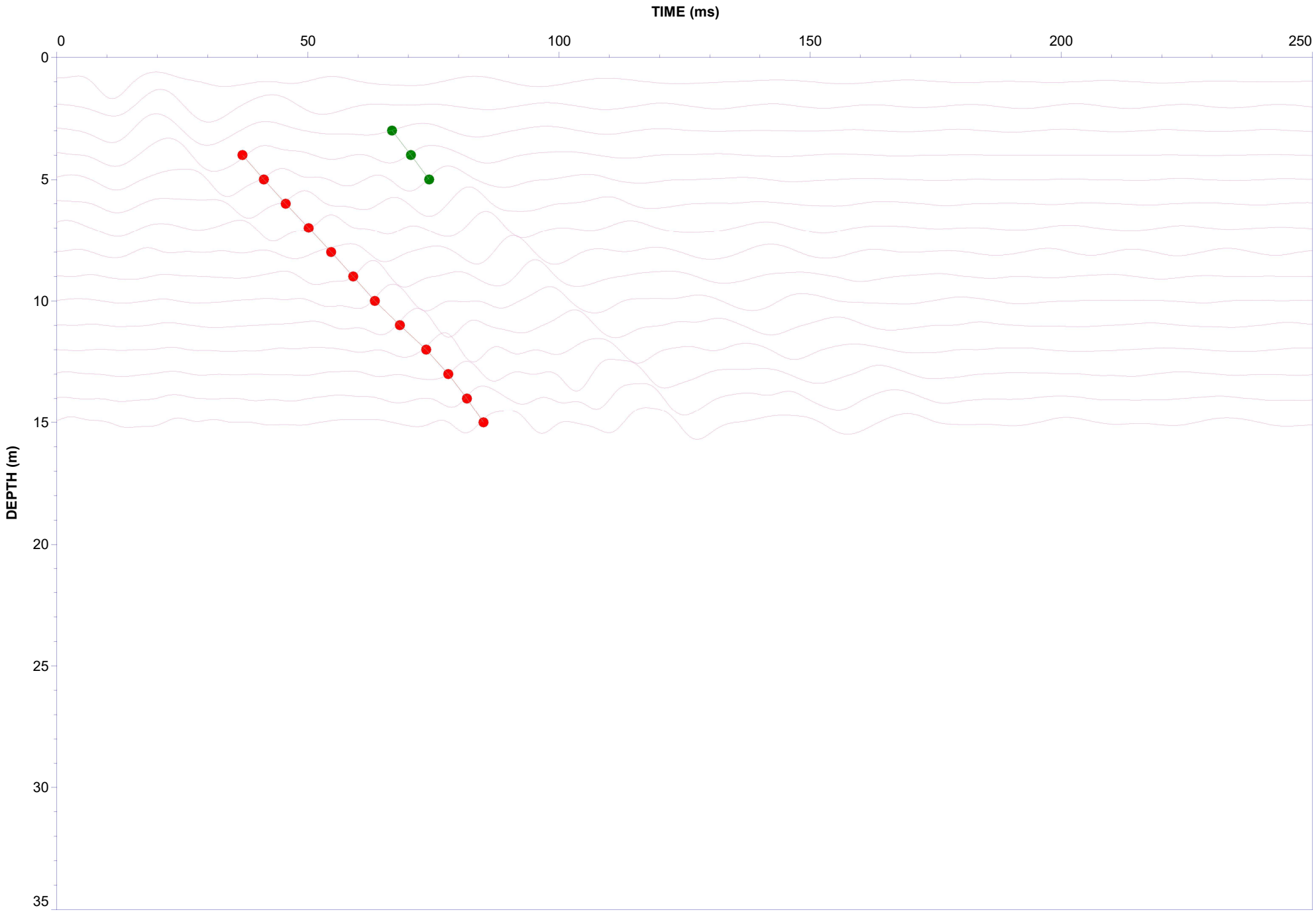
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-WRD-BH05B
Analysis: S wave-Geo X | Date: 2024-03-08



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-WRD-BH207
Analysis: S wave-Geo X | Date: 2024-03-11



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-WRD-BH212
Analysis: S wave-Geo X | Date: 2024-03-03



Seismic Cone Penetration Test Compression Wave (Vp) Tabular Results

CONETEC

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH201
Date:	2024-02-19
Seismic Source:	Wedge
Seismic Offset (m):	1.20
Source Depth (m):	0.10
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.00	2.80	2.95			
4.00	3.80	3.89	0.94	1.78	526
5.00	4.80	4.85	0.96	1.39	694
6.00	5.80	5.83	0.97	1.31	743

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH202
Date:	2024-02-16
Seismic Source:	Wedge
Seismic Offset (m):	0.95
Source Depth (m):	0.30
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.07			
2.00	1.80	1.78	0.70	1.62	432
3.00	2.80	2.67	0.90	1.28	703
4.00	3.80	3.63	0.95	0.93	1022
4.90	4.70	4.50	0.87	0.74	1187

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH203
Date:	2024-02-14
Seismic Source:	Wedge
Seismic Offset (m):	1.00
Source Depth (m):	0.30
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.20	3.00	2.88			
4.20	4.00	3.83	0.95	0.88	1088
5.20	5.00	4.81	0.97	0.80	1209
6.20	6.00	5.79	0.98	0.75	1311
7.20	7.00	6.77	0.99	0.78	1271
8.20	8.00	7.77	0.99	0.71	1401
9.20	9.00	8.76	0.99	0.61	1618
10.20	10.00	9.75	0.99	0.62	1600
11.20	11.00	10.75	1.00	0.54	1831
12.20	12.00	11.74	1.00	0.59	1700
15.20	15.00	14.73	2.99	1.71	1746
16.20	16.00	15.73	1.00	0.59	1686
19.20	19.00	18.73	1.00	0.61	1643
20.20	20.00	19.73	1.00	0.63	1587
21.20	21.00	20.72	1.00	0.59	1704
22.20	22.00	21.72	1.00	0.59	1704

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH204
Date:	2024-02-18
Seismic Source:	Wedge
Seismic Offset (m):	1.20
Source Depth (m):	0.10
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.15	0.95	1.47			
2.15	1.95	2.21	0.73	0.77	949
3.15	2.95	3.09	0.89	0.92	961
4.15	3.95	4.03	0.94	0.64	1460
5.15	4.95	5.00	0.96	0.69	1399
6.15	5.95	5.97	0.98	0.55	1771
7.15	6.95	6.95	0.98	0.69	1427
8.15	7.95	7.94	0.99	0.69	1433
9.15	8.95	8.93	0.99	0.55	1797
10.15	9.95	9.92	0.99	0.55	1800
11.15	10.95	10.92	0.99	0.55	1803
12.15	11.95	11.91	1.00	0.55	1805
13.15	12.95	12.91	1.00	0.55	1807
14.15	13.95	13.90	1.00	0.55	1808
15.15	14.95	14.90	1.00	0.55	1809
15.52	15.32	15.27	0.37	0.20	1833

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH205
Date:	2024-02-26
Seismic Source:	Wedge
Seismic Offset (m):	1.65
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.70			
2.00	1.80	2.16	0.47	0.90	518
3.00	2.80	2.91	0.75	0.93	806
5.00	4.80	4.70	1.79	1.54	1161
6.00	5.80	5.65	0.95	0.66	1441
19.00	18.80	18.47	12.83	8.06	1592
20.00	19.80	19.47	1.00	0.62	1601
21.00	20.80	20.47	1.00	0.62	1597
22.00	21.80	21.46	1.00	0.63	1587
23.00	22.80	22.46	1.00	0.62	1615
24.00	23.80	23.46	1.00	0.54	1859
25.00	24.80	24.46	1.00	0.53	1880
26.00	25.80	25.45	1.00	0.53	1882

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW03AB
Date:	2024-03-13
Seismic Source:	Wedge
Seismic Offset (m):	1.70
Source Depth (m):	0.30
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.03	0.83	1.78			
2.00	1.80	2.27	0.49	0.47	1033
2.43	2.23	2.57	0.31	0.24	1294

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW08AB
Date:	2024-03-20
Seismic Source:	Plate
Seismic Offset (m):	2.40
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.15	2.95	3.80			
4.15	3.95	4.62	0.82	0.50	1643
5.15	4.95	5.50	0.88	0.56	1571
6.15	5.95	6.42	0.92	0.61	1500
7.15	6.95	7.35	0.94	0.61	1536
9.12	8.92	9.24	1.88	1.16	1629
11.12	10.92	11.18	1.94	1.16	1678
12.15	11.95	12.19	1.01	0.65	1558
13.12	12.92	13.14	0.95	0.61	1562
14.12	13.92	14.13	0.98	0.57	1719
17.12	16.92	17.09	2.96	1.68	1766
21.12	20.92	21.06	3.97	2.22	1785
23.12	22.92	23.05	1.99	1.19	1674
24.12	23.92	24.04	1.00	0.66	1508
25.12	24.92	25.04	1.00	0.68	1455
26.12	25.92	26.03	1.00	0.67	1480
27.12	26.92	27.03	1.00	0.67	1484
28.12	27.92	28.02	1.00	0.71	1404
31.12	30.92	31.01	2.99	1.74	1716
32.12	31.92	32.01	1.00	0.61	1635
33.12	32.92	33.01	1.00	0.57	1741
34.12	33.92	34.01	1.00	0.56	1782

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-BH202
Date:	2024-03-15
Seismic Source:	Plate
Seismic Offset (m):	5.60
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
5.05	4.85	7.41			
6.05	5.85	8.10	0.69	0.44	1555
7.05	6.85	8.85	0.75	0.47	1585
8.05	7.85	9.64	0.80	0.52	1530
9.05	8.85	10.47	0.83	0.53	1579
10.08	9.88	11.36	0.88	0.52	1691
12.05	11.85	13.11	1.75	1.00	1758
13.05	12.85	14.02	0.91	0.52	1742
14.05	13.85	14.94	0.92	0.50	1852
15.05	14.85	15.87	0.93	0.55	1701
16.05	15.85	16.81	0.94	0.50	1887
17.05	16.85	17.76	0.95	0.55	1728
18.05	17.85	18.71	0.95	0.55	1738
19.05	18.85	19.66	0.96	0.55	1747
20.05	19.85	20.63	0.96	0.55	1754
21.05	20.85	21.59	0.96	0.55	1761
22.05	21.85	22.56	0.97	0.55	1767
23.05	22.85	23.53	0.97	0.60	1624
24.05	23.85	24.50	0.97	0.57	1699
25.05	24.85	25.47	0.97	0.57	1703
26.02	25.82	26.42	0.95	0.52	1812
27.05	26.85	27.43	1.01	0.55	1840
28.05	27.85	28.41	0.98	0.55	1789
29.02	28.82	29.36	0.95	0.52	1821

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-BH207
Date:	2024-03-18
Seismic Source:	Plate
Seismic Offset (m):	2.60
Source Depth (m):	0.00
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
4.15	3.95	4.73			
6.12	5.92	6.47	1.74	1.14	1518
9.12	8.92	9.29	0.83	0.55	1527
10.12	9.92	10.26	0.96	0.59	1638
20.12	19.92	20.09	9.83	6.01	1635
21.12	20.92	21.08	0.99	0.63	1579
22.12	21.92	22.07	0.99	0.63	1580
23.12	22.92	23.07	0.99	0.66	1517
24.12	23.92	24.06	0.99	0.64	1550

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH201
Date:	2024-03-01
Seismic Source:	Wedge
Seismic Offset (m):	1.65
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.70			
3.00	2.80	2.91	1.21	1.93	630
4.00	3.80	3.78	0.87	1.02	847
5.00	4.80	4.70	0.92	1.13	818

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH202
Date:	2024-03-04
Seismic Source:	Wedge
Seismic Offset (m):	2.00
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
3.00	2.80	3.12			
4.00	3.80	3.95	0.82	0.54	1515
5.00	4.80	4.83	0.89	0.59	1502
6.00	5.80	5.76	0.93	0.60	1552
7.00	6.80	6.71	0.95	0.58	1625
8.00	7.80	7.67	0.96	0.51	1885
10.00	9.80	9.61	1.94	1.00	1943
11.00	10.80	10.59	0.98	0.50	1958

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH205
Date:	2024-03-08
Seismic Source:	Wedge
Seismic Offset (m):	1.40
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.46			
3.00	2.80	2.78	1.32	2.22	596
6.00	5.80	5.58	2.80	3.00	933
7.72	7.52	7.26	1.68	1.44	1168

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH207
Date:	2024-03-11
Seismic Source:	Wedge
Seismic Offset (m):	1.30
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
1.00	0.80	1.36			
2.00	1.80	1.91	0.55	0.74	746
3.00	2.80	2.73	0.82	0.88	926
4.00	3.80	3.64	0.91	0.94	975
5.00	4.80	4.59	0.95	0.84	1128

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH212
Date:	2024-03-03
Seismic Source:	Wedge
Seismic Offset (m):	2.20
Source Depth (m):	0.40
Geophone Offset (m):	0.20

SCPTu COMPRESSION WAVE VELOCITY TEST RESULTS - Vp

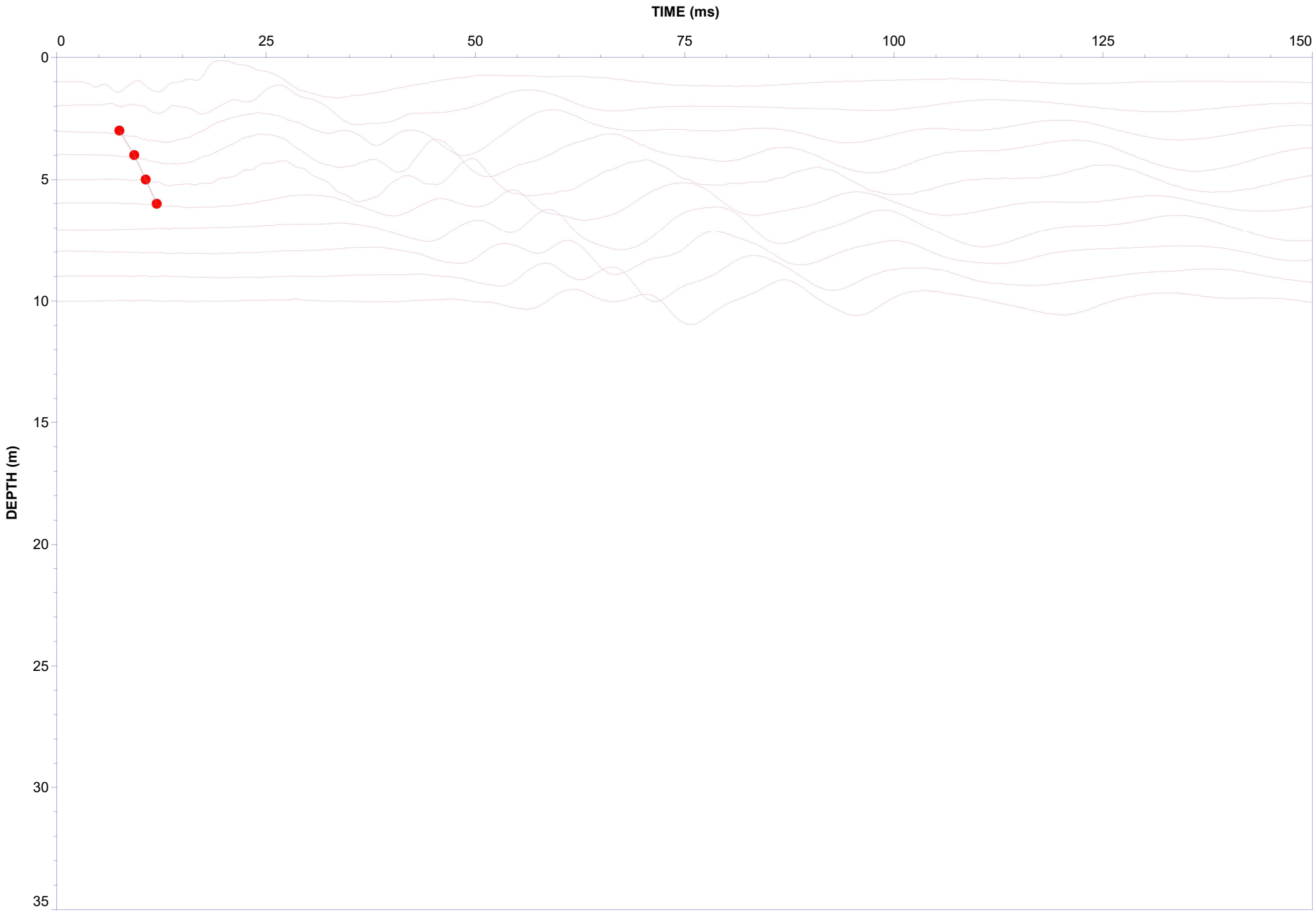
Tip Depth (m)	Geophone Depth (m)	Ray Path (m)	Ray Path Difference (m)	Travel Time Interval (ms)	Interval Velocity (m/s)
2.00	1.80	2.61			
3.00	2.80	3.26	0.65	0.52	1253
4.00	3.80	4.05	0.79	0.52	1535
5.00	4.80	4.92	0.87	0.52	1682
6.00	5.80	5.83	0.91	0.52	1763
9.00	8.80	8.68	2.85	1.66	1724
14.00	13.80	13.58	4.90	2.79	1758

Seismic Cone Penetration Test Compression Wave (Vp) Traces

CONETEC

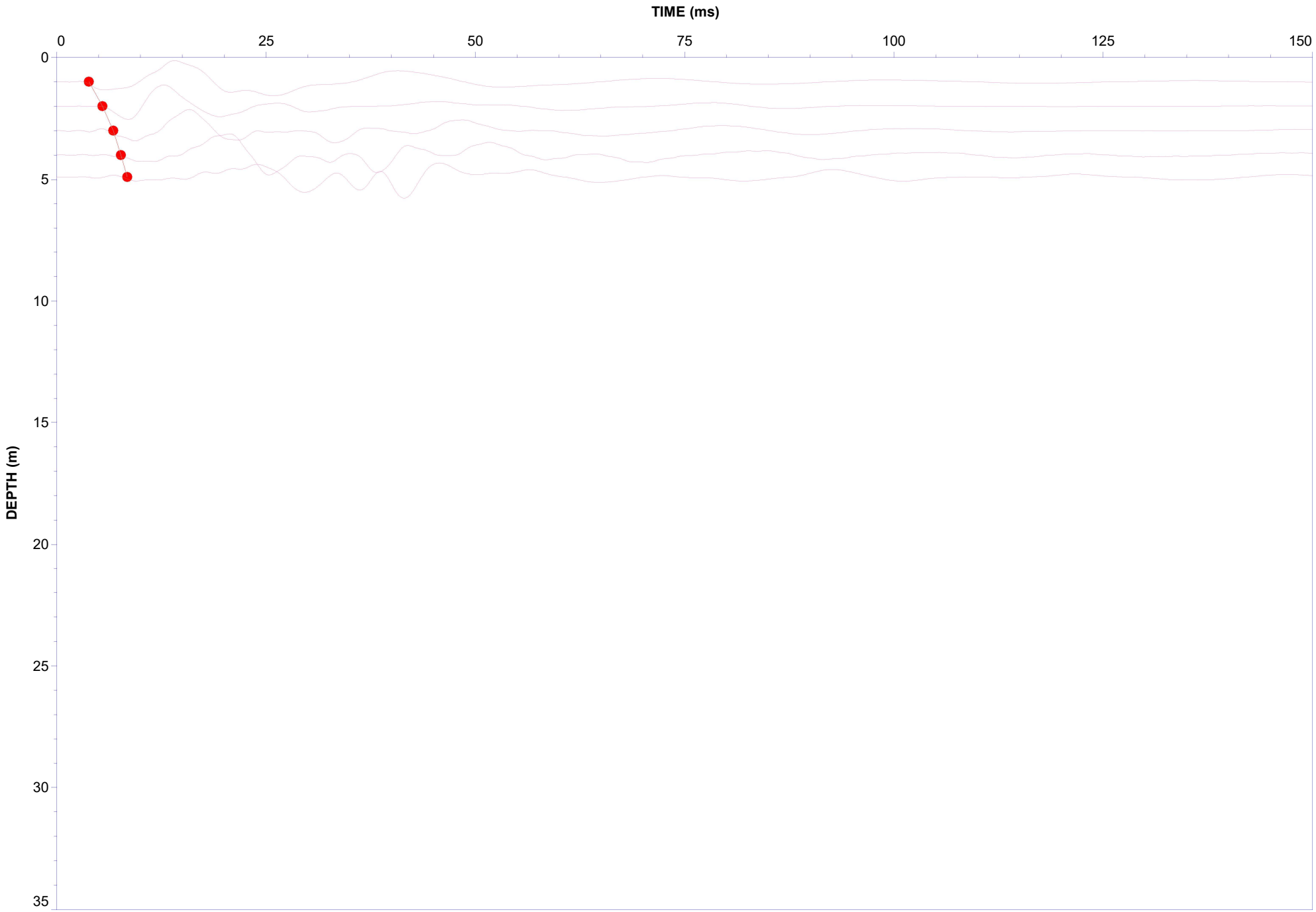
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: None | Sounding ID: SCPT24-LGE-BH201

Analysis: P wave-Geo X | Date: 2024-02-19



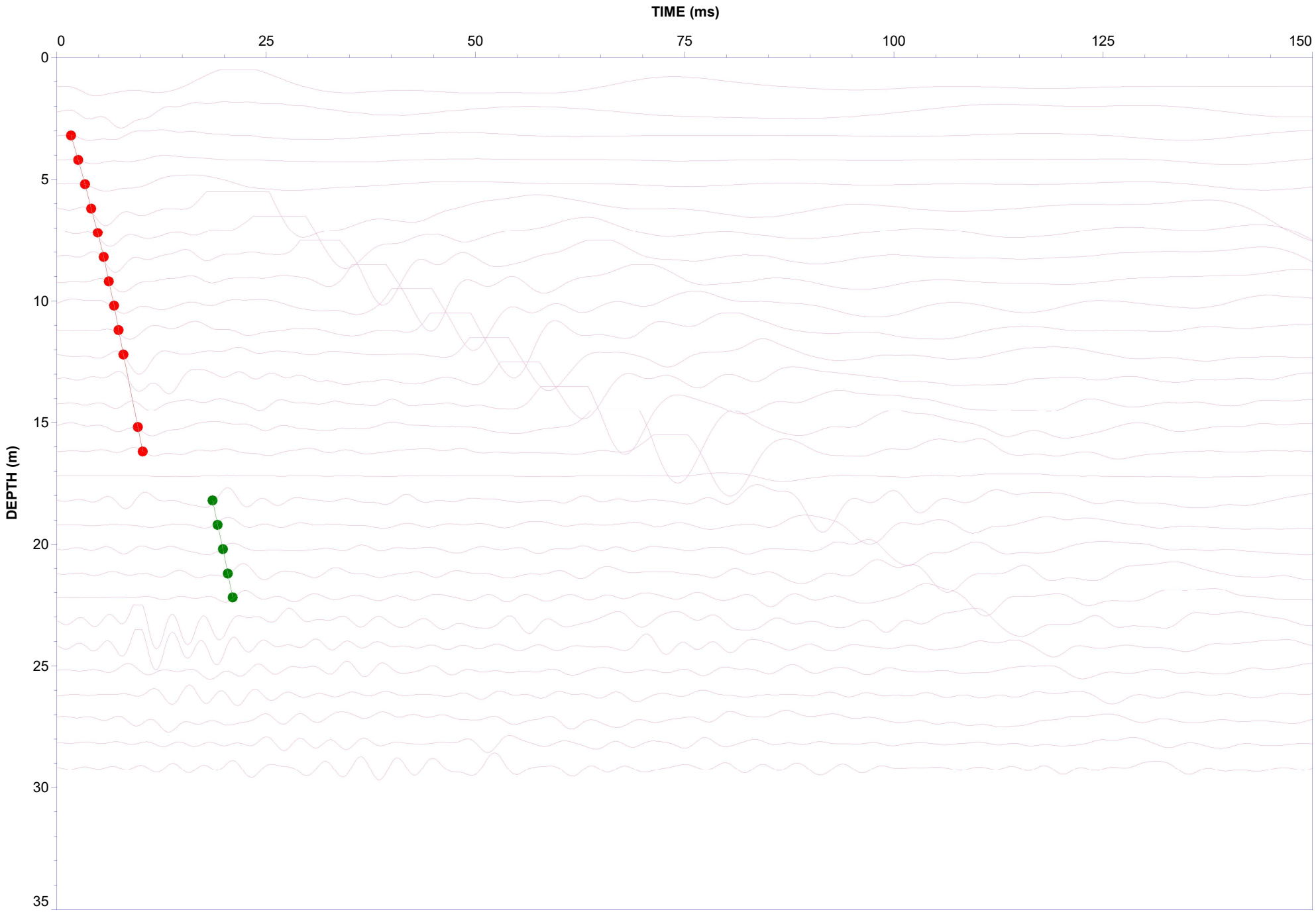
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: None | Sounding ID: SCPT24-LGE-BH202

Analysis: P wave-Geo X | Date: 2024-02-16



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-300 Hz | Sounding ID: SCPT24-LGE-BH203

Analysis: S wave-Geo X | Date: 2024-02-14



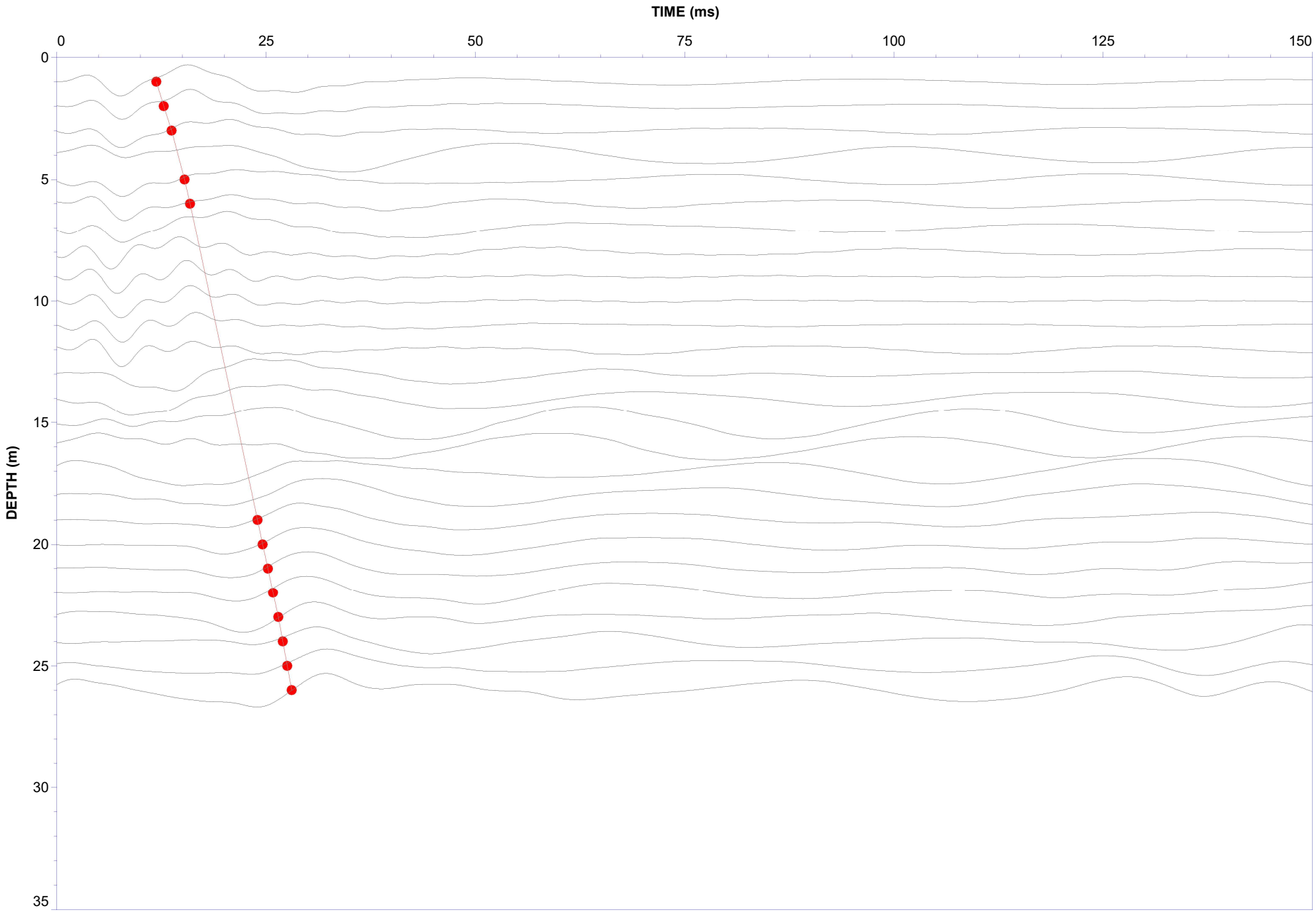
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: No Filter | Sounding ID: SCPT24-LGE-BH204

Analysis: P wave-Geo X | Date: 2024-02-18

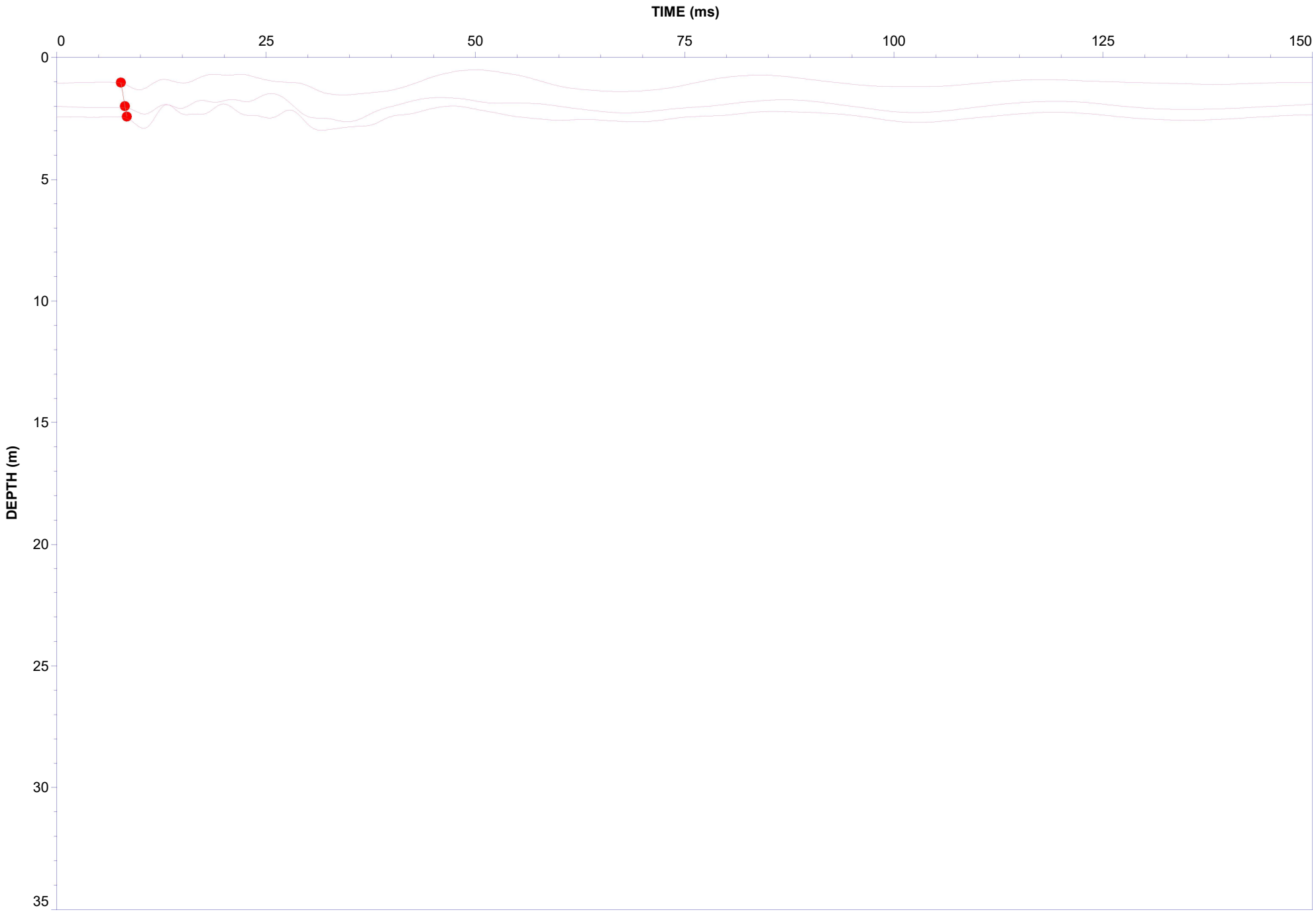


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-LGE-BH205

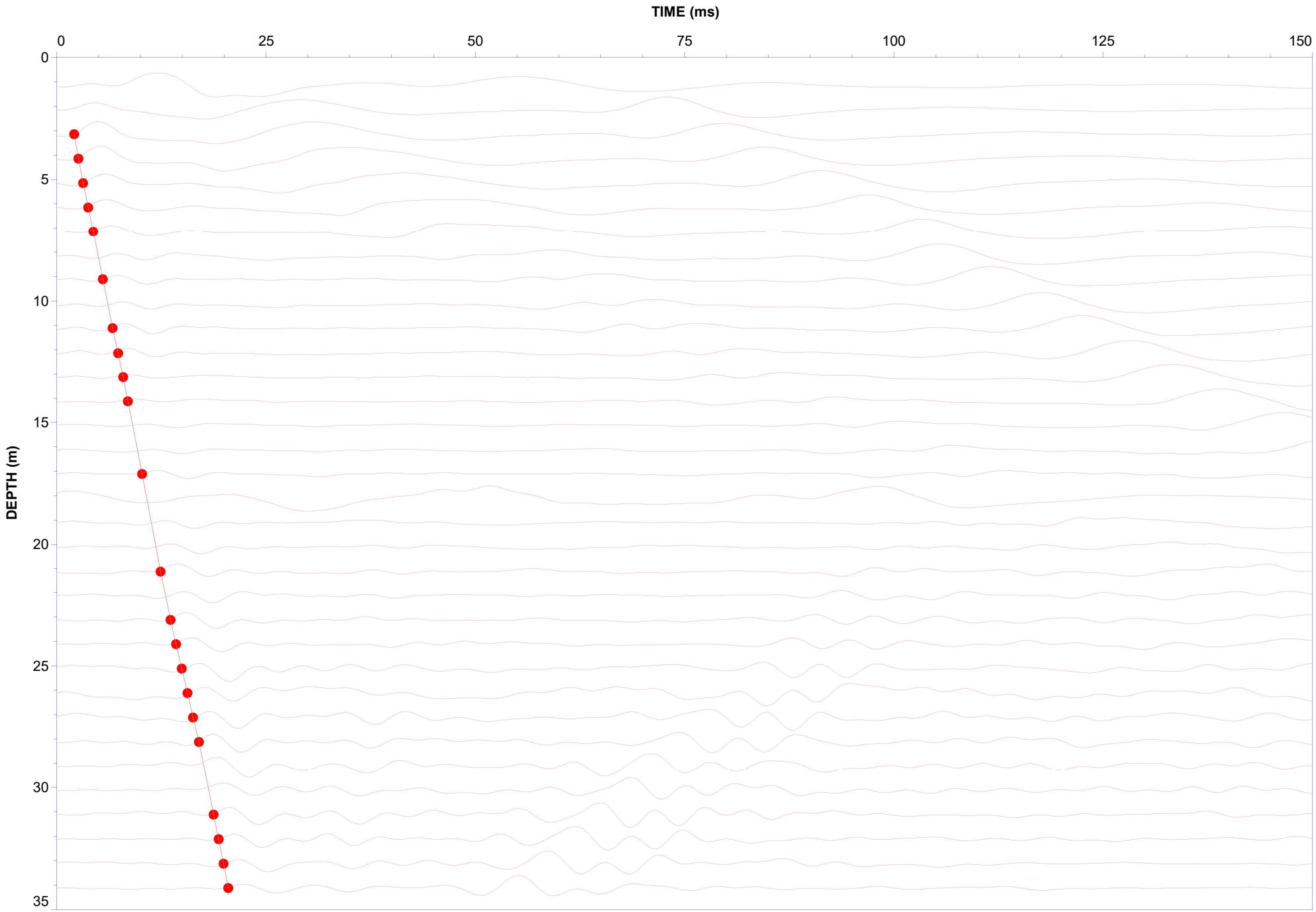
Analysis: P wave-Geo Z | Date: 2024-02-26



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-350 Hz | Sounding ID: SCPT24-TMF-MW03AB
Analysis: P wave-Geo X | Date: 2024-03-13

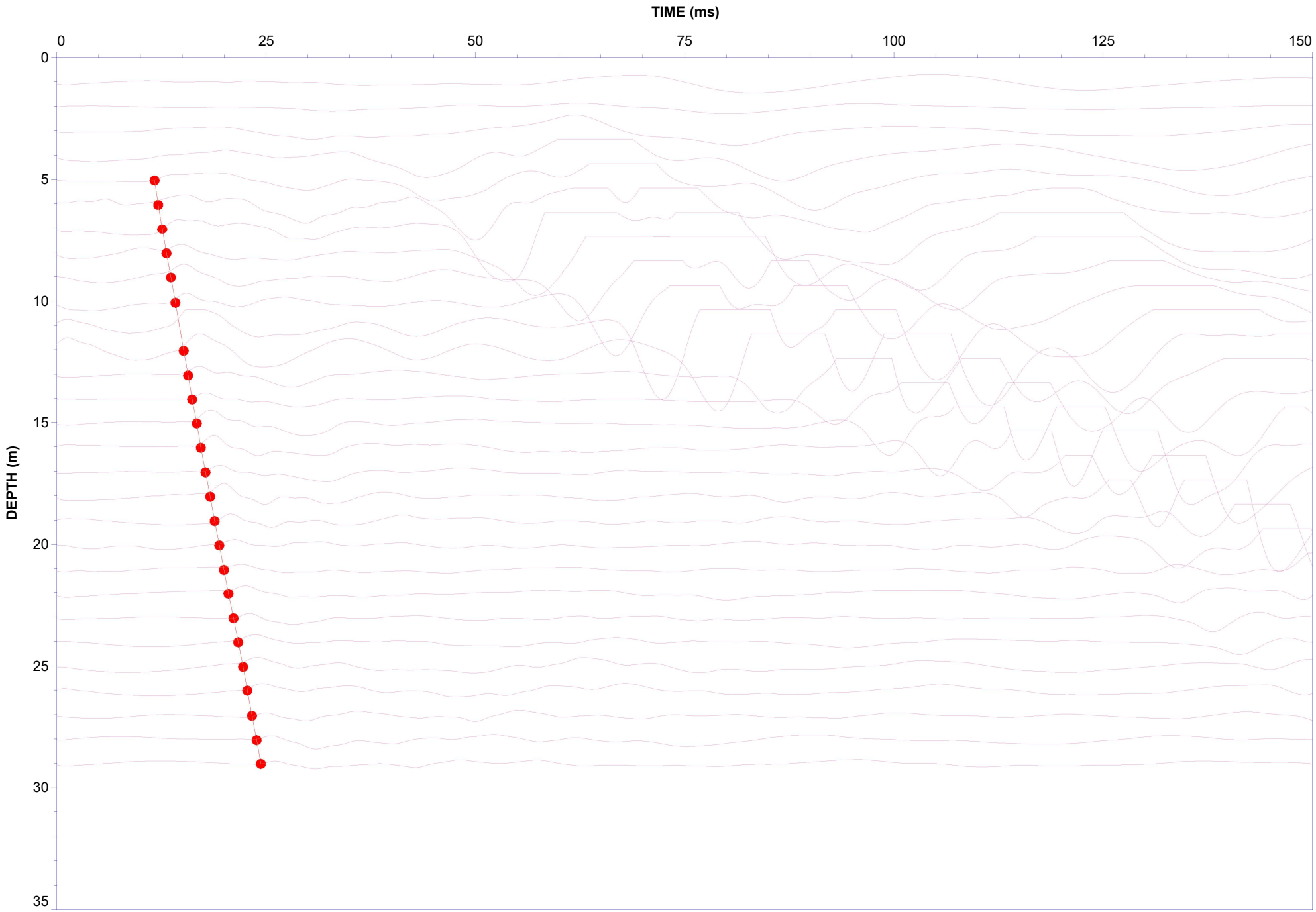


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-TMF-MW08AB
Analysis: P wave-Geo X | Date: 2024-03-20



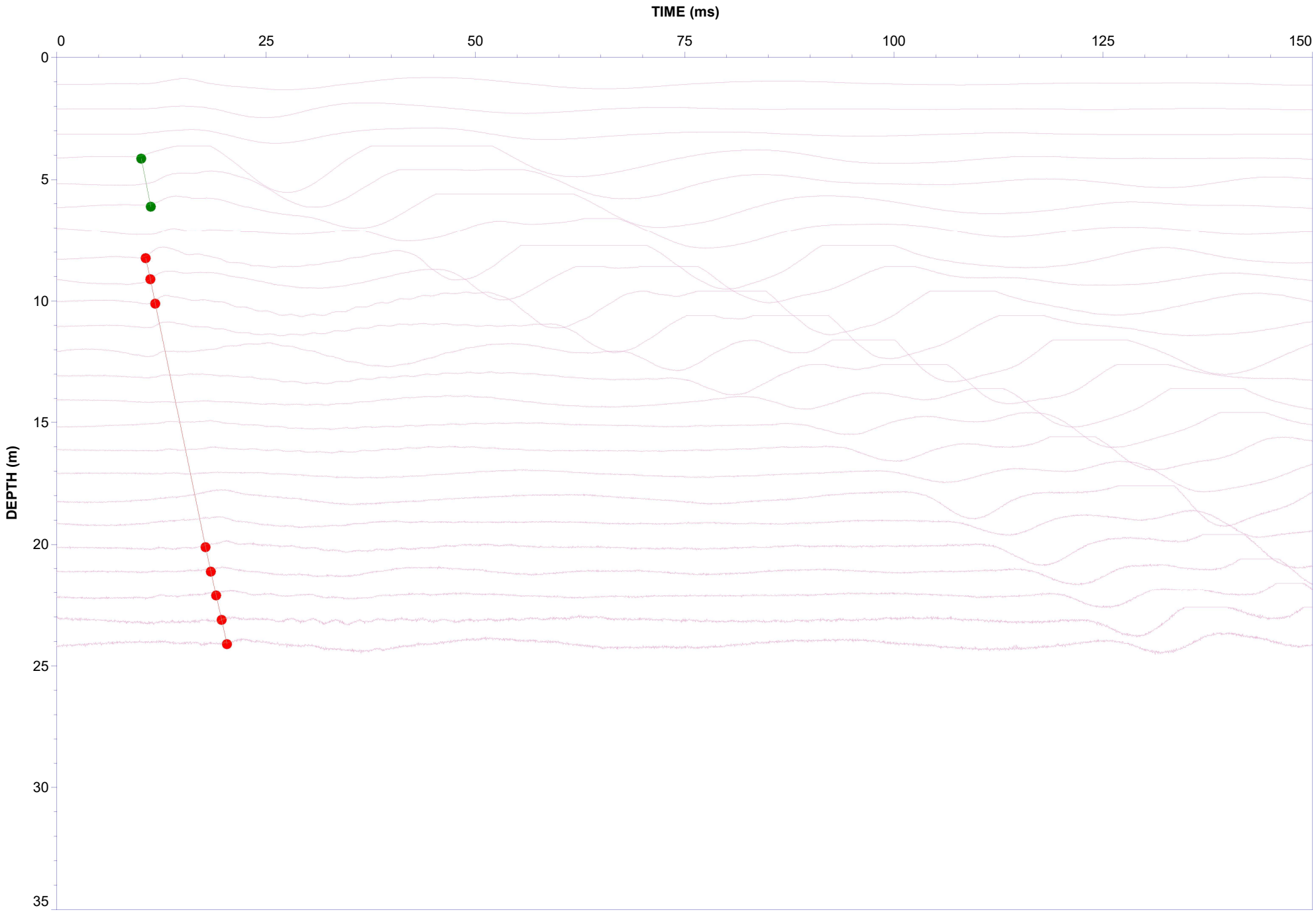
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-350 Hz | Sounding ID: SCPT24-TMF-BH202

Analysis: P wave-Geo X | Date: 2024-03-15

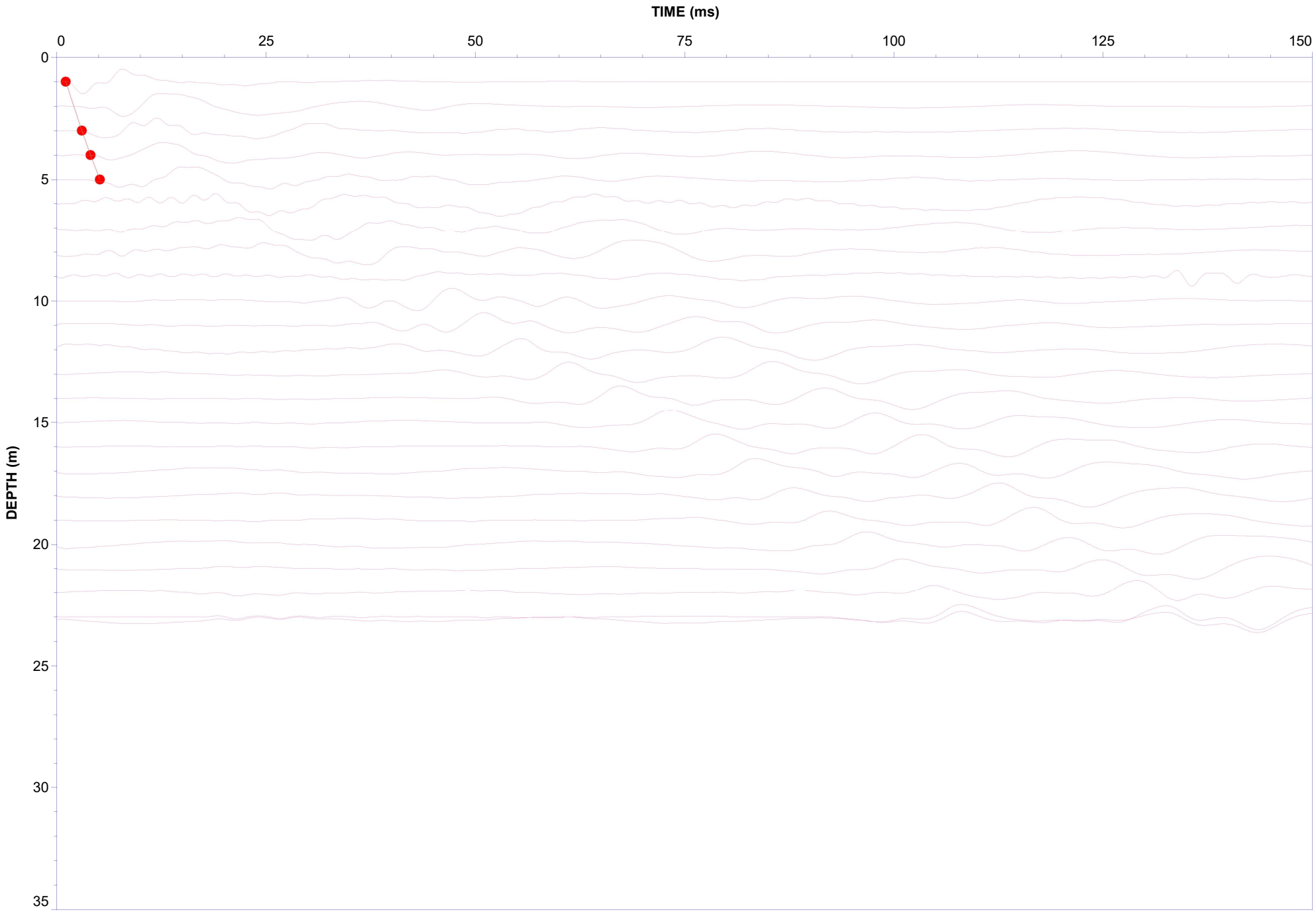


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: No Filter | Sounding ID: SCPT24-TMF-BH207

Analysis: P wave-Geo X | Date: 2024-03-18

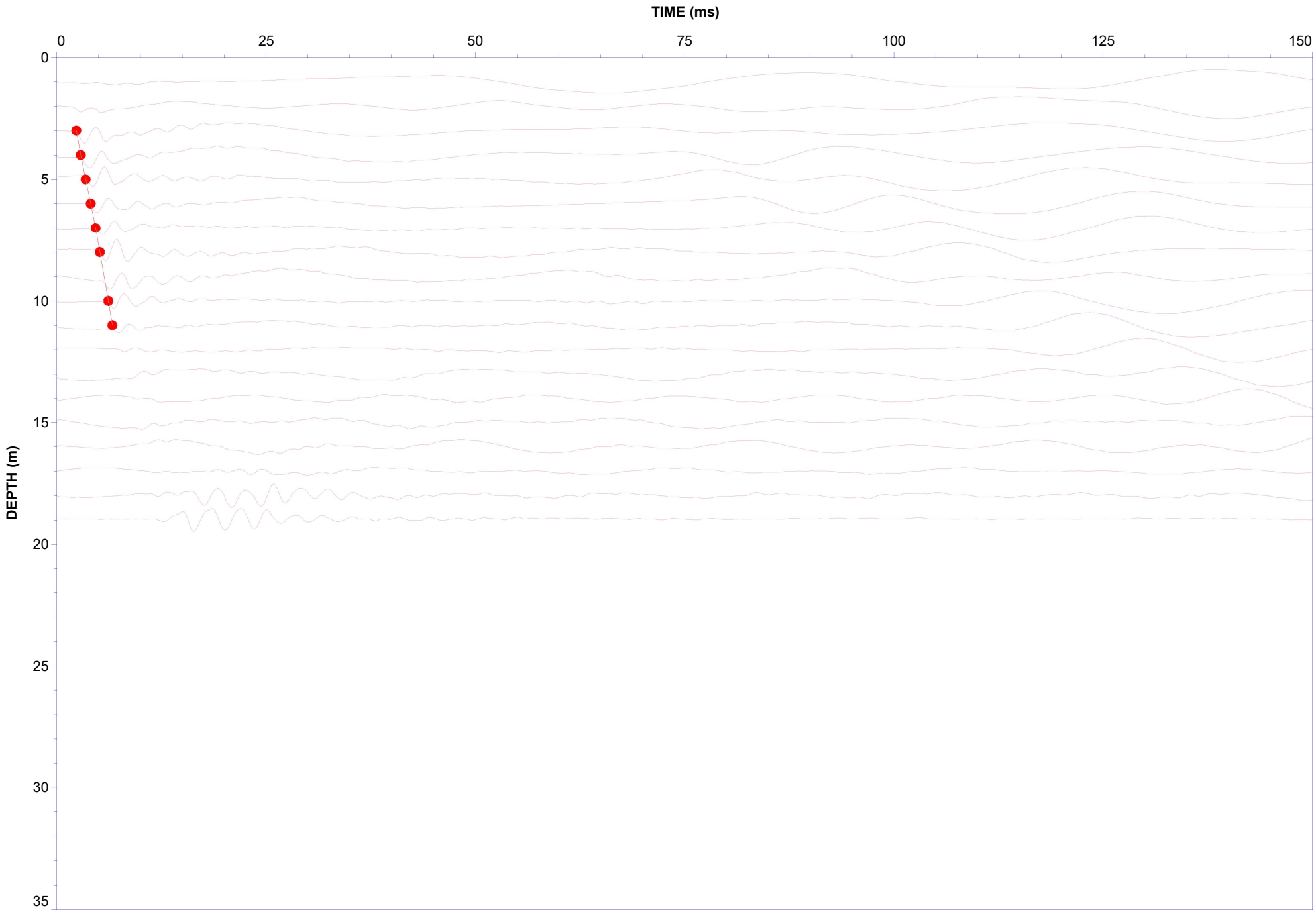


Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-WRD-BH201
Analysis: P wave-Geo X | Date: 2024-03-01



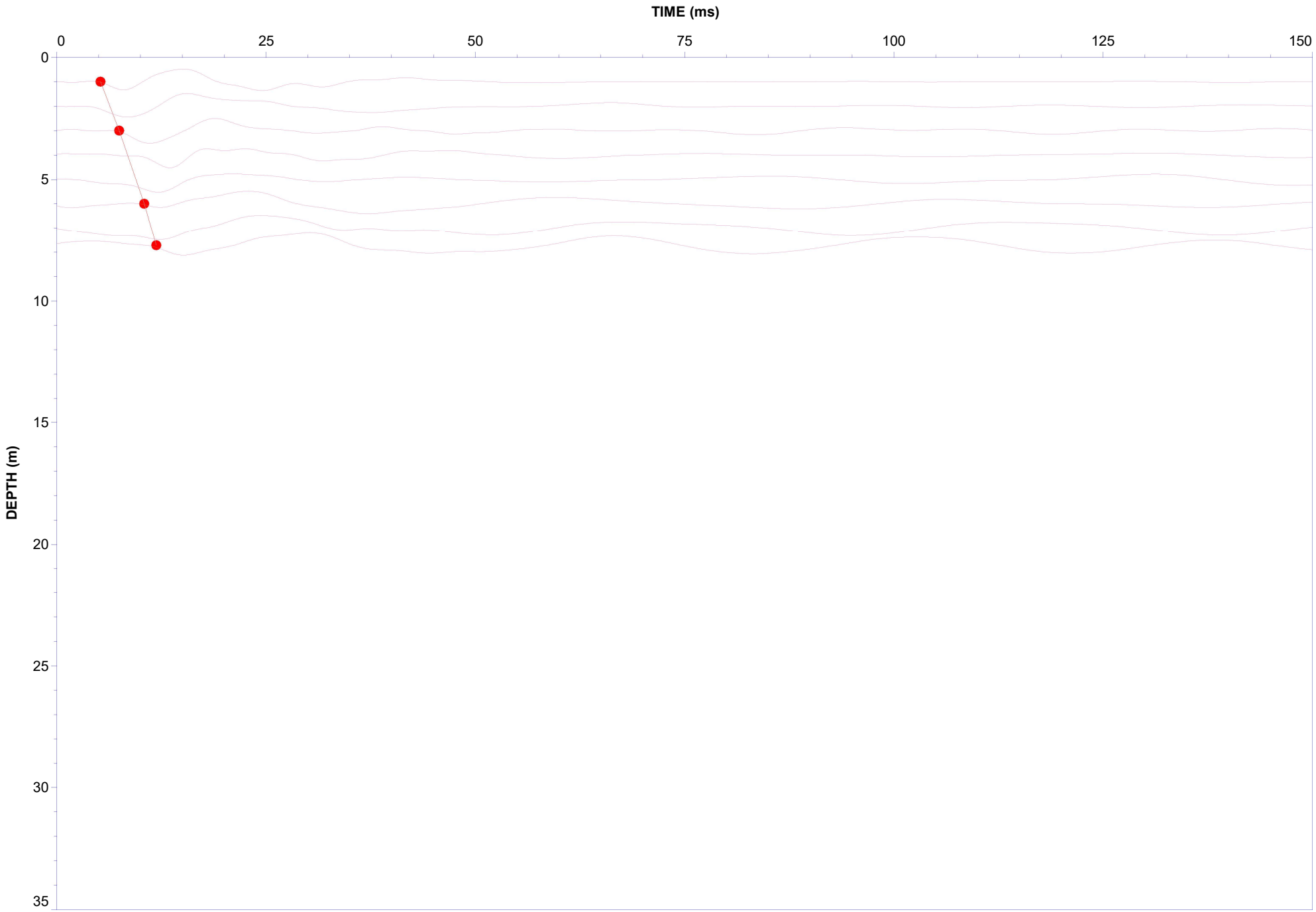
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-1000 Hz | Sounding ID: SCPT24-WRD-BH202

Analysis: P wave-Geo X | Date: 2024-03-04



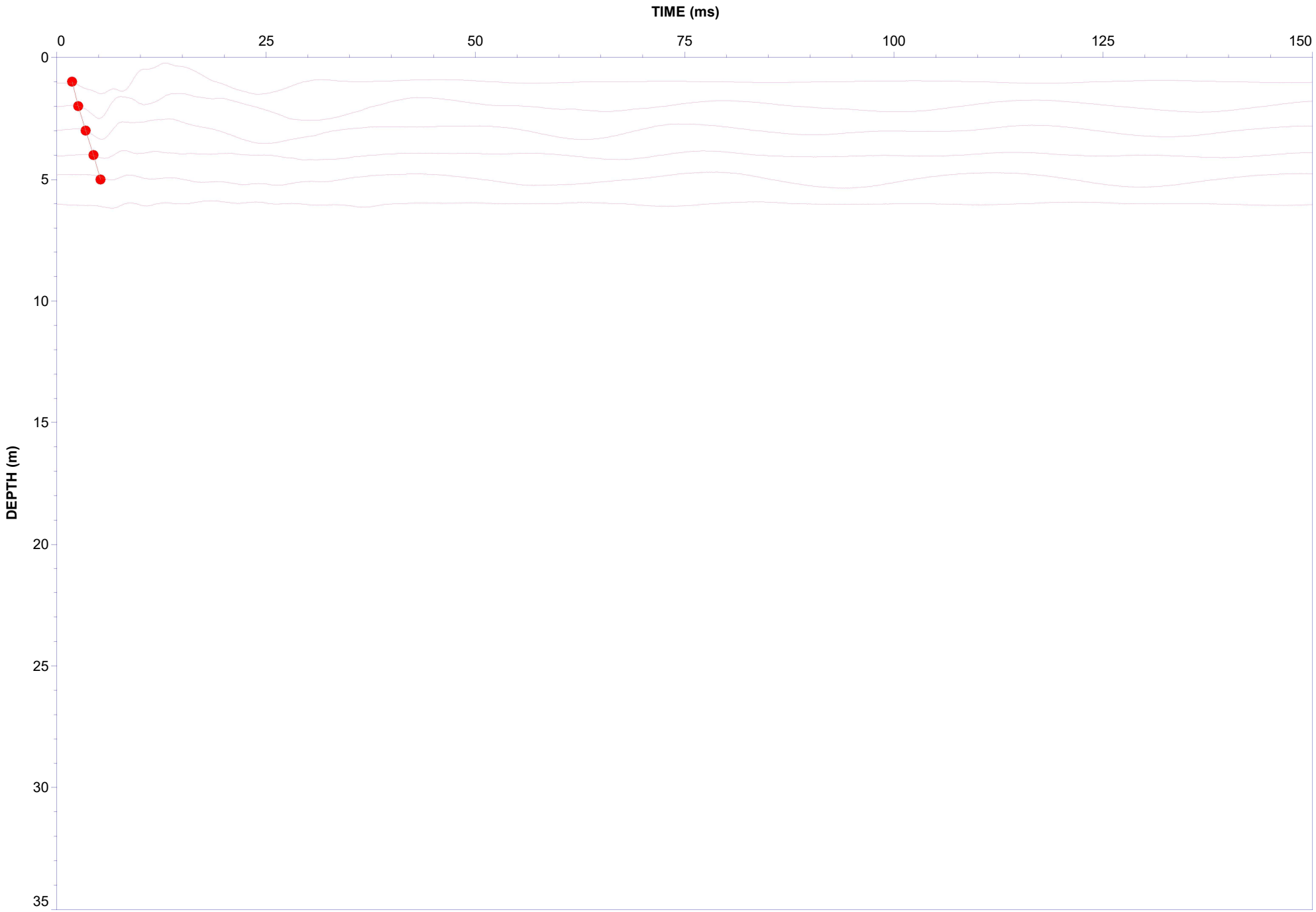
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-200 Hz | Sounding ID: SCPT24-WRD-BH205

Analysis: P wave-Geo X | Date: 2024-03-08



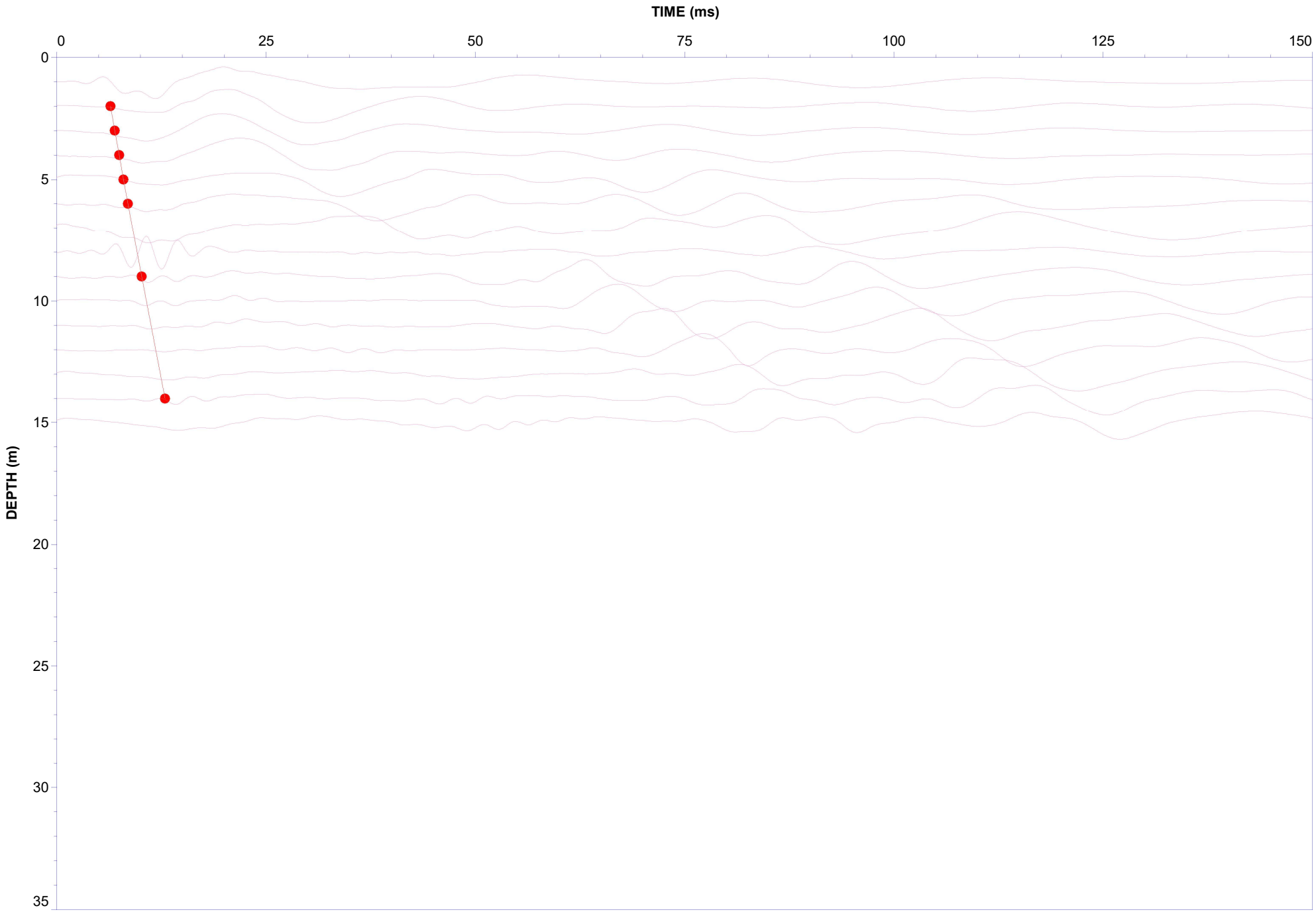
Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: None | Sounding ID: SCPT24-WRD-BH207

Analysis: P wave-Geo X | Date: 2024-03-11



Job No: 24-05-27159 | Client: Canada Nickel Company | Project: Crawford Mine - SRK | Filter: 0-350 Hz | Sounding ID: SCPT24-WRD-BH212

Analysis: P wave-Geo X | Date: 2024-03-03



Seismic Cone Penetration Test Poisson's Ratio Tabular Results

CONETEC

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH201
Date:	2024-02-19

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
2.80	3.80	212	526	0.40
3.80	4.80	213	694	0.45
4.80	5.80	214	743	0.46

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH202
Date:	2024-02-16

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
1.80	2.80	285	703	0.40
2.80	3.80	312	1022	0.45
3.80	4.70	331	1187	0.46

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH203
Date:	2024-02-14

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
4.00	5.00	227	1209	0.48
5.00	6.00	227	1311	0.49
6.00	7.00	208	1271	0.49
7.00	8.00	199	1401	0.49
8.00	9.00	182	1618	0.49
9.00	10.00	197	1600	0.49
10.00	11.00	210	1831	0.49
11.00	12.00	218	1700	0.49
12.00	13.00	214	1746	0.49
13.00	14.00	198	1746	0.49
14.00	15.00	182	1746	0.49
15.00	16.00	172	1686	0.50
18.00	19.00	168	1643	0.50
19.00	20.00	189	1587	0.49
20.00	21.00	229	1704	0.49
21.00	22.00	224	1704	0.49

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH204
Date:	2024-02-18

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
1.95	2.95	322	961	0.44
2.95	3.95	316	1460	0.48
3.95	4.95	291	1399	0.48
4.95	5.95	276	1771	0.49
5.95	6.95	212	1427	0.49
6.95	7.95	218	1433	0.49
7.95	8.95	214	1797	0.49
8.95	9.95	180	1800	0.50
9.95	10.95	209	1803	0.49
10.95	11.95	237	1805	0.49
11.95	12.95	244	1807	0.49
12.95	13.95	244	1808	0.49
13.95	14.95	244	1809	0.49
14.95	15.32	257	1833	0.49

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-LGE-BH205
Date:	2024-02-26

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
0.80	1.80	217	518	0.39
1.80	2.80	217	806	0.46
2.80	3.80	305	1161	0.46
3.80	4.80	306	1161	0.46
4.80	5.80	243	1441	0.49
5.80	6.80	195	1592	0.49
6.80	7.80	201	1592	0.49
7.80	8.80	172	1592	0.49
8.80	9.80	171	1592	0.49
9.80	10.80	207	1592	0.49
10.80	11.80	204	1592	0.49
11.80	12.80	183	1592	0.49
12.80	13.80	203	1592	0.49
13.80	14.80	184	1592	0.49
14.80	15.80	180	1592	0.49
15.80	16.80	175	1592	0.49
16.80	17.80	181	1592	0.49
17.80	18.80	208	1592	0.49
18.80	19.80	211	1601	0.49
19.80	20.80	213	1597	0.49
20.80	21.80	213	1587	0.49
21.80	22.80	213	1615	0.49
22.80	23.80	262	1859	0.49
23.80	24.80	262	1880	0.49
24.80	25.80	308	1882	0.49

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW03AB
Date:	2024-03-13

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
1.80	2.23	179	1294	0.49

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-MW08AB
Date:	2024-03-20

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
2.95	3.95	150	1643	0.50
3.95	4.95	161	1571	0.50
4.95	5.95	157	1500	0.49
5.95	6.95	185	1536	0.49
6.95	7.98	194	1629	0.49
7.98	8.92	185	1629	0.49
8.92	9.98	164	1678	0.50
9.98	10.92	182	1678	0.49
10.92	11.95	177	1558	0.49
11.95	12.92	181	1562	0.49
12.92	13.92	182	1719	0.49
13.92	14.92	161	1766	0.50
14.92	15.95	173	1766	0.50
15.95	16.92	153	1766	0.50
16.92	18.92	194	1785	0.49
18.92	19.92	218	1785	0.49
19.92	20.92	189	1785	0.49
20.92	21.92	213	1674	0.49
21.92	22.92	266	1674	0.49
22.92	23.92	252	1508	0.49
23.92	24.92	261	1455	0.48
24.92	25.92	222	1480	0.49
25.92	26.92	276	1484	0.48
26.92	27.92	268	1404	0.48
27.92	28.92	295	1716	0.49
28.92	29.92	281	1716	0.49
29.92	30.92	296	1716	0.49
30.92	31.92	296	1635	0.48
31.92	32.92	302	1741	0.49
32.92	33.92	305	1782	0.49

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-BH202
Date:	2024-03-15

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
4.85	5.85	149	1555	0.50
5.85	6.85	142	1585	0.50
6.85	7.85	180	1530	0.49
7.85	8.85	180	1579	0.49
8.85	9.88	187	1691	0.49
9.88	10.85	152	1758	0.50
10.85	11.85	123	1758	0.50
11.85	12.85	123	1742	0.50
12.85	13.85	144	1852	0.50
13.85	14.85	154	1701	0.50
14.85	15.85	161	1887	0.50
15.85	16.85	179	1728	0.50
16.85	17.85	201	1738	0.49
17.85	18.85	212	1747	0.49
18.85	19.85	229	1754	0.49
19.85	20.85	250	1761	0.49
20.85	21.85	258	1767	0.49
21.85	22.85	245	1624	0.49
22.85	23.85	260	1699	0.49
23.85	24.85	239	1703	0.49
24.85	25.82	296	1812	0.49
25.82	26.85	311	1840	0.49
26.85	27.85	316	1789	0.48
27.85	28.82	321	1821	0.48

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-TMF-BH207
Date:	2024-03-18

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
3.95	4.92	281	1518	0.48
4.92	5.92	248	1518	0.49
8.05	8.92	145	1527	0.50
8.92	9.92	139	1638	0.50
9.92	10.92	144	1635	0.50
10.92	11.92	143	1635	0.50
11.92	12.92	139	1635	0.50
12.92	13.92	135	1635	0.50
13.92	14.92	162	1635	0.50
14.92	15.92	169	1635	0.50
15.92	16.92	176	1635	0.49
16.92	17.92	219	1635	0.49
17.92	18.92	264	1635	0.49
18.92	19.92	250	1635	0.49
19.92	20.92	257	1579	0.49
20.92	21.92	273	1580	0.49
21.92	22.92	347	1517	0.47
22.92	23.92	347	1550	0.47

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH201
Date:	2024-03-01

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
0.80	1.80	99	630	0.49
1.80	2.80	169	630	0.46
2.80	3.80	169	847	0.48
3.80	4.80	169	818	0.48

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH202
Date:	2024-03-04

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
3.80	4.80	217	1502	0.49
4.80	5.80	217	1552	0.49
5.80	6.80	227	1625	0.49
6.80	7.80	227	1885	0.49
7.80	8.80	239	1943	0.49
8.80	9.80	228	1943	0.49
9.80	10.80	171	1958	0.50

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH205
Date:	2024-03-08

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
2.80	3.80	170	933	0.48
3.80	5.80	164	933	0.48
5.80	7.52	223	1168	0.48

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH207
Date:	2024-03-11

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
1.80	2.80	85	926	0.50
2.80	3.80	85	975	0.50
3.80	4.80	85	1128	0.50

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Sounding ID:	SCPT24-WRD-BH212
Date:	2024-03-03

SCPTu POISSON'S RATIO RESULTS

Depth From (m)	Depth To (m)	Vs Interval Velocity (m/s)	Vp Interval Velocity (m/s)	Poisson's Ratio
2.80	3.80	212	1535	0.49
3.80	4.80	219	1682	0.49
4.80	5.80	210	1763	0.49
5.80	6.80	205	1724	0.49
6.80	7.80	213	1724	0.49
7.80	8.80	220	1724	0.49
8.80	9.80	226	1758	0.49
9.80	10.80	196	1758	0.49
10.80	11.80	187	1758	0.49
11.80	12.80	223	1758	0.49
12.80	13.80	265	1758	0.49

Soil Behaviour Type (SBT) Scatter Plots

CONETEC

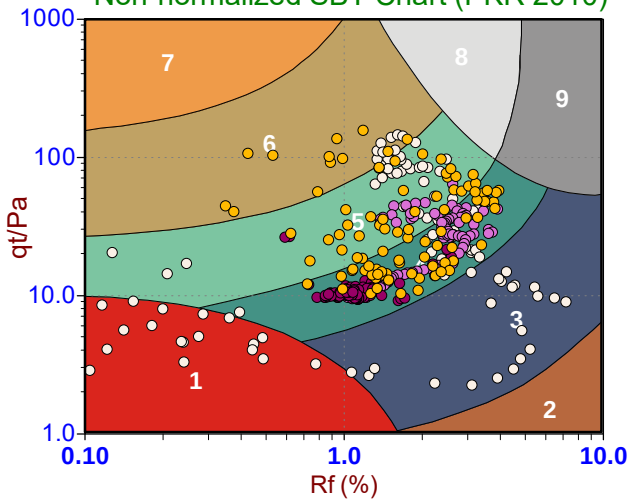
CONETEC

Canada Nickel Company

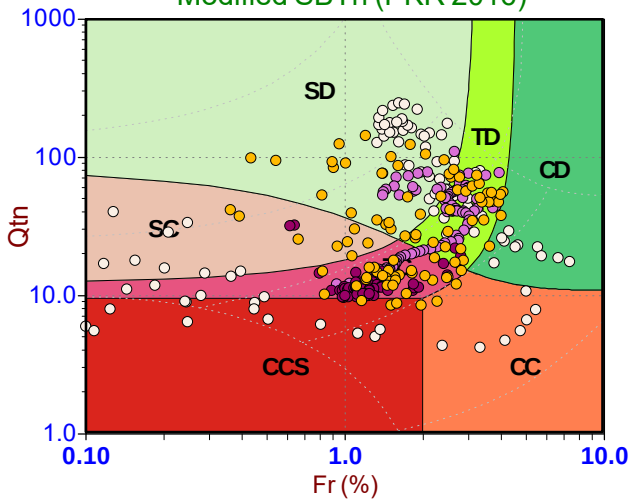
Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²

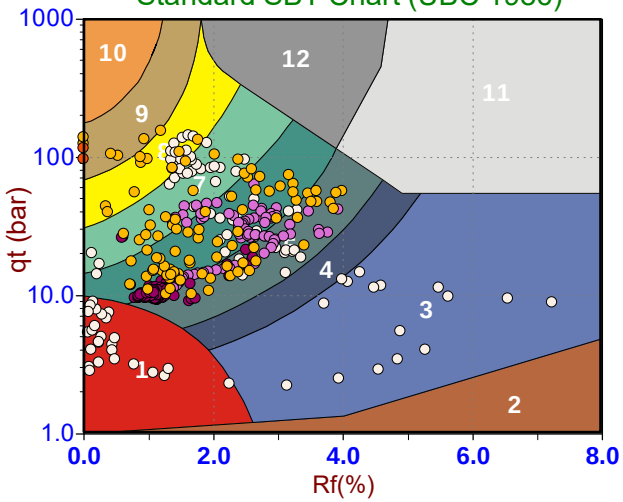
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

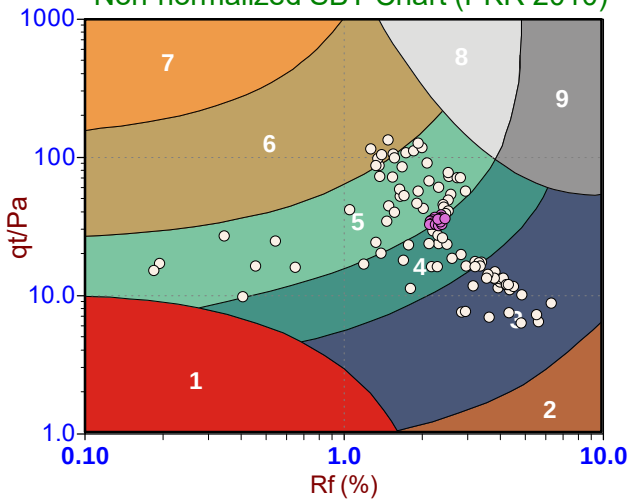
CONETEC

Canada Nickel Company

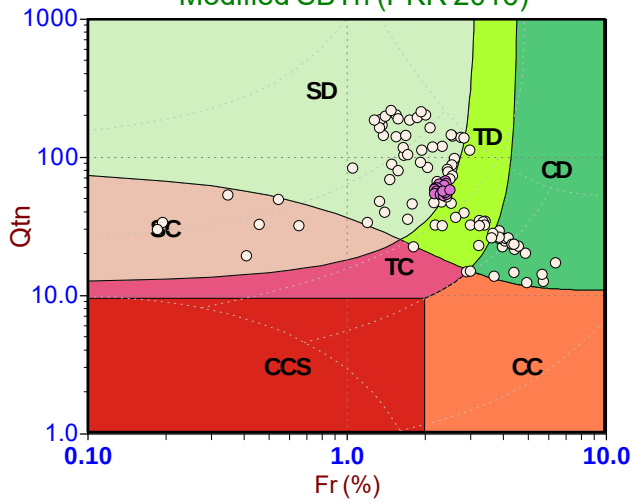
Job No: 24-05-27159
Date: 2024-02-20 13:25
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201B
Cone: 958:T1500F15U35 Area=15 cm²

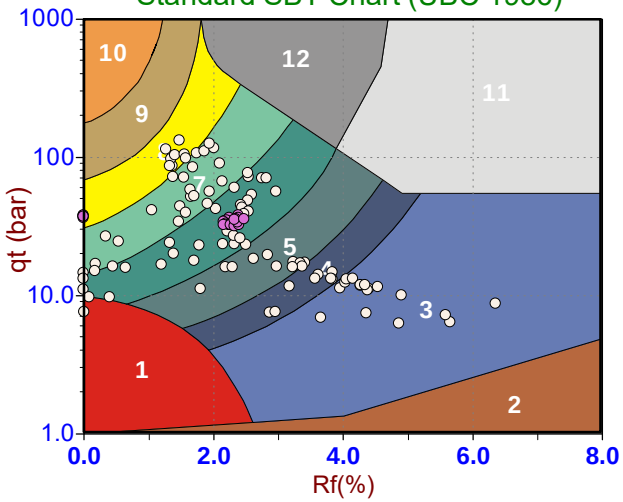
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

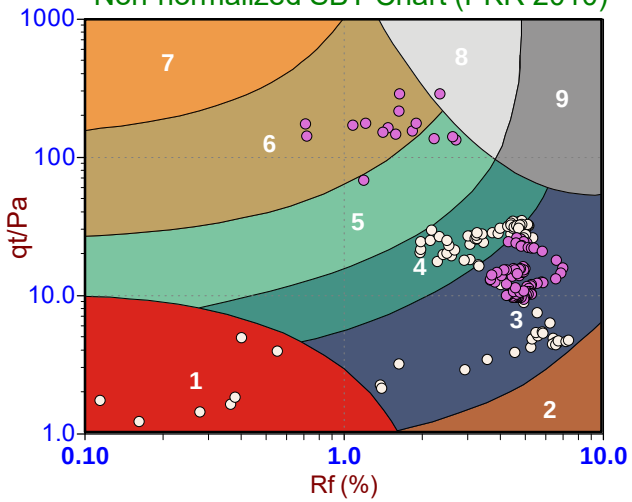
CONETEC

Canada Nickel Company

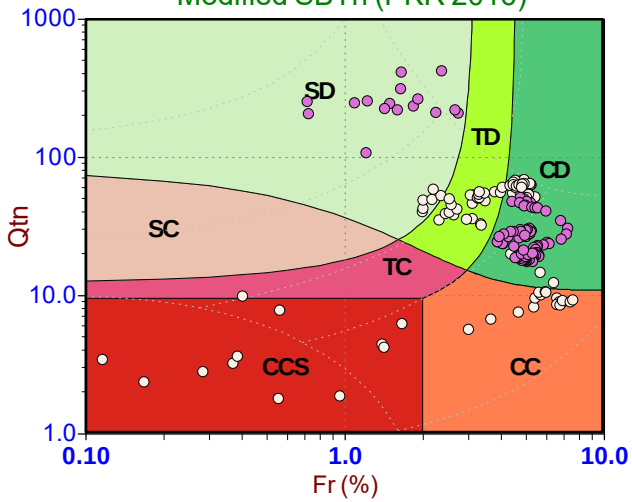
Job No: 24-05-27159
Date: 2024-02-16 14:19
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202
Cone: 958:T1500F15U35 Area=15 cm²

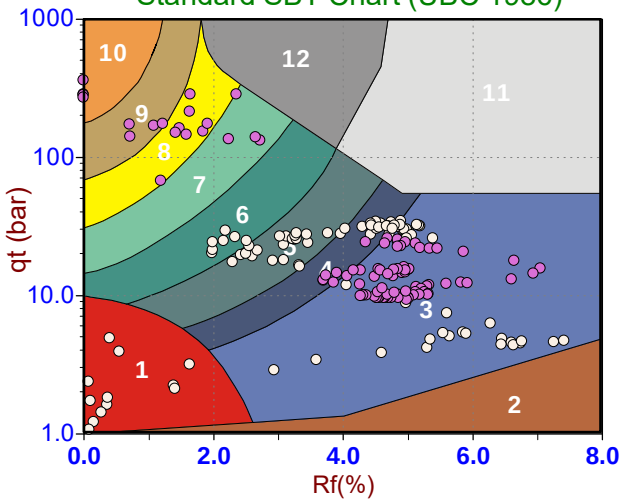
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

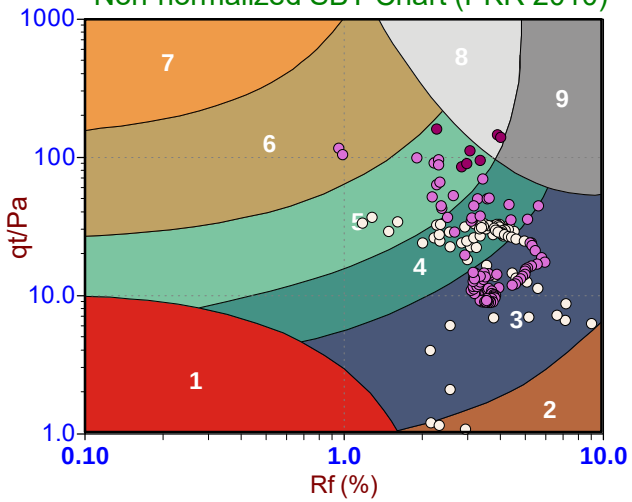
CONETEC

Canada Nickel Company

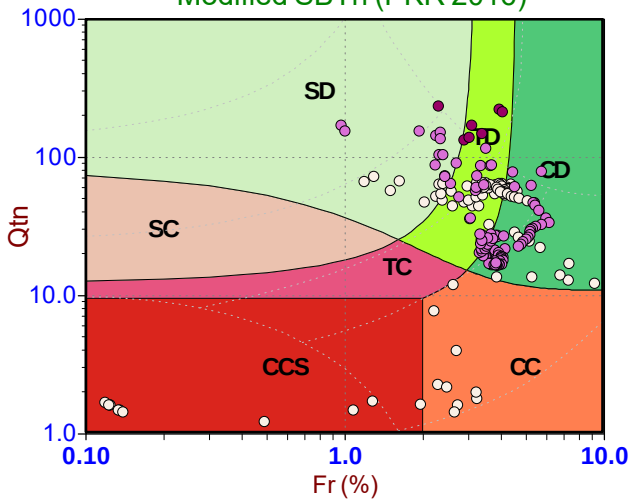
Job No: 24-05-27159
Date: 2024-02-17 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202B
Cone: 958:T1500F15U35 Area=15 cm²

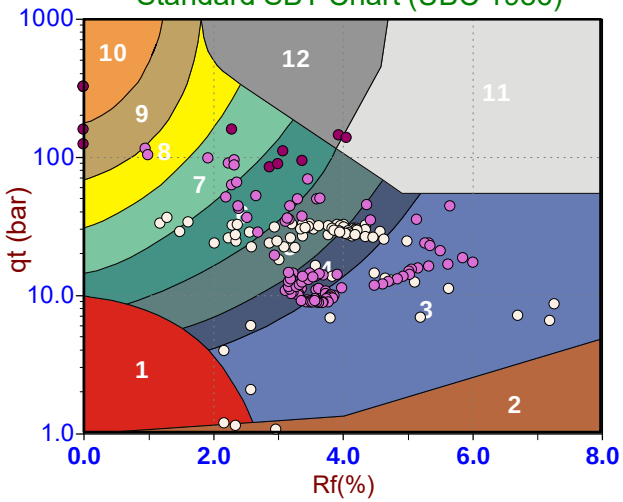
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

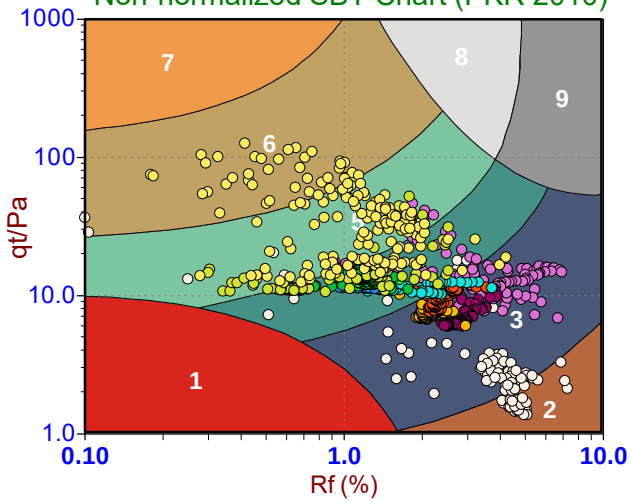
CONETEC

Canada Nickel Company

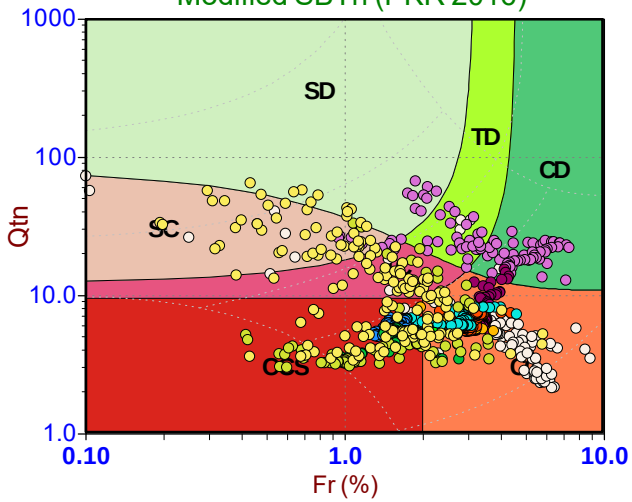
Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²

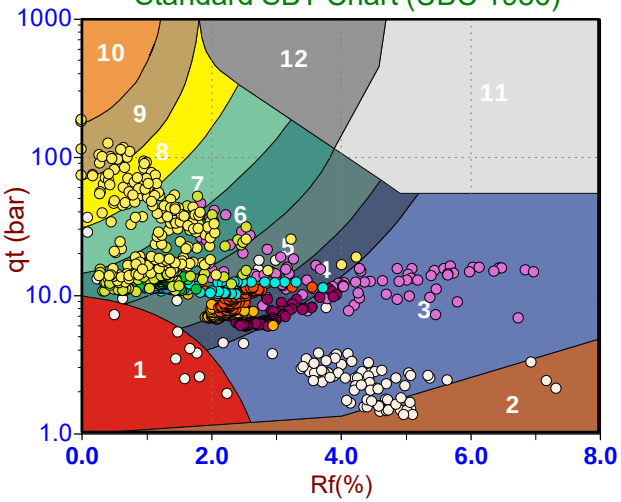
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

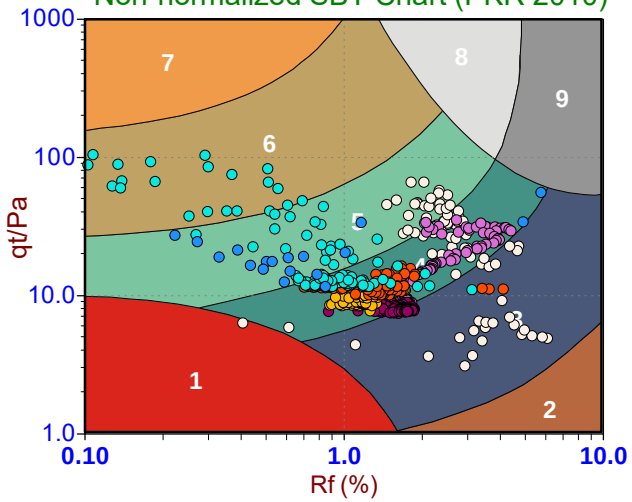
CONETEC

Canada Nickel Company

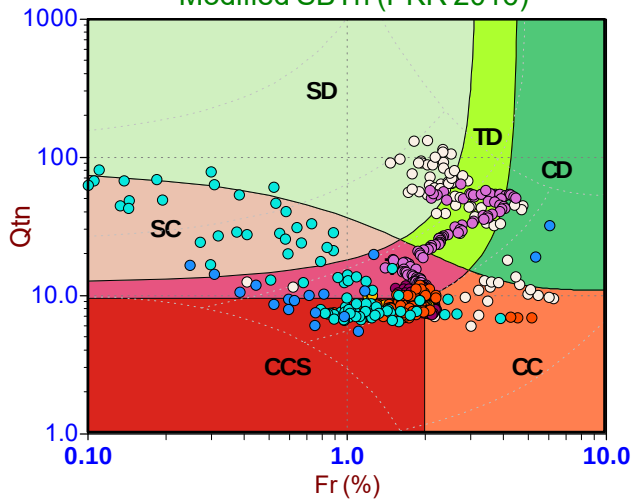
Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²

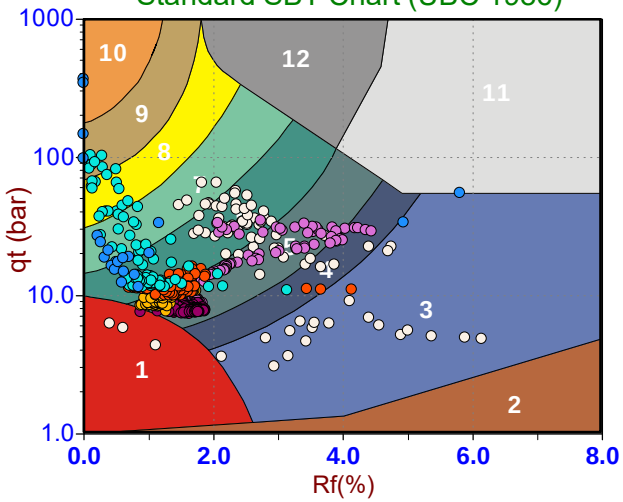
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

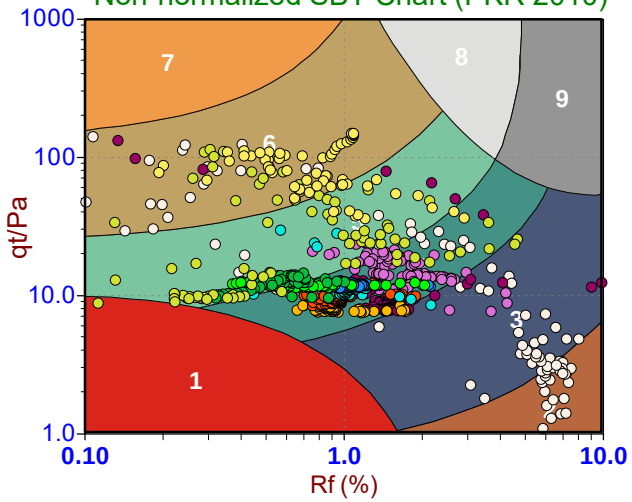
CONETEC

Canada Nickel Company

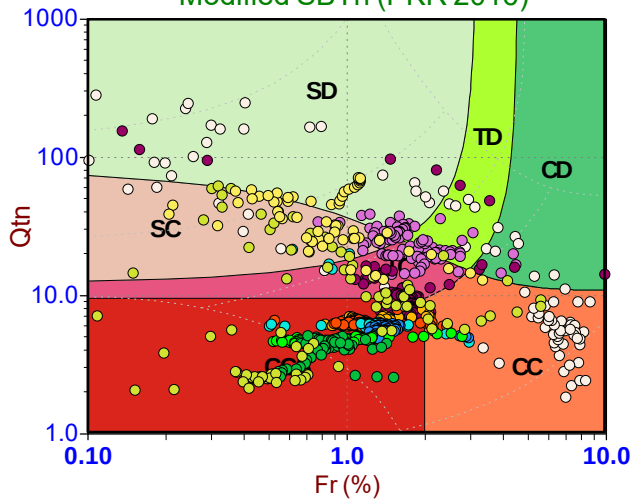
Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²

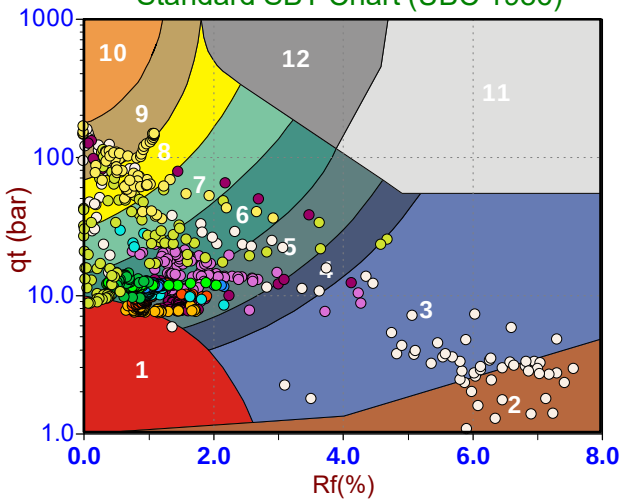
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

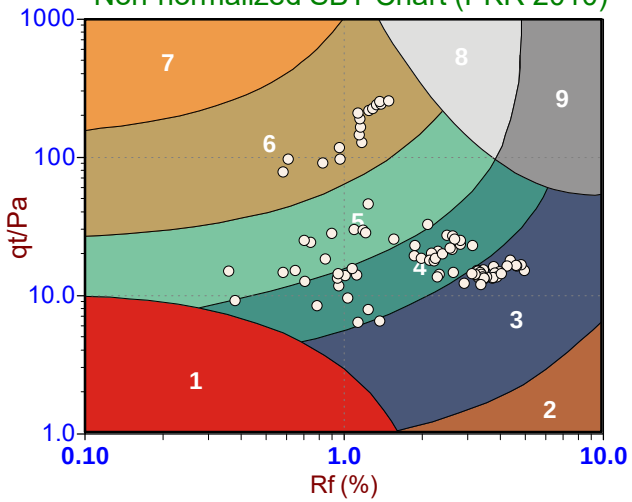
CONETEC

Canada Nickel Company

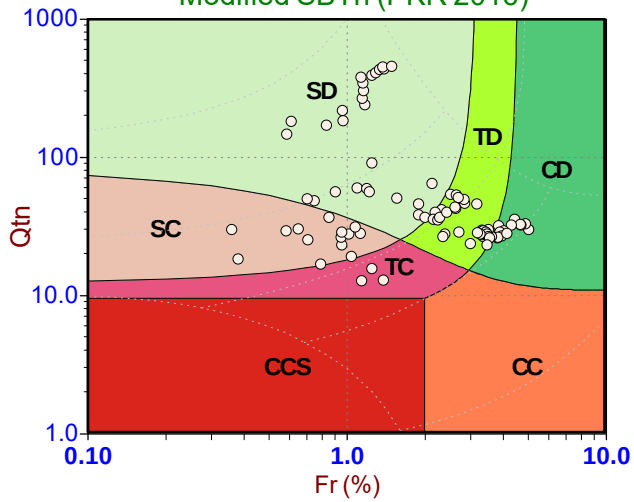
Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²

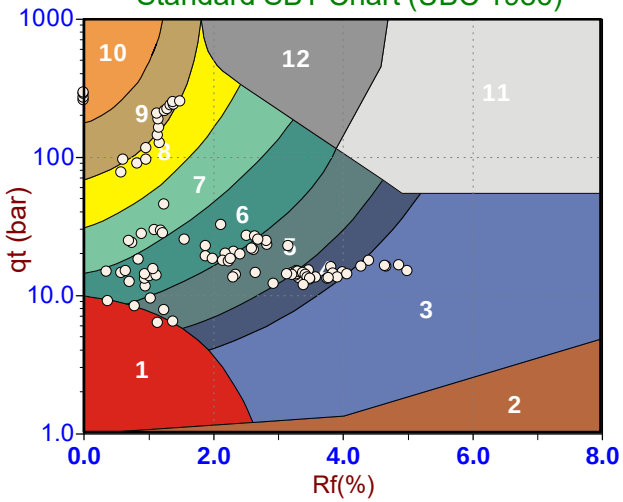
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

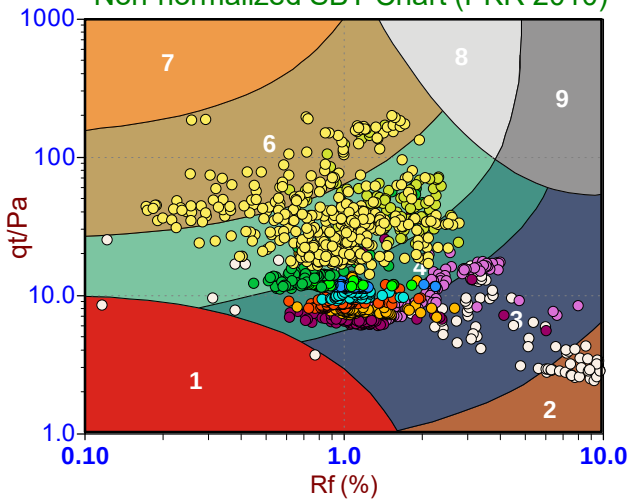
CONETEC

Canada Nickel Company

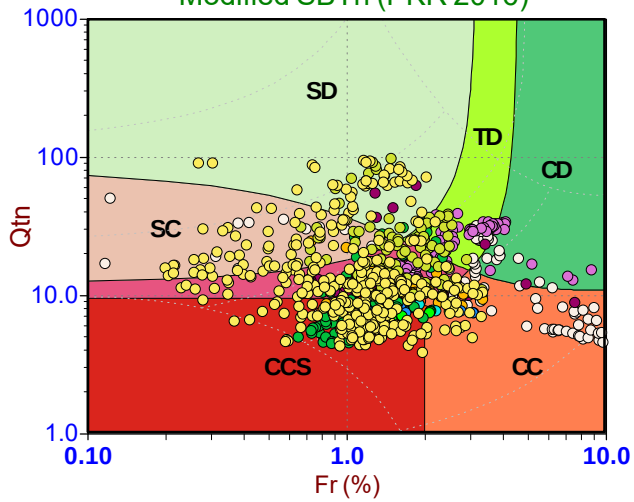
Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²

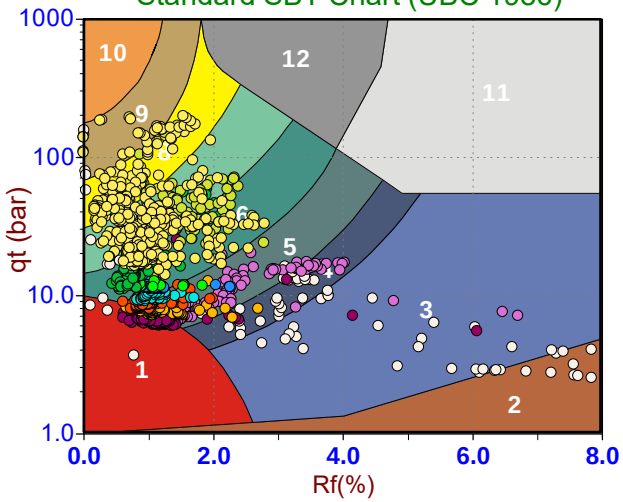
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

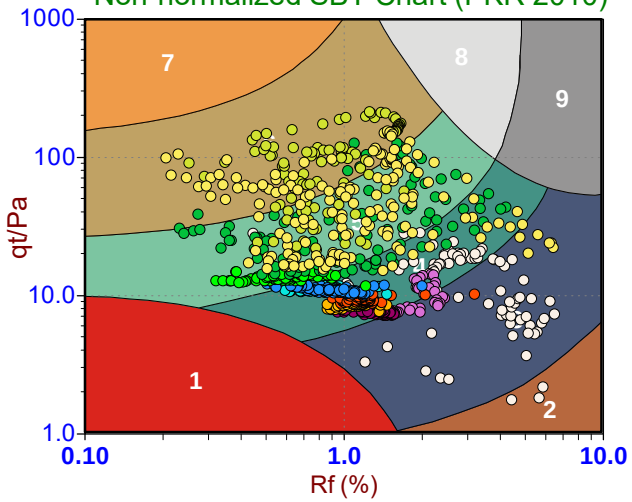
CONETEC

Canada Nickel Company

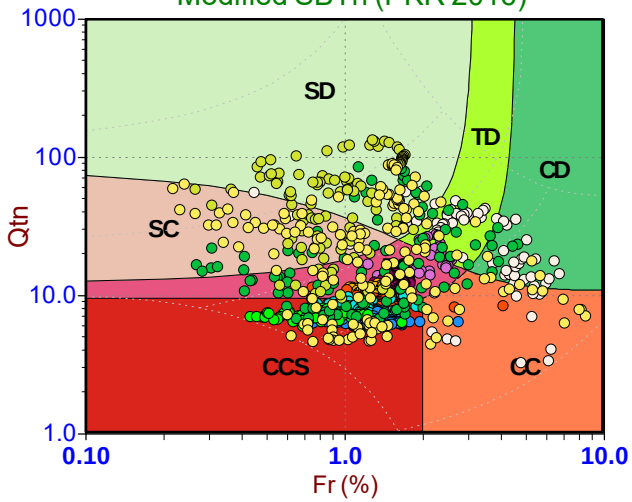
Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²

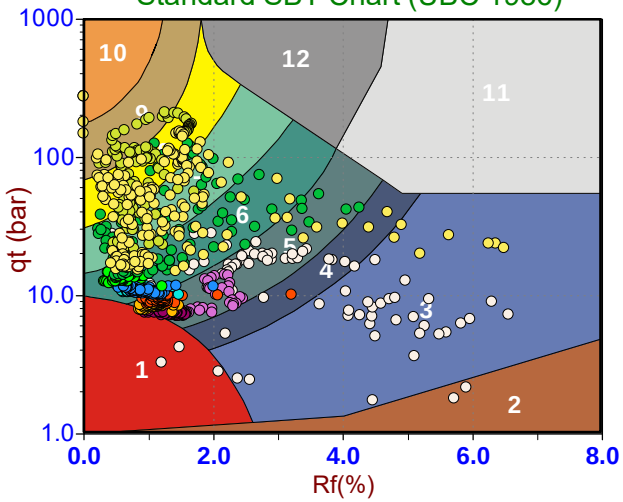
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

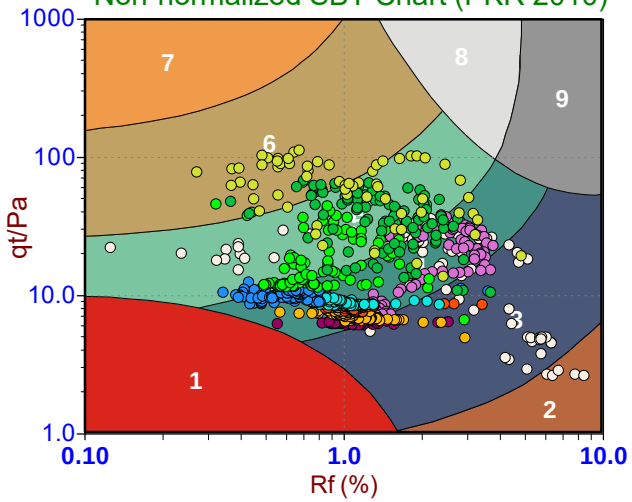
CONETEC

Canada Nickel Company

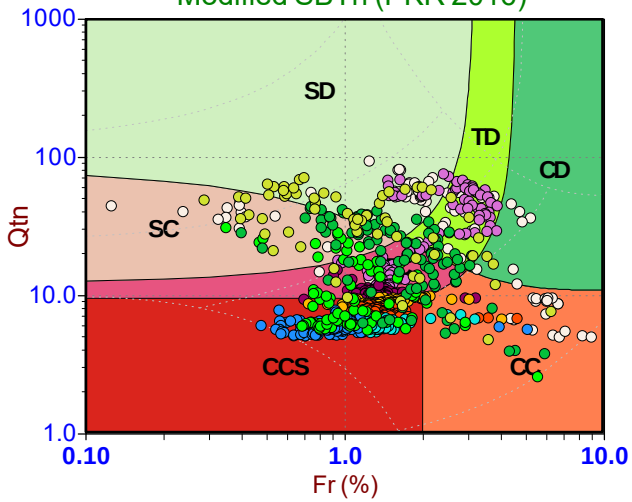
Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²

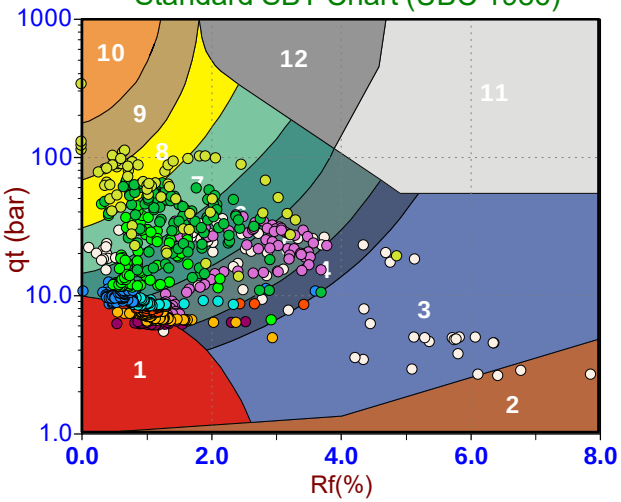
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

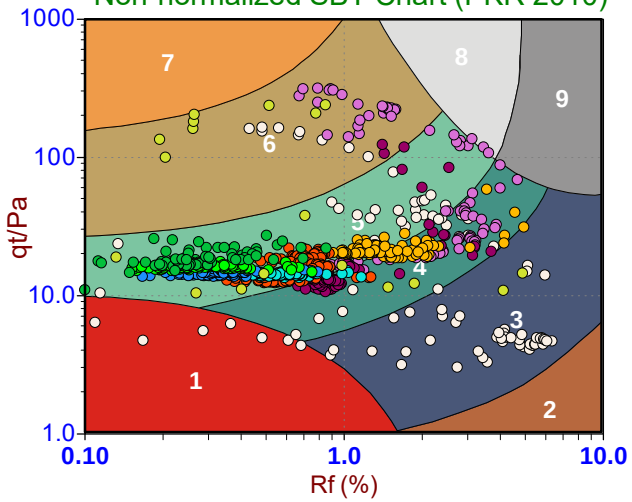
CONETEC

Canada Nickel Company

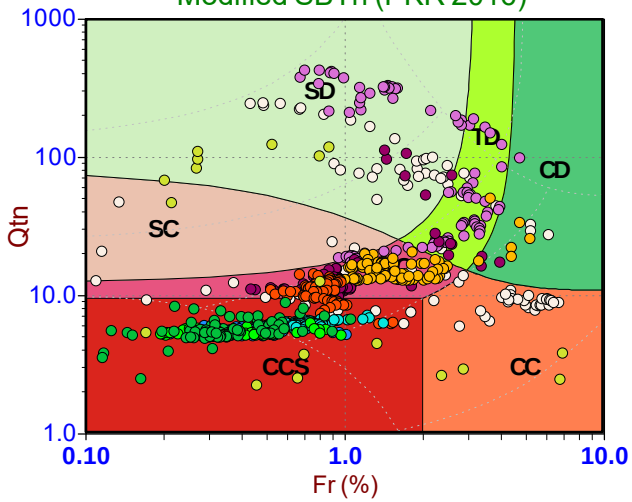
Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²

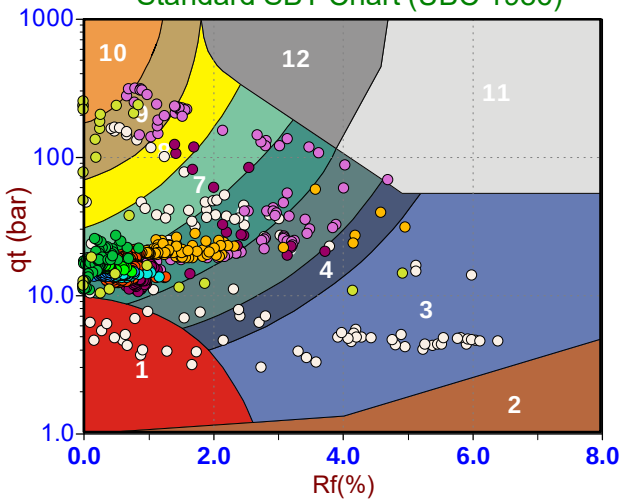
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

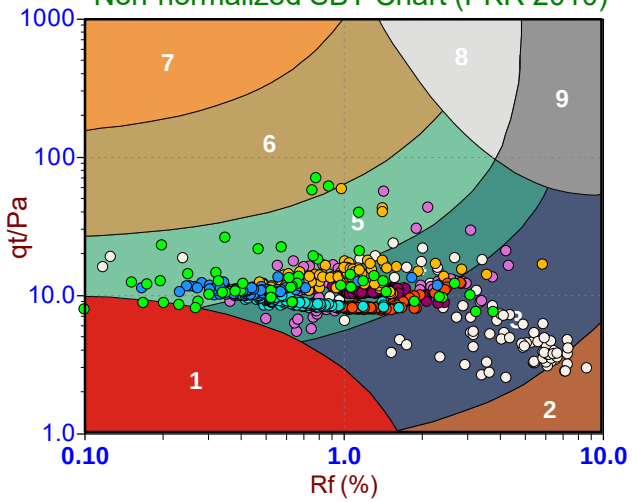
CONETEC

Canada Nickel Company

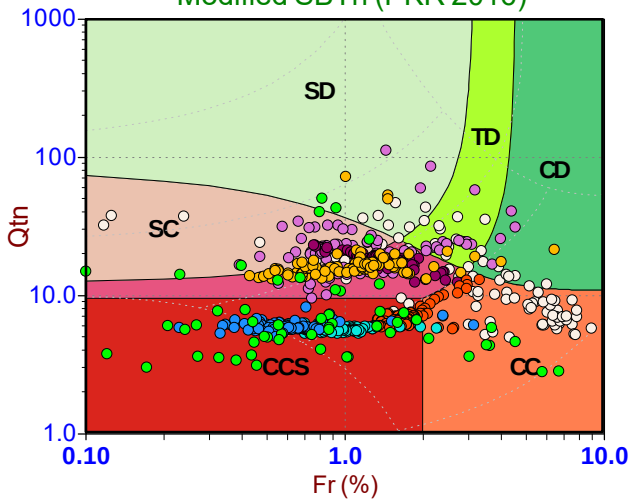
Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²

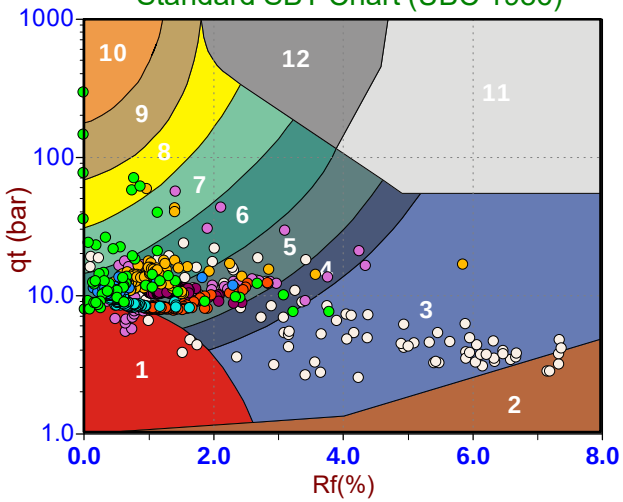
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

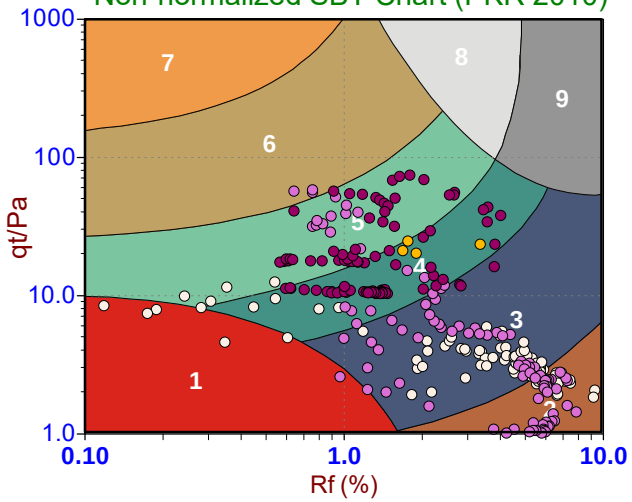
CONETEC

Canada Nickel Company

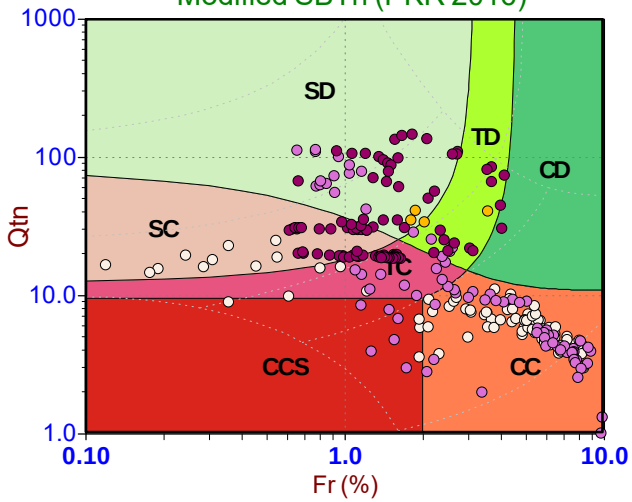
Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²

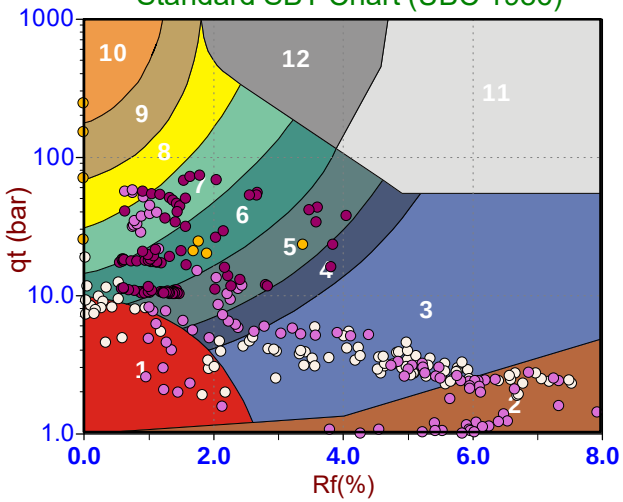
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

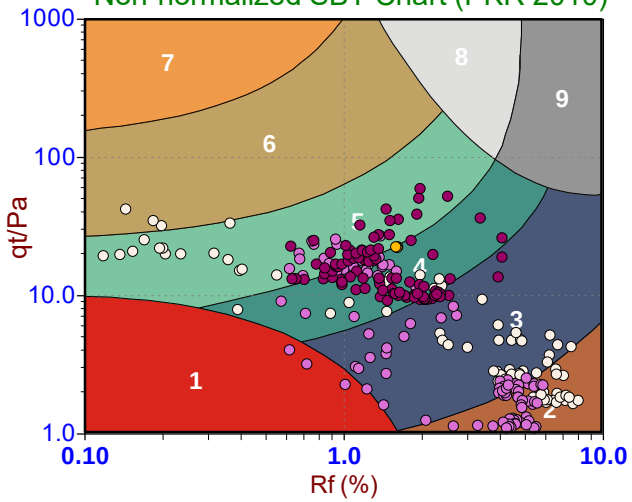
CONETEC

Canada Nickel Company

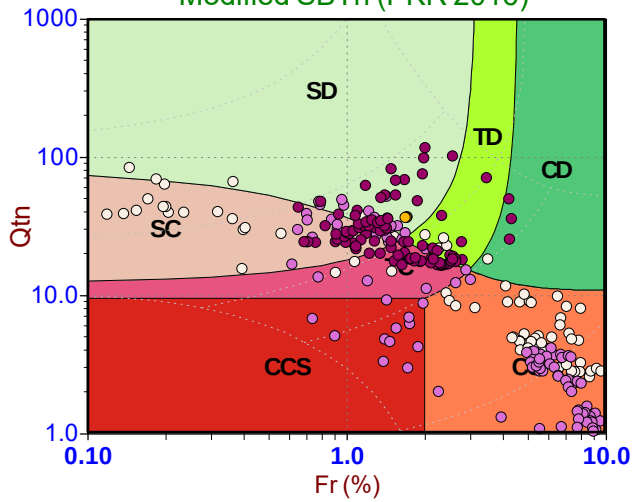
Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²

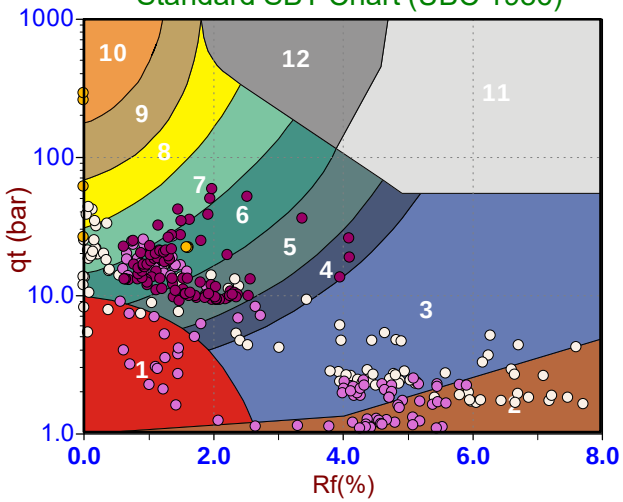
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

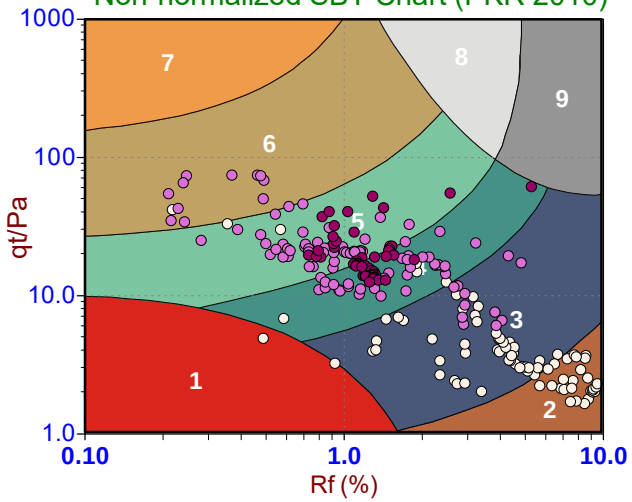
CONETEC

Canada Nickel Company

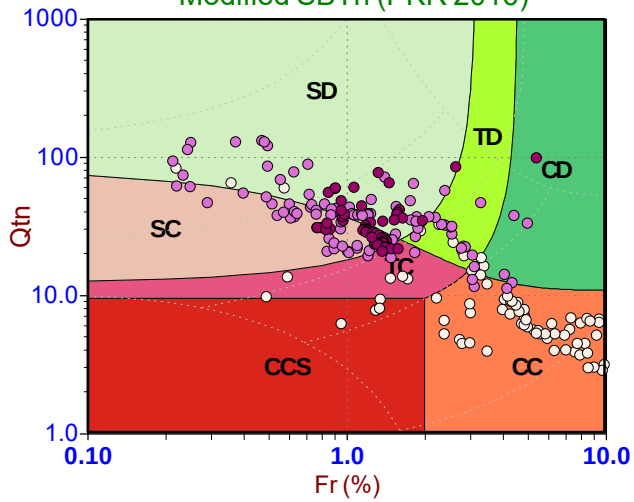
Job No: 24-05-27159
Date: 2024-03-12 09:14
Site: Crawford Mine - SRK

Sounding: CPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²

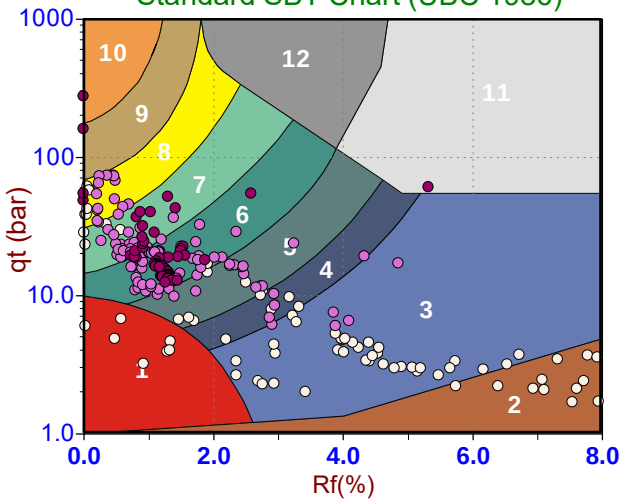
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

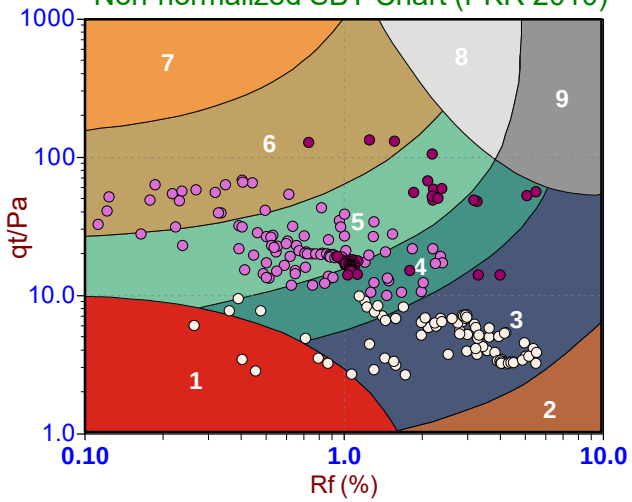
CONETEC

Canada Nickel Company

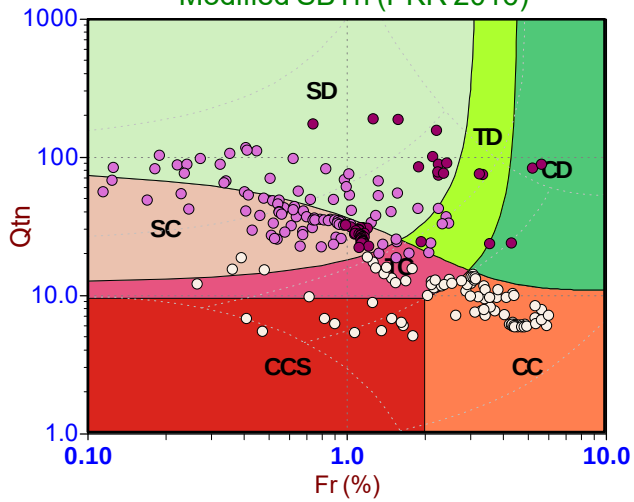
Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²

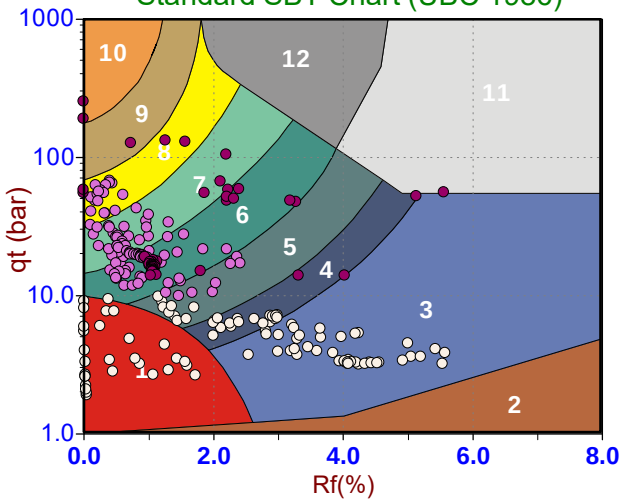
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

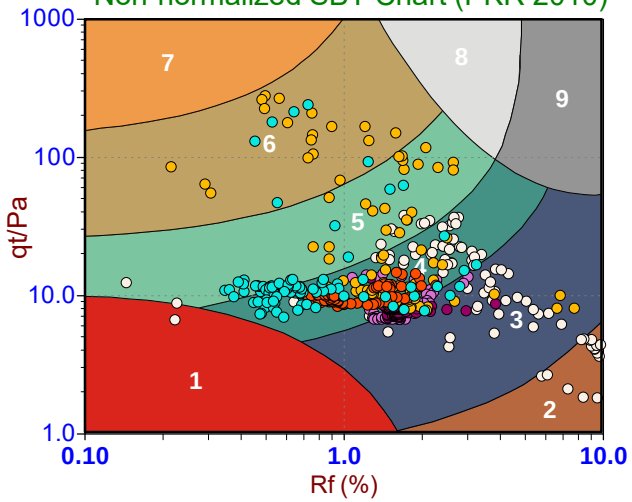
CONETEC

Canada Nickel Company

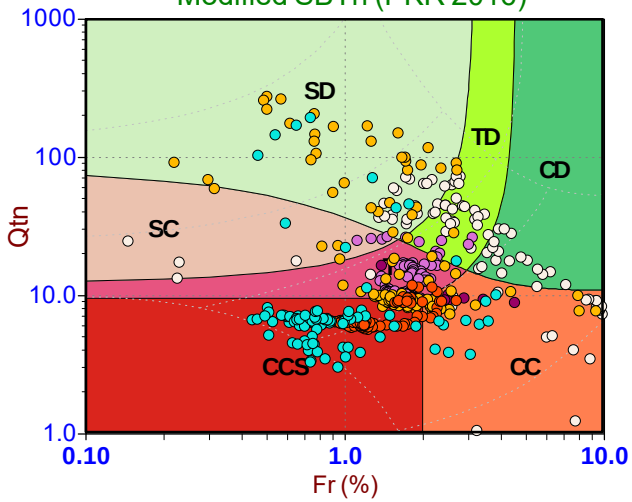
Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²

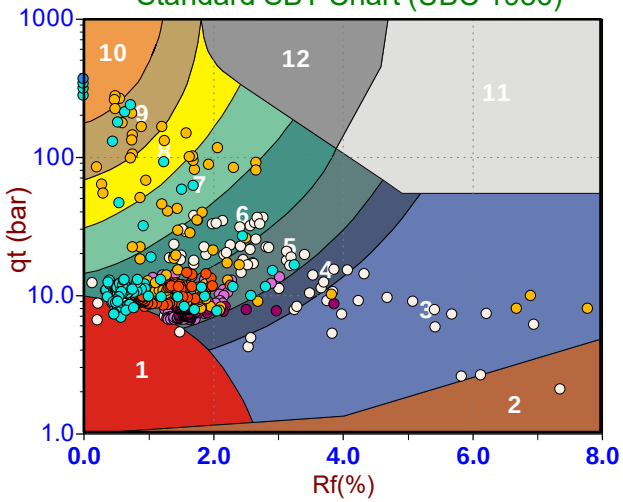
Non-normalized SBT Chart (PKR 2010)



Modified SBTn (PKR 2016)



Standard SBT Chart (UBC 1986)



Depth Ranges

- >0.0 to 2.5 m
- >2.5 to 5.0 m
- >5.0 to 7.5 m
- >7.5 to 10.0 m
- >10.0 to 12.5 m
- >12.5 to 15.0 m
- >15.0 to 17.5 m
- >17.5 to 20.0 m
- >20.0 to 22.5 m
- >22.5 to 25.0 m
- >25.0 m

Legend

- Sensitive, Fine Grained
- Organic Soils
- Clays
- Silt Mixtures
- Sand Mixtures
- Sands
- Gravelly Sand to Sand
- Stiff Sand to Clayey Sand
- Very Stiff Fine Grained

Legend

- CCS (Cont. sensitive clay like)
- CC (Cont. clay like)
- TC (Cont. transitional)
- SC (Cont. sand like)
- CD (Dil. clay like)
- TD (Dil. transitional)
- SD (Dil. sand like)

Legend

- Sensitive Fines
- Organic Soil
- Clay
- Silty Clay
- Clayey Silt
- Silt
- Sandy Silt
- Silty Sand/Sand
- Sand
- Gravelly Sand
- Stiff Fine Grained
- Cemented Sand

Pore Pressure Dissipation Summary and Pore Pressure Dissipation Plots

CONETEC

Job No: 24-05-27159
Client: Canada Nickel Company
Project: Crawford Mine - SRK
Start Date: 2024-02-14
End Date: 2024-03-22

CPTu PORE PRESSURE DISSIPATION SUMMARY

Sounding ID	File Name	Cone Area (cm^2)	Duration (s)	Test Depth (m)	$U_{initial}$ (m)	U_{max} (m)	U_{min} (m)	U_{final} (m)	Equilibrium Pore Pressure U_{eq} (m)	Estimated Equilibrium Pore Pressure U_{eq} (m)	Calculated Phreatic Surface (m)	Percent Dissipation (%)	t_{50} $(s)_1$	Assumed Rigidity Index (I_r)	c_h $(cm^2/min)_2$	Refer to Notation Number
SCPT24-LGE-BH201	24-05-27159_SP201	15	405	1.000	-4.5	3.4	-7.5	0.3								
SCPT24-LGE-BH201	24-05-27159_SP201	15	305	2.000	-6.2	7.1	-6.9	2.1								
SCPT24-LGE-BH201	24-05-27159_SP201	15	490	3.000	58.8	82.1	57.6	57.7								
SCPT24-LGE-BH201	24-05-27159_SP201	15	200	4.000	55.2	59.8	50.6	58.6								
SCPT24-LGE-BH201	24-05-27159_SP201	15	11100	7.500	-4.4	37.4	-4.4	13.6		4.6	2.9	73	3768	100	0.2	4
SCPT24-LGE-BH201	24-05-27159_SP201	15	225	10.000	16.7	16.7	4.2	7.1	7.1		2.9					
SCPT24-LGE-BH201	24-05-27159_SP201	15	1040	10.025	8.6	9.9	6.2	7.7	7.7		2.3					
SCPT24-LGE-BH202	24-05-27159_SP202	15	240	4.650	-2.0	-0.6	-4.5	-4.5								
SCPT24-LGE-BH202B	24-05-27159_SP202B	15	500	5.000	7.8	49.4	2.0	48.8								
SCPT24-LGE-BH202B	24-05-27159_SP202B	15	255	5.250	-6.4	-4.1	-6.4	-4.4								
SCPT24-LGE-BH203	24-05-27159_SP203	15	7800	7.500	41.9	41.9	24.6	24.6								
SCPT24-LGE-BH203	24-05-27159_SP203	15	9780	12.500	66.6	66.6	39.6	39.6								
SCPT24-LGE-BH203	24-05-27159_SP203	15	10320	17.500	82.0	82.0	35.3	35.3		14.3	3.2	69	4178	100	0.2	3
SCPT24-LGE-BH203	24-05-27159_SP203	15	3840	22.500	82.4	82.4	26.8	26.8		19.3	3.2	88	335	100	2.1	3
SCPT24-LGE-BH203	24-05-27159_SP203	15	485	28.175	68.5	74.0	30.5	30.5		25.0	3.2	89	83	100	8.4	3
SCPT24-LGE-BH204	24-05-27159_SP204	15	11040	7.500	49.9	49.9	25.1	25.1		4.8	2.7	55	8035	100	0.1	4
SCPT24-LGE-BH204	24-05-27159_SP204	15	10800	12.500	73.3	74.2	20.9	20.9		9.8	2.7	83	2330	100	0.3	4, 5
SCPT24-LGE-BH204	24-05-27159_SP204	15	950	12.500	73.3	9.8	9.8	9.8	9.8		2.7					5
SCPT24-LGE-BH204	24-05-27159_SP204	15	1500	14.775	12.2	31.3	6.5	11.0	11.0		3.8	100	29	100	24.7	
SCPT24-LGE-BH205	24-05-27159_SP205	15	10560	7.500	45.5	45.6	25.5	25.5								
SCPT24-LGE-BH205	24-05-27159_SP205	15	8220	12.500	66.3	66.3	38.4	38.4								
SCPT24-LGE-BH205	24-05-27159_SP205	15	9120	17.500	78.5	79.1	38.2	38.2		14.3	3.2	63	4994	100	0.1	4
SCPT24-LGE-BH205	24-05-27159_SP205	15	5820	22.500	75.2	75.2	23.3	23.3		19.3	3.2	93	581	100	1.2	4
SCPT24-LGE-BH205	24-05-27159_SP205	15	820	26.725	39.7	39.7	23.5	23.5	23.5		3.2	100	6	100	127.4	
SCPT24-TMF-MW03AB	24-05-27159_SPTMF03AB	15	250	1.025	-3.9	-0.1	-3.9	-0.1	0.0							
SCPT24-TMF-MW03AB	24-05-27159_SPTMF03AB	15	213	2.000	-2.8	-1.1	-6.7	-1.1								
SCPT24-TMF-MW03AB	24-05-27159_SPTMF03AB	15	2280	2.425	-0.7	1.2	-6.6	1.2	1.2		1.2					
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	205	1.150	-0.2	1.3	-4.5	1.2	1.2		-0.1					
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	16140	7.500	35.7	35.7	20.3	20.3		7.6	-0.1	55	12138	100	0.1	4
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	660	7.950	38.6	38.6	34.2	34.2								
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	300	8.175	35.7	38.0	34.6	35.1								
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	14160	12.500	54.4	54.7	30.1	30.1		12.6	-0.1	59	9156	100	0.1	4
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	315	15.125	67.0	68.5	61.8	61.8								
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	6420	17.500	75.3	75.3	41.3	41.3								6
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	337	17.500	75.3	20.0	19.9	19.9	19.9		-2.4					6
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	325	18.125	72.2	72.8	63.5	63.6								
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	250	22.125	29.0	52.9	29.0	36.3		21.8	0.3	53	196	100	3.6	4

CONETEC

Job No: 24-05-27159
Client: Canada Nickel Company
Project: Crawford Mine - SRK
Start Date: 2024-02-14
End Date: 2024-03-22

CPTu PORE PRESSURE DISSIPATION SUMMARY

Sounding ID	File Name	Cone Area (cm^2)	Duration (s)	Test Depth (m)	$U_{initial}$ (m)	U_{max} (m)	U_{min} (m)	U_{final} (m)	Equilibrium Pore Pressure U_{eq} (m)	Estimated Equilibrium Pore Pressure U_{eq} (m)	Calculated Phreatic Surface (m)	Percent Dissipation (%)	t_{50} $(s)_1$	Assumed Rigidity Index (I_r)	c_h $(cm^2/min)_2$	Refer to Notation Number
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	900	22.500	36.9	64.3	32.5	32.5		22.2	0.3	76	329	100	2.1	4
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	600	27.500	61.5	73.7	36.0	36.0		27.2	0.3	81	161	100	4.4	4
SCPT24-TMF-MW08AB	24-05-27159_SPTMF08AB	15	300	34.125	42.2	42.2	33.5	33.8	33.8		0.3					
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	290	1.050	-2.1	2.3	-4.9	2.1								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	215	3.050	29.7	29.7	23.2	27.5								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	15240	7.500	38.5	38.5	21.3	21.3								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	380	9.050	44.2	44.2	37.7	39.5								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	11460	12.500	55.6	57.0	30.8	30.8								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	220	13.050	55.7	57.9	54.5	54.5								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	4380	17.500	65.2	67.7	33.8	33.8								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	205	21.050	6.2	49.7	6.2	42.8								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	295	24.050	34.5	43.2	25.8	25.8								
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	205	25.050	31.3	35.3	26.3	26.3	26.3		-1.3					
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	225	27.050	45.5	45.7	28.5	28.5	28.5		-1.5					
SCPT24-TMF-BH202	24-05-27159_SPTMF202	15	285	29.025	53.7	62.8	1.3	60.3								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	300	1.075	2.8	3.6	1.9	2.5								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	250	3.150	21.6	40.3	19.4	40.3								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	250	4.150	42.8	42.8	36.7	39.3								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	19320	7.500	40.2	40.2	19.5	19.5		8.3	-0.8	65	8172	100	0.1	4
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	690	8.250	40.3	40.4	34.4	34.4								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	640	8.750	42.3	42.3	36.2	36.3								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	230	10.125	48.8	48.8	44.7	44.7								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	11820	12.500	52.9	55.9	29.1	29.1		13.3	-0.8	63	6215	100	0.1	4
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	275	16.125	64.5	65.6	56.1	56.2								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	7260	17.500	74.1	74.1	36.6	36.6		18.3	-0.8	67	3122	100	0.2	4
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	380	18.125	72.5	73.5	63.1	63.1								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	900	22.500	27.5	48.0	26.1	28.2								
SCPT24-TMF-BH207	24-05-27159_SPTMF207	15	2640	24.175	23.5	26.8	8.8	25.0	25.0		-0.8					
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	230	3.000	-3.0	0.0	-3.2	0.0								
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	195	5.000	8.8	20.6	8.7	20.6								
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	1180	6.000	31.6	39.2	29.3	38.7								
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	175	7.000	53.6	53.6	40.4	47.0								
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	210	7.500	0.6	0.6	-1.7	-1.7								
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	27000	9.225	30.3	50.4	28.8	28.8								
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	9840	12.500	63.8	64.3	34.4	34.4		5.5	7.0	51	9451	100	0.1	4
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	5640	17.500	80.7	80.7	38.8	38.8		10.5	7.0	60	3814	100	0.2	4
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	600	22.500	82.3	82.3	15.5	15.5	15.5		7.0	100	7	100	105.0	

Job No:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford Mine - SRK
Start Date:	2024-02-14
End Date:	2024-03-22

CPTu PORE PRESSURE DISSIPATION SUMMARY

Sounding ID	File Name	Cone Area (cm^2)	Duration (s)	Test Depth (m)	$U_{initial}$ (m)	U_{max} (m)	U_{min} (m)	U_{final} (m)	Equilibrium Pore Pressure U_{eq} (m)	Estimated Equilibrium Pore Pressure U_{eq} (m)	Calculated Phreatic Surface (m)	Percent Dissipation (%)	t_{50} $(s)_1$	Assumed Rigidity Index (I_r)	c_h $(cm^2/min)_2$	Refer to Notation Number
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	680	22.800	78.6	78.6	16.2	16.2		15.8	7.0	99	8	100	83.7	4
SCPT24-WRD-BH201	24-05-27159_SPWRD201	15	110	23.125	14.6	17.3	14.6	15.9	15.9		7.2					
SCPT24-WRD-BH202	24-05-27159_SPWRD202	15	1060	1.000	-1.6	1.1	-1.6	1.1	1.1		-0.1					
SCPT24-WRD-BH202	24-05-27159_SPWRD202	15	24720	7.500	41.0	42.2	21.4	21.4		7.6	-0.1	60	13839	100	0.1	4
SCPT24-WRD-BH202	24-05-27159_SPWRD202	15	8640	12.500	56.5	56.5	29.3	29.3		12.6	-0.1	62	4967	100	0.1	4
SCPT24-WRD-BH202	24-05-27159_SPWRD202	15	5340	17.500	55.0	58.9	20.2	20.2		17.6	-0.1	94	929	100	0.8	4
SCPT24-WRD-BH202	24-05-27159_SPWRD202	15	205	18.950	46.3	46.3	15.1	37.9								
SCPT24-WRD-BH205	24-05-27159_SPWRD205	15	225	4.000	-1.6	5.4	-3.3	4.5	4.5		-0.5					
SCPT24-WRD-BH205	24-05-27159_SPWRD205	15	14940	7.525	50.3	56.1	28.3	28.3		8.0	-0.5	58	9960	100	0.1	4
SCPT24-WRD-BH205	24-05-27159_SPWRD205	15	820	7.725	-1.0	12.9	-9.2	12.9								
SCPT24-WRD-BH205B	24-05-27159_SPWRD205B	15	190	3.000	2.2	3.1	2.2	2.7								
SCPT24-WRD-BH205B	24-05-27159_SPWRD205B	15	720	5.000	7.3	18.4	-1.1	5.5	5.5		-0.5					
SCPT24-WRD-BH205B	24-05-27159_SPWRD205B	15	420	7.650	38.5	40.8	1.0	40.4								
CPT24-WRD-BH207	24-05-27159_CPWRD207	15	9060	5.000	49.2	55.4	15.2	15.5		4.6	0.4	79	3024	100	0.2	3
SCPT24-WRD-BH207	24-05-27159_SPWRD207	15	555	1.000	0.2	0.9	-1.3	0.6	0.6		0.4					
SCPT24-WRD-BH207	24-05-27159_SPWRD207	15	400	6.250	-2.1	-1.5	-9.5	-1.5								
SCPT24-WRD-BH212	24-05-27159_SPWRD212	15	320	1.000	0.6	2.0	0.2	1.2								
SCPT24-WRD-BH212	24-05-27159_SPWRD212	15	190	5.000	39.5	39.5	31.9	35.0								
SCPT24-WRD-BH212	24-05-27159_SPWRD212	15	11460	7.500	50.2	50.2	25.5	25.5		4.8	2.7	54	8598	100	0.1	4
SCPT24-WRD-BH212	24-05-27159_SPWRD212	15	8400	12.575	67.6	67.6	21.4	21.4		9.9	2.7	80	2064	100	0.3	4
SCPT24-WRD-BH212	24-05-27159_SPWRD212	15	375	15.000	0.6	31.2	-3.1	12.3	12.3		2.7					

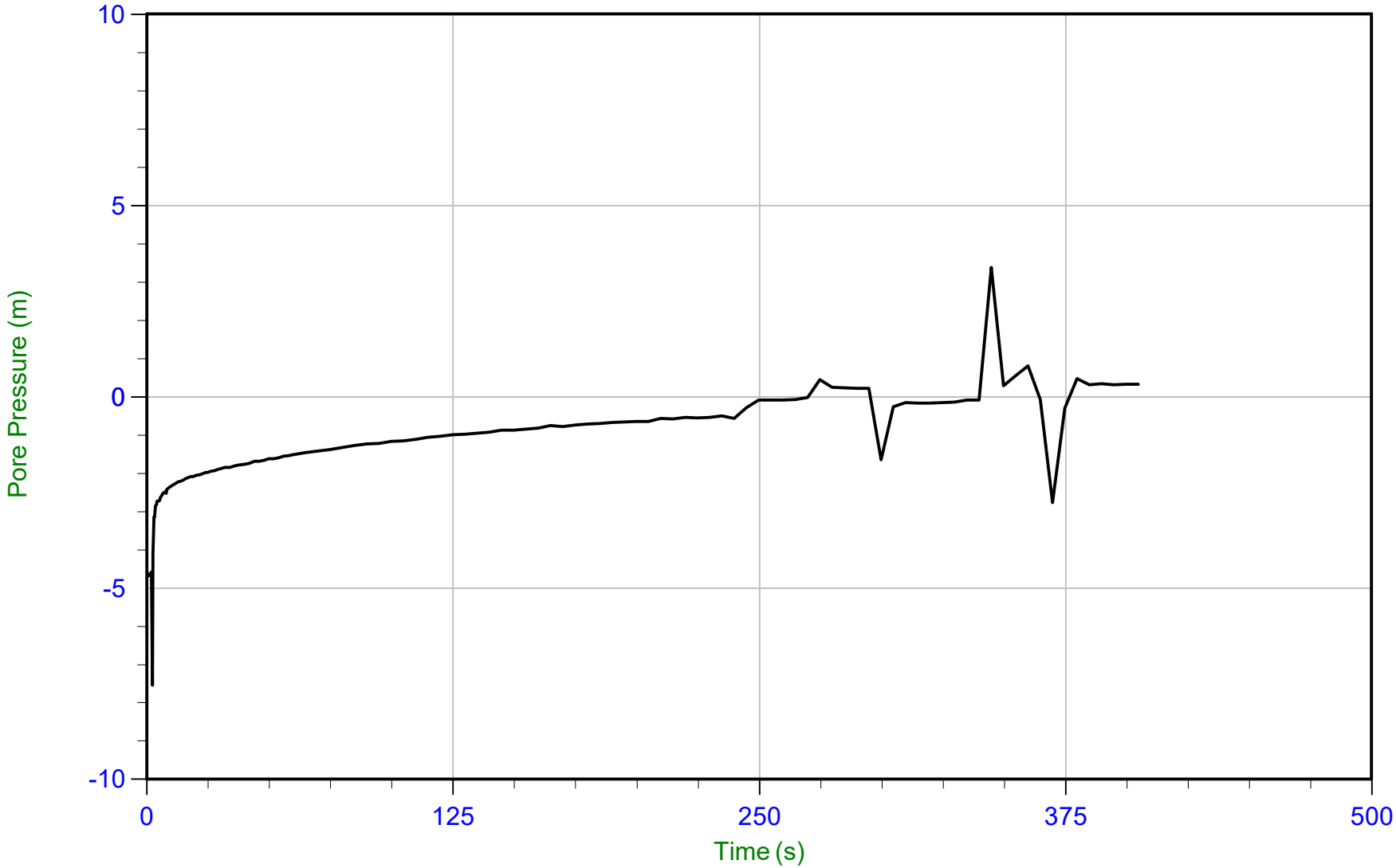
1. Time for 50 percent dissipation based on U_{max}, U_{min}, and the applied U_{eq}. Note the time is relative to where U_{max} occurred.
2. Teh and Houlsby, 1991.
3. Equilibrium pore pressure estimated based on a hydrostatic assumption from the assumed phreatic surface.
4. Equilibrium pore pressure estimated based on the nearest pore pressure dissipation test that reached equilibrium.
5. The cone was left downhole over night on 2024-02-18. The PPD was completed at the same depth on the morning of 2024-02-19.
6. The cone was left downhole over night on 2024-03-20. The PPD was completed at the same depth on the morning of 2024-03-21.

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 1.000 m / 3.281 ft
Duration: 405.0 s

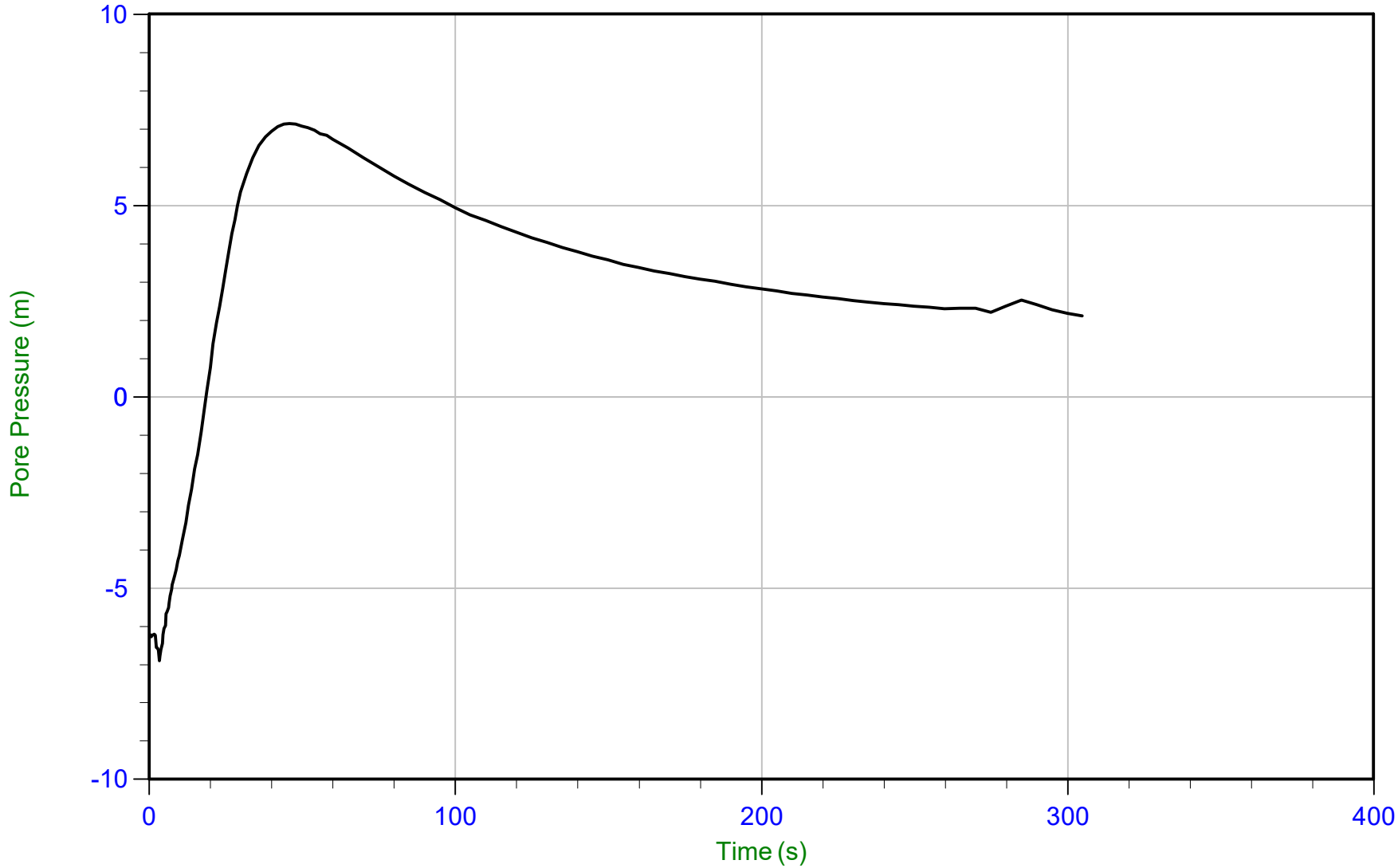
u Min: -7.5 m
u Max: 3.4 m
u Final: 0.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 2.000 m / 6.562 ft
Duration: 305.0 s

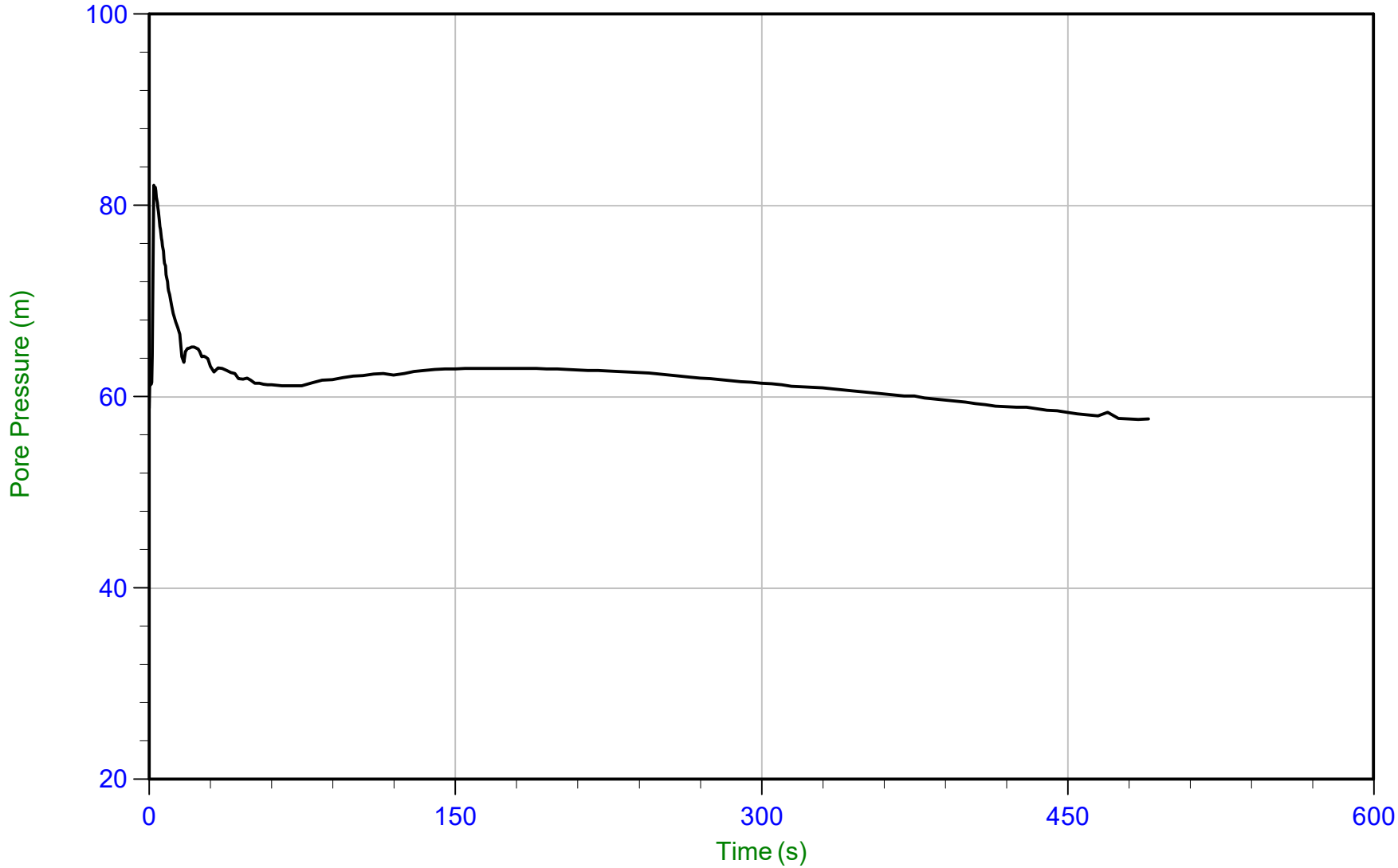
u Min: -6.9 m
u Max: 7.1 m
u Final: 2.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 3.000 m / 9.842 ft
Duration: 490.0 s

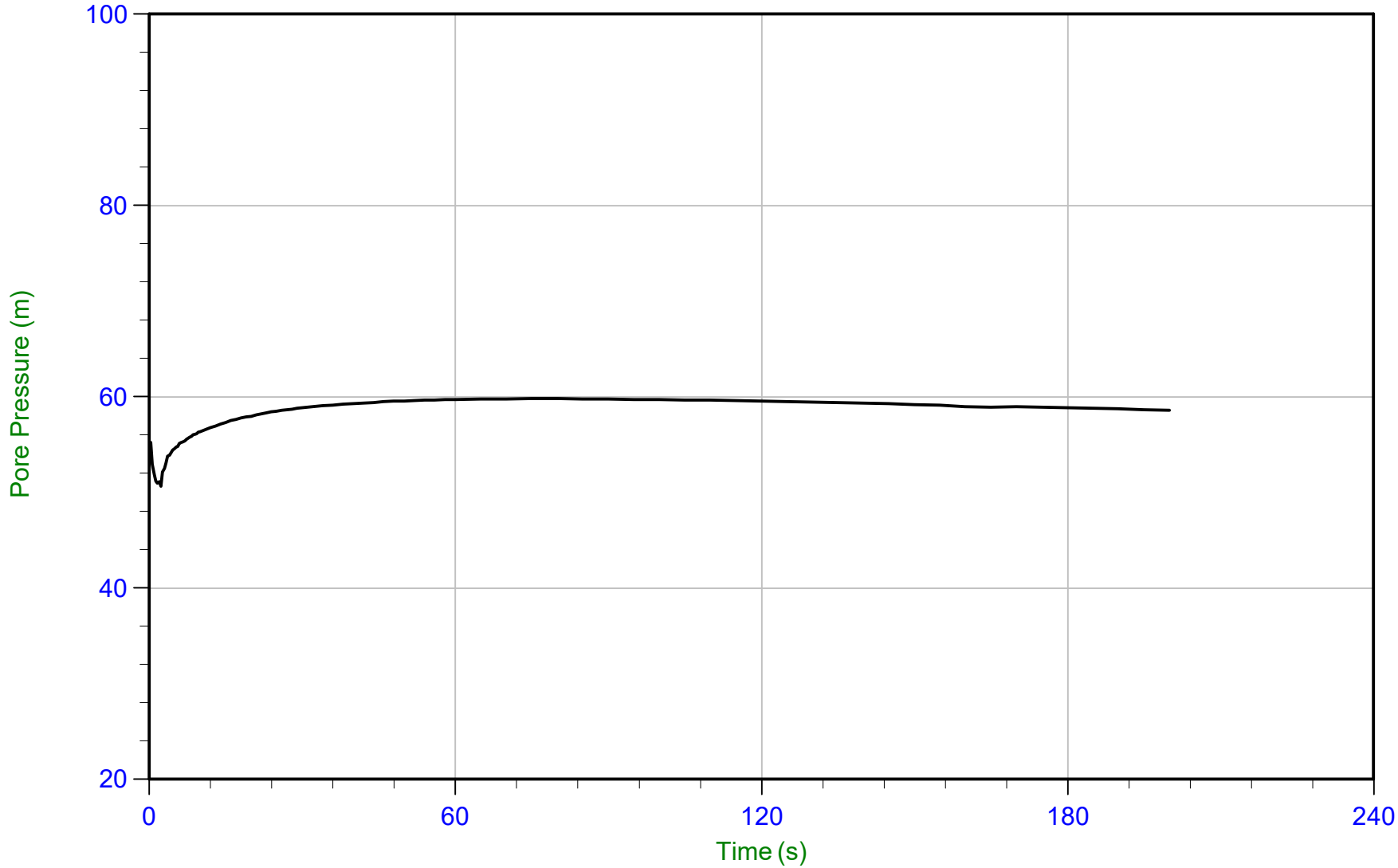
u Min: 57.6 m
u Max: 82.1 m
u Final: 57.7 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 4.000 m / 13.123 ft
Duration: 200.0 s

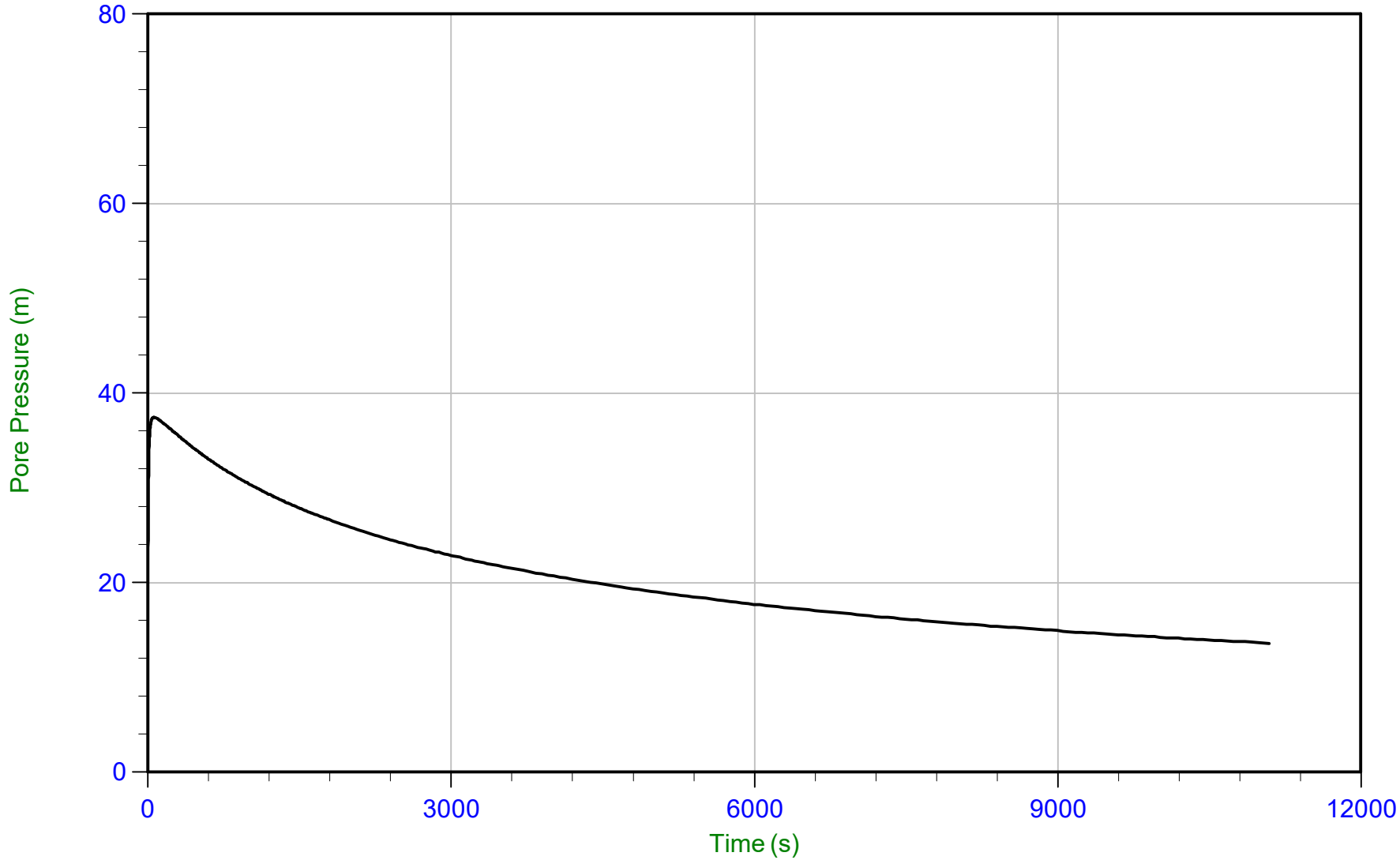
u Min: 50.6 m
u Max: 59.8 m
u Final: 58.6 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 11100.0 s

u Min: -4.4 m
u Max: 37.4 m
u Final: 13.6 m

WT: 2.9 m / 9.5 ft
Ueq: 4.6 m
U(50): 21.02 m

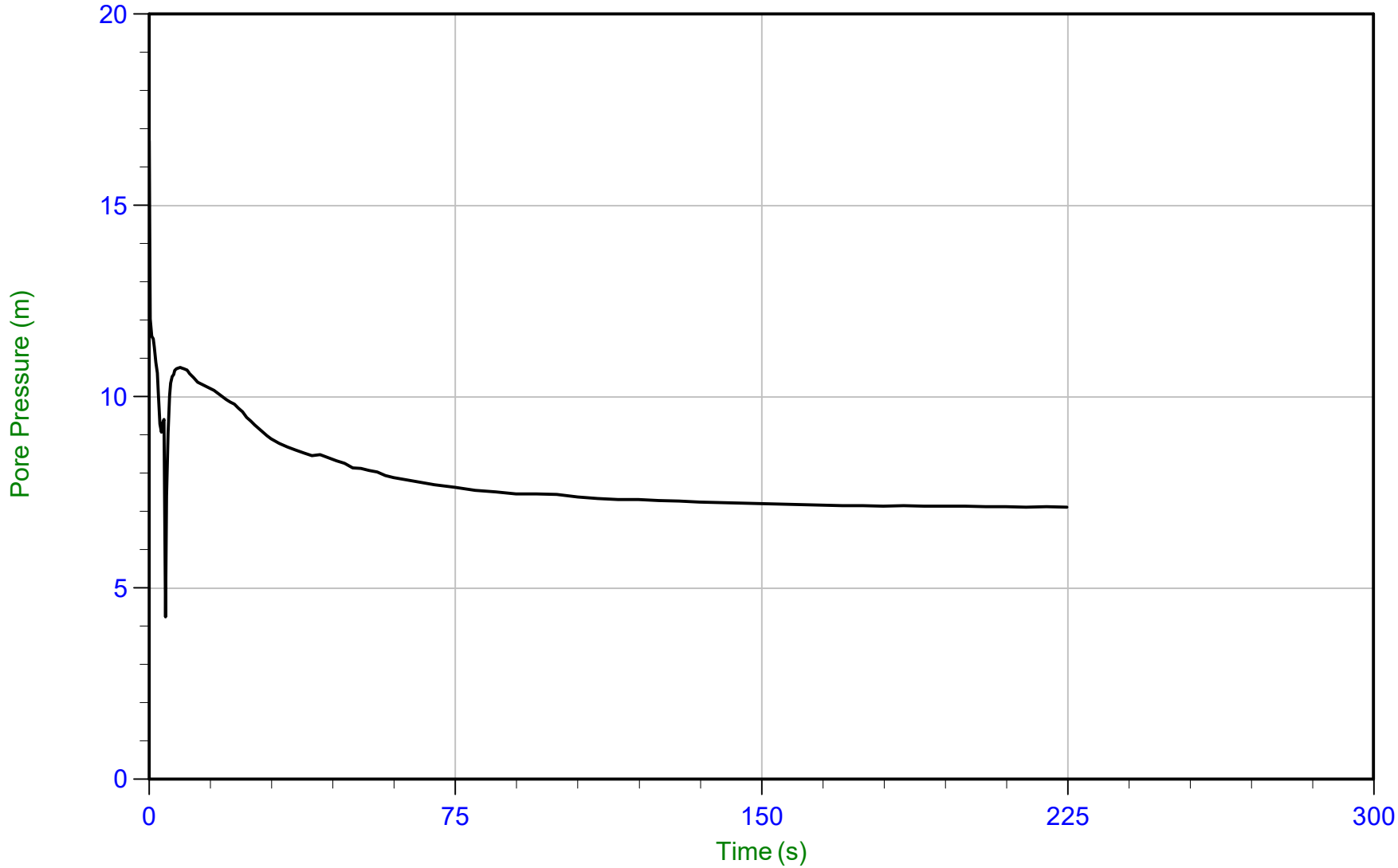
T(50): 3767.9 s
Ir: 100
Ch: 0.2 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 10.000 m / 32.808 ft
Duration: 225.0 s

u Min: 4.2 m
u Max: 16.7 m
u Final: 7.1 m

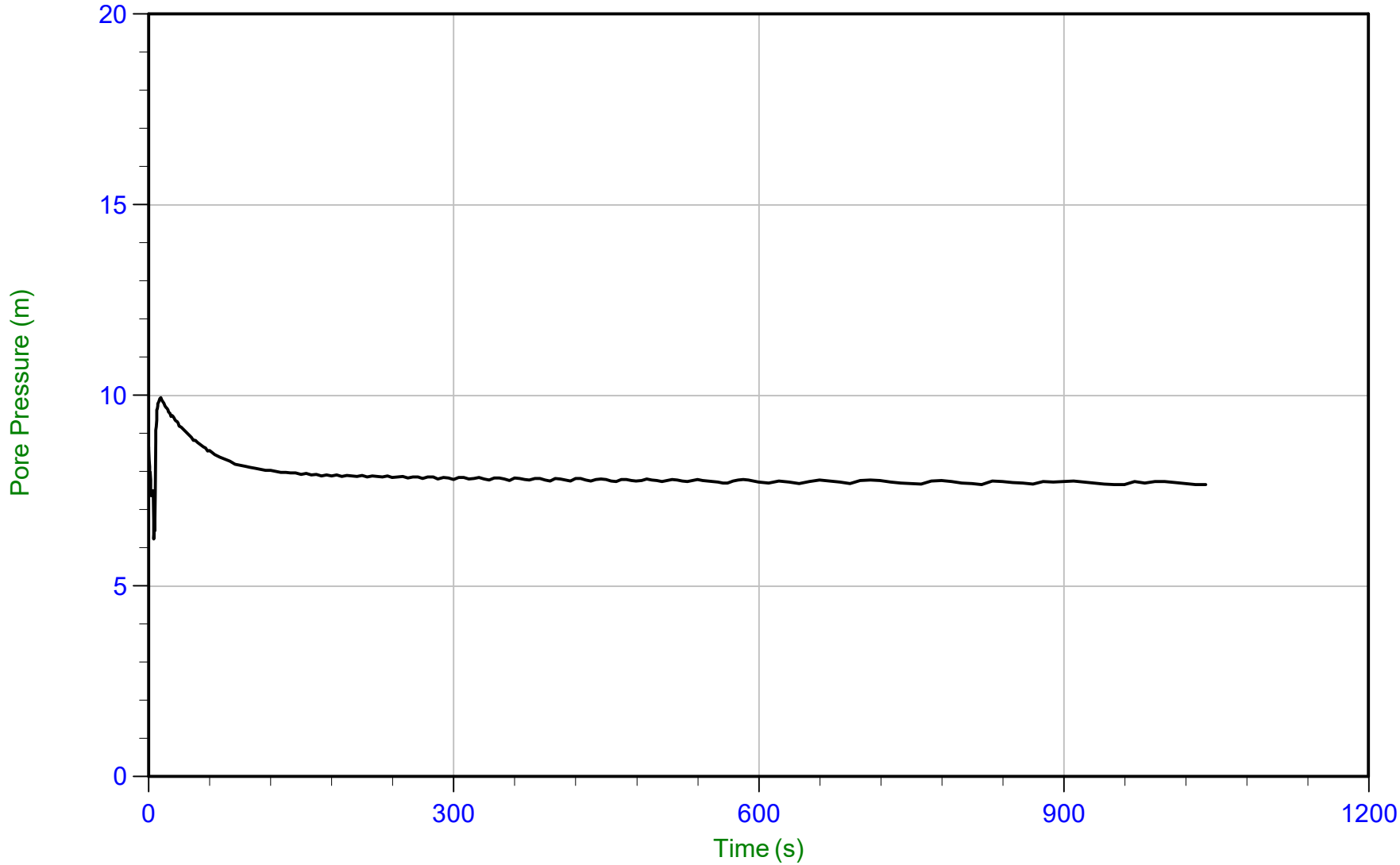
WT: 2.9 m / 9.5 ft
Ueq: 7.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-19 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP201.PPF2
Depth: 10.025 m / 32.890 ft
Duration: 1040.0 s

u Min: 6.2 m
u Max: 9.9 m
u Final: 7.7 m

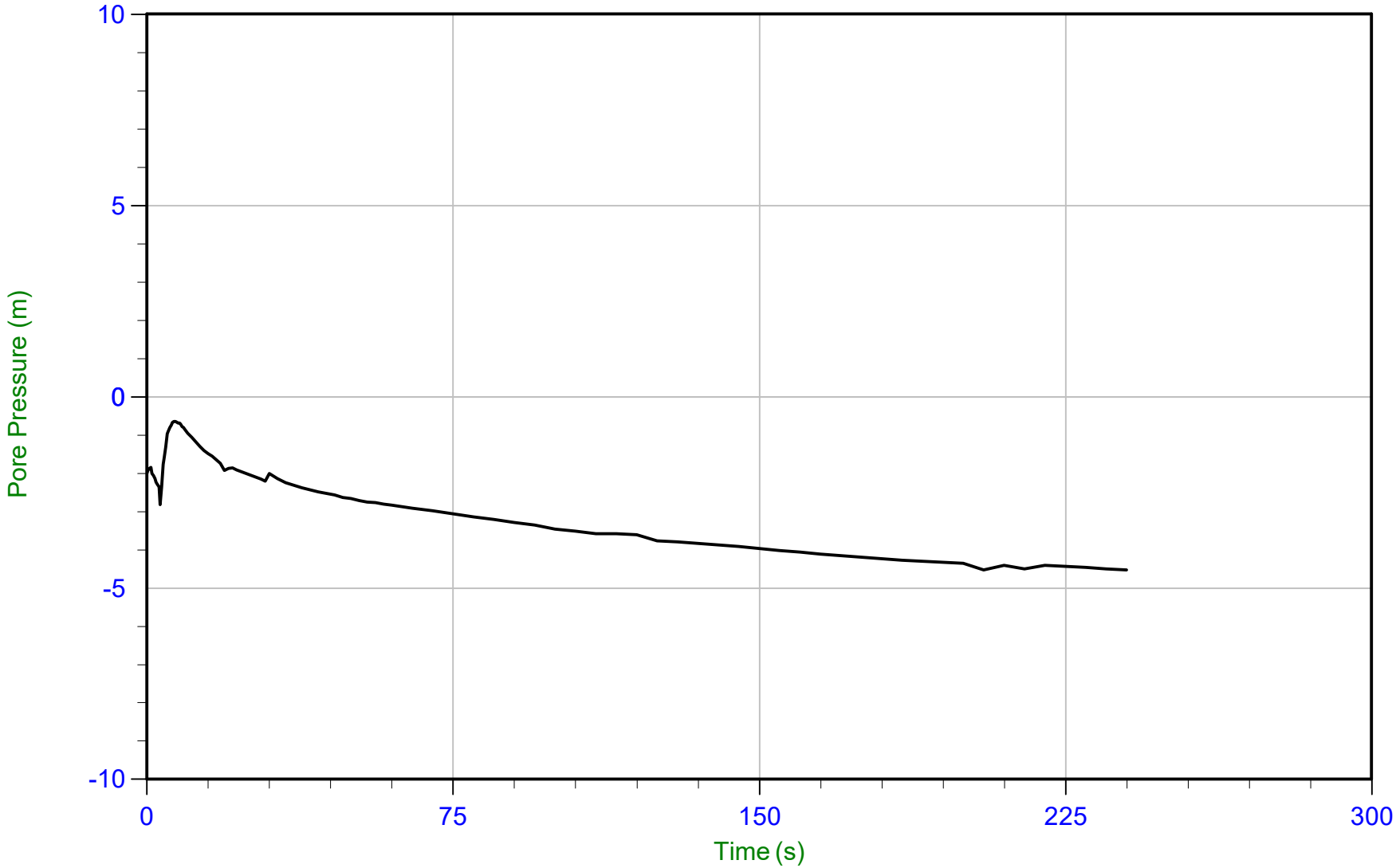
WT: 2.3 m / 7.5 ft
Ueq: 7.7 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-16 14:19
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP202.PPF2
Depth: 4.650 m / 15.256 ft
Duration: 240.0 s

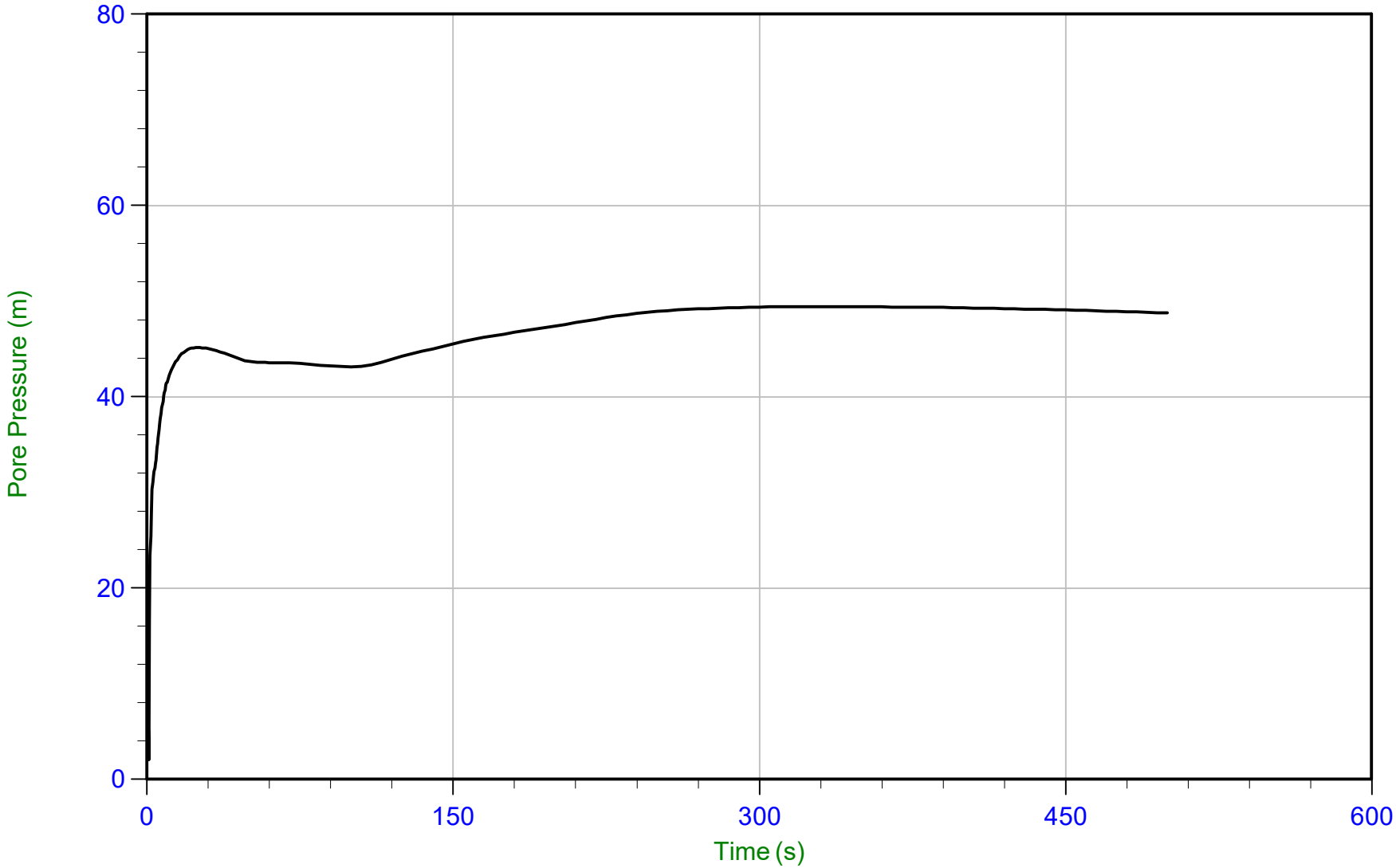
u Min: -4.5 m
u Max: -0.6 m
u Final: -4.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-17 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202B
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP202B.PPF2
Depth: 5.000 m / 16.404 ft
Duration: 500.0 s

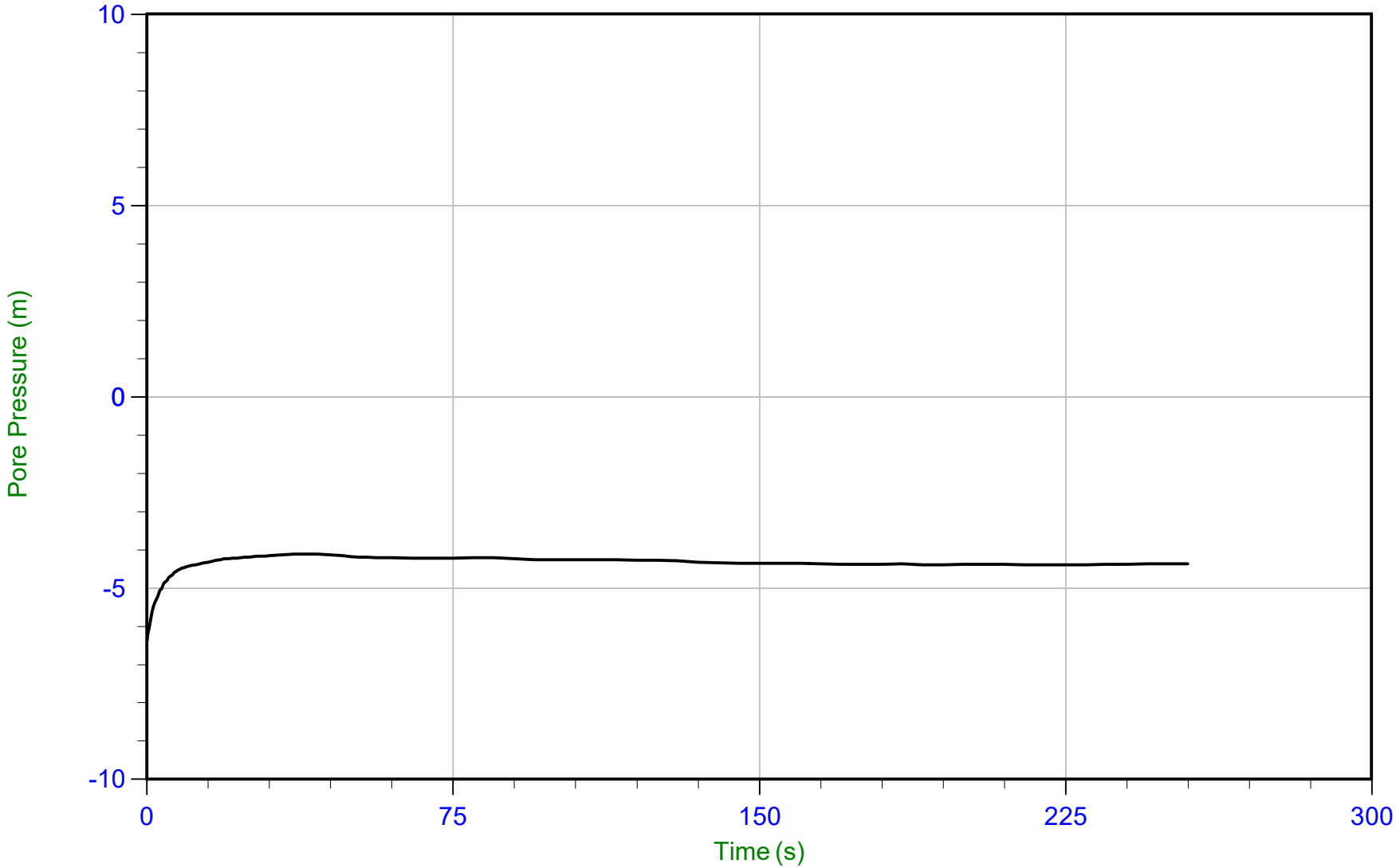
u Min: 2.0 m
u Max: 49.4 m
u Final: 48.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-17 13:05
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH202B
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP202B.PPF2
Depth: 5.250 m / 17.224 ft
Duration: 255.0 s

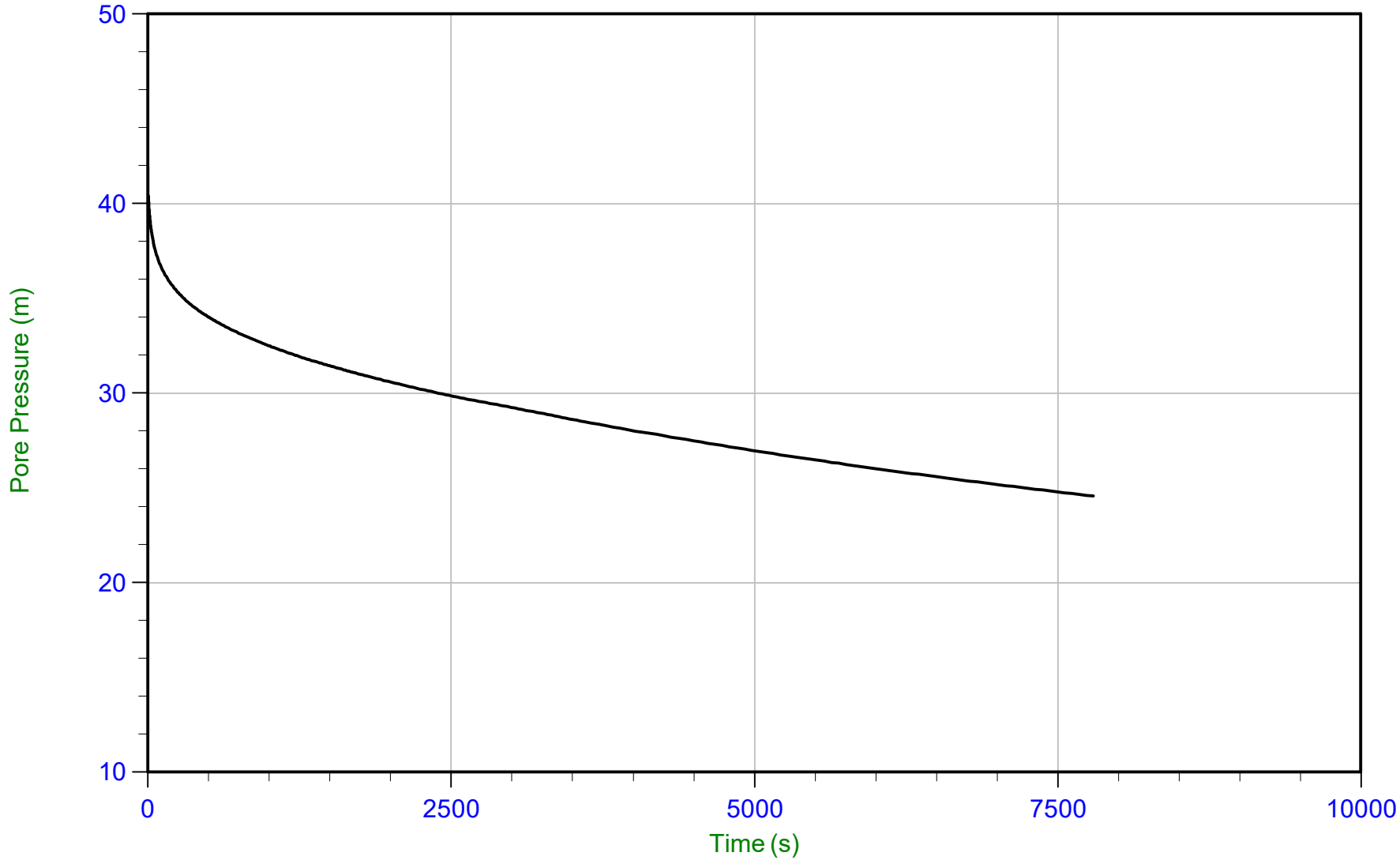
u Min: -6.4 m
u Max: -4.1 m
u Final: -4.4 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP203.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 7800.0 s

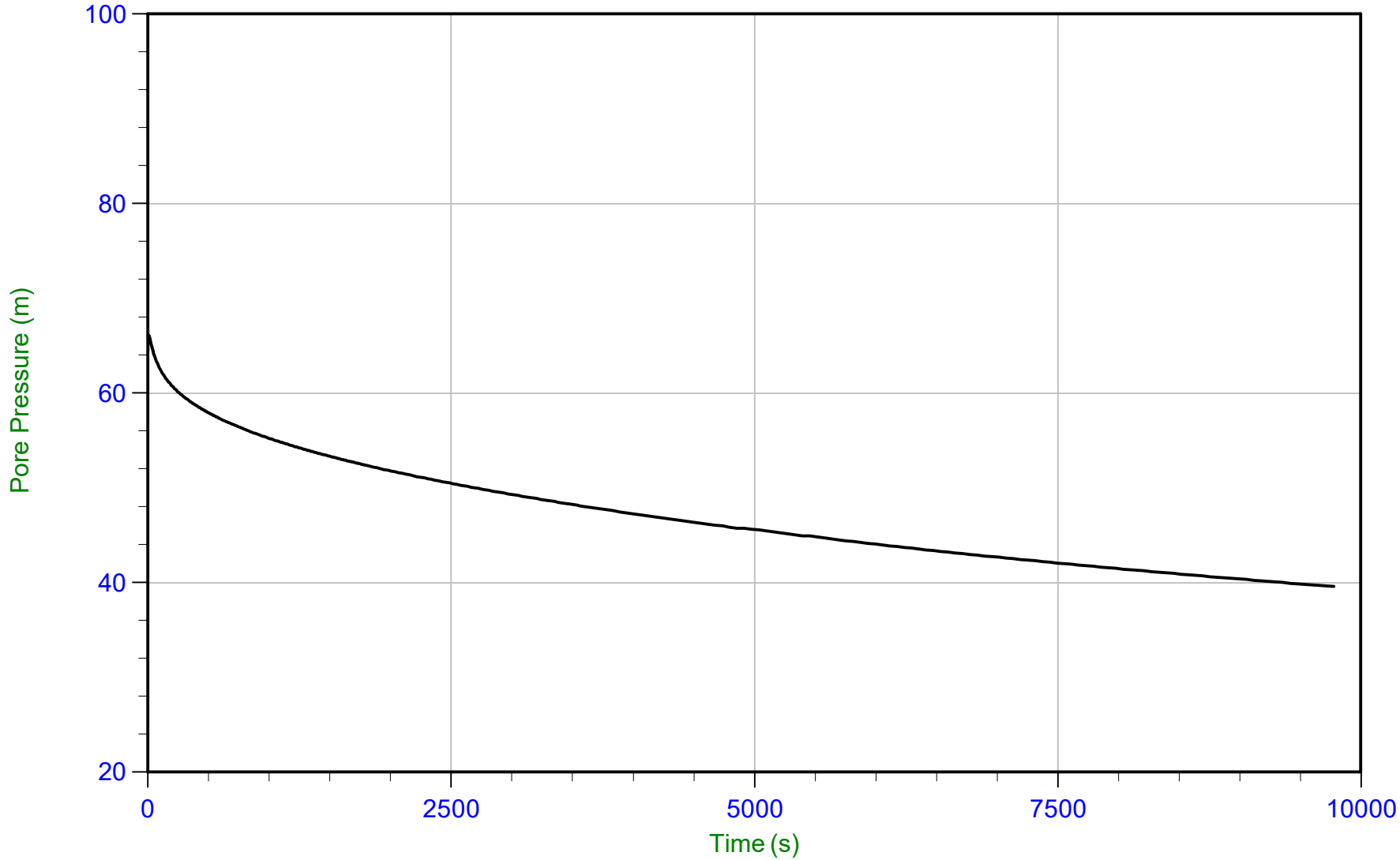
u Min: 24.6 m
u Max: 41.9 m
u Final: 24.6 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP203.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 9780.0 s

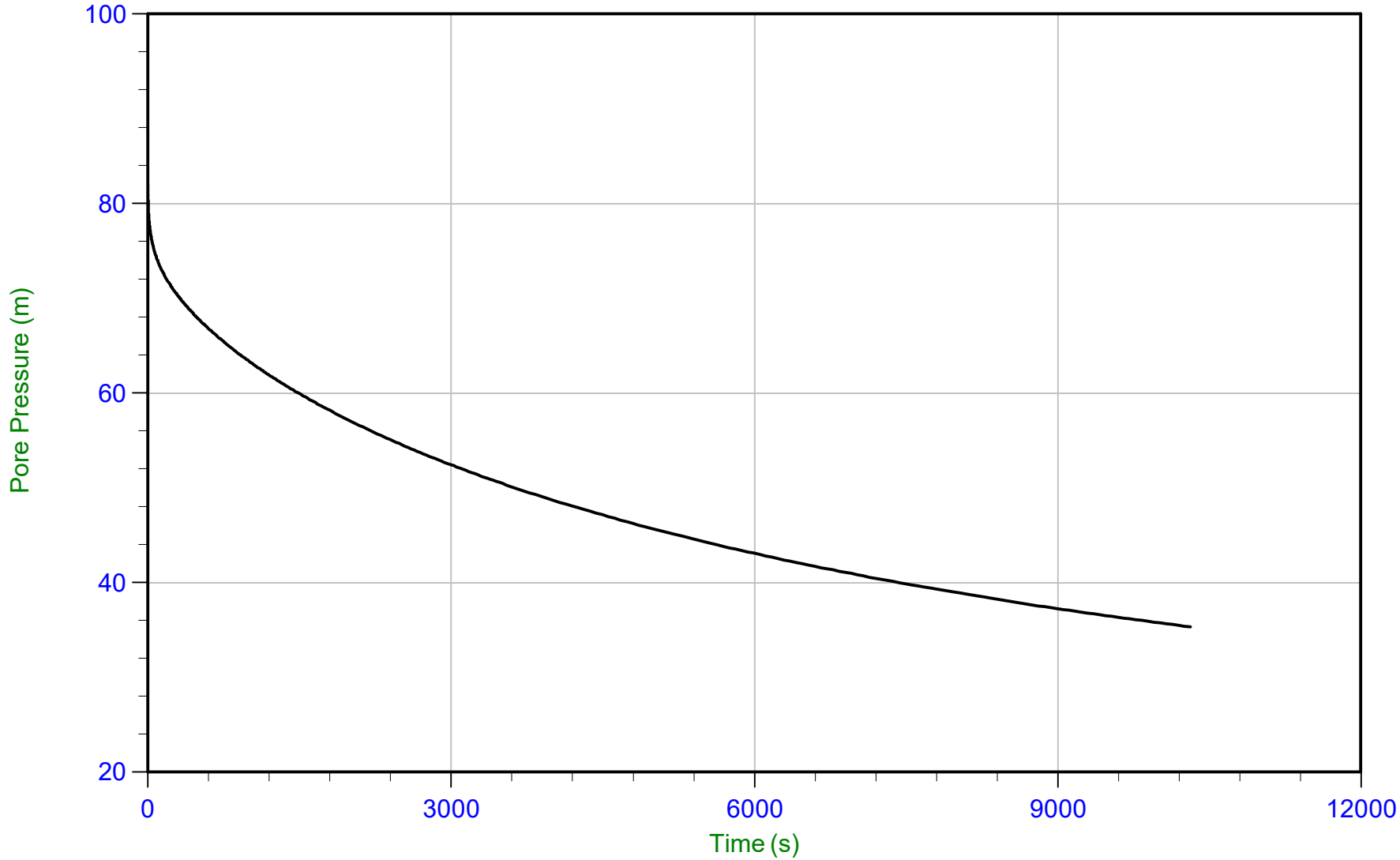
u Min: 39.6 m
u Max: 66.6 m
u Final: 39.6 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP203.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 10320.0 s

u Min: 35.3 m
u Max: 82.0 m
u Final: 35.3 m

WT: 3.2 m / 10.5 ft
Ueq: 14.3 m
U(50): 48.16 m

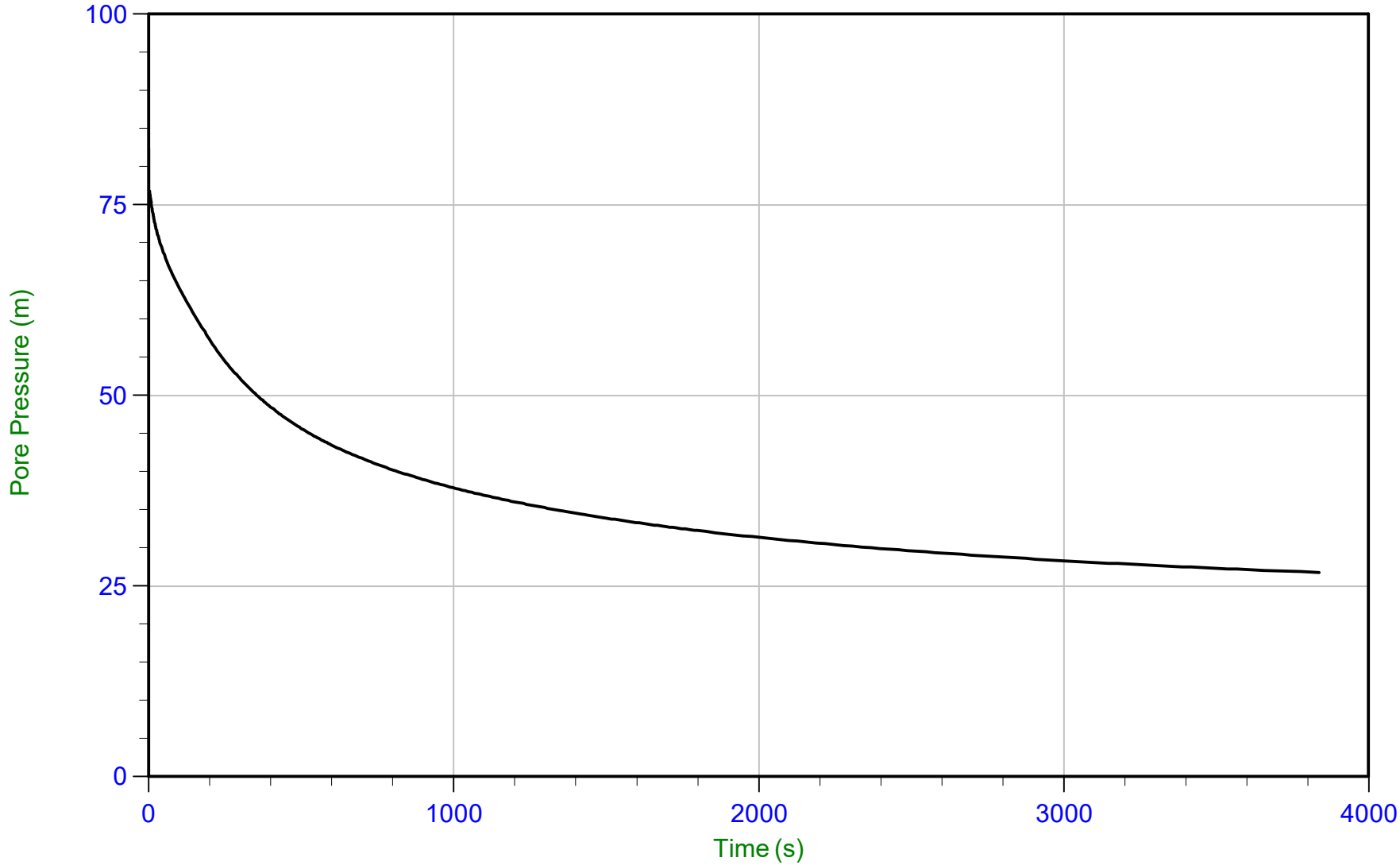
T(50): 4178.5 s
Ir: 100
Ch: 0.2 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP203.PPF2
Depth: 22.500 m / 73.818 ft
Duration: 3840.0 s

u Min: 26.8 m
u Max: 82.4 m
u Final: 26.8 m

WT: 3.2 m / 10.5 ft
Ueq: 19.3 m
U(50): 50.84 m

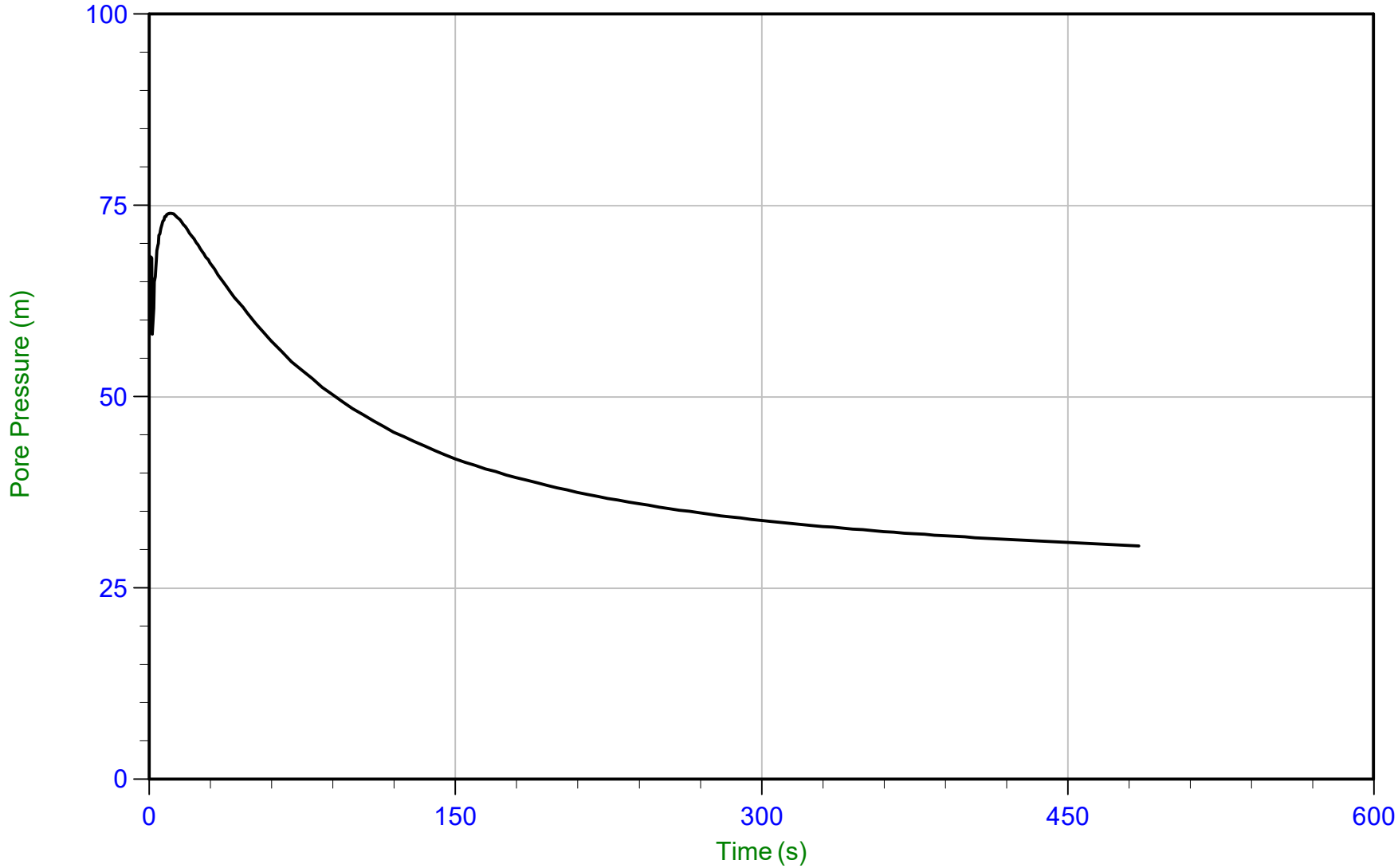
T(50): 334.8 s
Ir: 100
Ch: 2.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-14 14:13
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH203
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP203.PPF2
Depth: 28.175 m / 92.437 ft
Duration: 485.0 s

u Min: 30.5 m
u Max: 74.0 m
u Final: 30.5 m

WT: 3.2 m / 10.5 ft
Ueq: 25.0 m
U(50): 49.48 m

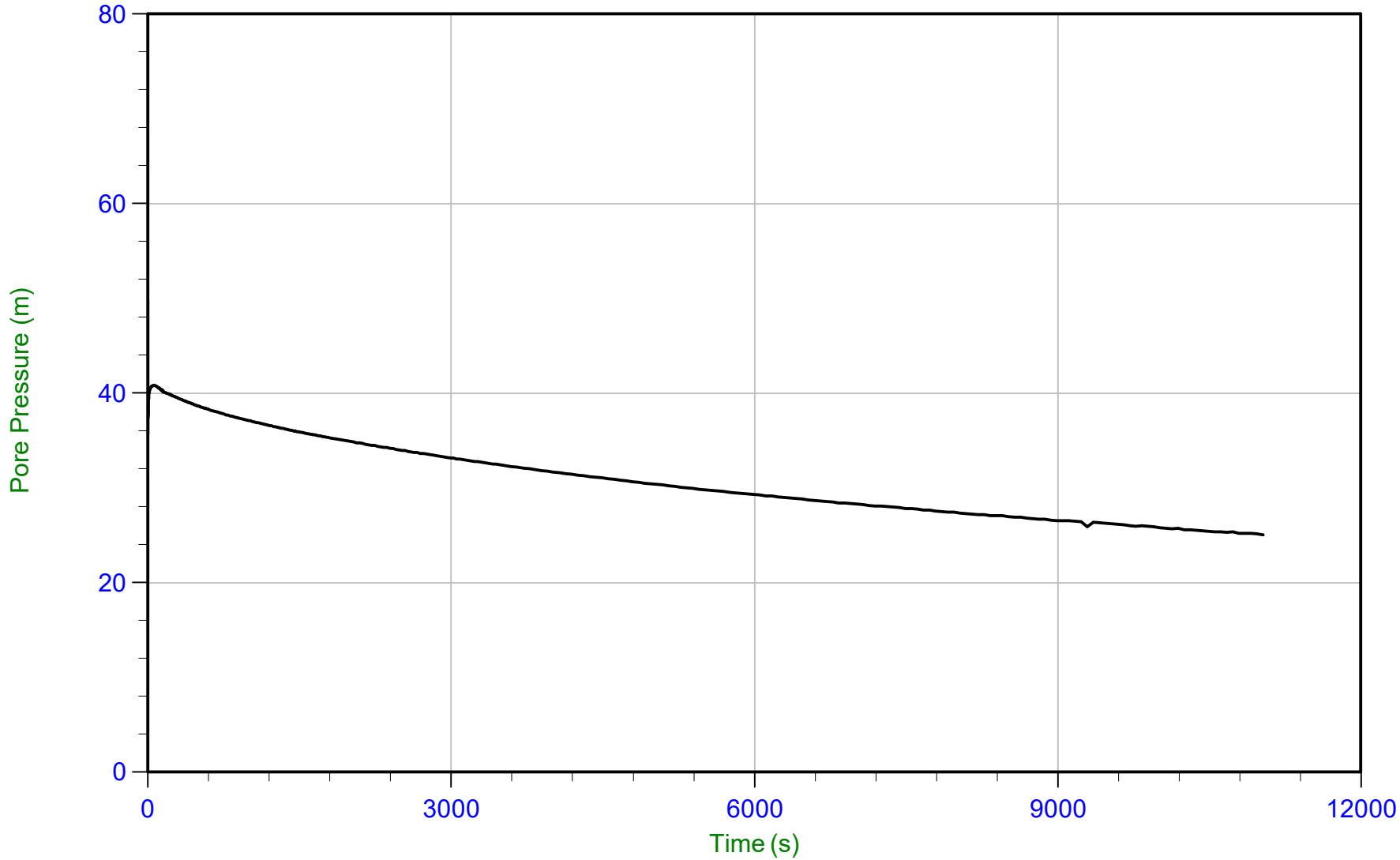
T(50): 83.1 s
Ir: 100
Ch: 8.4 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP204.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 11040.0 s

u Min: 25.1 m
u Max: 49.9 m
u Final: 25.1 m

WT: 2.7 m / 8.9 ft
Ueq: 4.8 m
U(50): 27.35 m

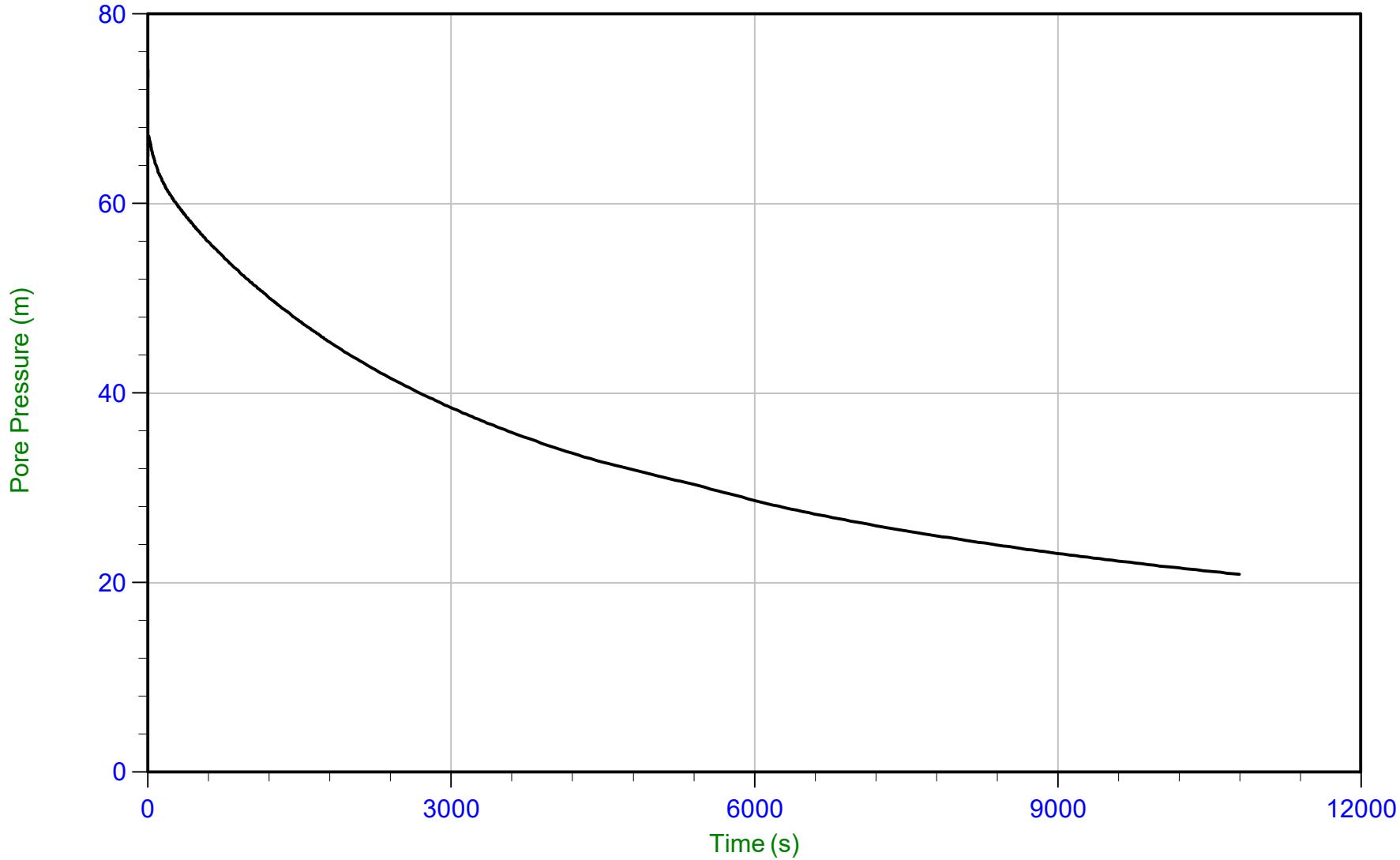
T(50): 8034.8 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP204.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 10800.0 s

u Min: 20.9 m
u Max: 74.2 m
u Final: 20.9 m

WT: 2.7 m / 8.9 ft
Ueq: 9.8 m
U(50): 41.99 m

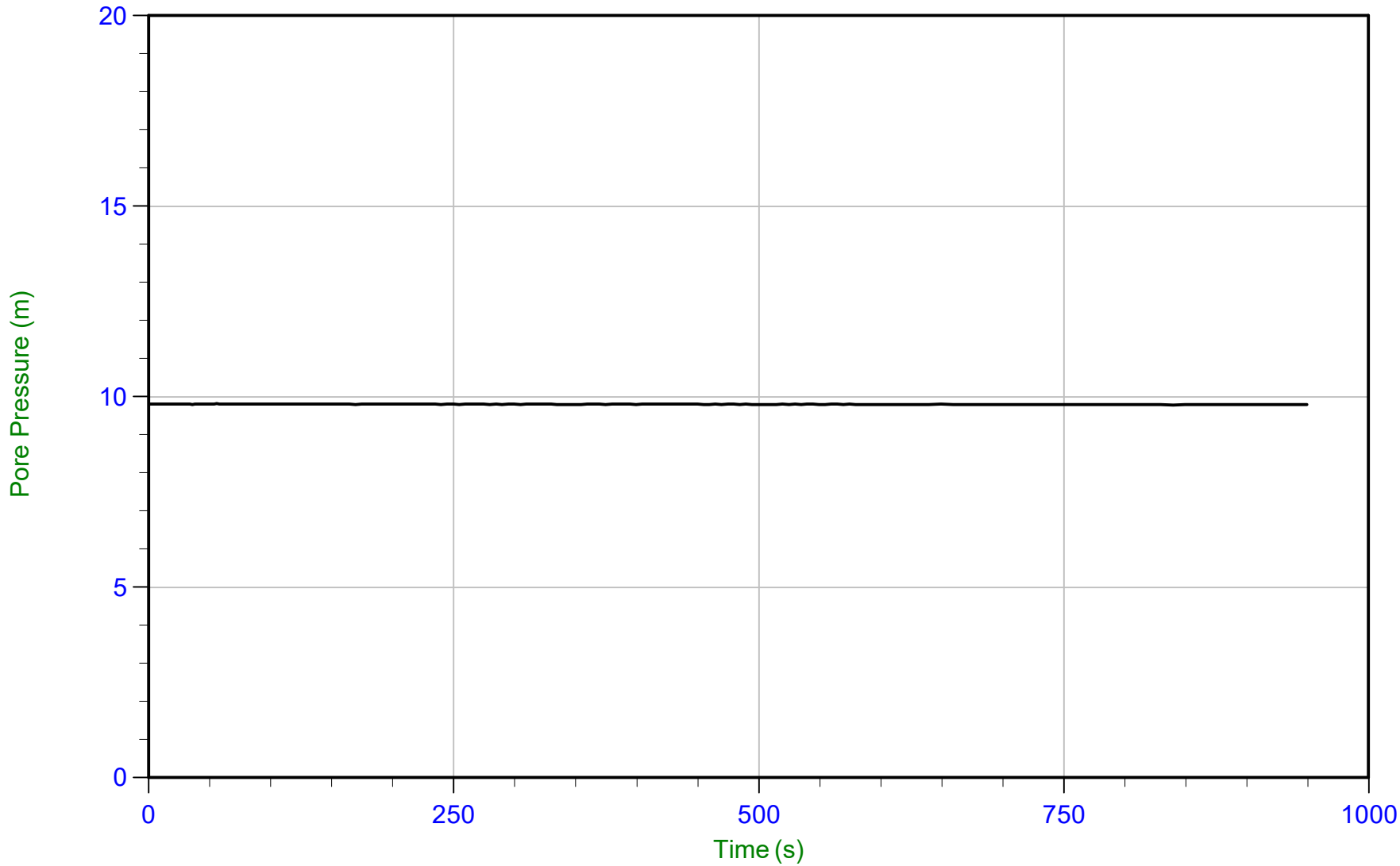
T(50): 2330.4 s
Ir: 100
Ch: 0.3 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP204.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 950.0 s

u Min: 9.8 m
u Max: 9.8 m
u Final: 9.8 m

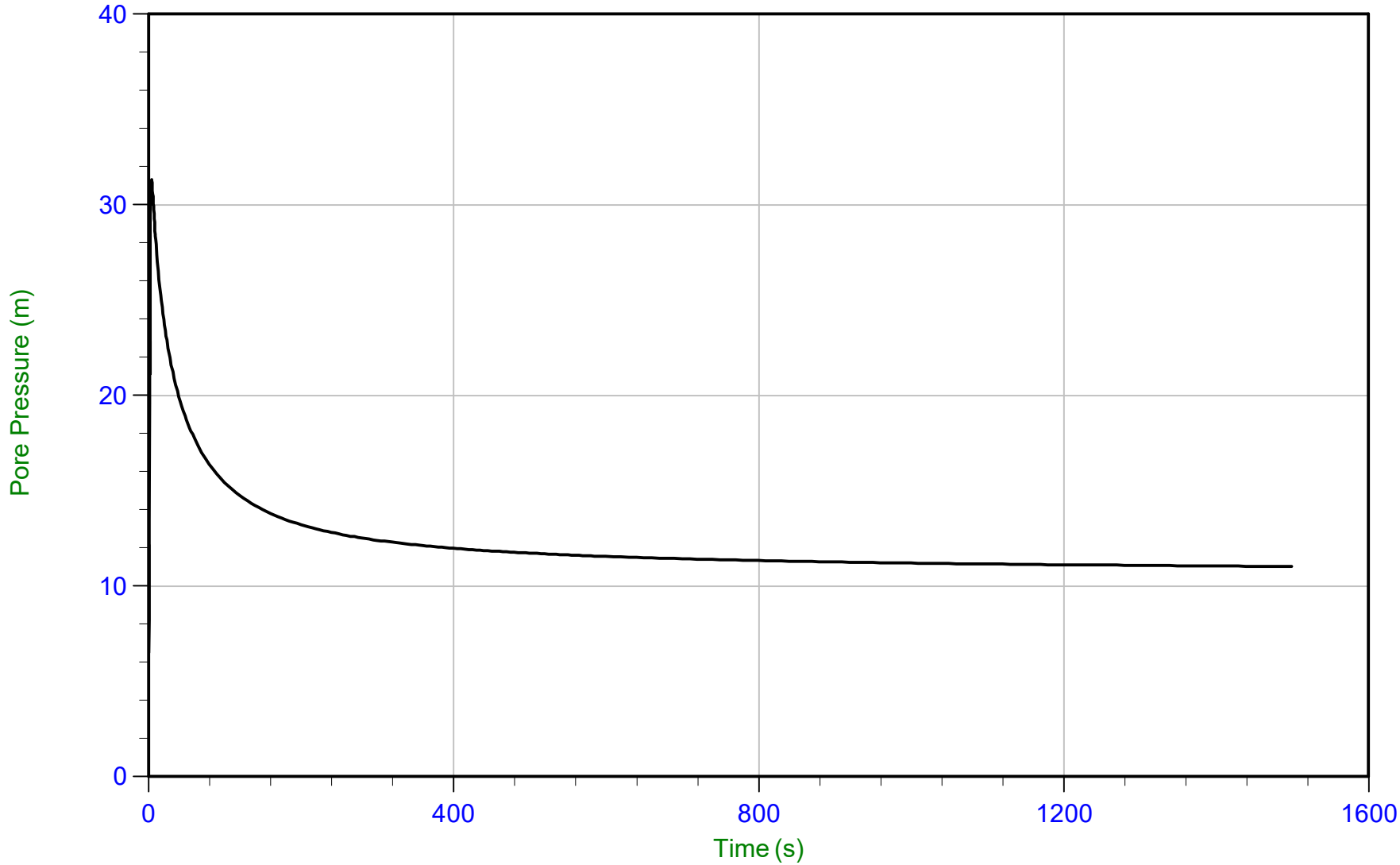
WT: 2.7 m / 8.9 ft
Ueq: 9.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-18 10:33
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH204
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP204.PPF2
Depth: 14.775 m / 48.474 ft
Duration: 1500.0 s

u Min: 6.5 m
u Max: 31.3 m
u Final: 11.0 m

WT: 3.8 m / 12.4 ft
Ueq: 11.0 m
U(50): 21.16 m

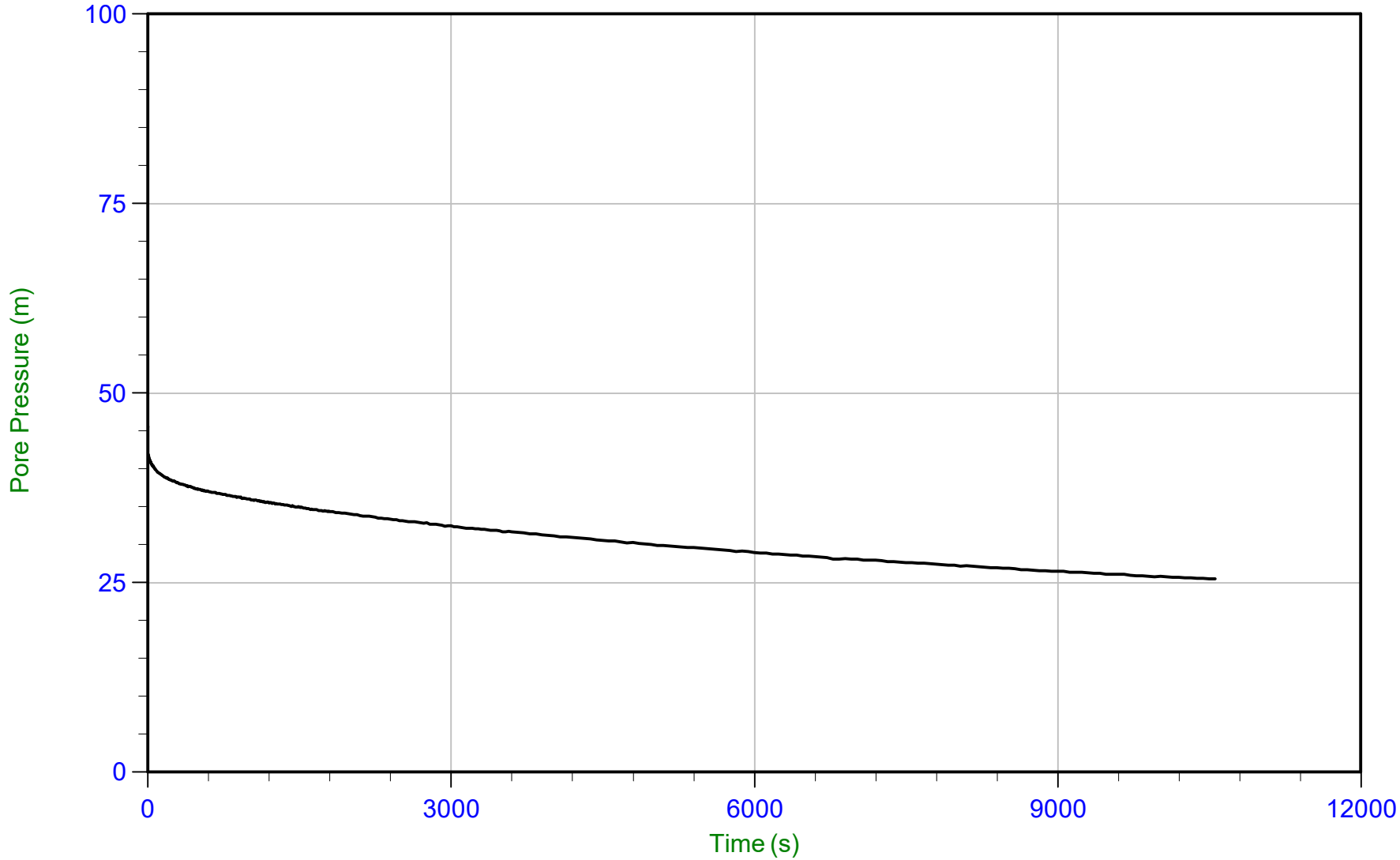
T(50): 28.5 s
Ir: 100
Ch: 24.7 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP205.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 10560.0 s

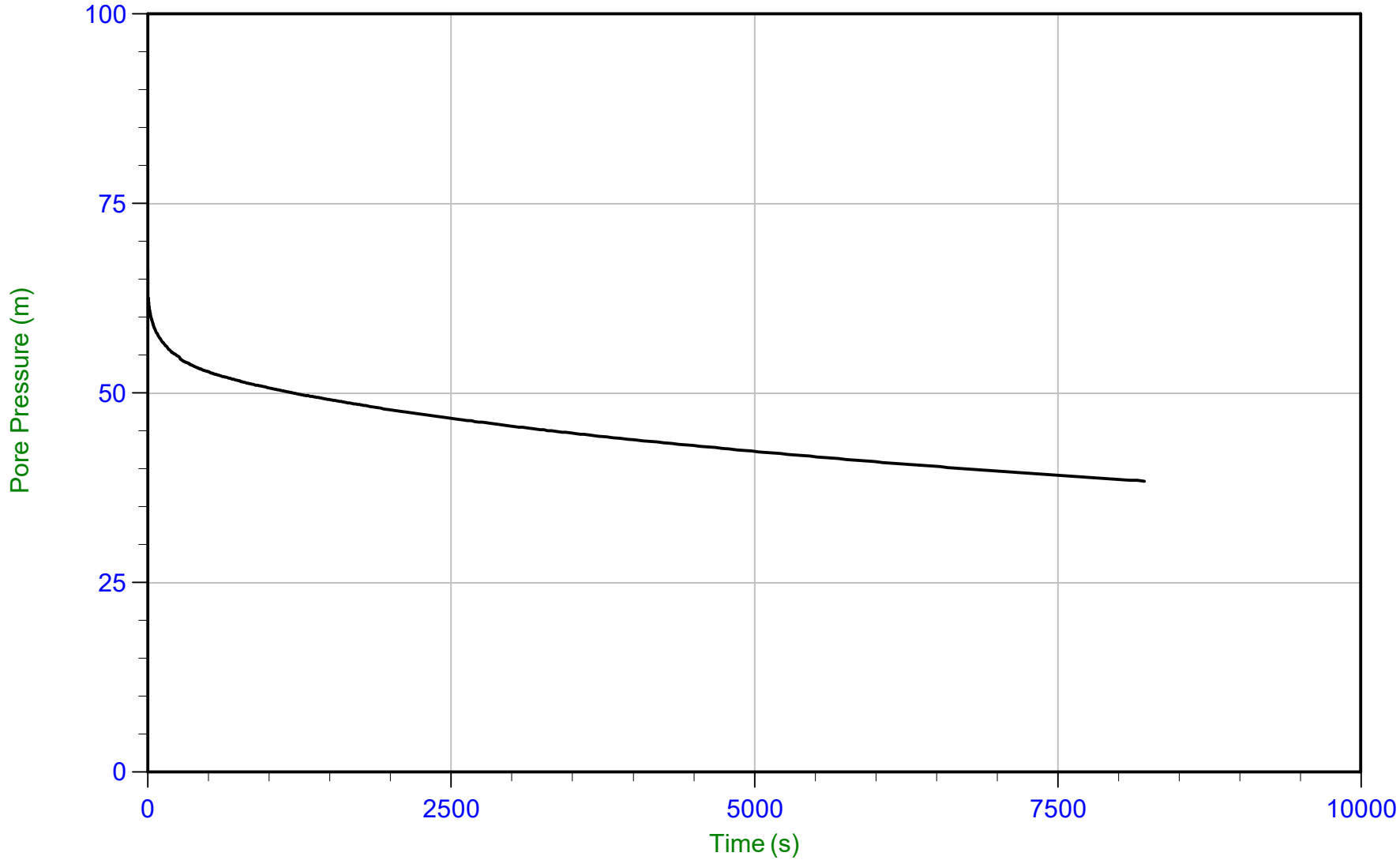
u Min: 25.5 m
u Max: 45.6 m
u Final: 25.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP205.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 8220.0 s

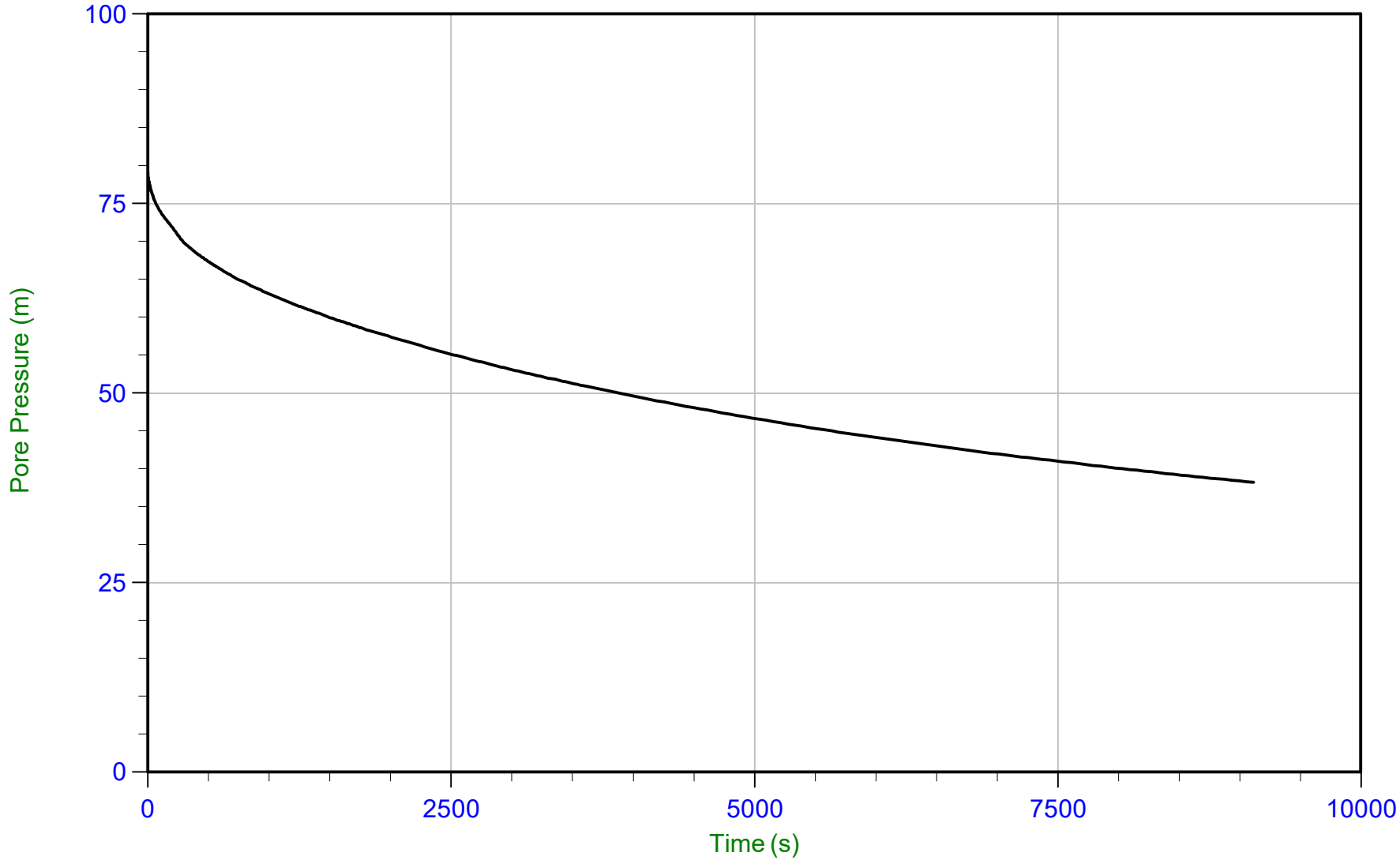
u Min: 38.4 m
u Max: 66.3 m
u Final: 38.4 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP205.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 9120.0 s

u Min: 38.2 m
u Max: 79.1 m
u Final: 38.2 m

WT: 3.2 m / 10.6 ft
Ueq: 14.3 m
U(50): 46.69 m

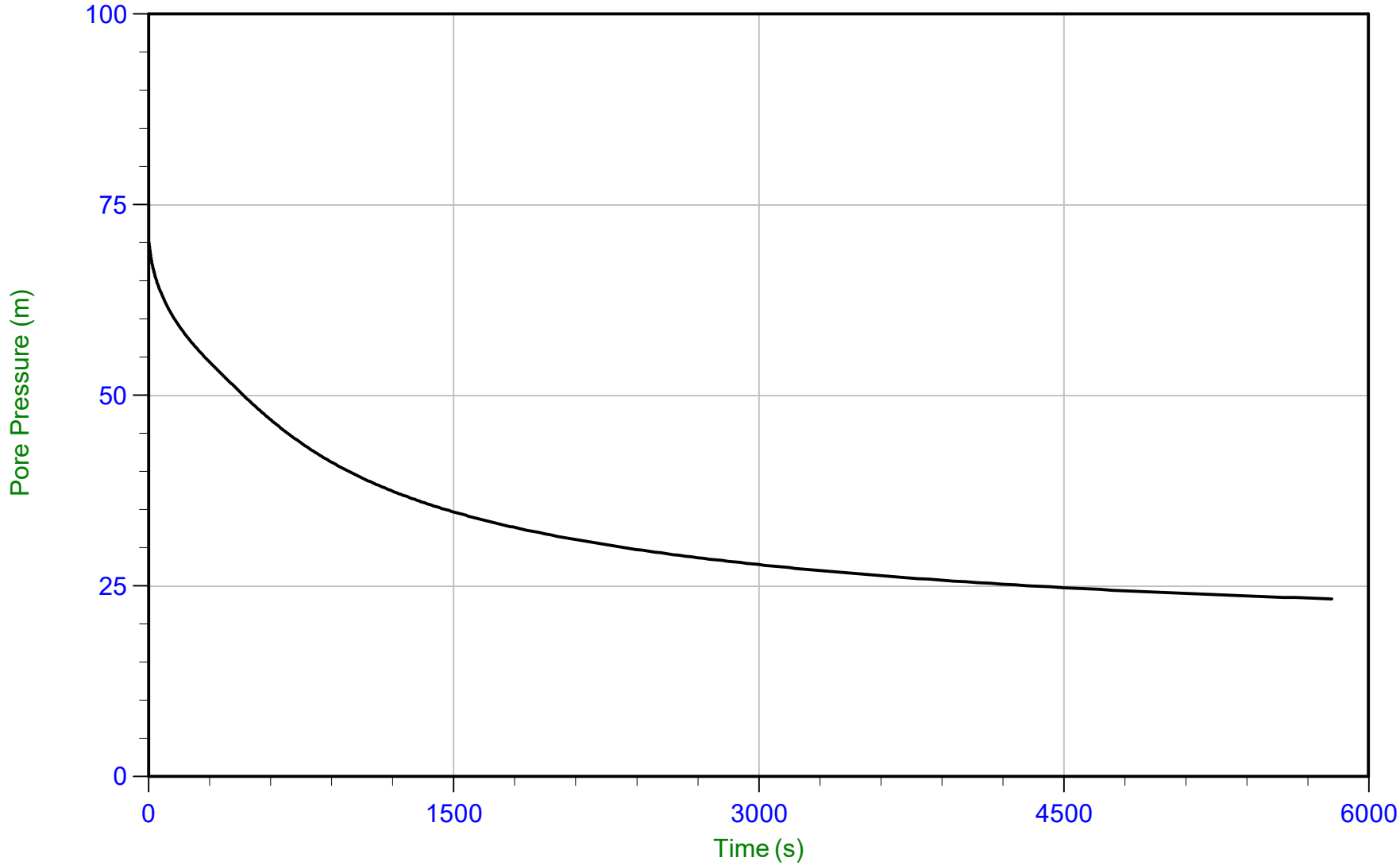
T(50): 4994.2 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP205.PPF2
Depth: 22.500 m / 73.818 ft
Duration: 5820.0 s

u Min: 23.3 m
u Max: 75.2 m
u Final: 23.3 m

WT: 3.2 m / 10.6 ft
Ueq: 19.3 m
U(50): 47.24 m

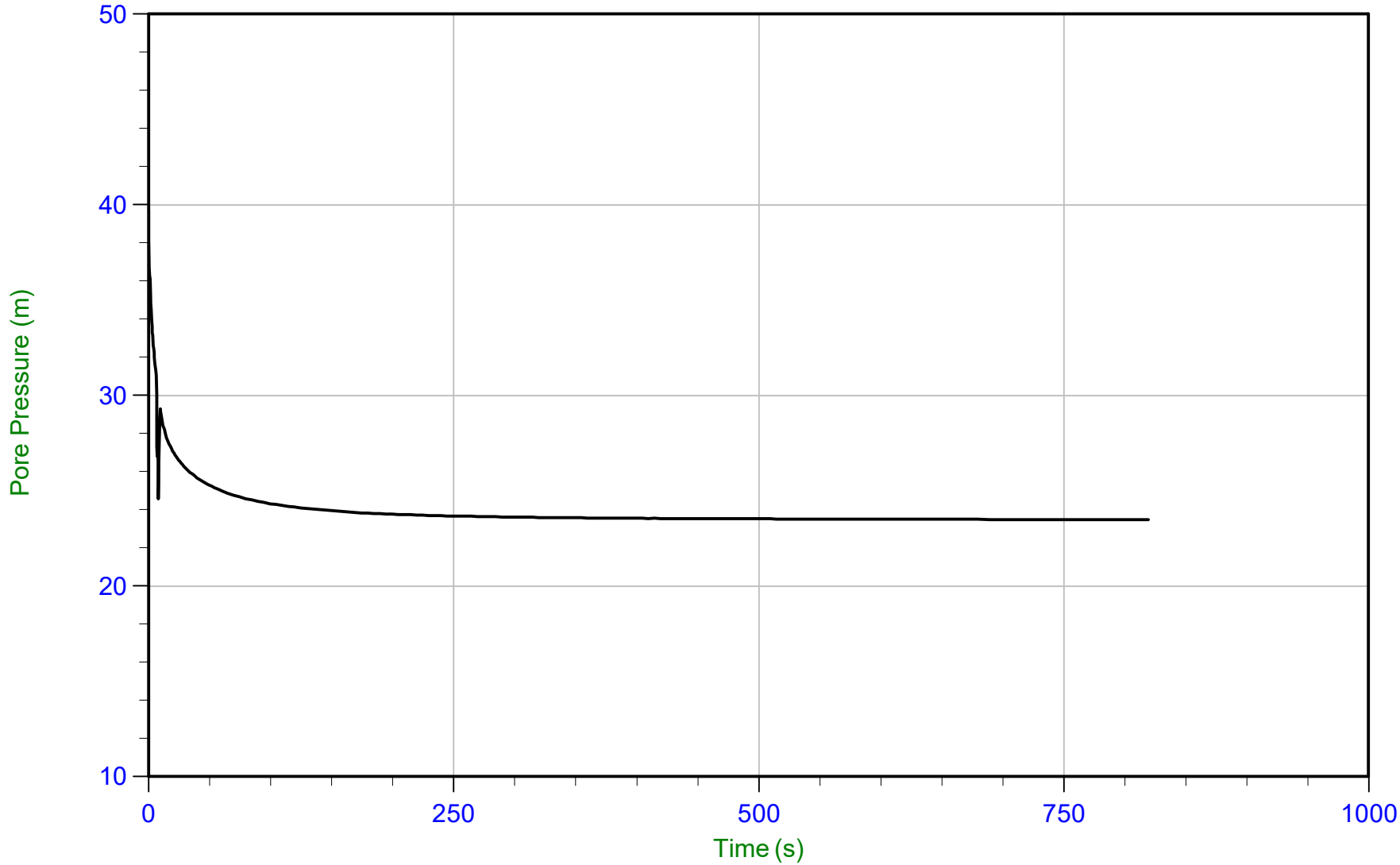
T(50): 580.8 s
Ir: 100
Ch: 1.2 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-02-26 15:18
Site: Crawford Mine - SRK

Sounding: SCPT24-LGE-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SP205.PPF2
Depth: 26.725 m / 87.679 ft
Duration: 820.0 s

u Min: 23.5 m
u Max: 39.7 m
u Final: 23.5 m

WT: 3.2 m / 10.6 ft
Ueq: 23.5 m
U(50): 31.61 m

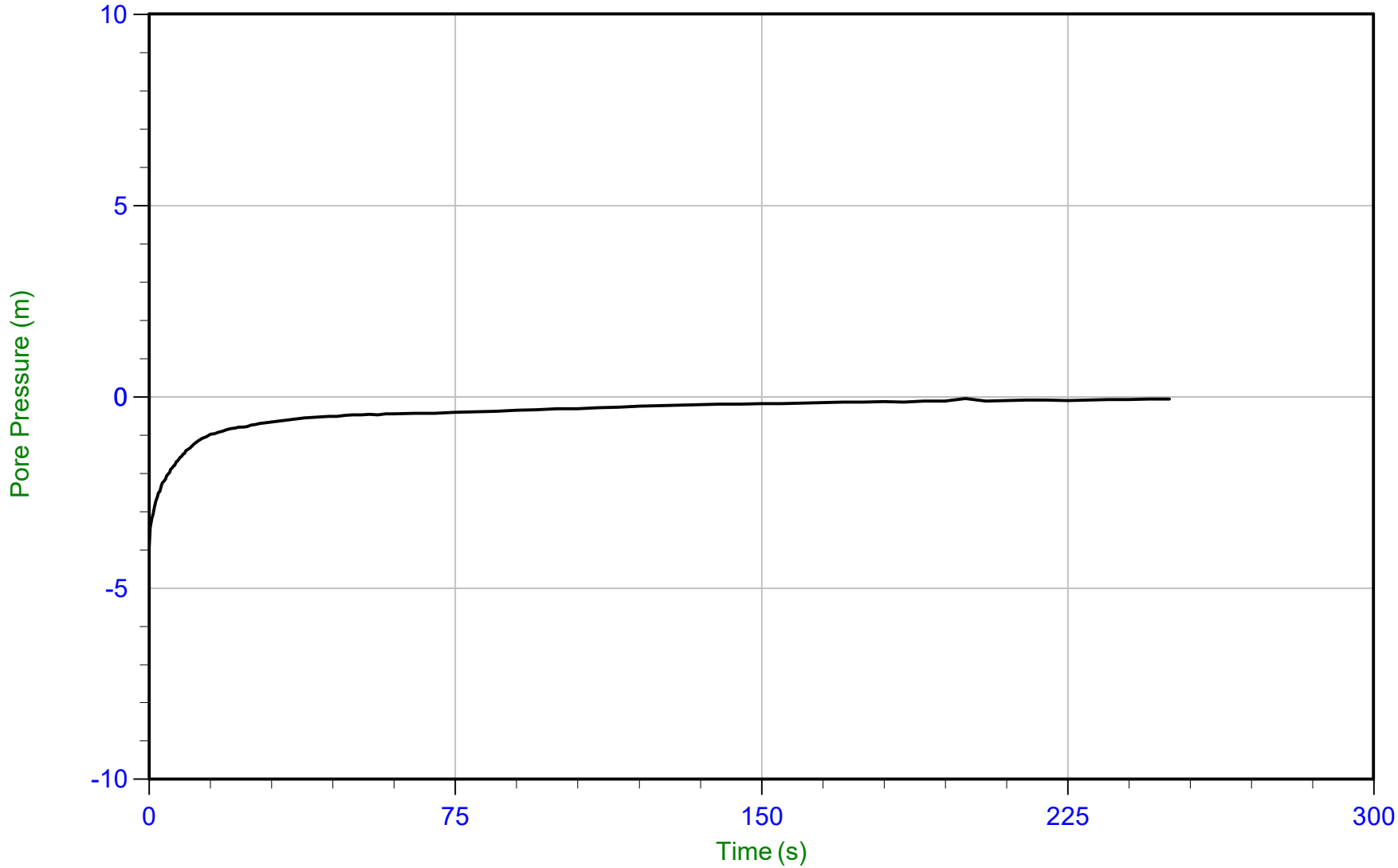
T(50): 5.5 s
Ir: 100
Ch: 127.4 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF03AB.PPF2
Depth: 1.025 m / 3.363 ft
Duration: 250.0 s

u Min: -3.9 m
u Max: -0.1 m
u Final: -0.1 m

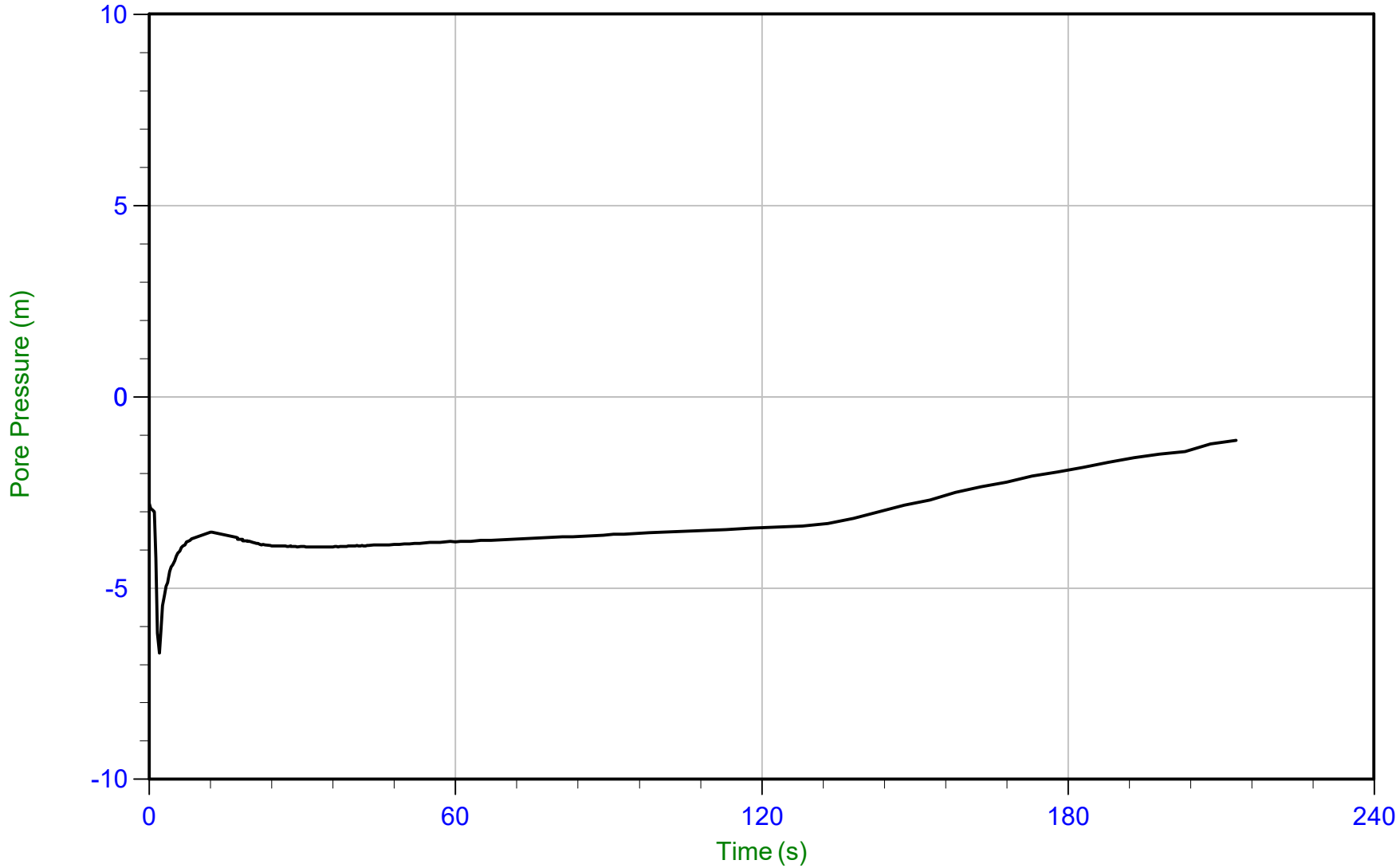
WT: 1.0 m / 3.4 ft
Ueq: 0.0 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF03AB.PPF2
Depth: 2.000 m / 6.562 ft
Duration: 213.1 s

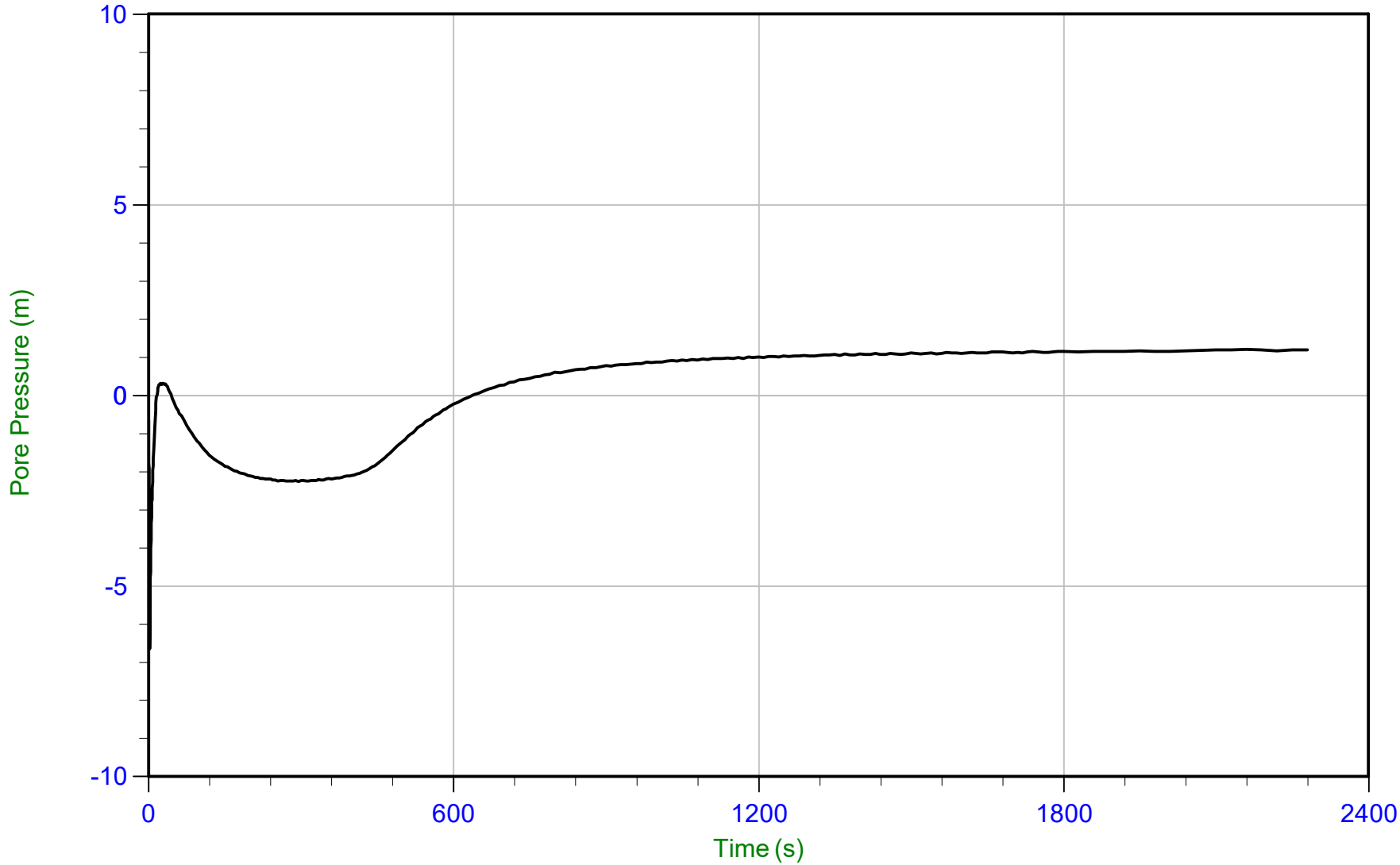
u Min: -6.7 m
u Max: -1.1 m
u Final: -1.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-13 13:29
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW03AB
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF03AB.PPF2
Depth: 2.425 m / 7.956 ft
Duration: 2280.0 s

u Min: -6.6 m
u Max: 1.2 m
u Final: 1.2 m

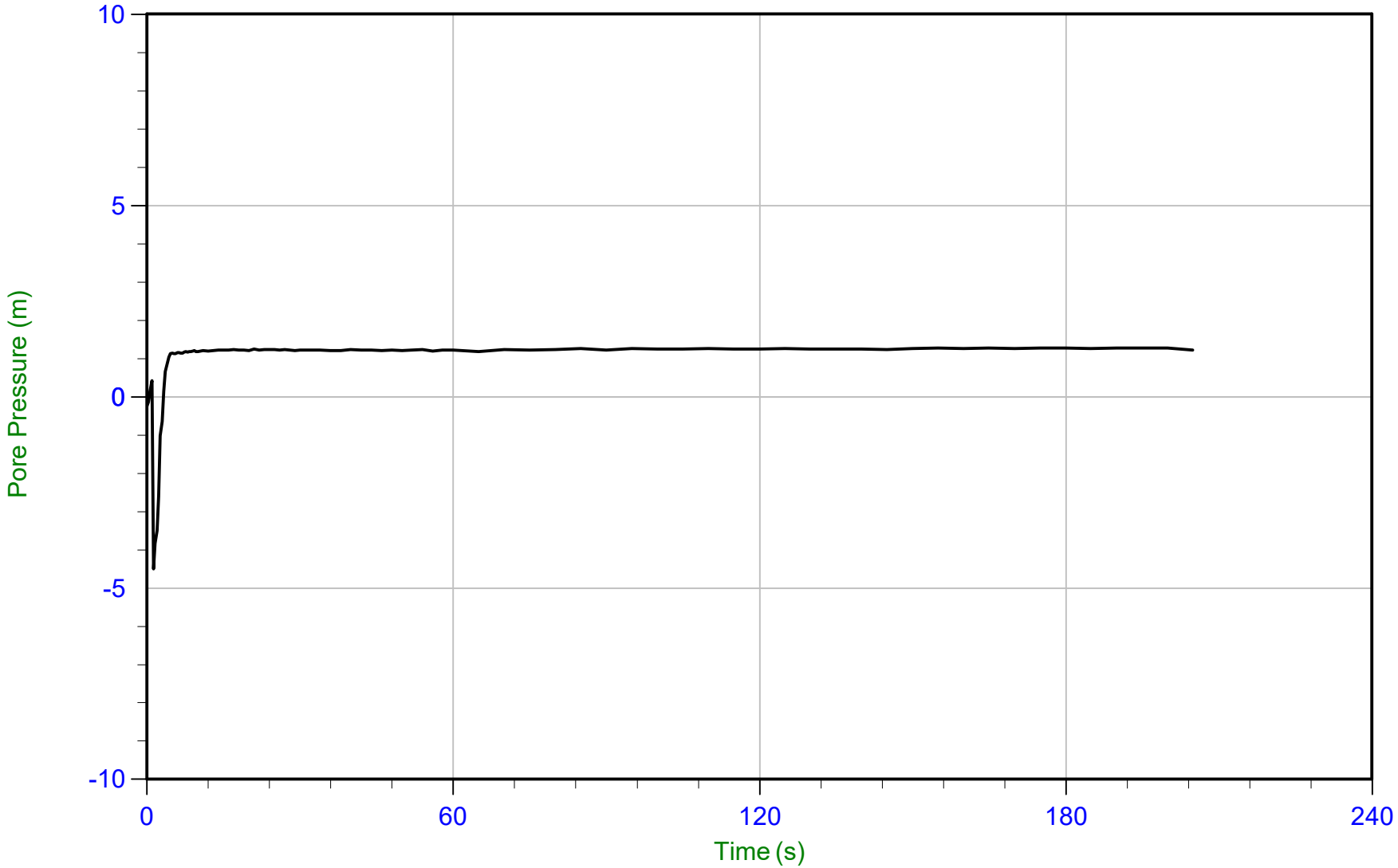
WT: 1.2 m / 4.0 ft
Ueq: 1.2 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 1.150 m / 3.773 ft
Duration: 205.0 s

u Min: -4.5 m
u Max: 1.3 m
u Final: 1.2 m

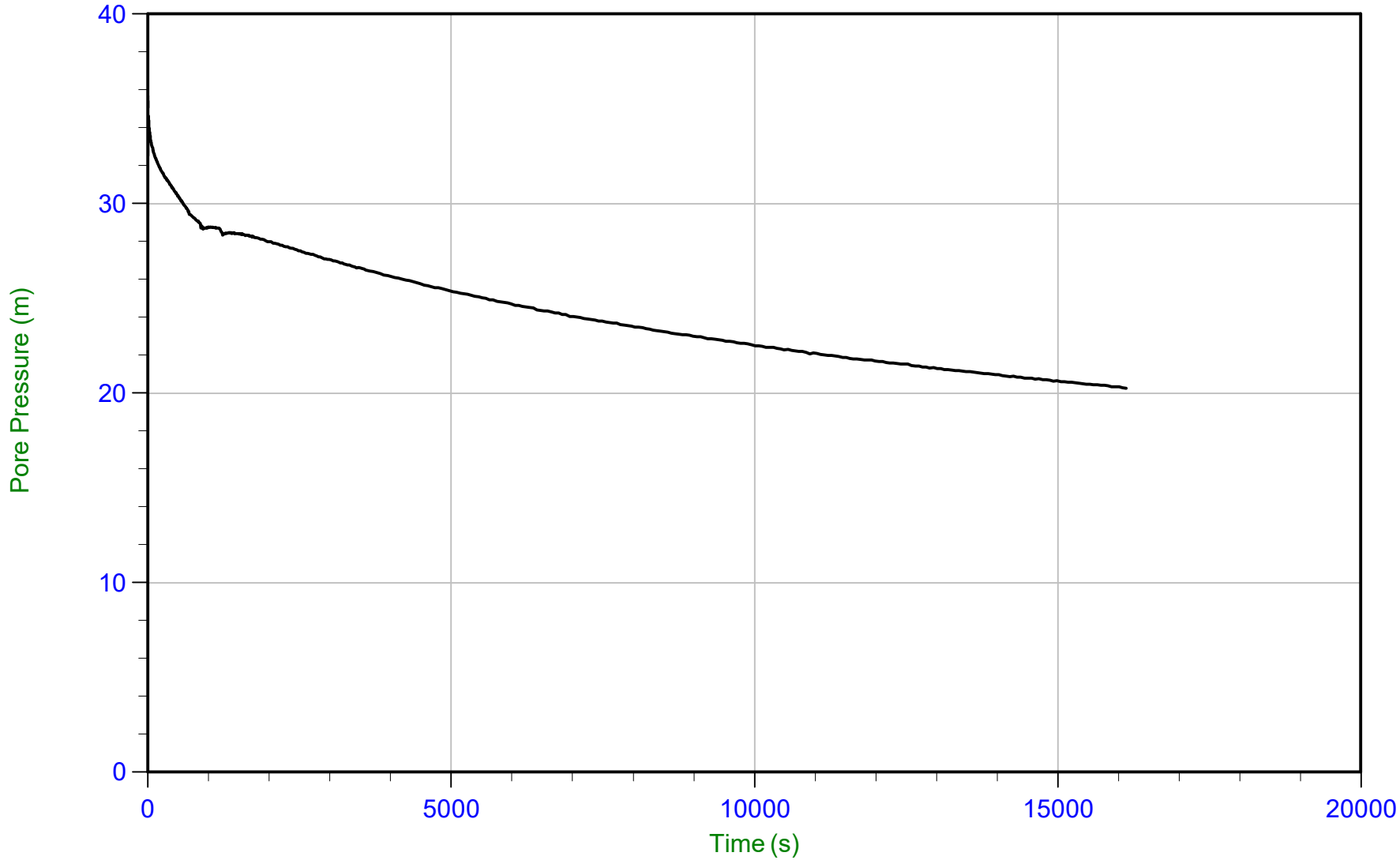
WT: -0.1 m / -0.2 ft
Ueq: 1.2 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 16140.0 s

u Min: 20.3 m
u Max: 35.7 m
u Final: 20.3 m

WT: -0.1 m / -0.3 ft
Ueq: 7.6 m
U(50): 21.65 m

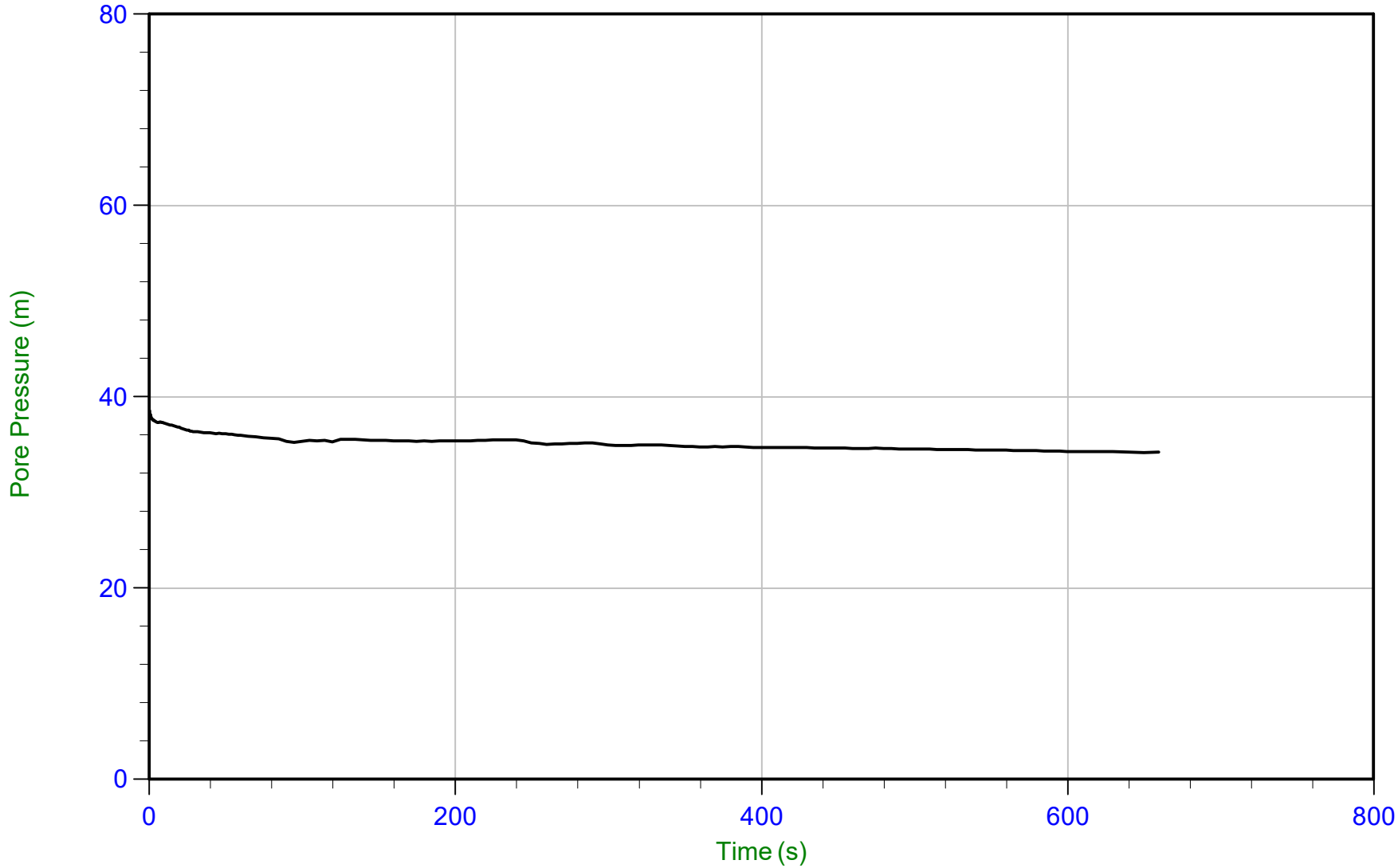
T(50): 12138.4 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 7.950 m / 26.082 ft
Duration: 660.0 s

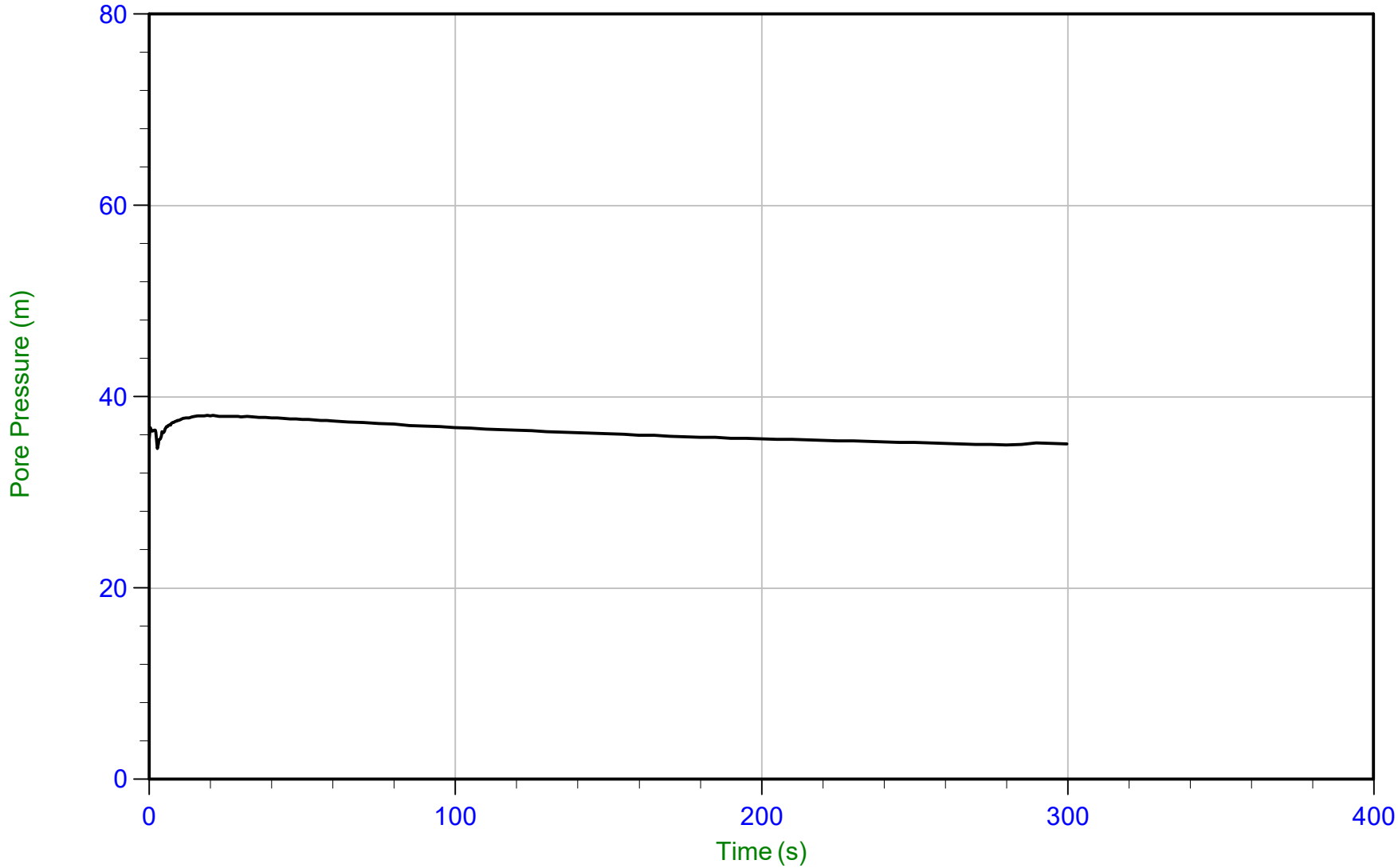
u Min: 34.2 m
u Max: 38.6 m
u Final: 34.2 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 8.175 m / 26.821 ft
Duration: 300.0 s

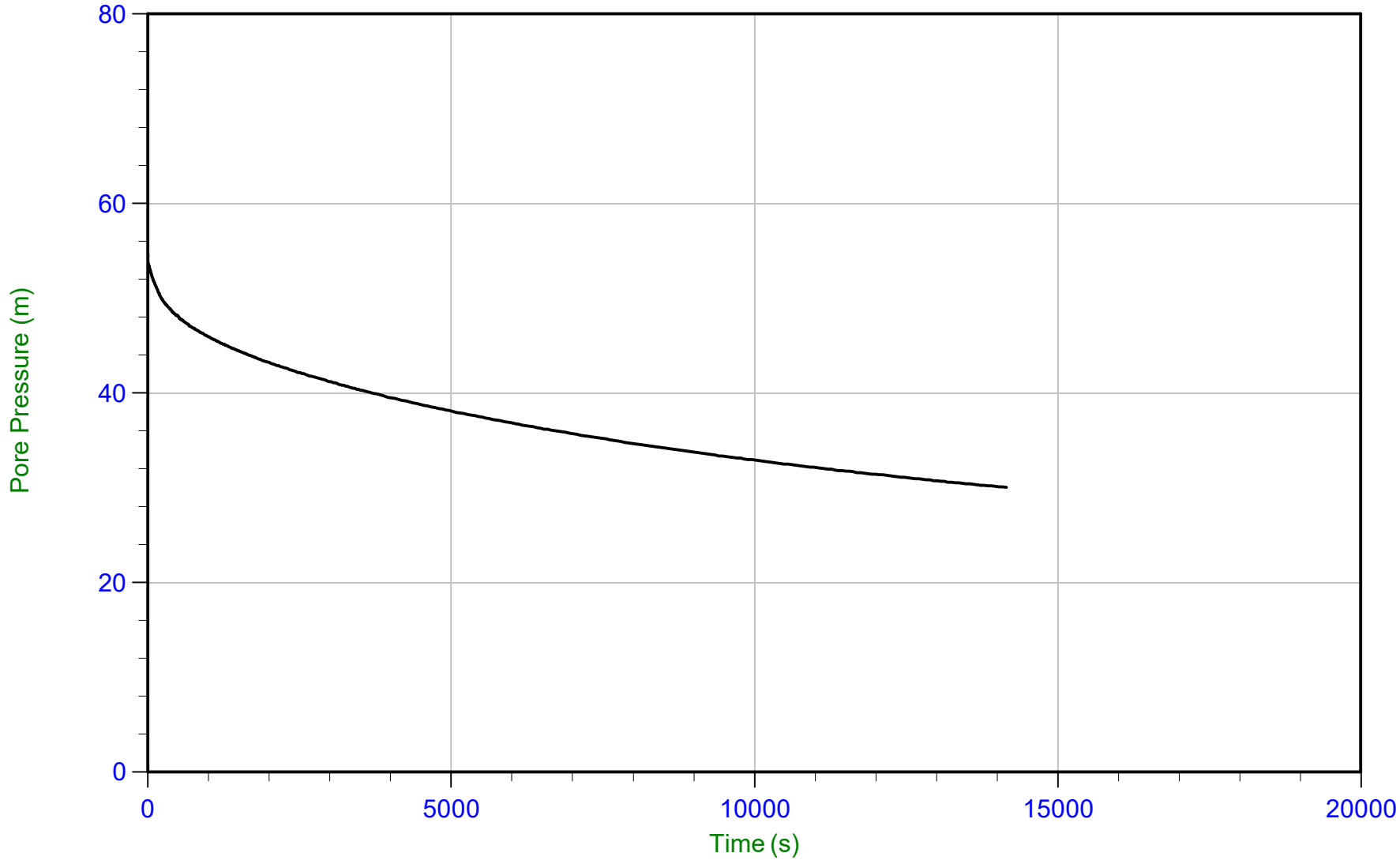
u Min: 34.6 m
u Max: 38.0 m
u Final: 35.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 14160.0 s

u Min: 30.1 m
u Max: 54.7 m
u Final: 30.1 m

WT: -0.1 m / -0.3 ft
Ueq: 12.6 m
U(50): 33.64 m

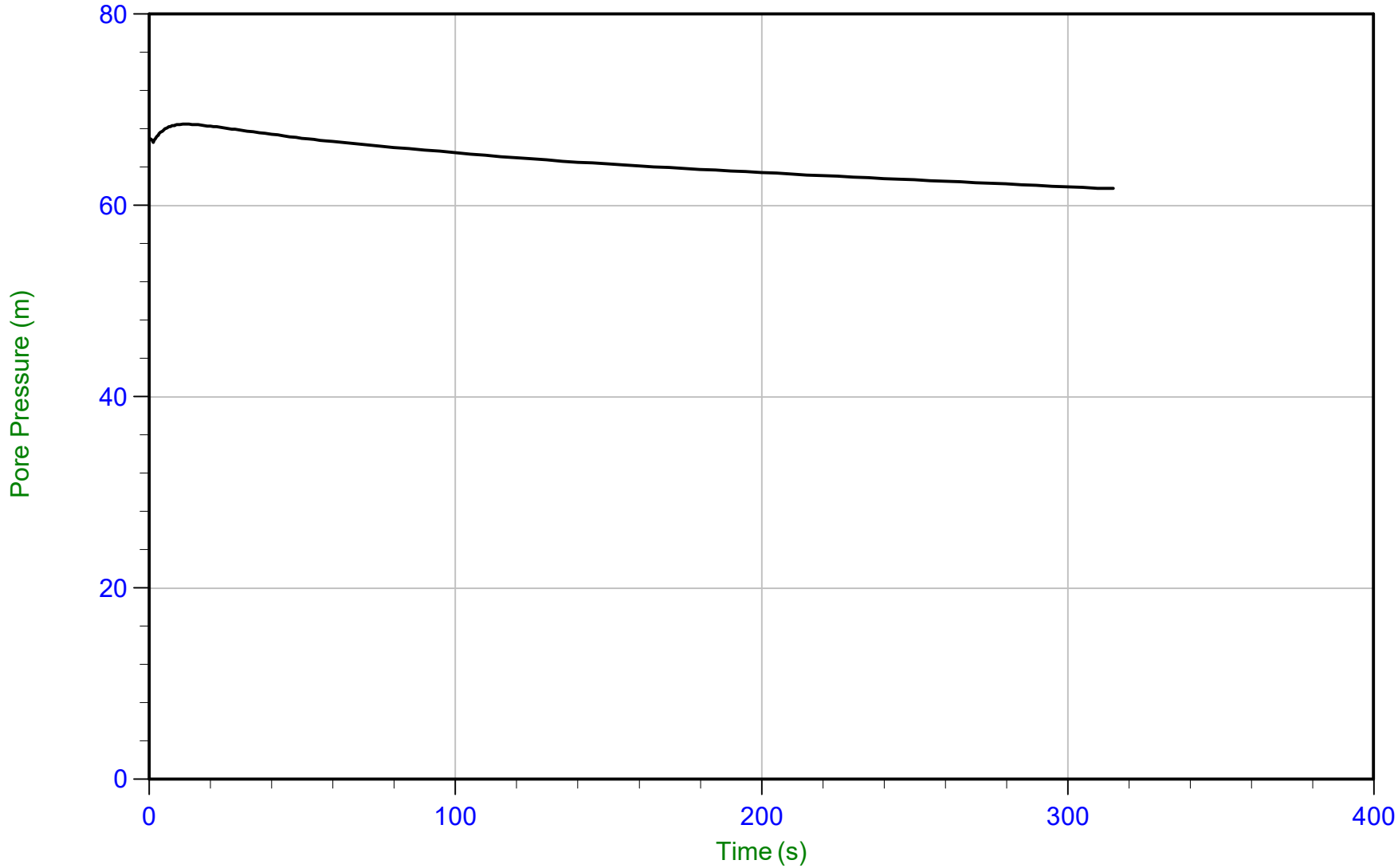
T(50): 9155.5 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 15.125 m / 49.622 ft
Duration: 315.0 s

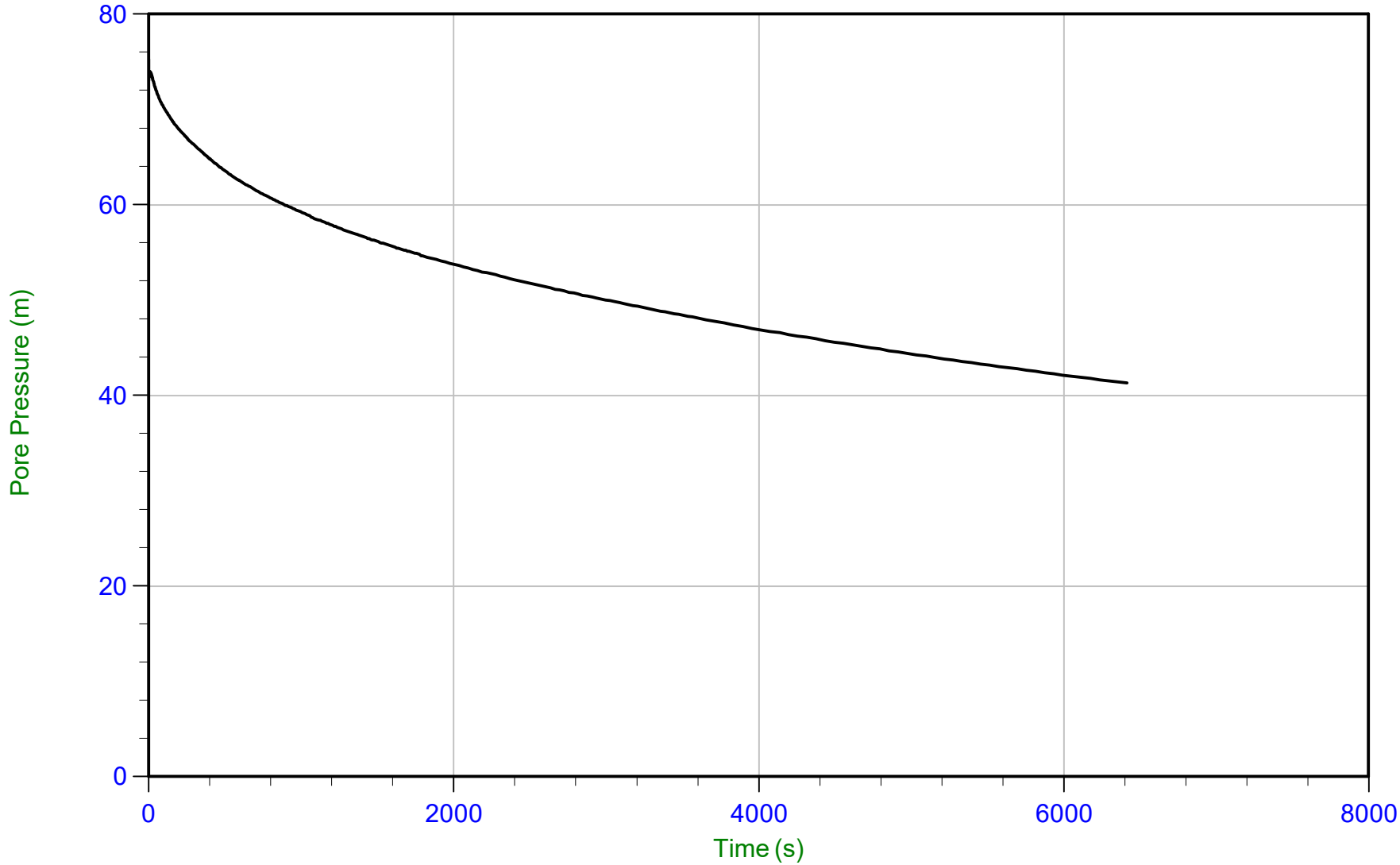
u Min: 61.8 m
u Max: 68.5 m
u Final: 61.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 6420.0 s

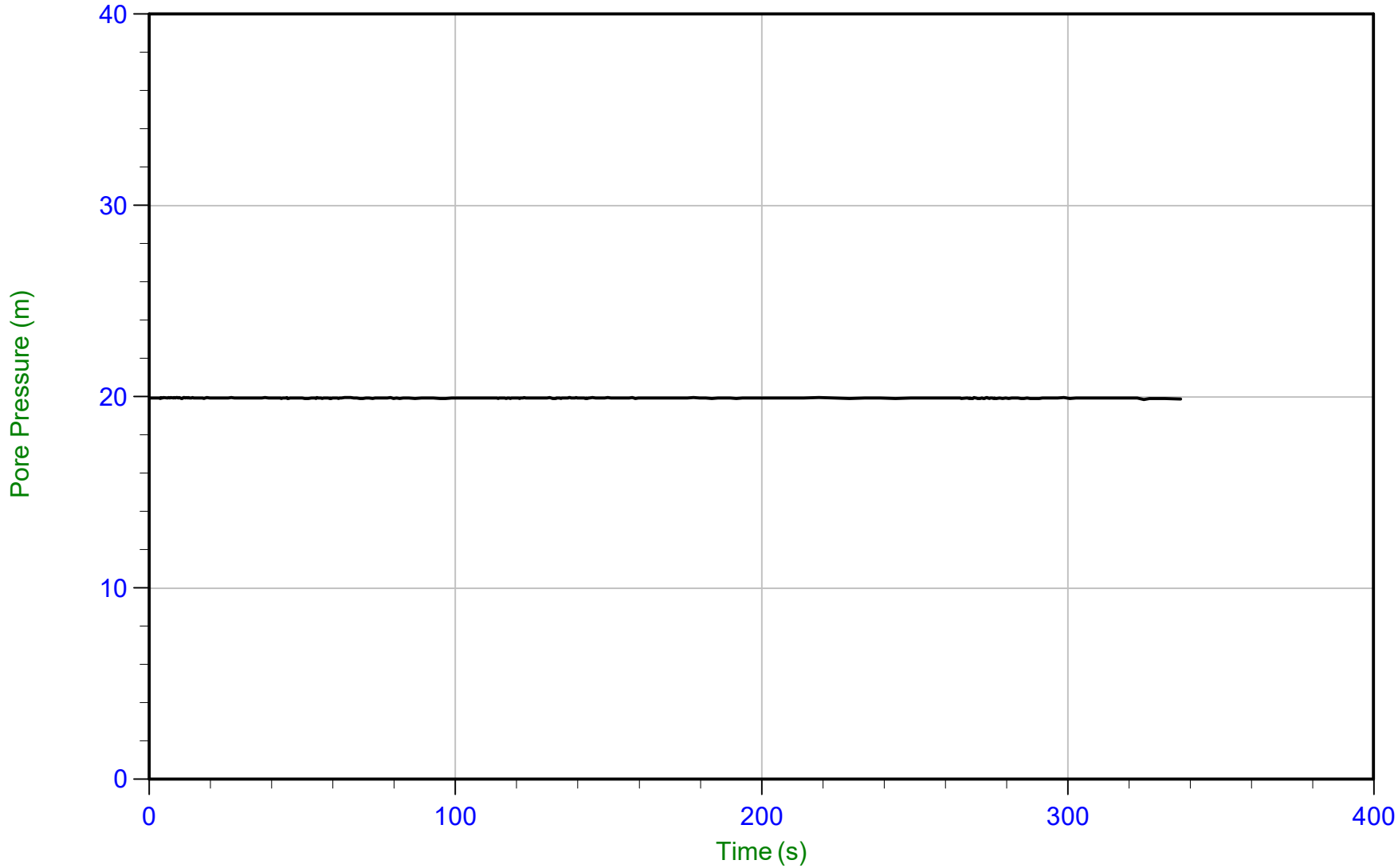
u Min: 41.3 m
u Max: 75.3 m
u Final: 41.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 337.0 s

u Min: 19.9 m
u Max: 20.0 m
u Final: 19.9 m

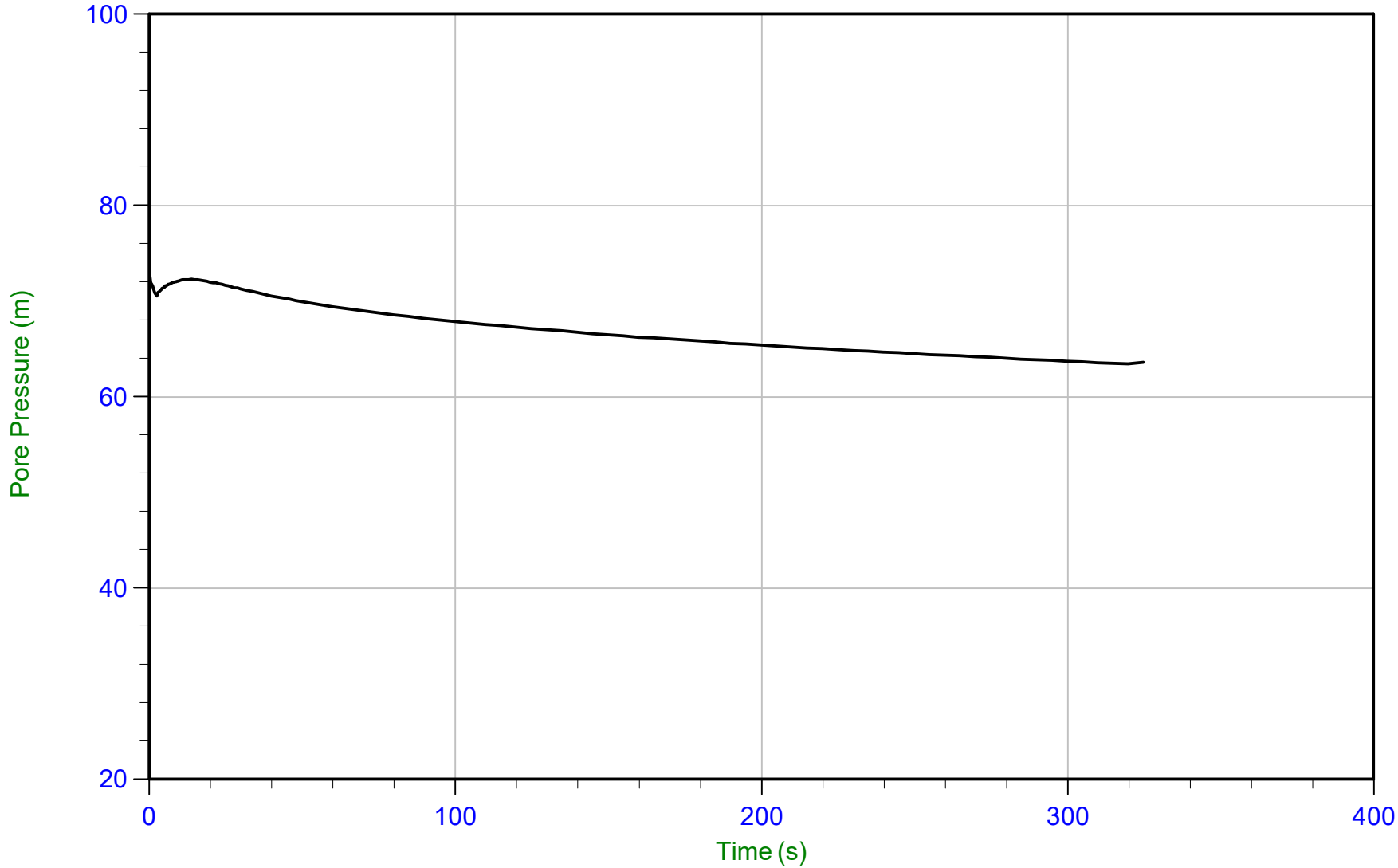
WT: -2.4 m / -7.9 ft
Ueq: 19.9 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 18.125 m / 59.465 ft
Duration: 325.0 s

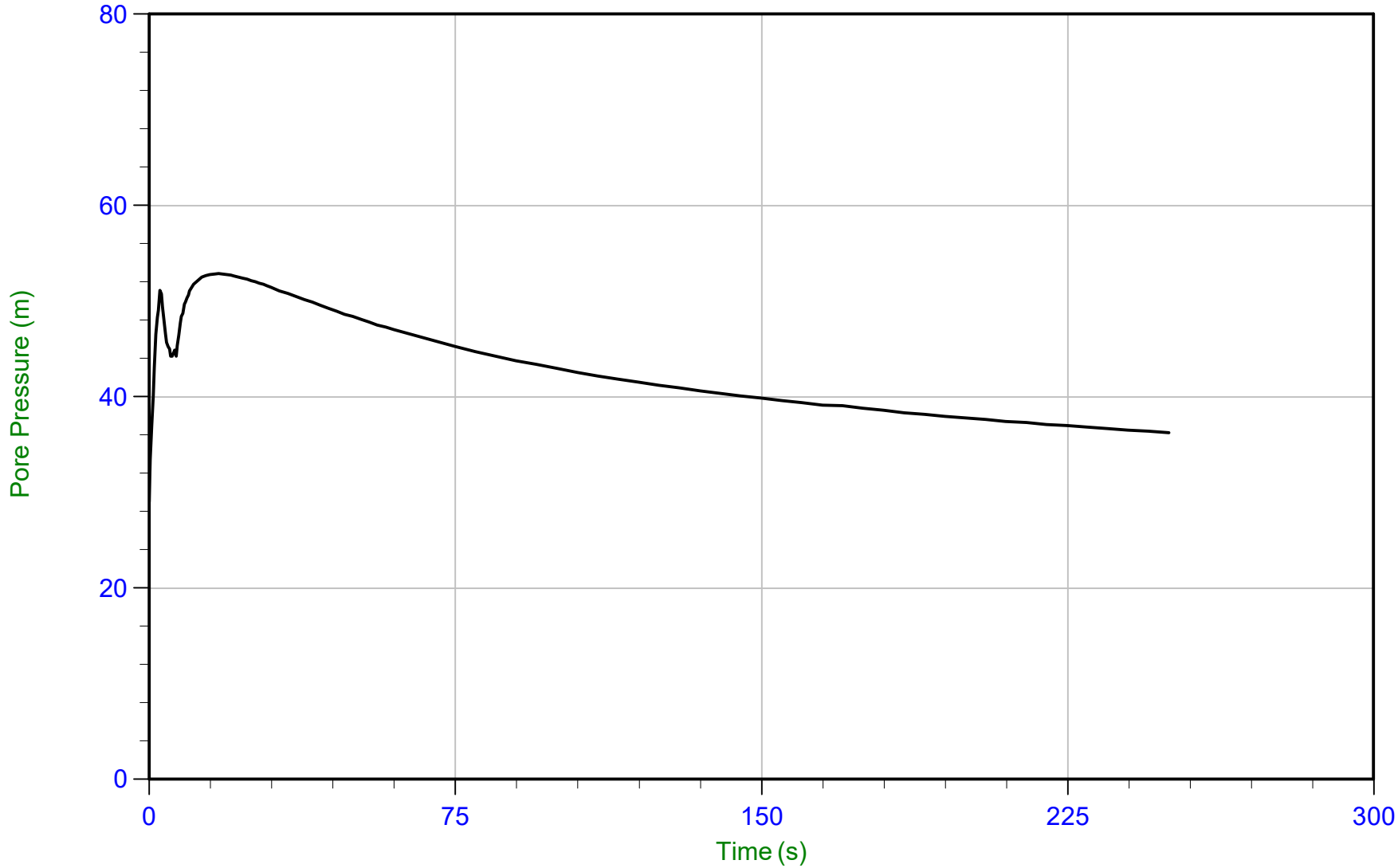
u Min: 63.5 m
u Max: 72.8 m
u Final: 63.6 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 22.125 m / 72.588 ft
Duration: 250.0 s

u Min: 29.0 m
u Max: 52.9 m
u Final: 36.3 m

WT: 0.3 m / 1.1 ft
Ueq: 21.8 m
U(50): 37.34 m

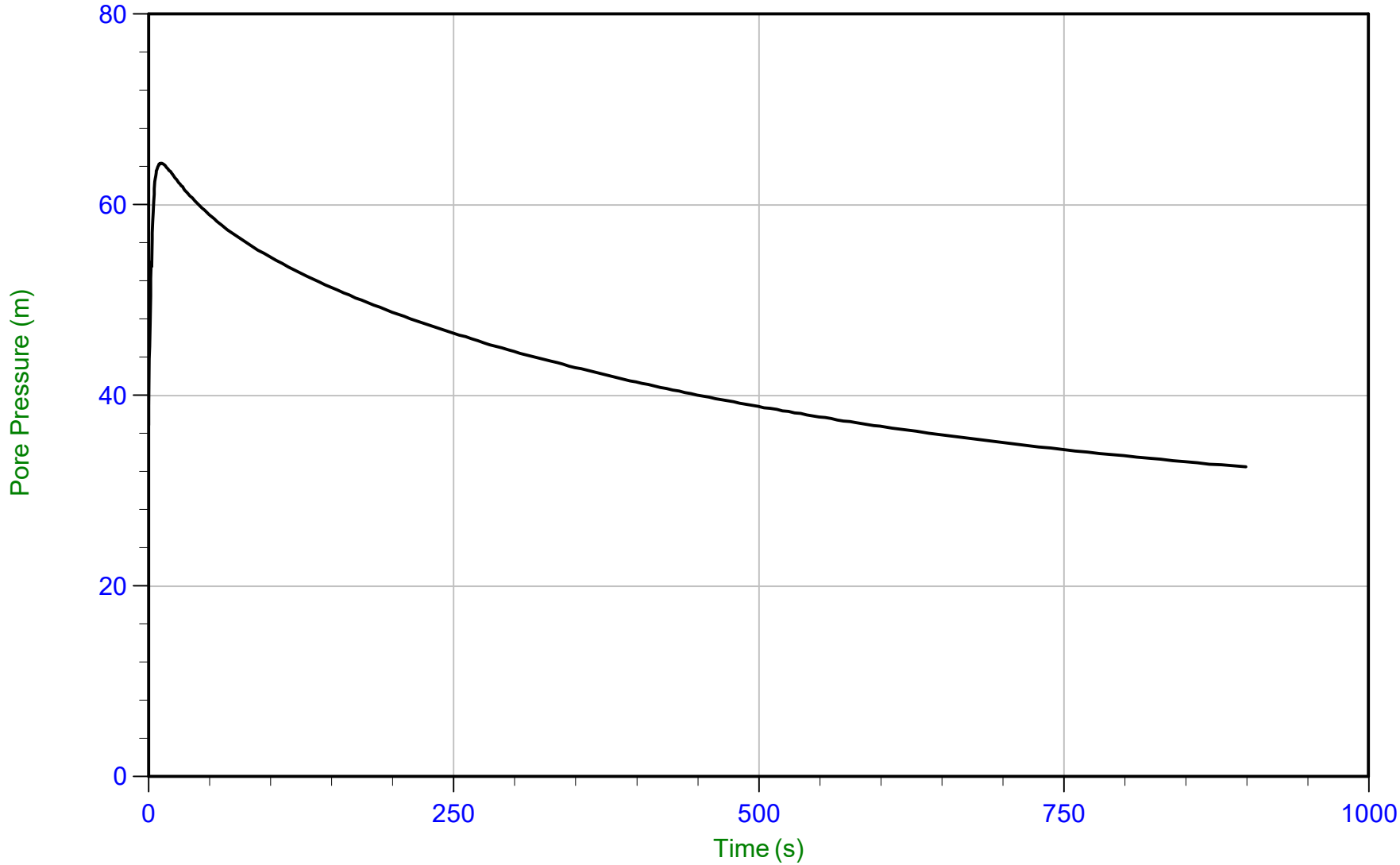
T(50): 196.0 s
Ir: 100
Ch: 3.6 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 22.500 m / 73.818 ft
Duration: 900.0 s

u Min: 32.5 m
u Max: 64.3 m
u Final: 32.5 m

WT: 0.3 m / 1.1 ft
Ueq: 22.2 m
U(50): 43.25 m

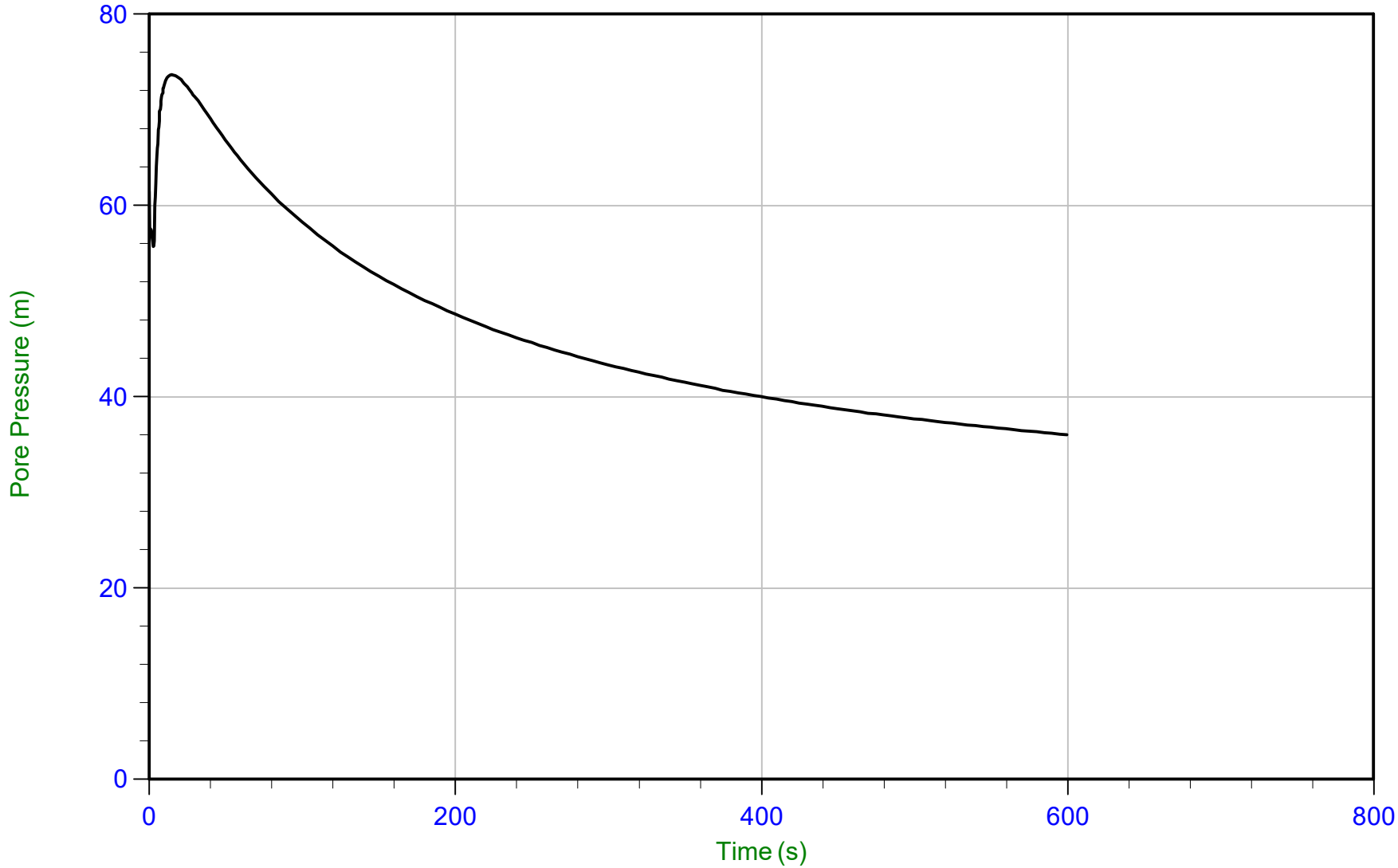
T(50): 329.5 s
Ir: 100
Ch: 2.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 27.500 m / 90.222 ft
Duration: 600.0 s

u Min: 36.0 m
u Max: 73.7 m
u Final: 36.0 m

WT: 0.3 m / 1.1 ft
Ueq: 27.2 m
U(50): 50.43 m

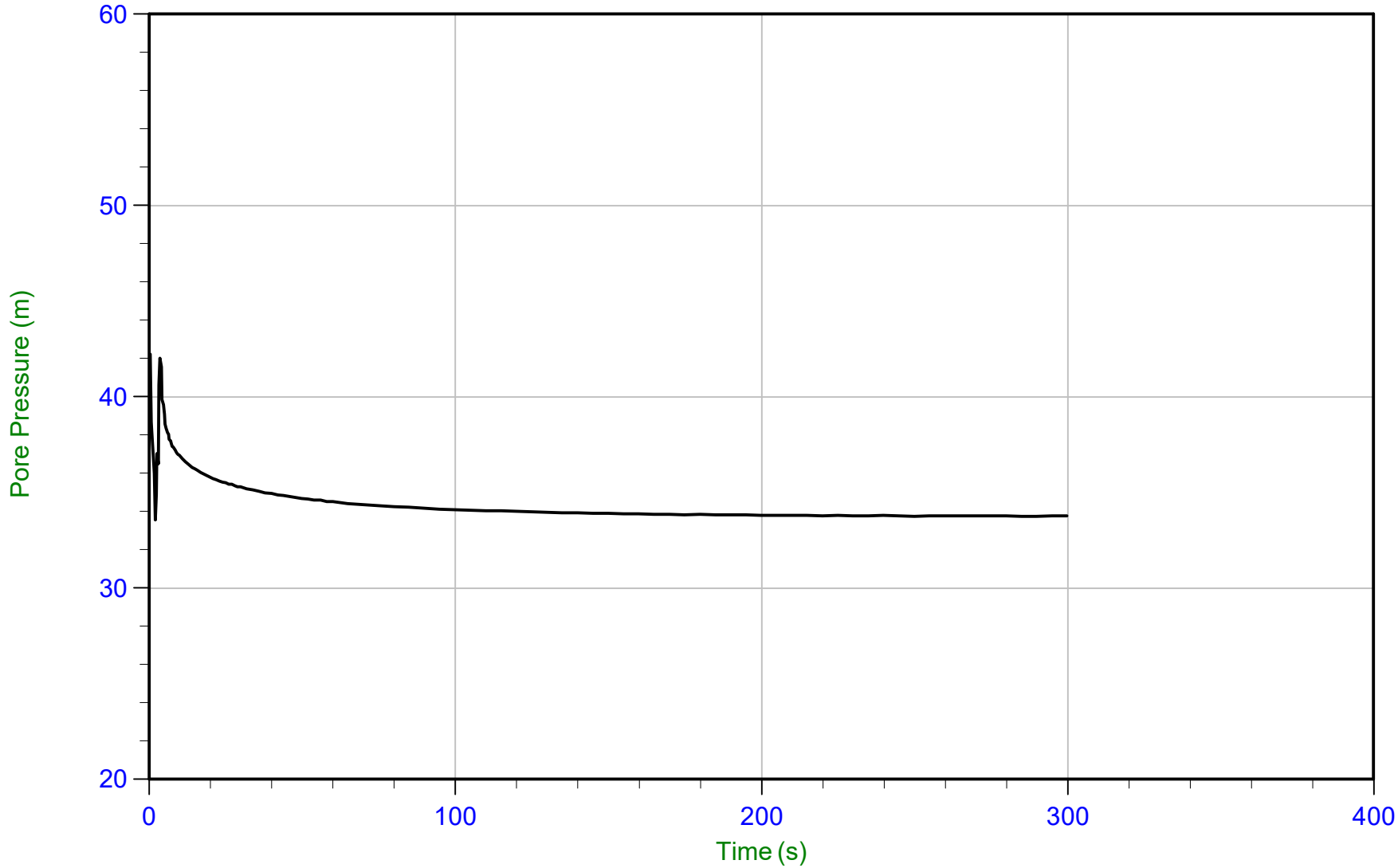
T(50): 160.7 s
Ir: 100
Ch: 4.4 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-20 13:16
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-MW08AB
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF08AB.PPF2
Depth: 34.125 m / 111.957 ft
Duration: 300.0 s

u Min: 33.5 m
u Max: 42.2 m
u Final: 33.8 m

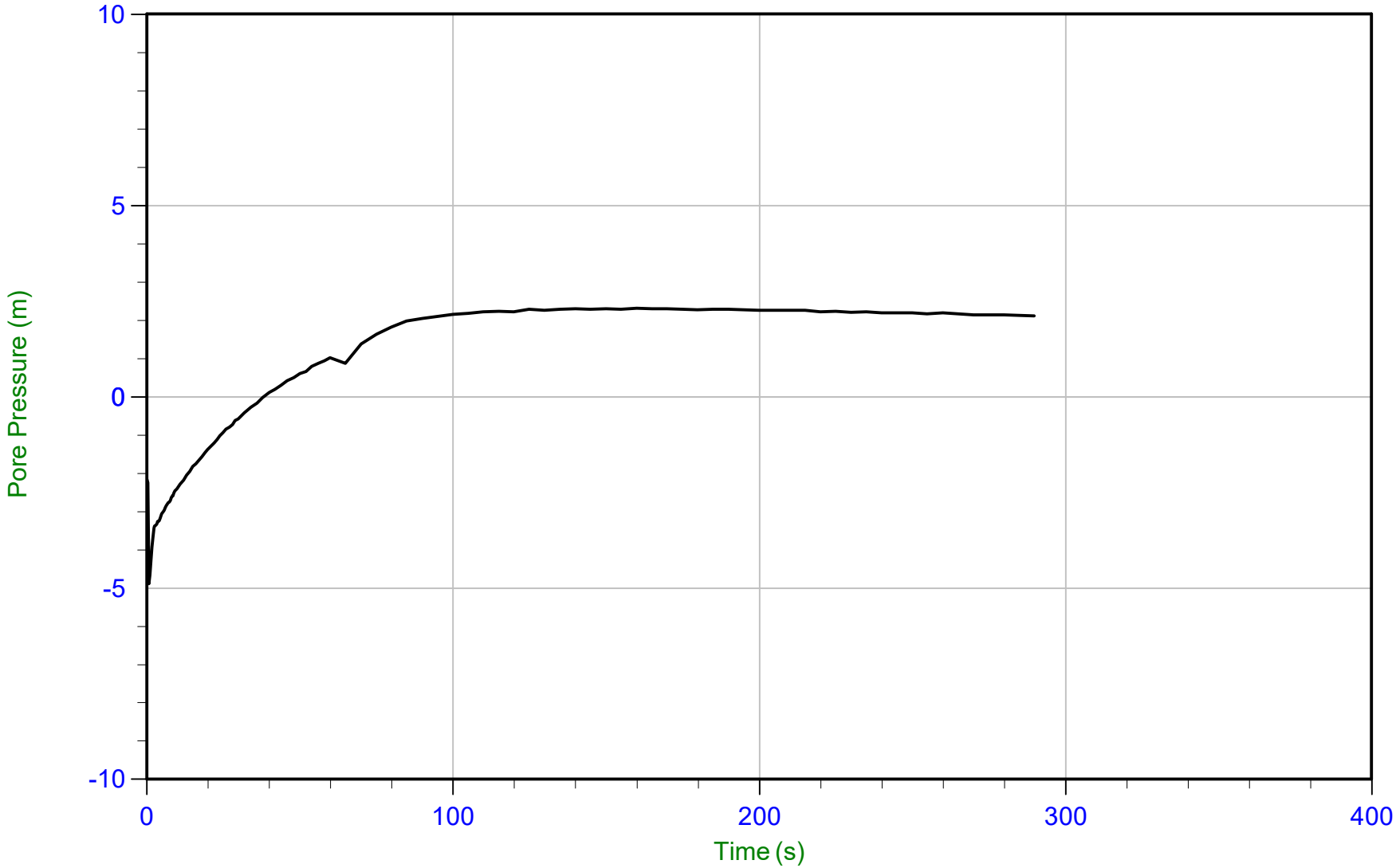
WT: 0.3 m / 1.1 ft
Ueq: 33.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 1.050 m / 3.445 ft
Duration: 290.0 s

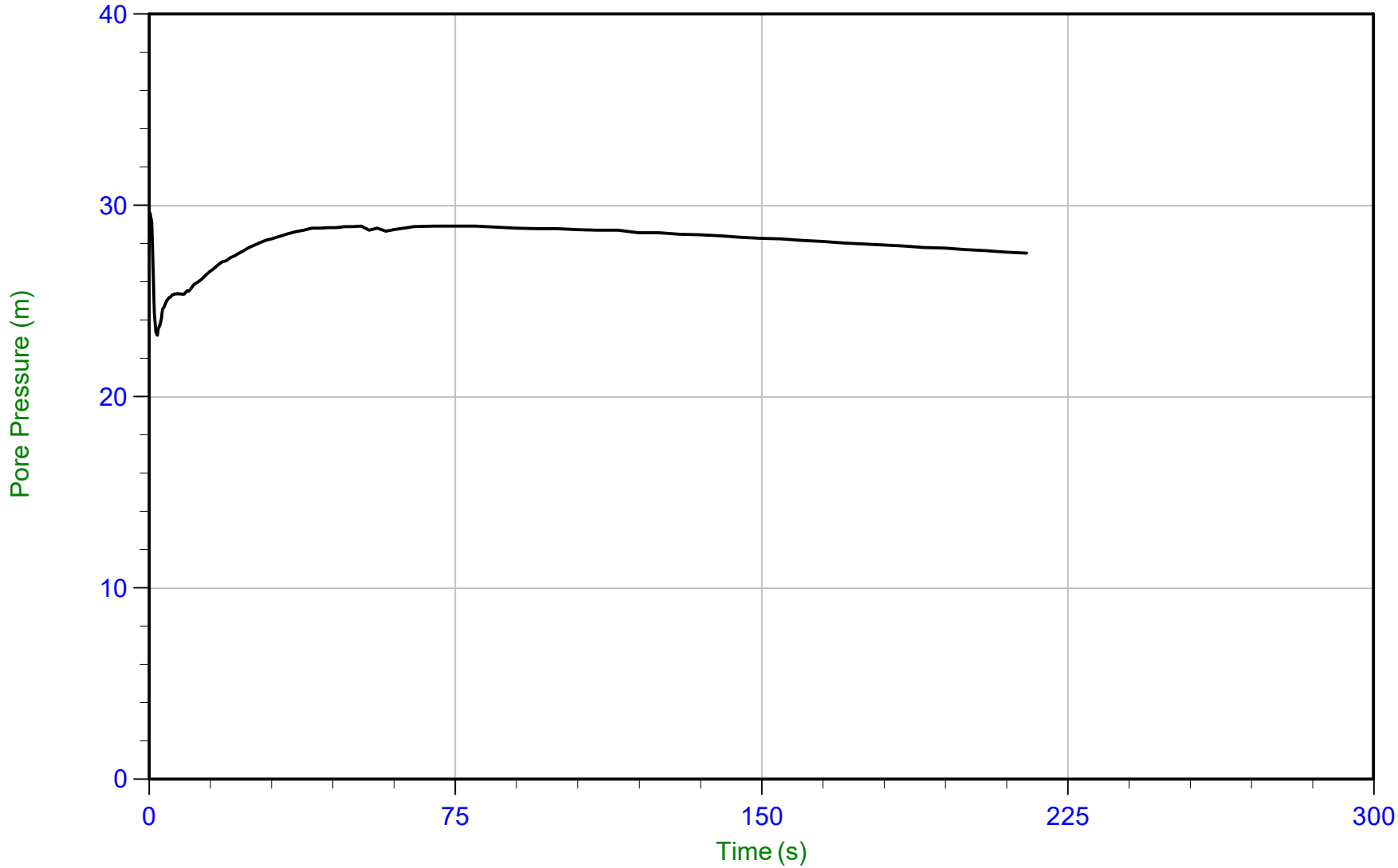
u Min: -4.9 m
u Max: 2.3 m
u Final: 2.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 3.050 m / 10.006 ft
Duration: 215.0 s

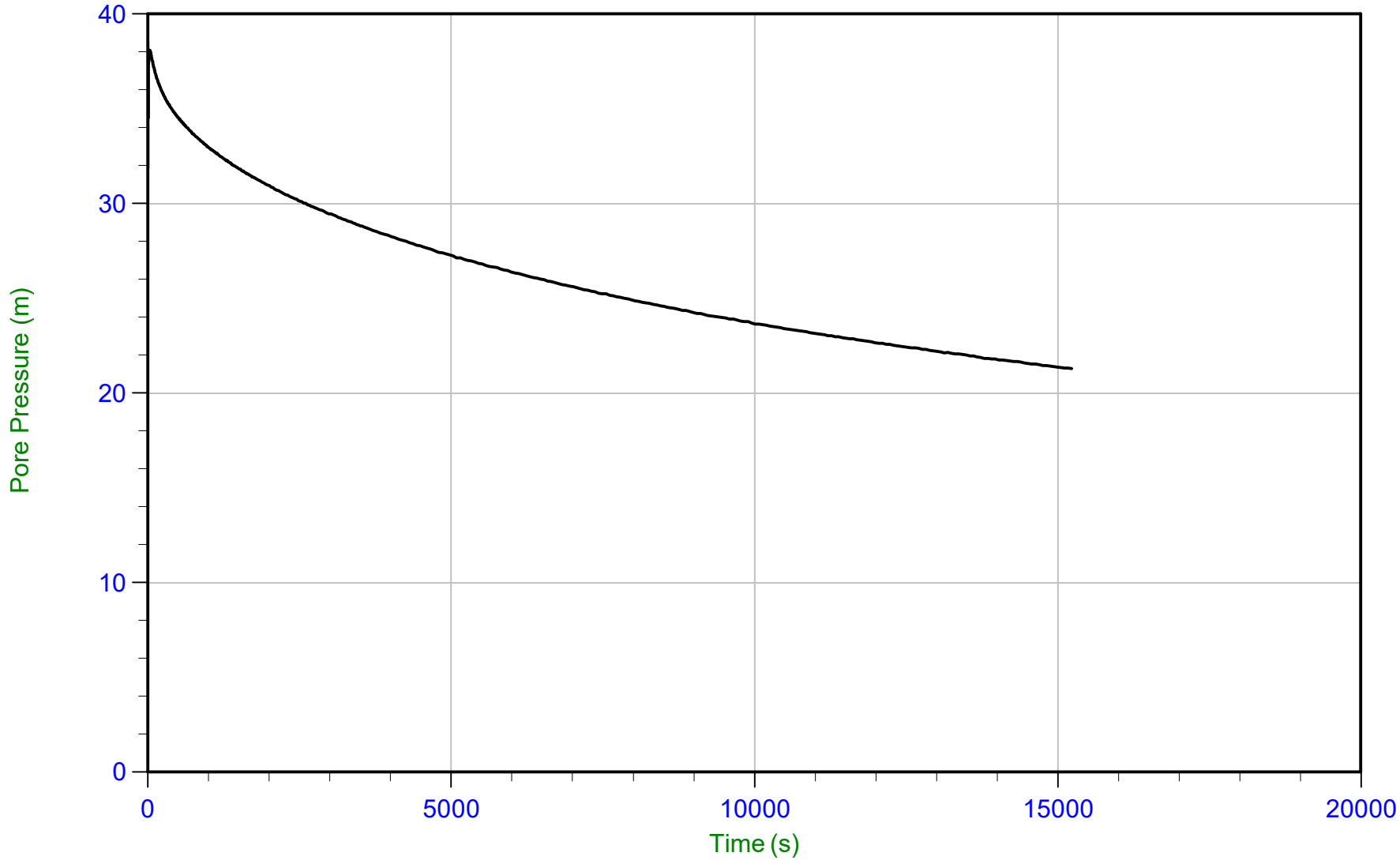
u Min: 23.2 m
u Max: 29.7 m
u Final: 27.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 15240.0 s

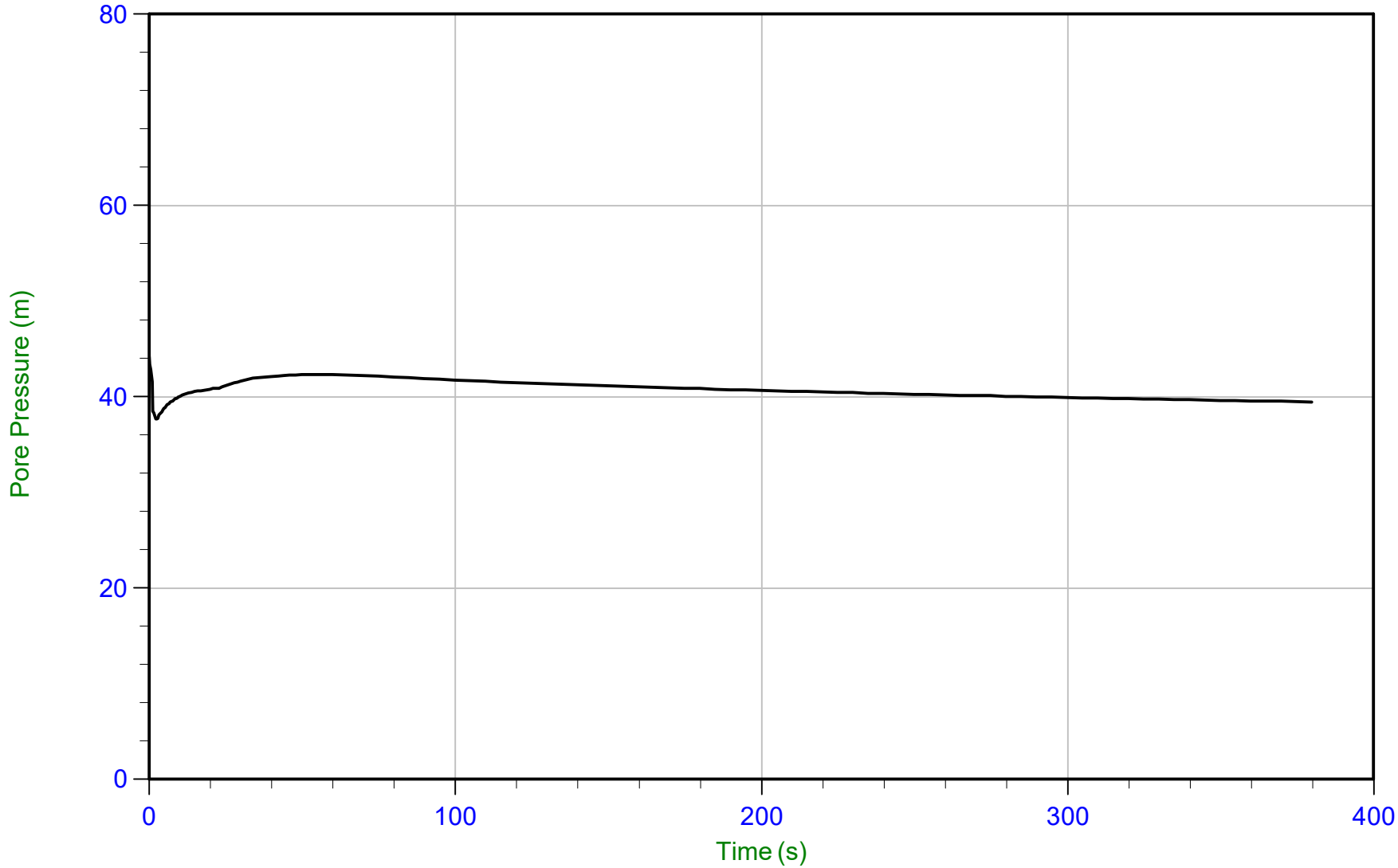
u Min: 21.3 m
u Max: 38.5 m
u Final: 21.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 9.050 m / 29.691 ft
Duration: 380.0 s

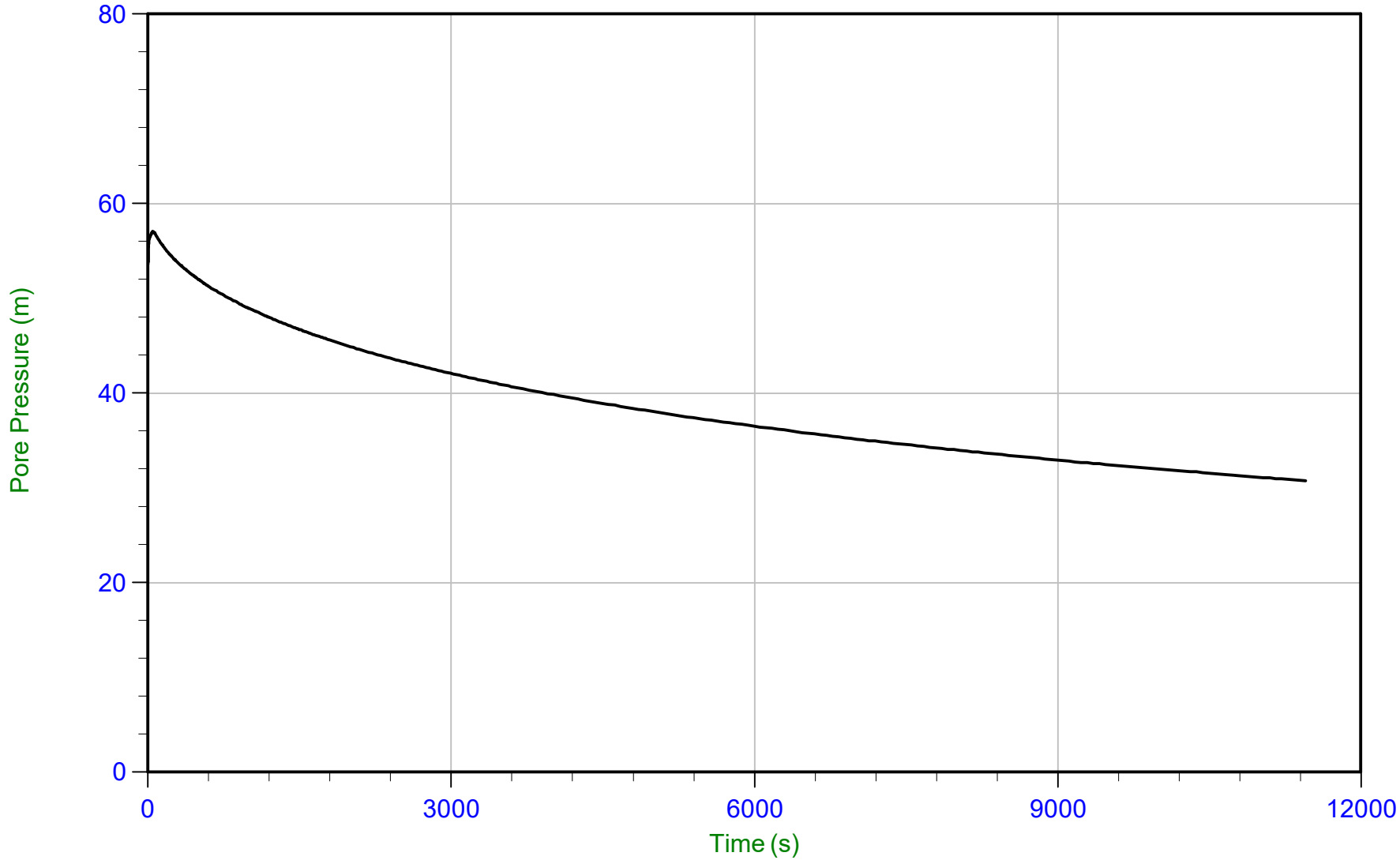
u Min: 37.7 m
u Max: 44.2 m
u Final: 39.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 11460.0 s

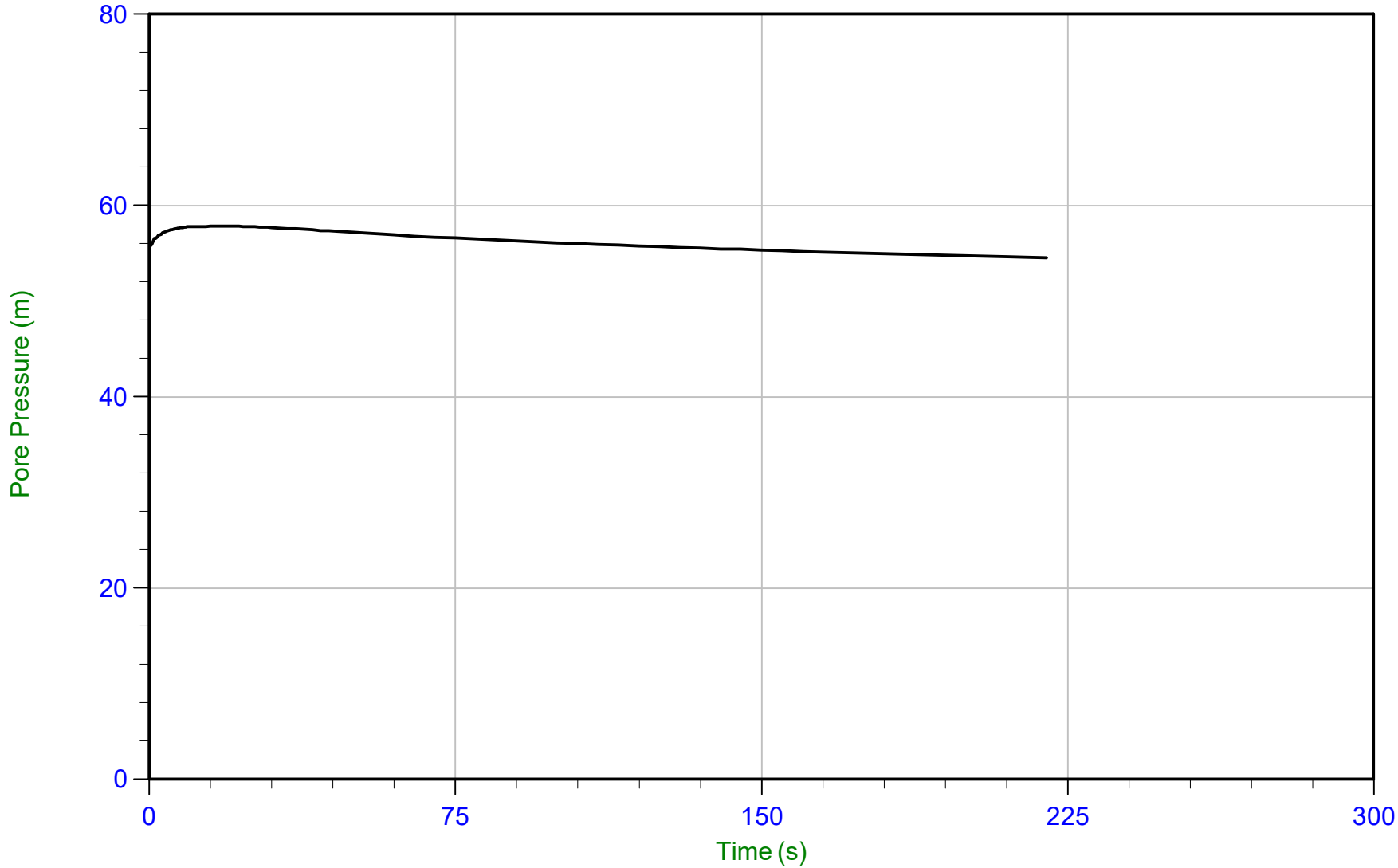
u Min: 30.8 m
u Max: 57.0 m
u Final: 30.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 13.050 m / 42.814 ft
Duration: 220.0 s

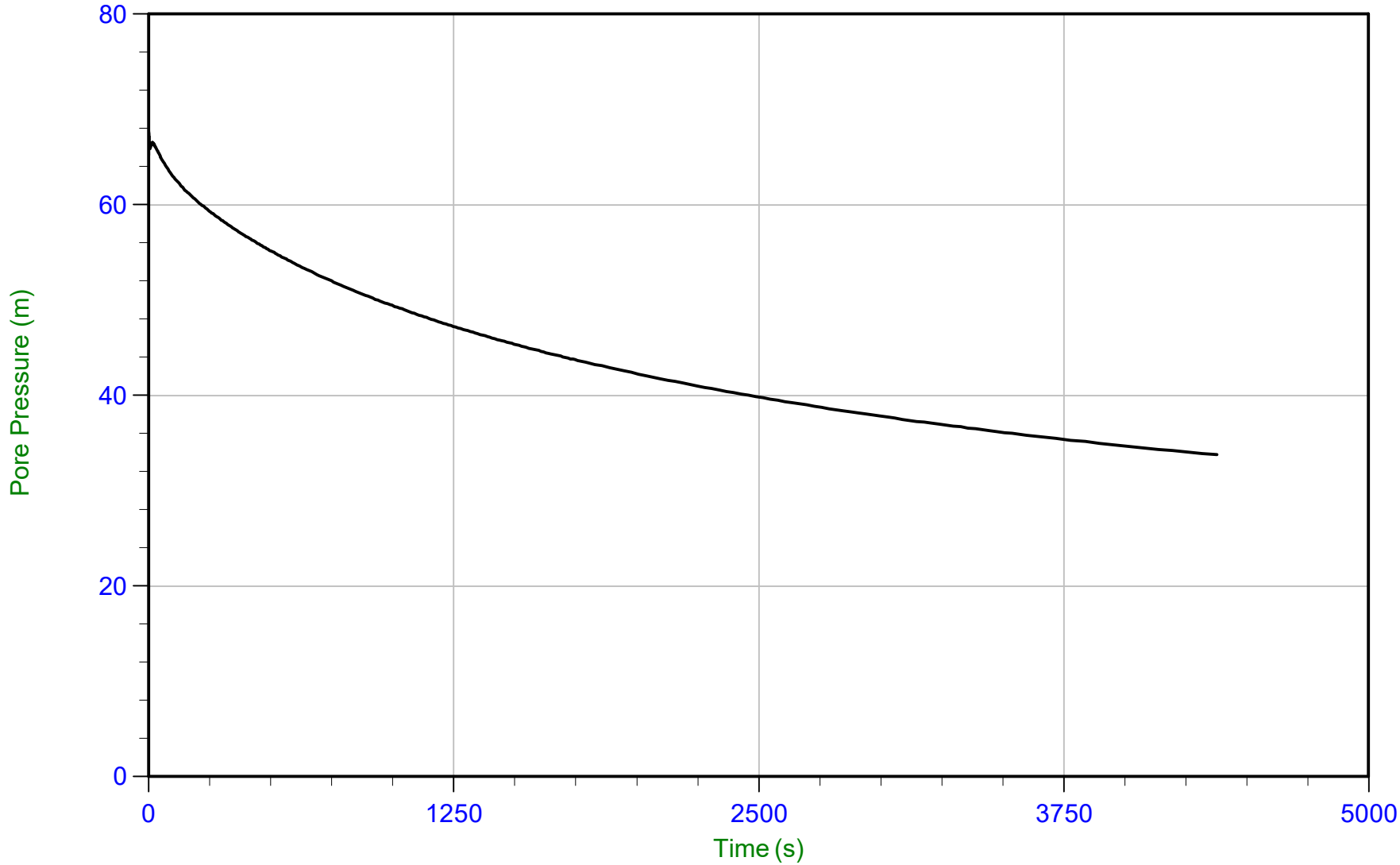
u Min: 54.5 m
u Max: 57.9 m
u Final: 54.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 4380.0 s

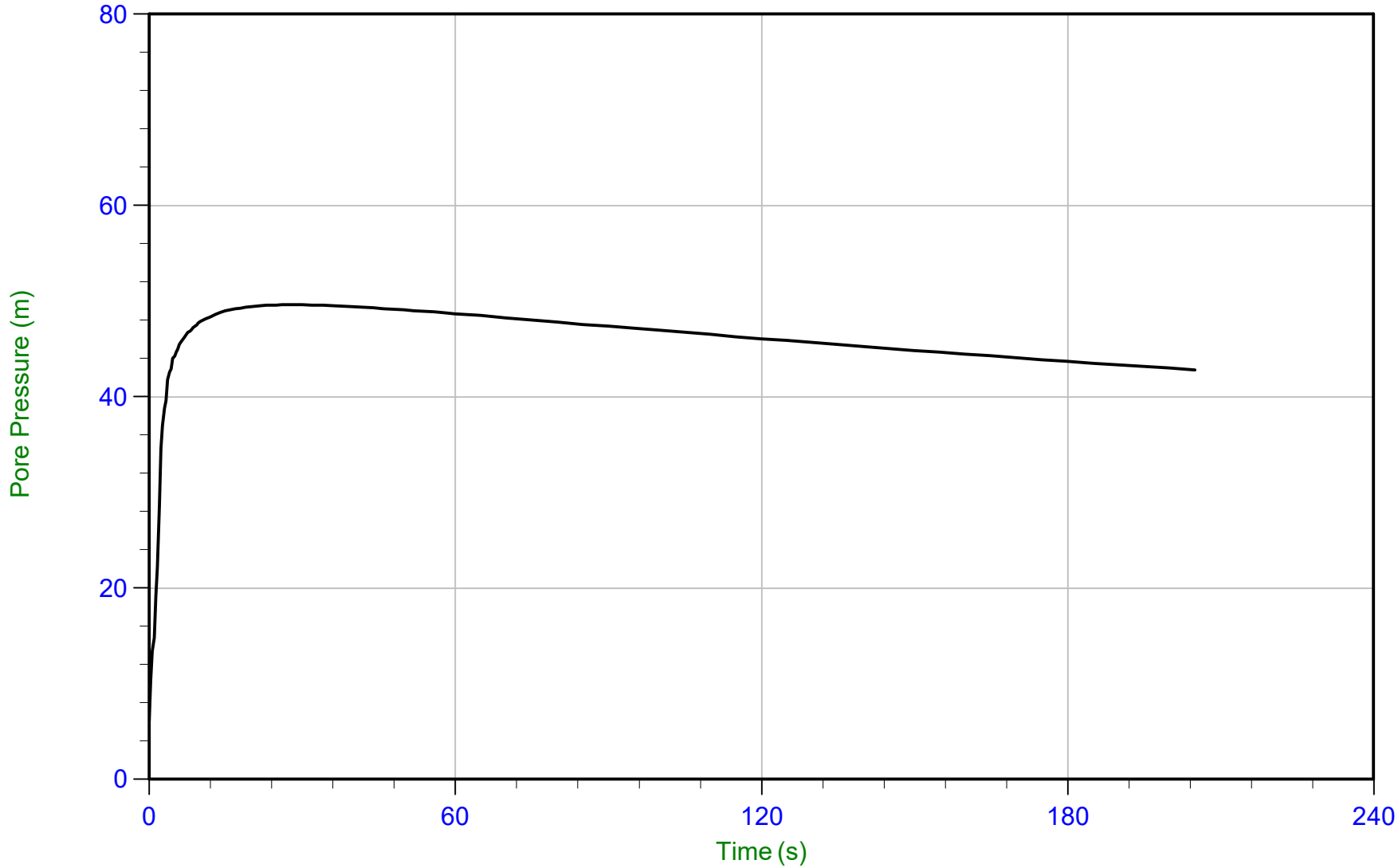
u Min: 33.8 m
u Max: 67.7 m
u Final: 33.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 21.050 m / 69.061 ft
Duration: 205.0 s

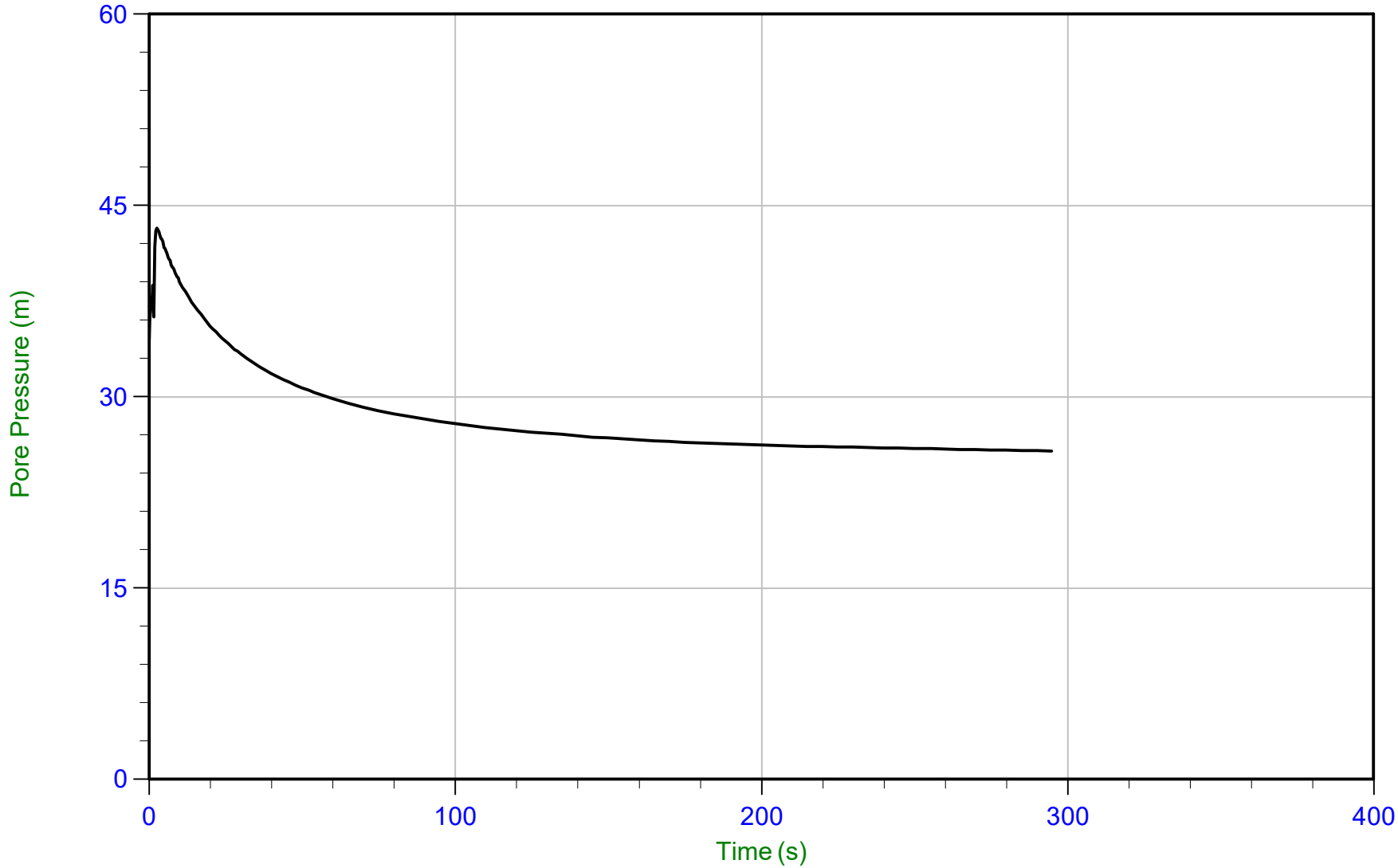
u Min: 6.2 m
u Max: 49.7 m
u Final: 42.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 24.050 m / 78.903 ft
Duration: 295.0 s

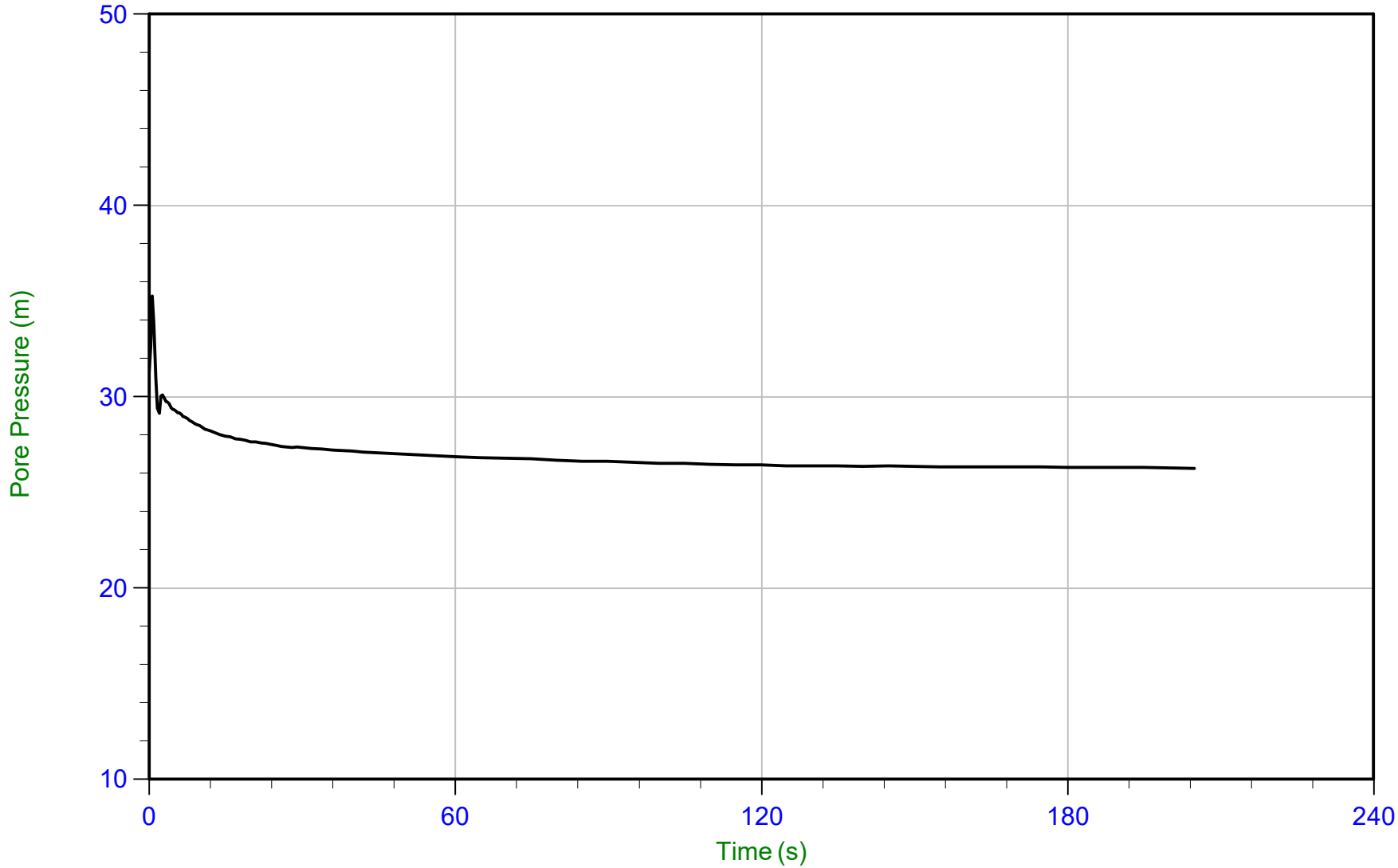
u Min: 25.8 m
u Max: 43.2 m
u Final: 25.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 25.050 m / 82.184 ft
Duration: 205.0 s

u Min: 26.3 m
u Max: 35.3 m
u Final: 26.3 m

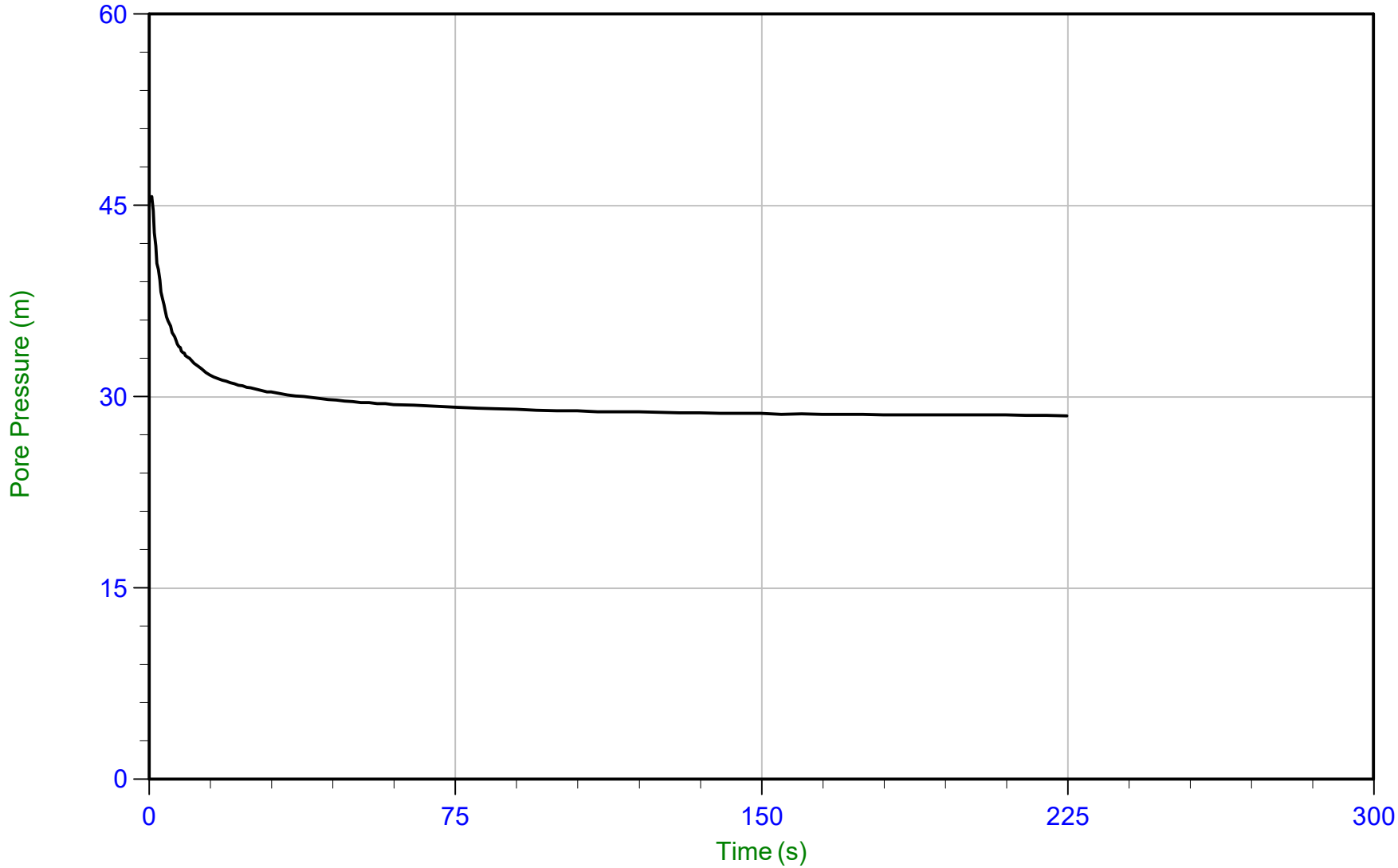
WT: -1.2 m / -4.1 ft
Ueq: 26.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 27.050 m / 88.746 ft
Duration: 225.0 s

u Min: 28.5 m
u Max: 45.7 m
u Final: 28.5 m

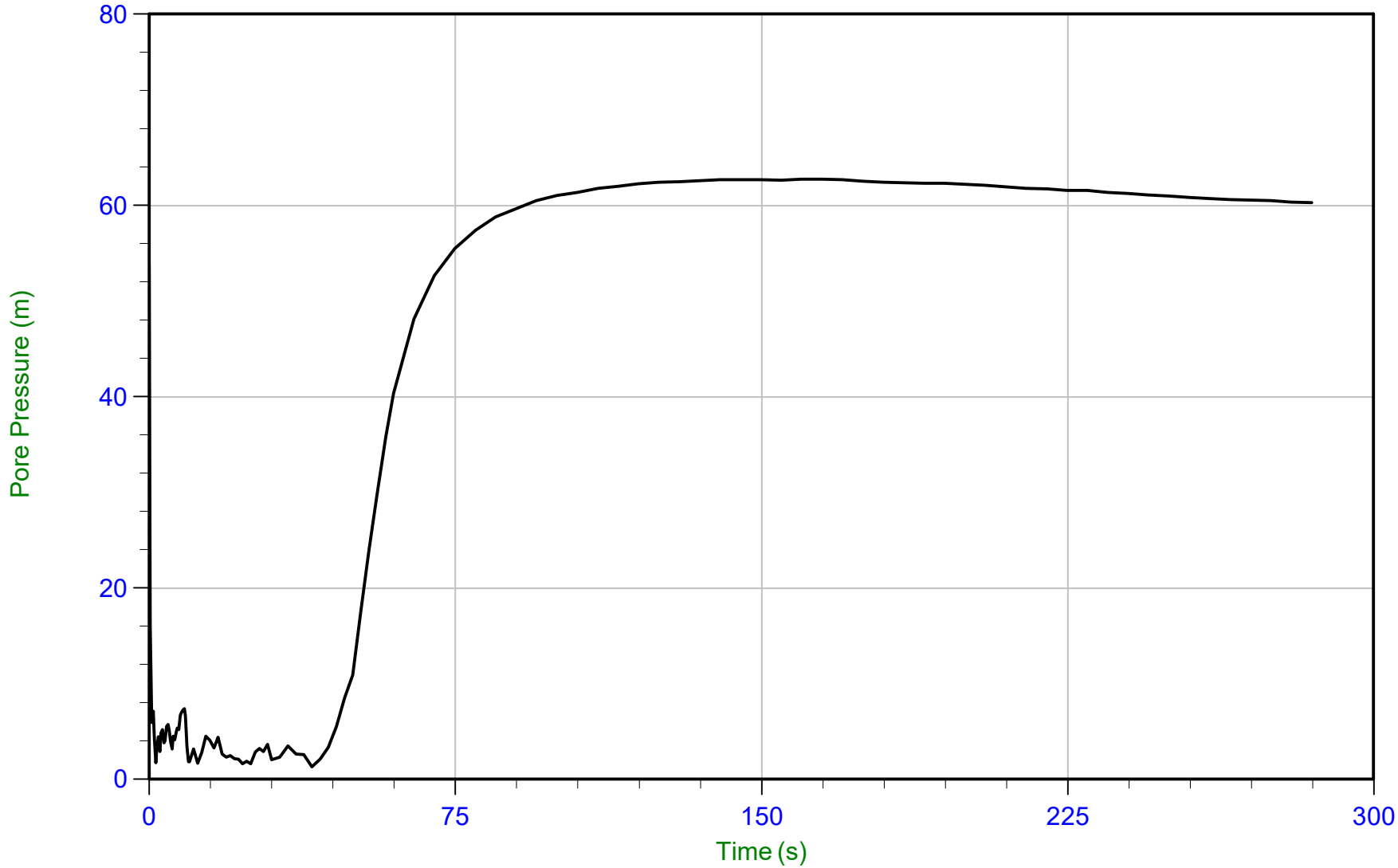
WT: -1.4 m / -4.8 ft
Ueq: 28.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-15 09:39
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH202
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF202.PPF2
Depth: 29.025 m / 95.225 ft
Duration: 285.0 s

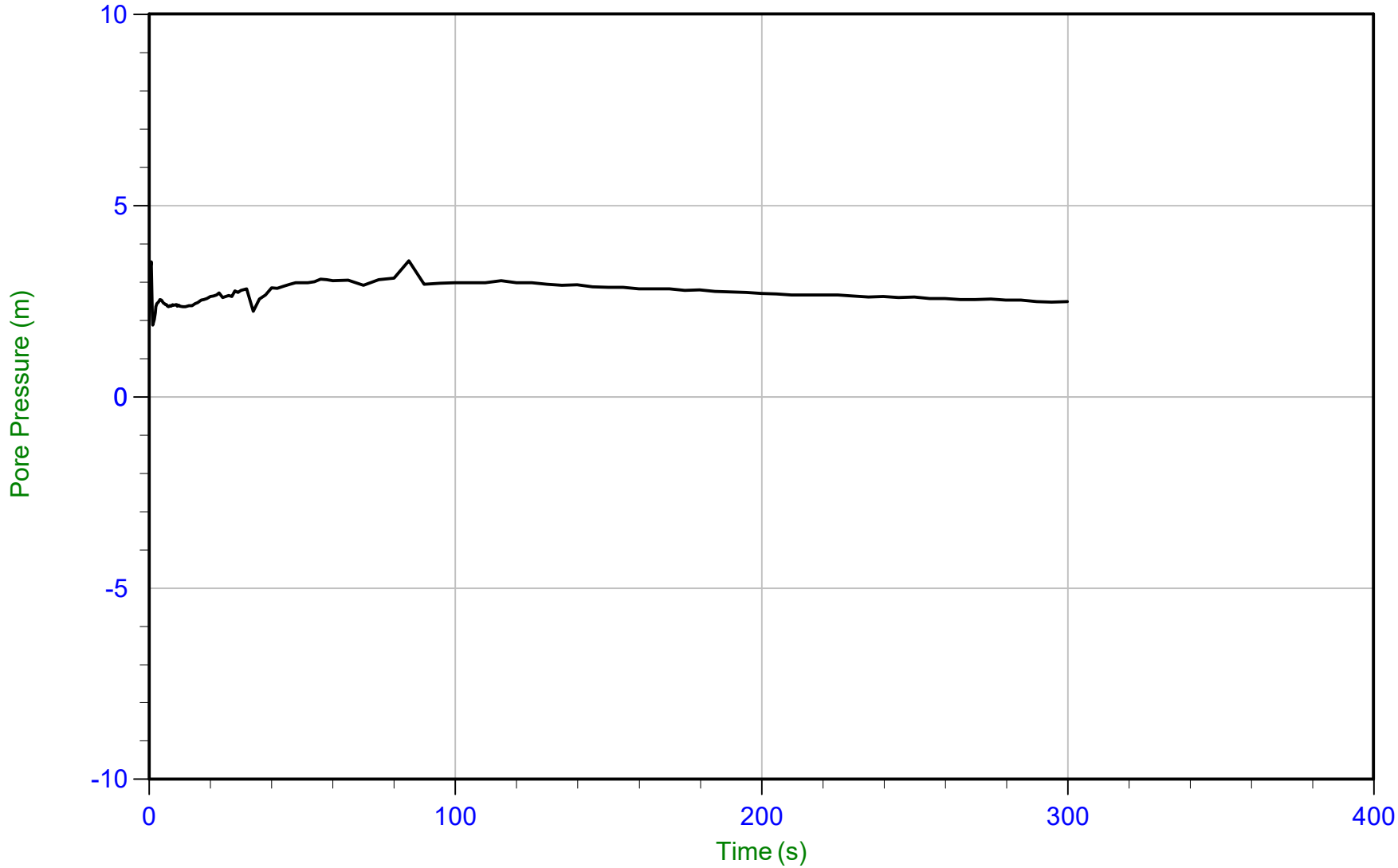
u Min: 1.3 m
u Max: 62.8 m
u Final: 60.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 1.075 m / 3.527 ft
Duration: 300.0 s

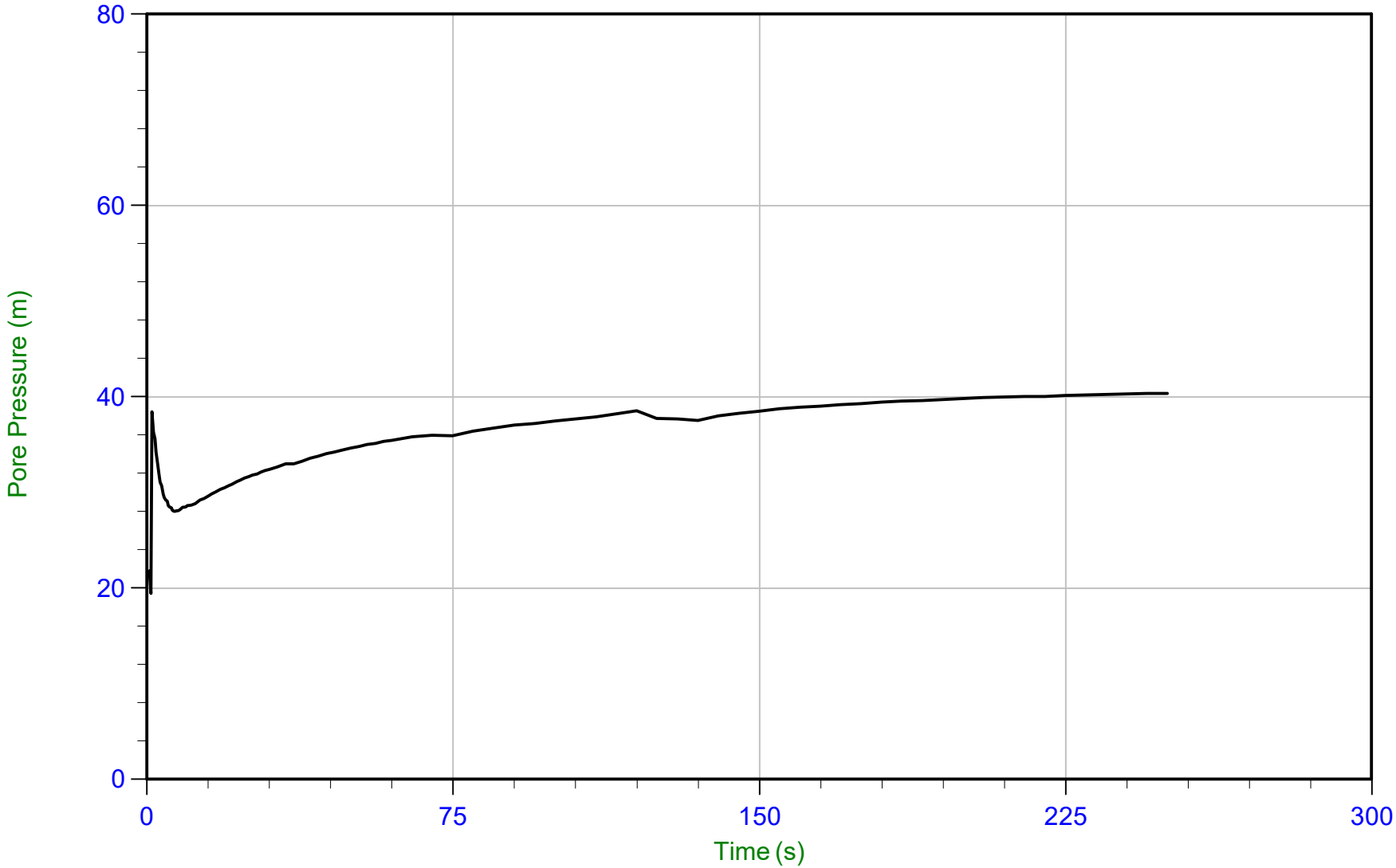
u Min: 1.9 m
u Max: 3.6 m
u Final: 2.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 3.150 m / 10.335 ft
Duration: 250.0 s

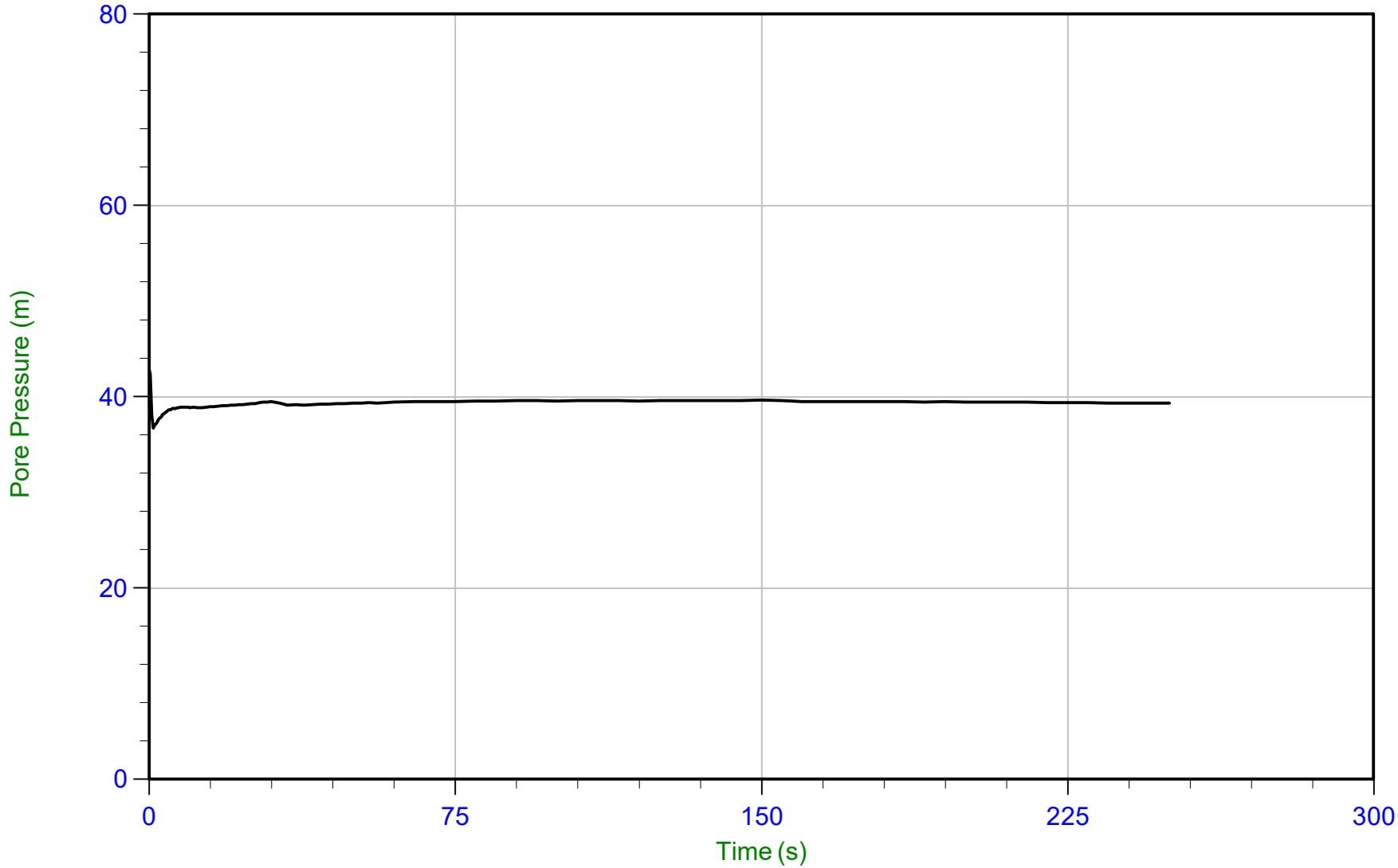
u Min: 19.4 m
u Max: 40.3 m
u Final: 40.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 4.150 m / 13.615 ft
Duration: 250.0 s

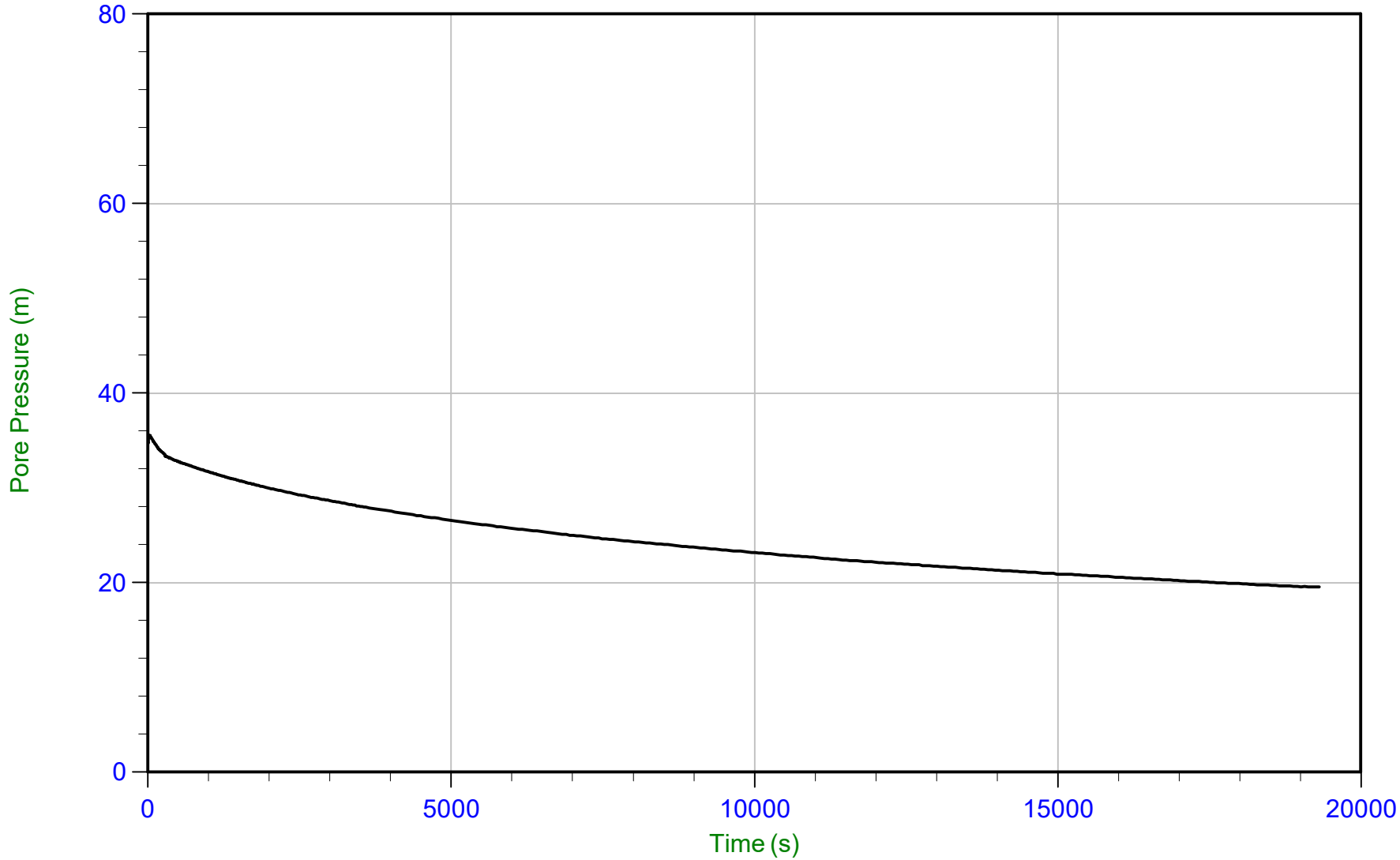
u Min: 36.7 m
u Max: 42.8 m
u Final: 39.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 19320.0 s

u Min: 19.5 m
u Max: 40.2 m
u Final: 19.5 m

WT: -0.8 m / -2.6 ft
Ueq: 8.3 m
U(50): 24.25 m

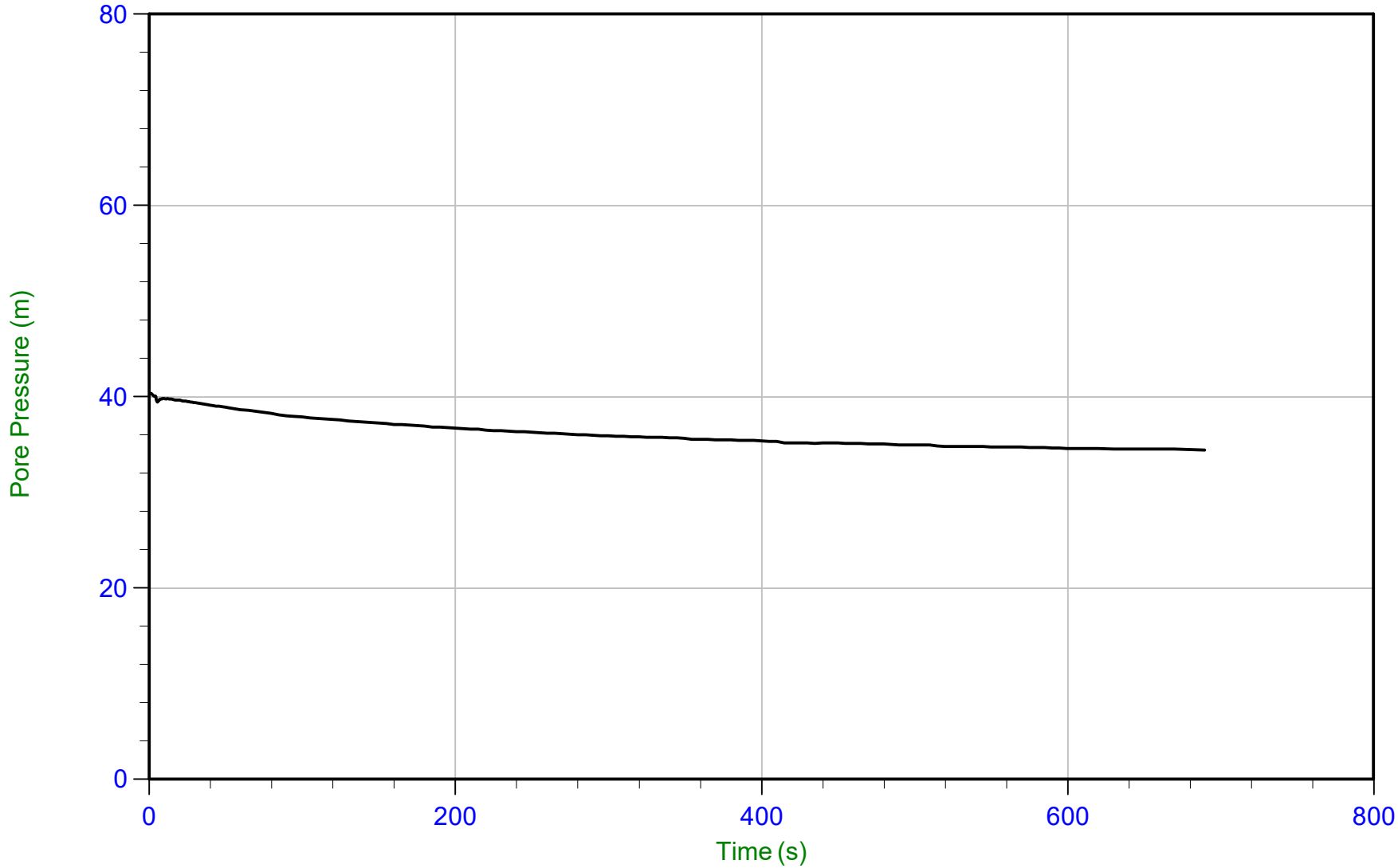
T(50): 8172.4 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 8.250 m / 27.067 ft
Duration: 690.0 s

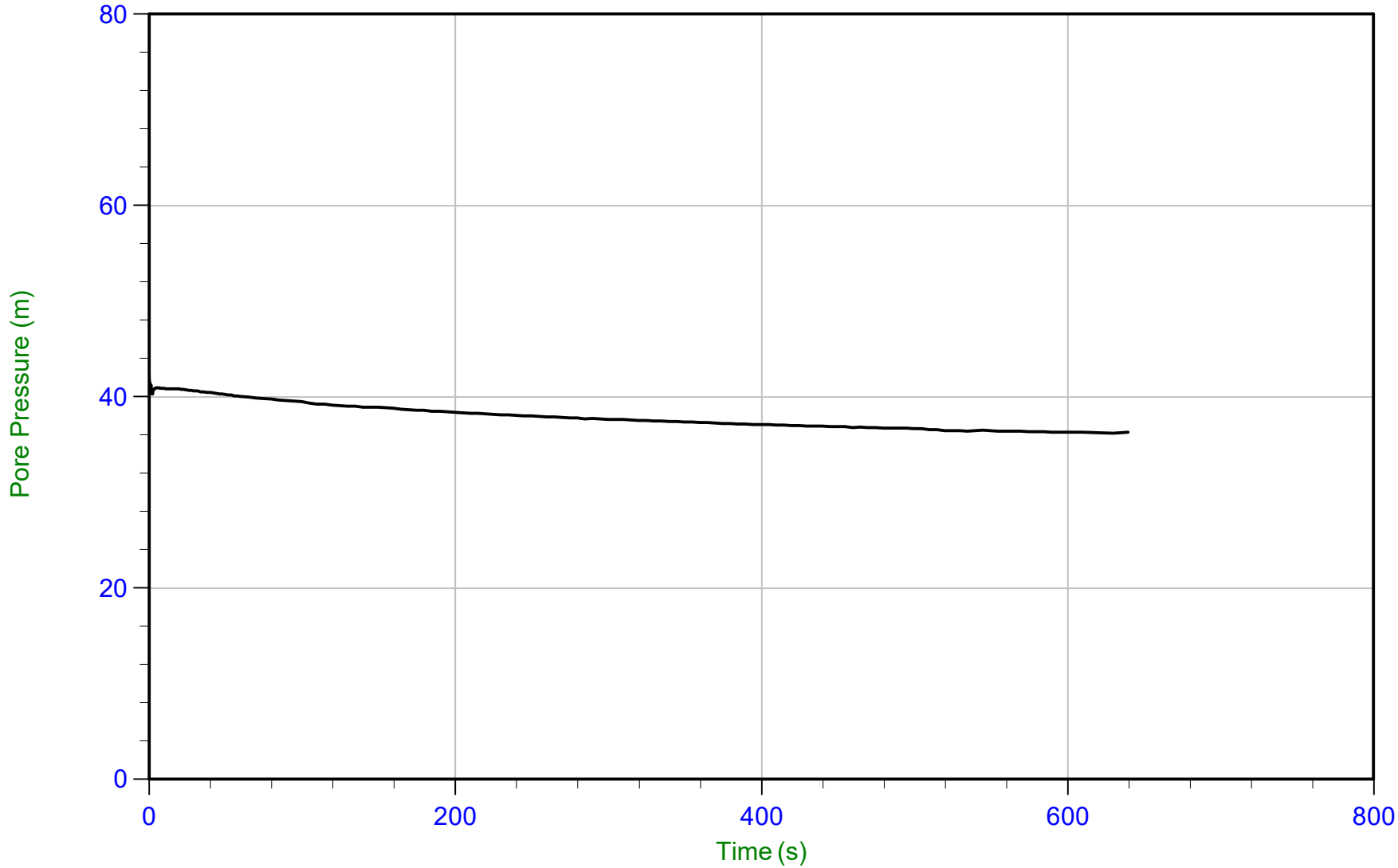
u Min: 34.4 m
u Max: 40.4 m
u Final: 34.4 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 8.750 m / 28.707 ft
Duration: 640.0 s

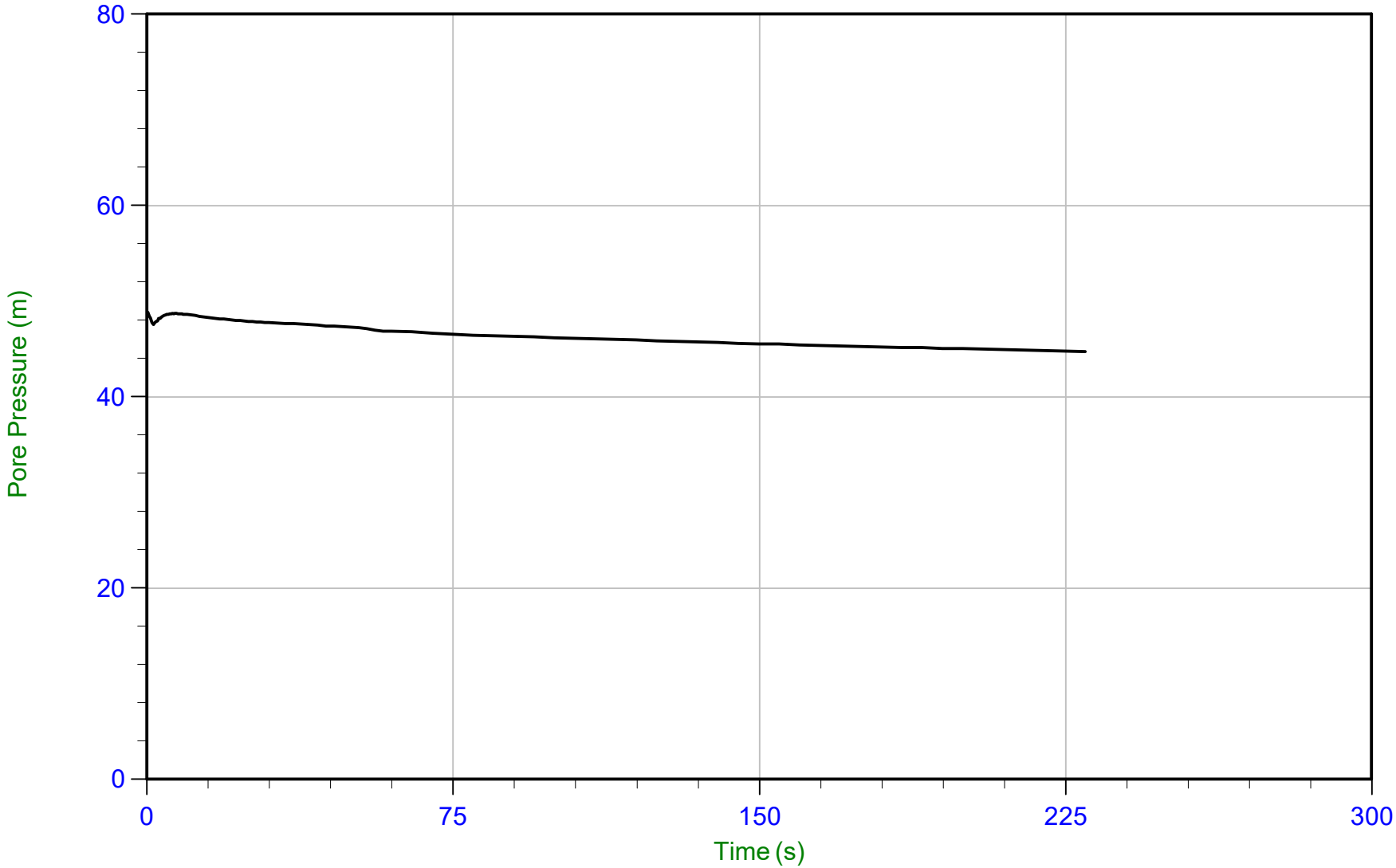
u Min: 36.2 m
u Max: 42.3 m
u Final: 36.3 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 10.125 m / 33.218 ft
Duration: 230.0 s

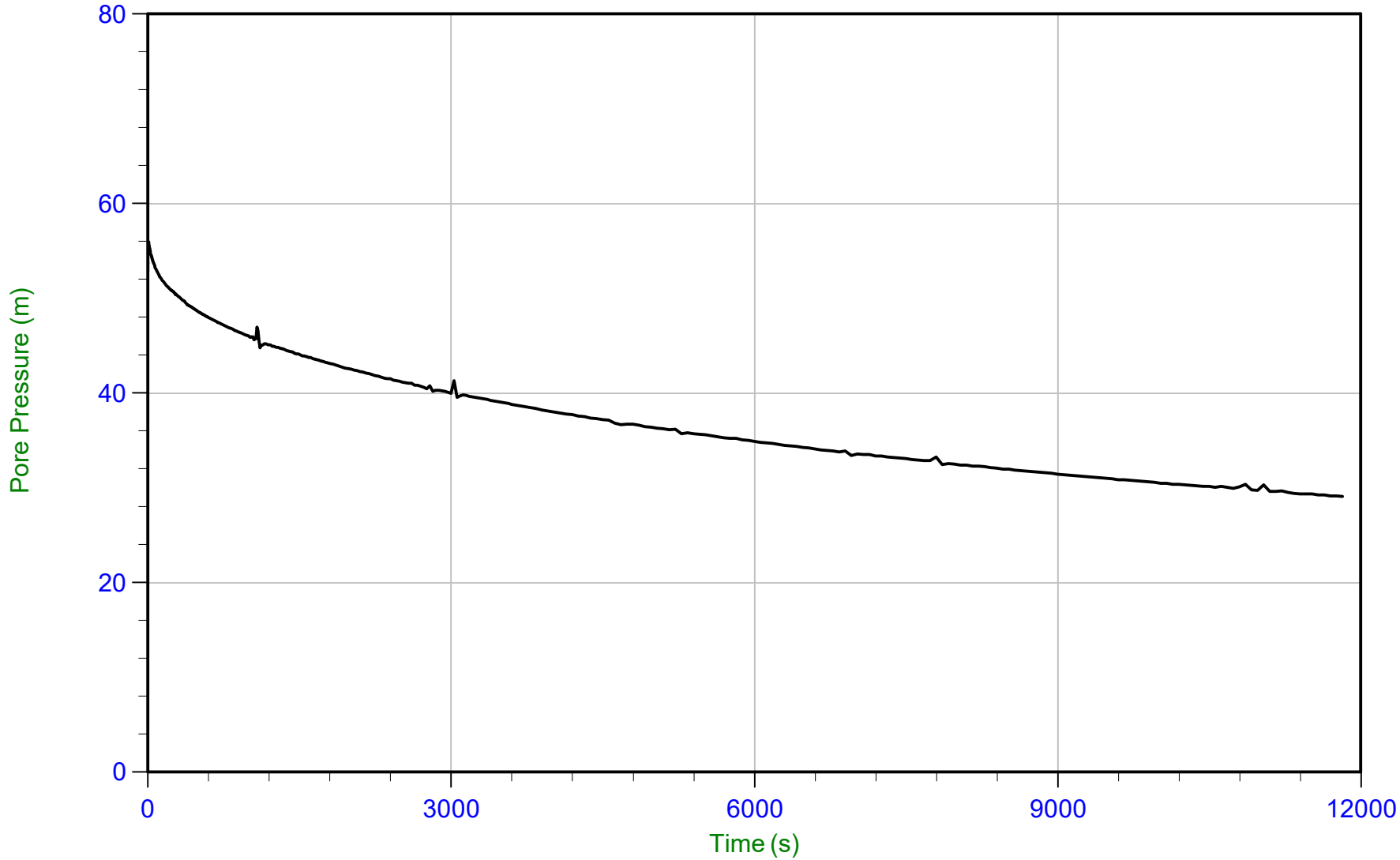
u Min: 44.7 m
u Max: 48.8 m
u Final: 44.7 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 11820.0 s

u Min: 29.1 m
u Max: 55.9 m
u Final: 29.1 m

WT: -0.8 m / -2.6 ft
Ueq: 13.3 m
U(50): 34.62 m

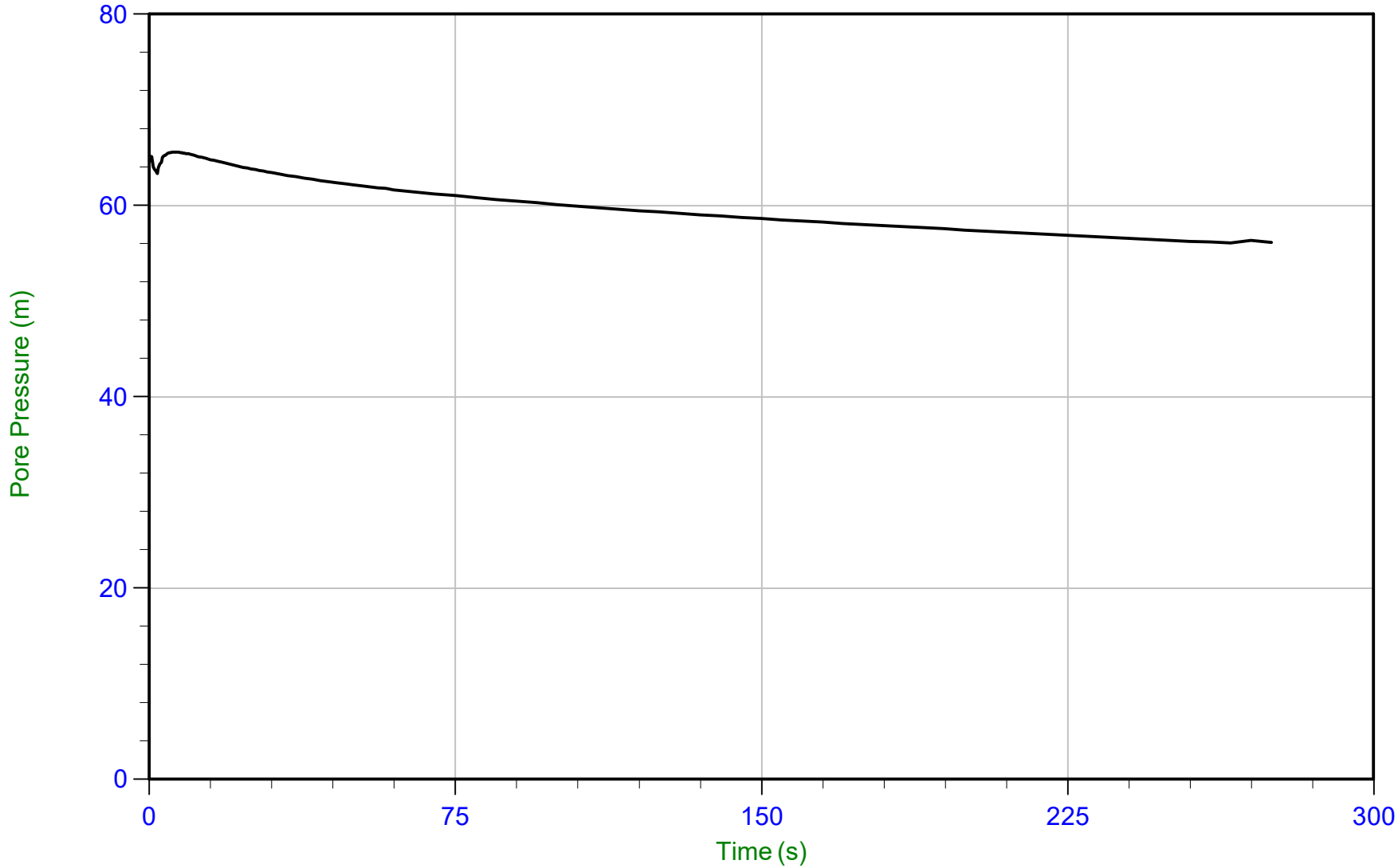
T(50): 6214.5 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 16.125 m / 52.903 ft
Duration: 275.0 s

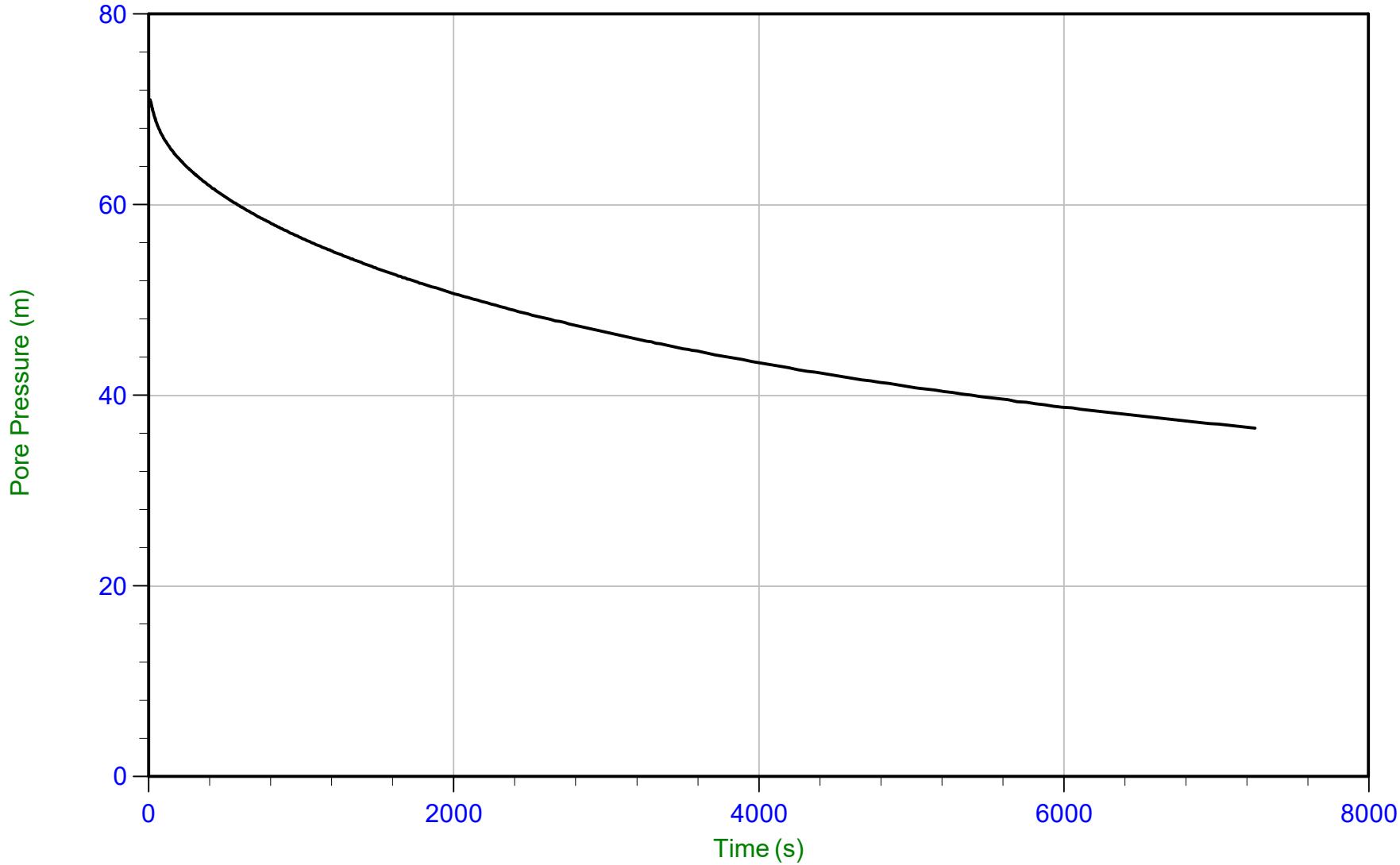
u Min: 56.1 m
u Max: 65.6 m
u Final: 56.2 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 7260.0 s

u Min: 36.6 m
u Max: 74.1 m
u Final: 36.6 m

WT: -0.8 m / -2.6 ft
Ueq: 18.3 m
U(50): 46.21 m

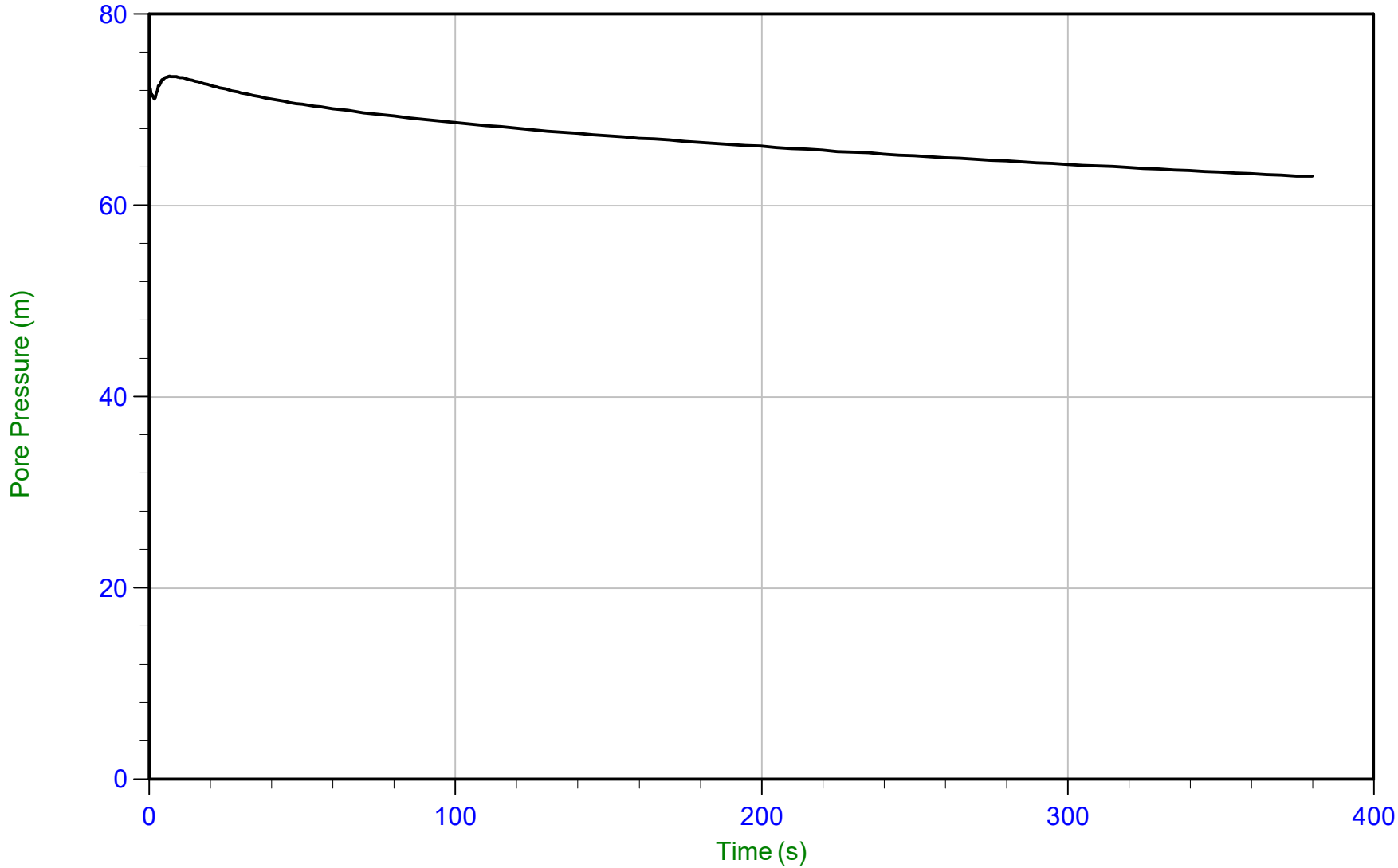
T(50): 3121.6 s
Ir: 100
Ch: 0.2 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 18.125 m / 59.465 ft
Duration: 380.0 s

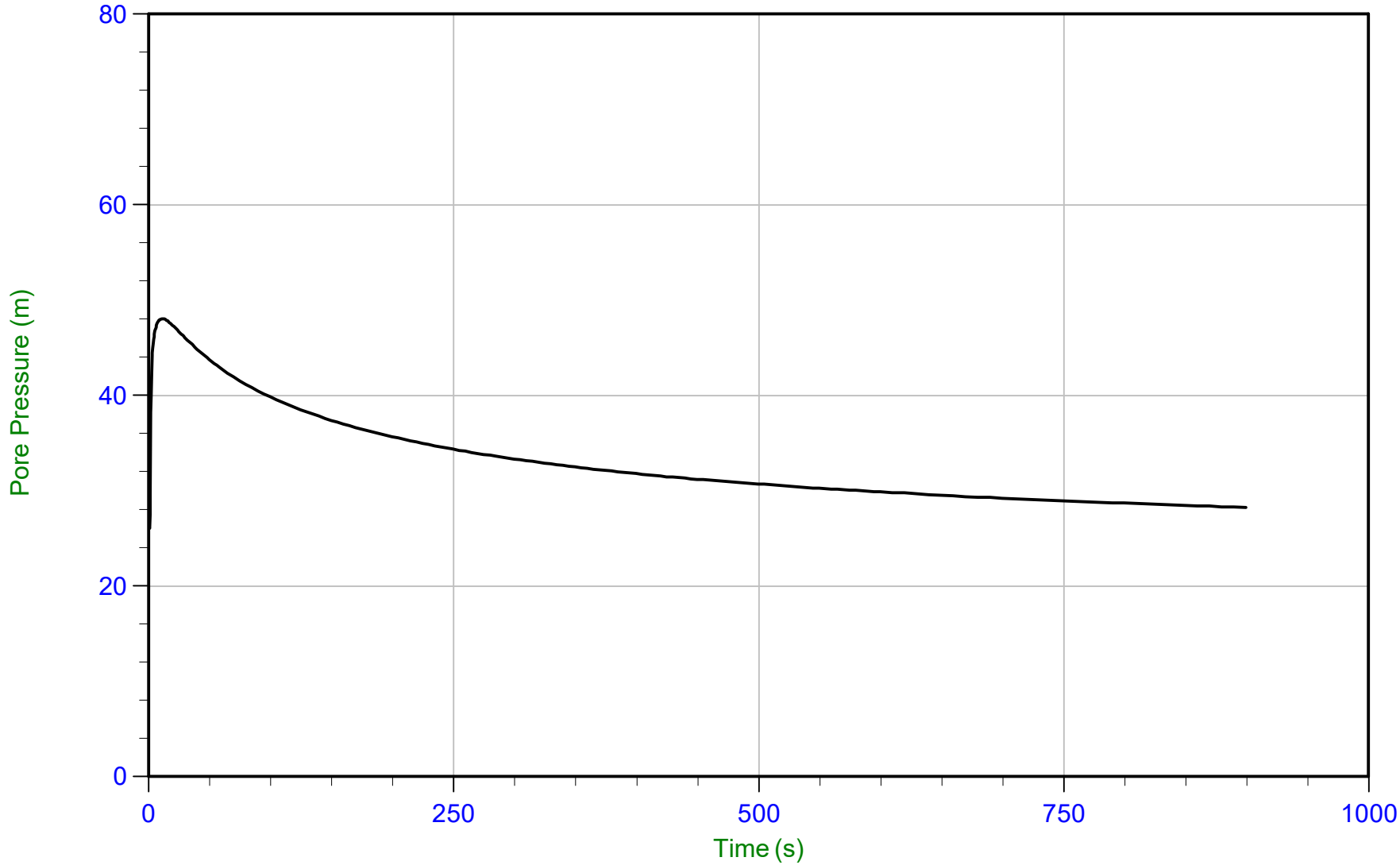
u Min: 63.1 m
u Max: 73.5 m
u Final: 63.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 22.500 m / 73.818 ft
Duration: 900.0 s

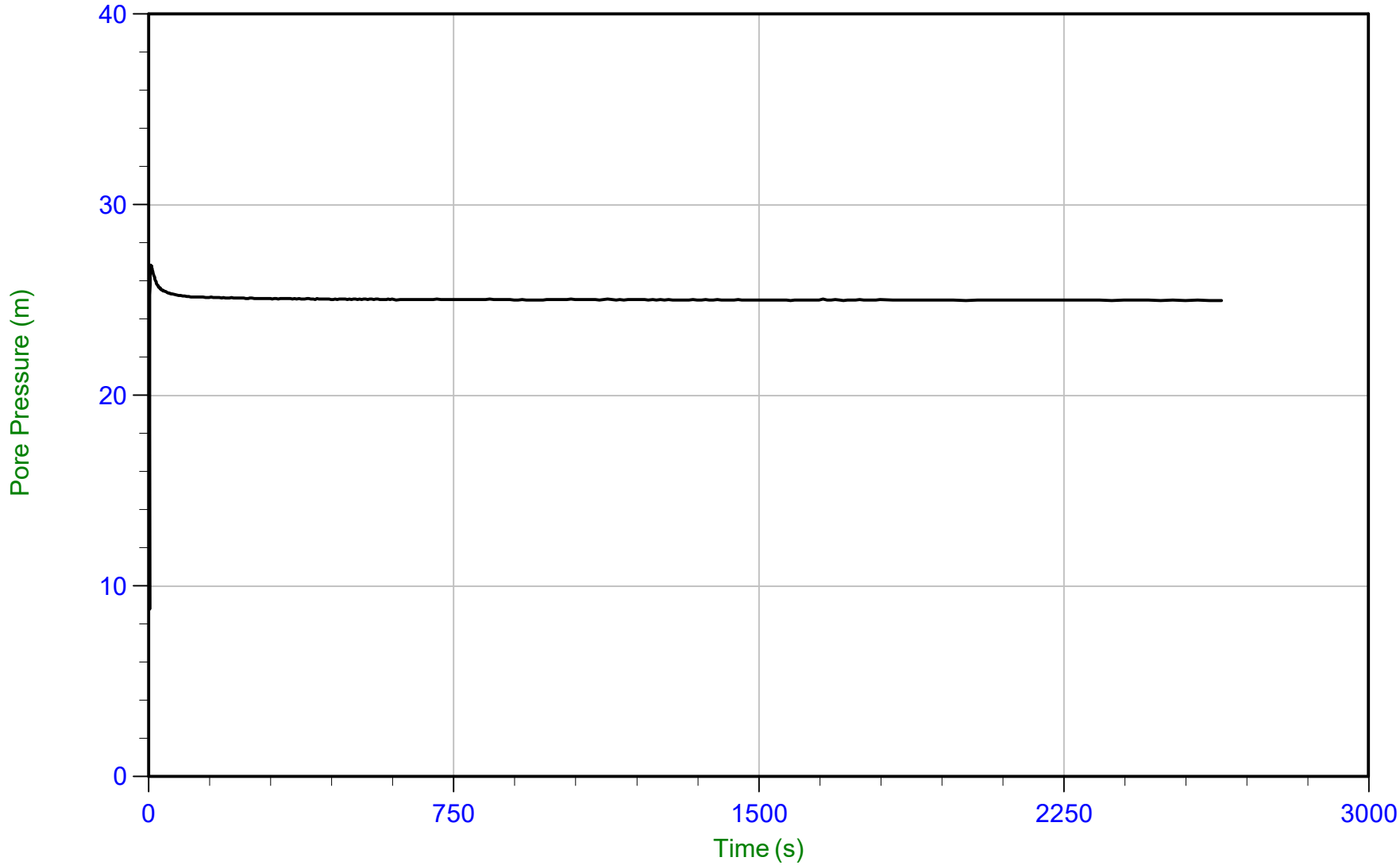
u Min: 26.1 m
u Max: 48.0 m
u Final: 28.2 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-18 13:44
Site: Crawford Mine - SRK

Sounding: SCPT24-TMF-BH207
Cone: 762:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPTMF207.PPF2
Depth: 24.175 m / 79.313 ft
Duration: 2640.0 s

u Min: 8.8 m
u Max: 26.8 m
u Final: 25.0 m

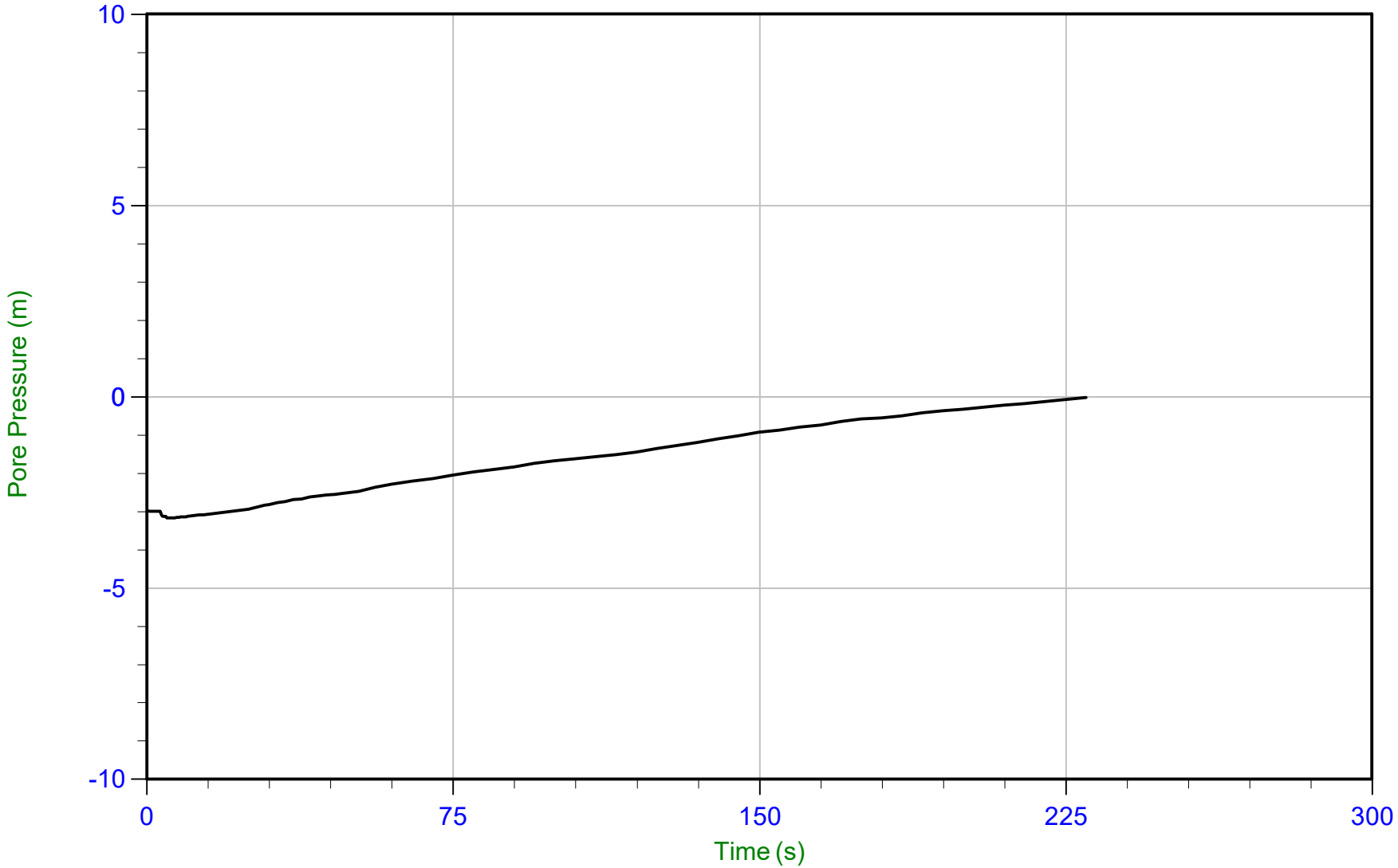
WT: -0.8 m / -2.7 ft
Ueq: 25.0 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 3.000 m / 9.842 ft
Duration: 230.0 s

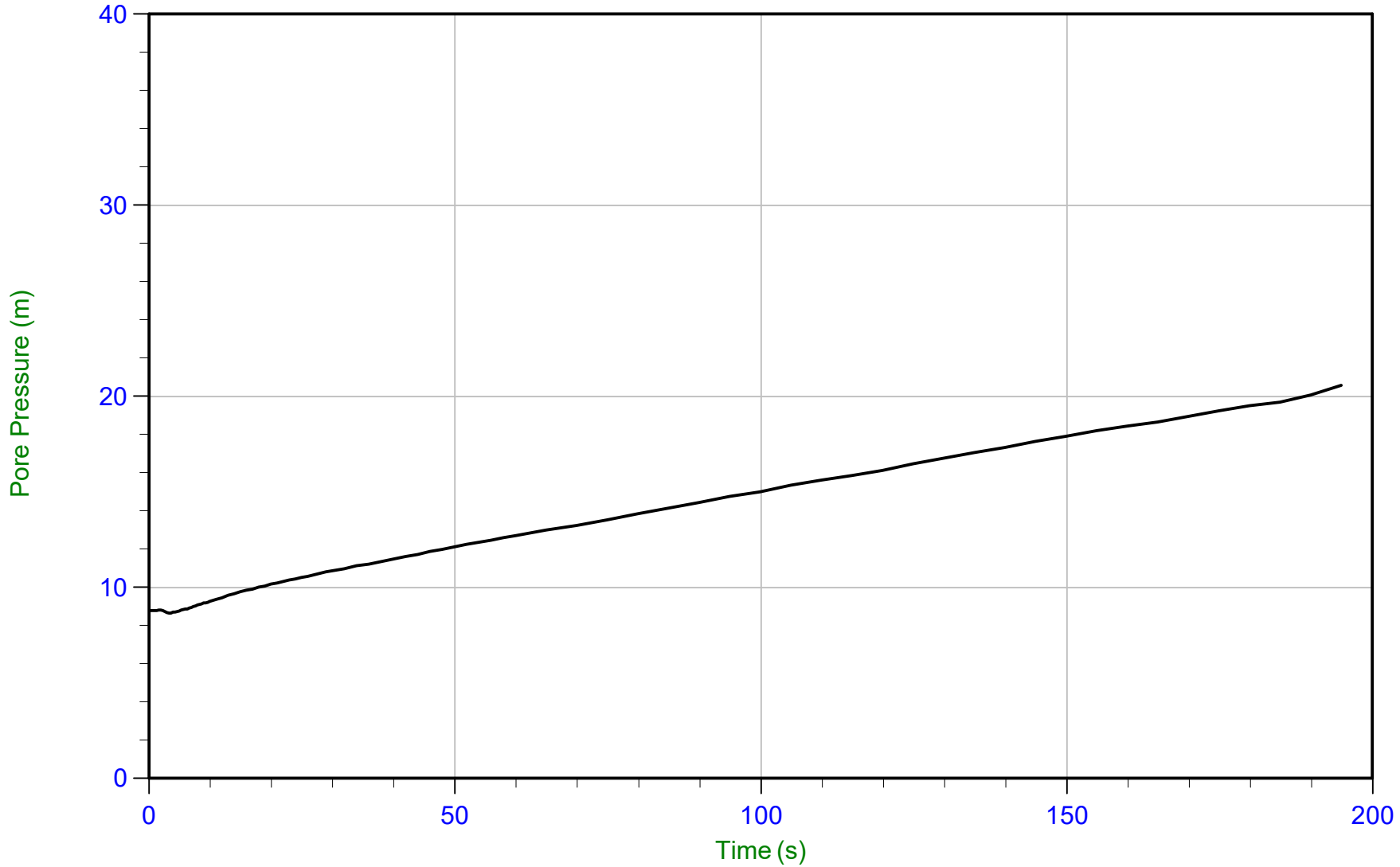
u Min: -3.2 m
u Max: -0.0 m
u Final: -0.0 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 5.000 m / 16.404 ft
Duration: 195.0 s

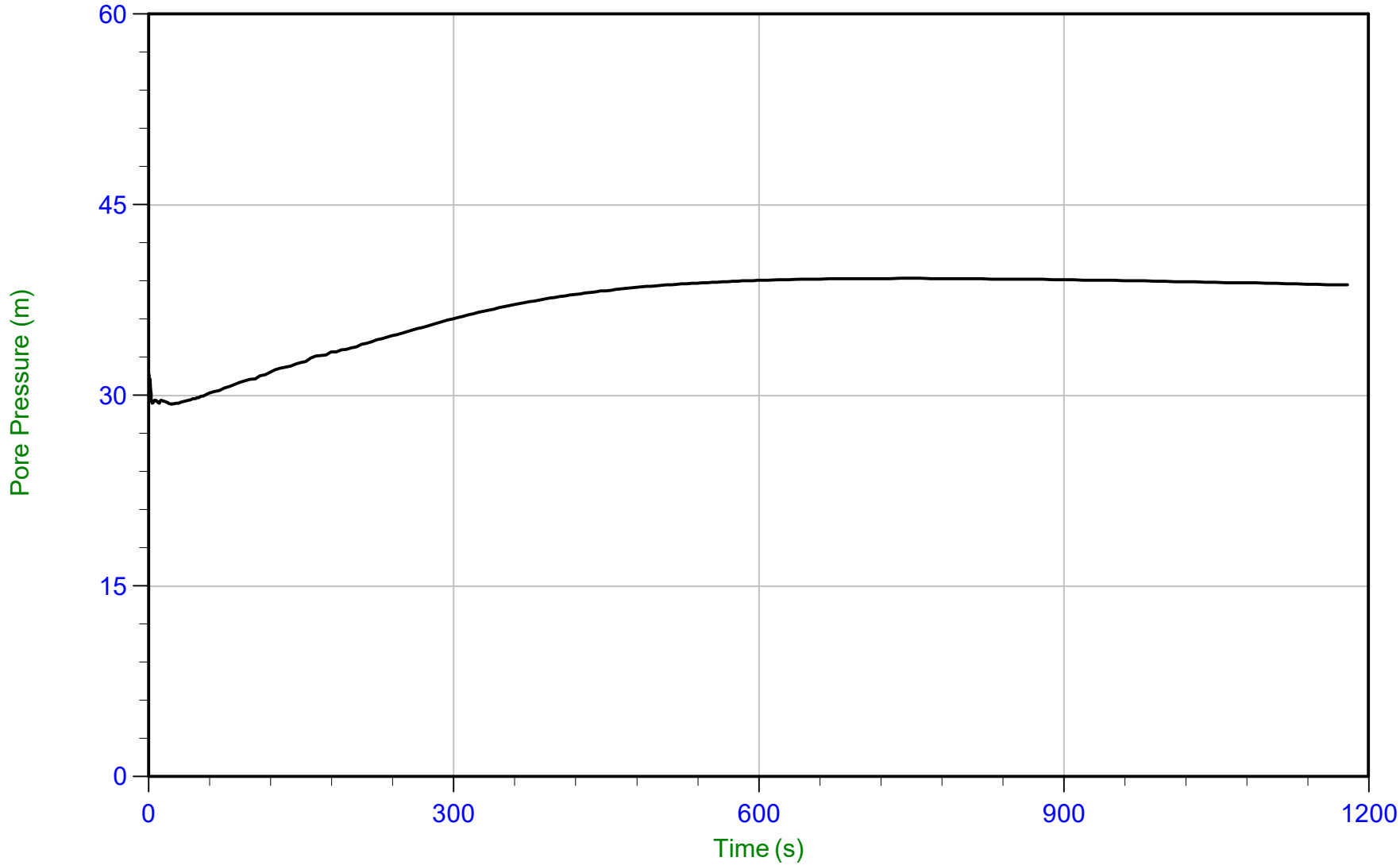
u Min: 8.7 m
u Max: 20.6 m
u Final: 20.6 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 6.000 m / 19.685 ft
Duration: 1180.0 s

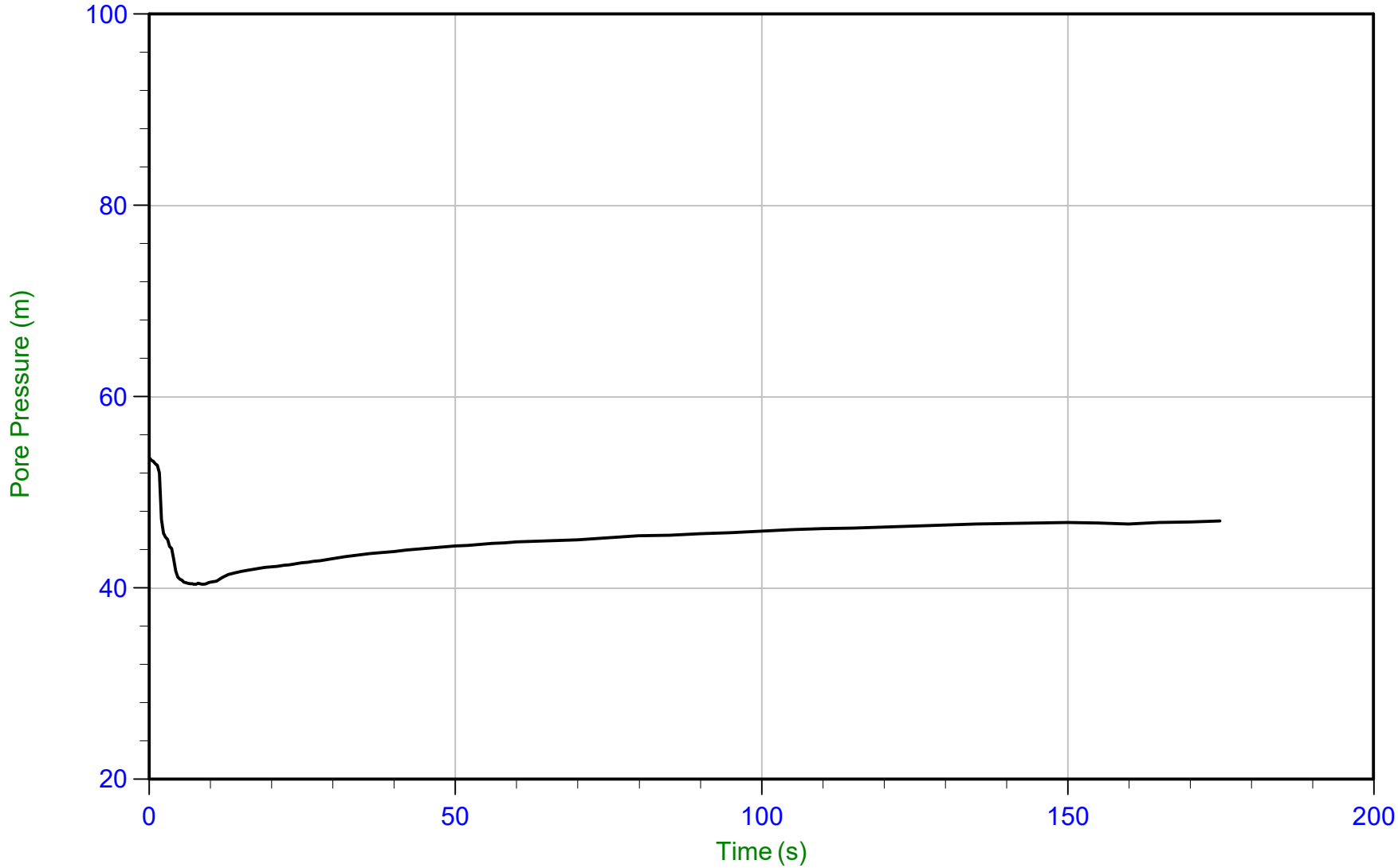
u Min: 29.3 m
u Max: 39.2 m
u Final: 38.7 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 7.000 m / 22.966 ft
Duration: 175.0 s

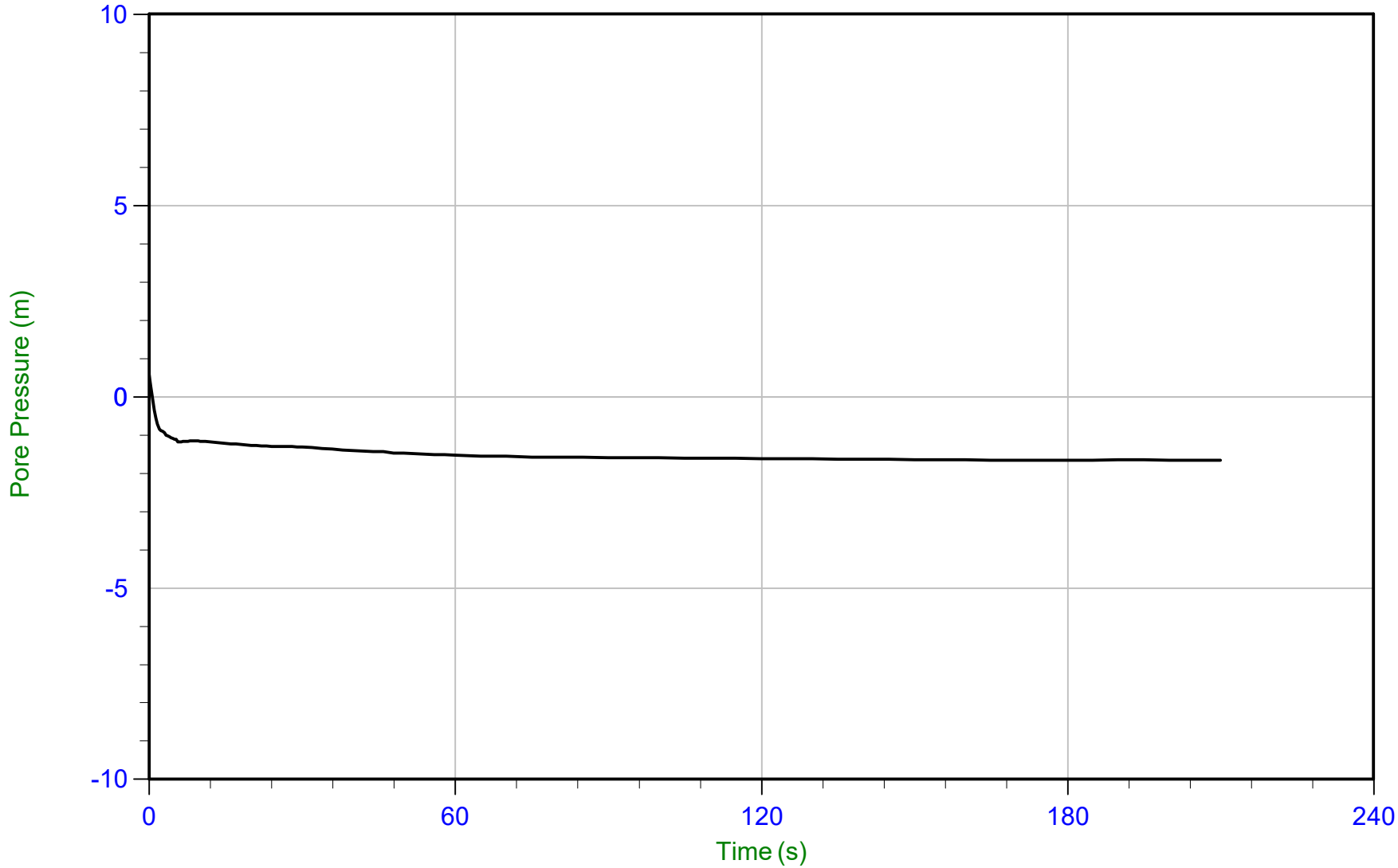
u Min: 40.4 m
u Max: 53.6 m
u Final: 47.0 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 210.0 s

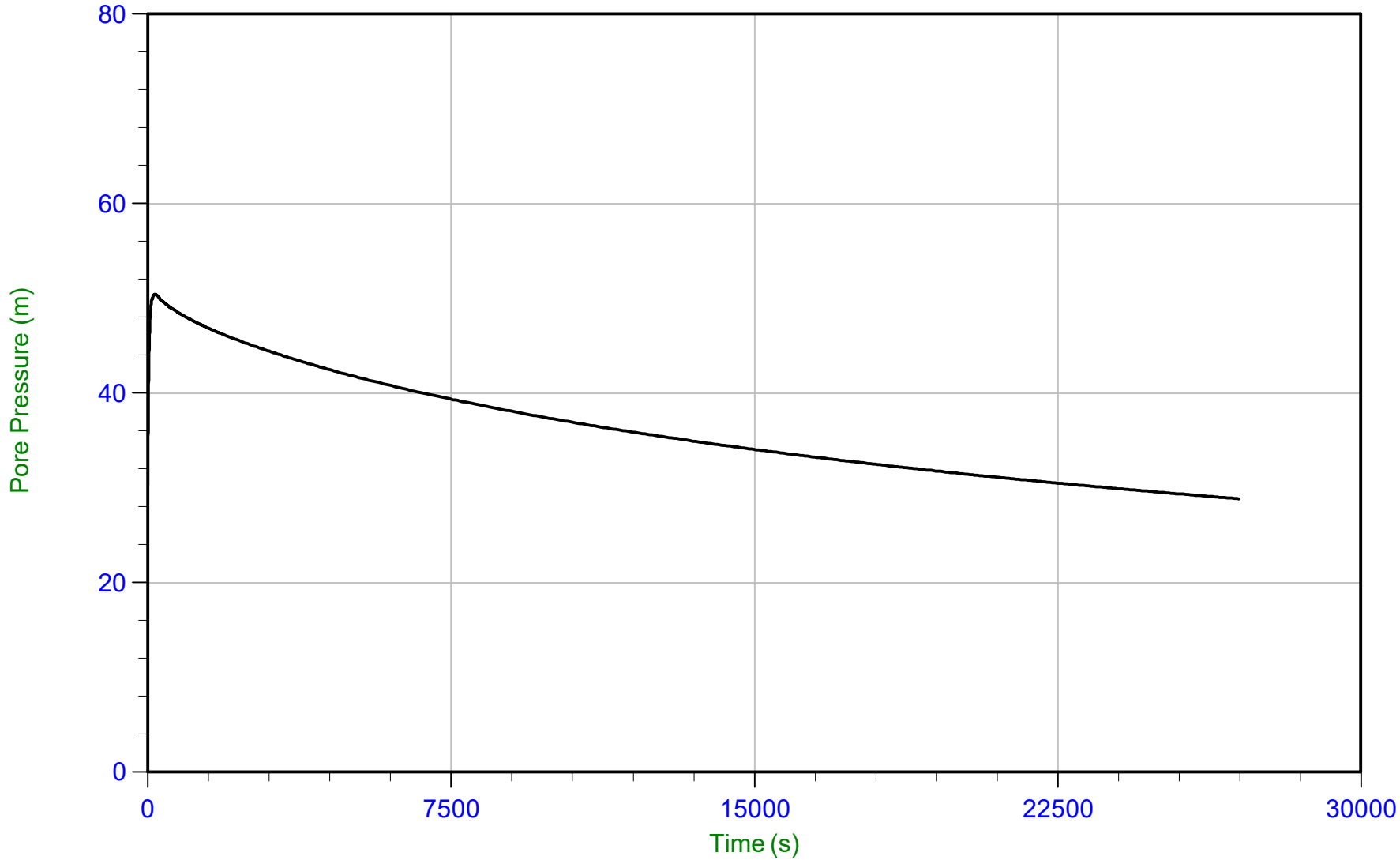
u Min: -1.7 m
u Max: 0.6 m
u Final: -1.7 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 9.225 m / 30.265 ft
Duration: 27000.0 s

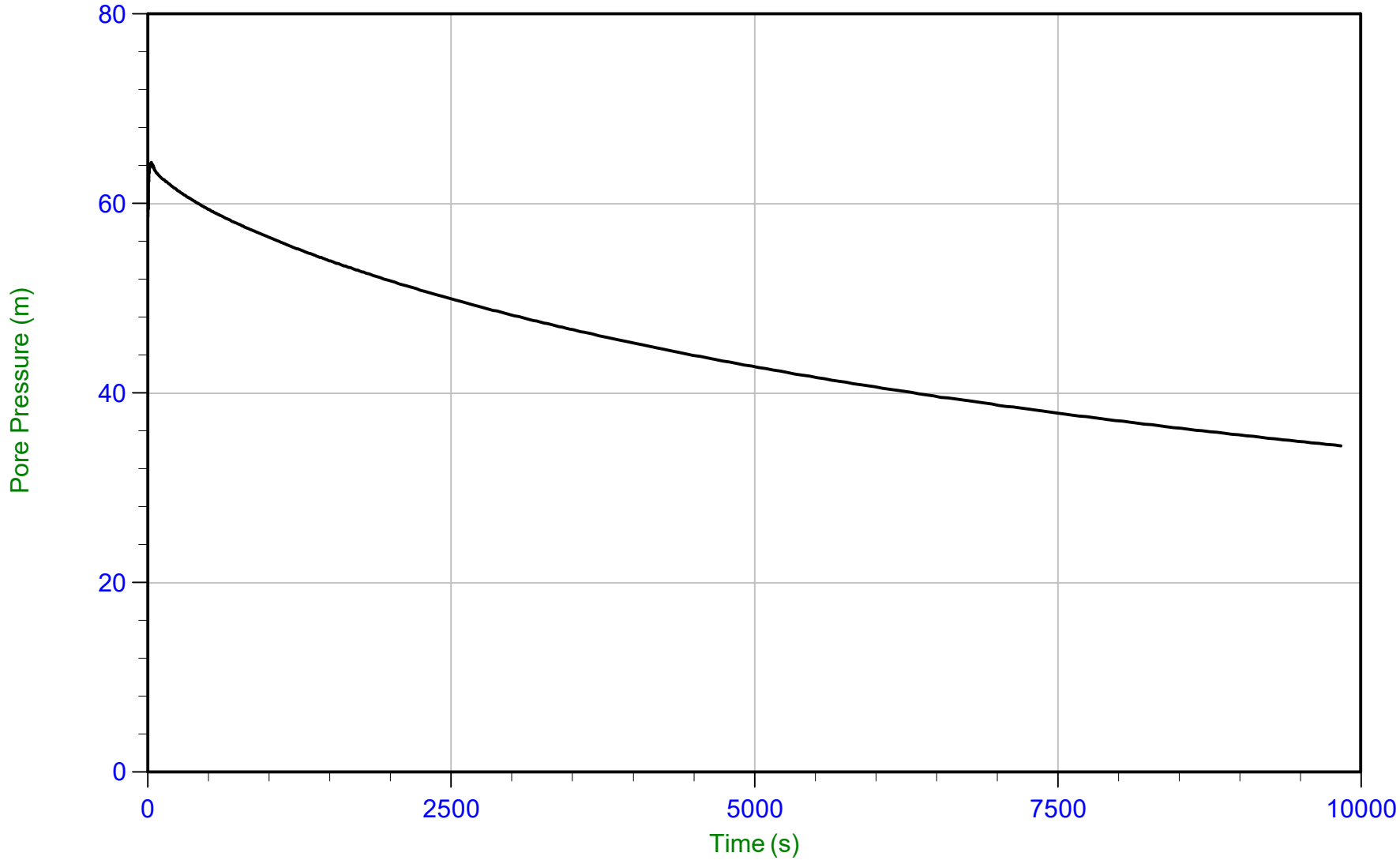
u Min: 28.8 m
u Max: 50.4 m
u Final: 28.8 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 9840.0 s

u Min: 34.4 m
u Max: 64.3 m
u Final: 34.4 m

WT: 7.0 m / 23.0 ft
Ueq: 5.5 m
U(50): 34.91 m

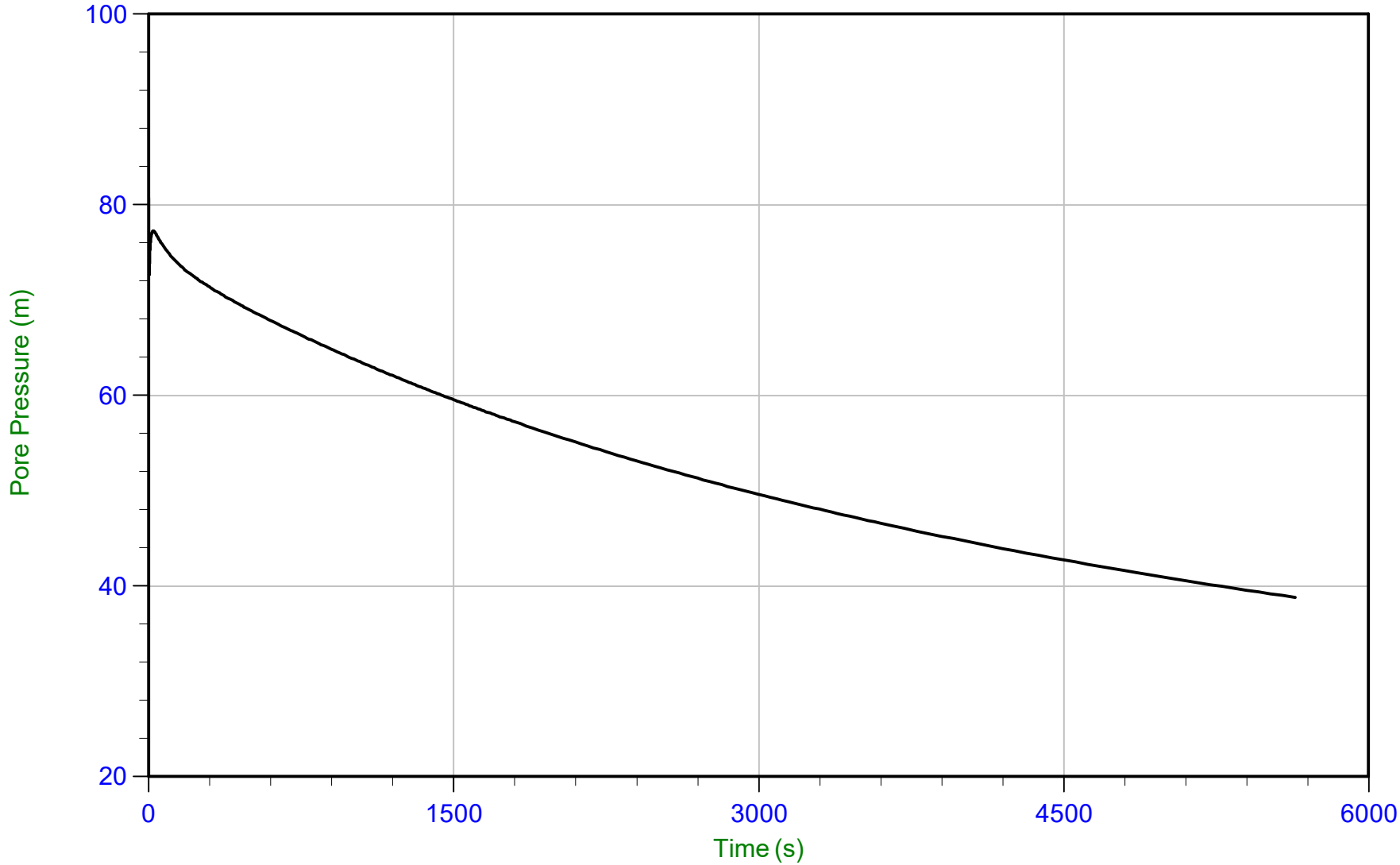
T(50): 9451.4 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 5640.0 s

u Min: 38.8 m
u Max: 80.7 m
u Final: 38.8 m

WT: 7.0 m / 23.0 ft
Ueq: 10.5 m
U(50): 45.60 m

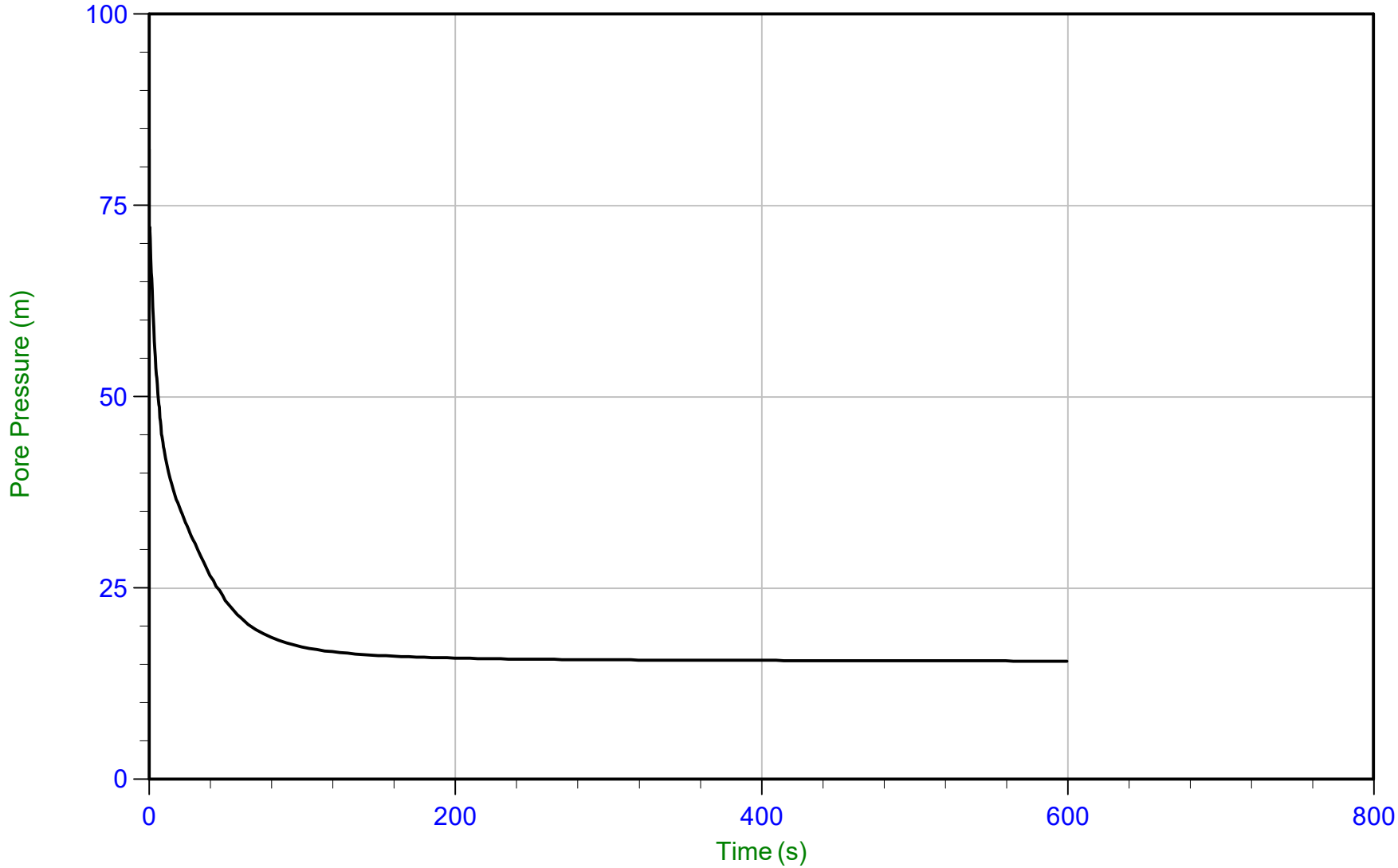
T(50): 3814.4 s
Ir: 100
Ch: 0.2 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 22.500 m / 73.818 ft
Duration: 600.0 s

u Min: 15.5 m
u Max: 82.3 m
u Final: 15.5 m

WT: 7.0 m / 23.0 ft
Ueq: 15.5 m
U(50): 48.92 m

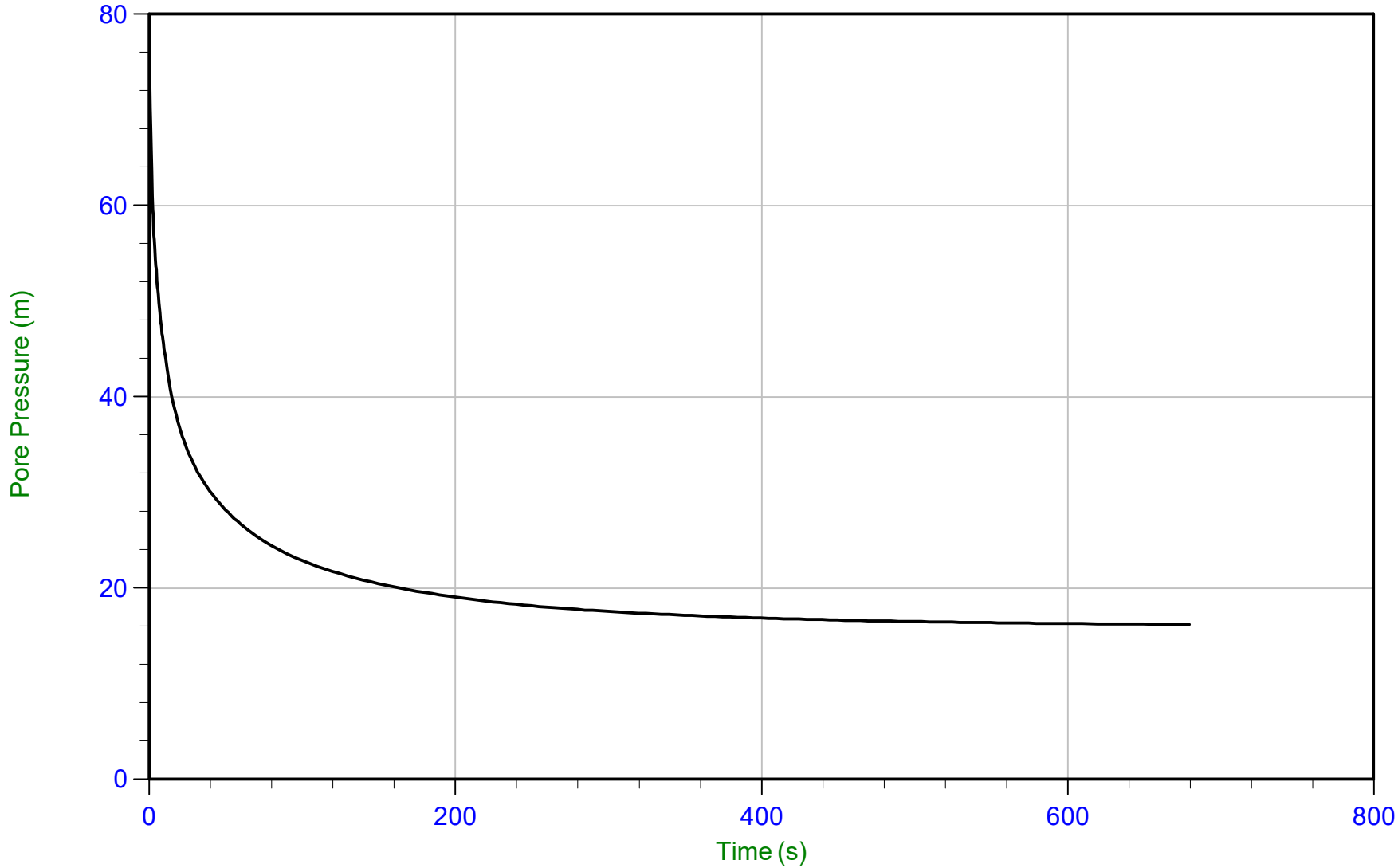
T(50): 6.7 s
Ir: 100
Ch: 105.0 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 22.800 m / 74.802 ft
Duration: 680.0 s

u Min: 16.2 m
u Max: 78.6 m
u Final: 16.2 m

WT: 7.0 m / 23.0 ft
Ueq: 15.8 m
U(50): 47.18 m

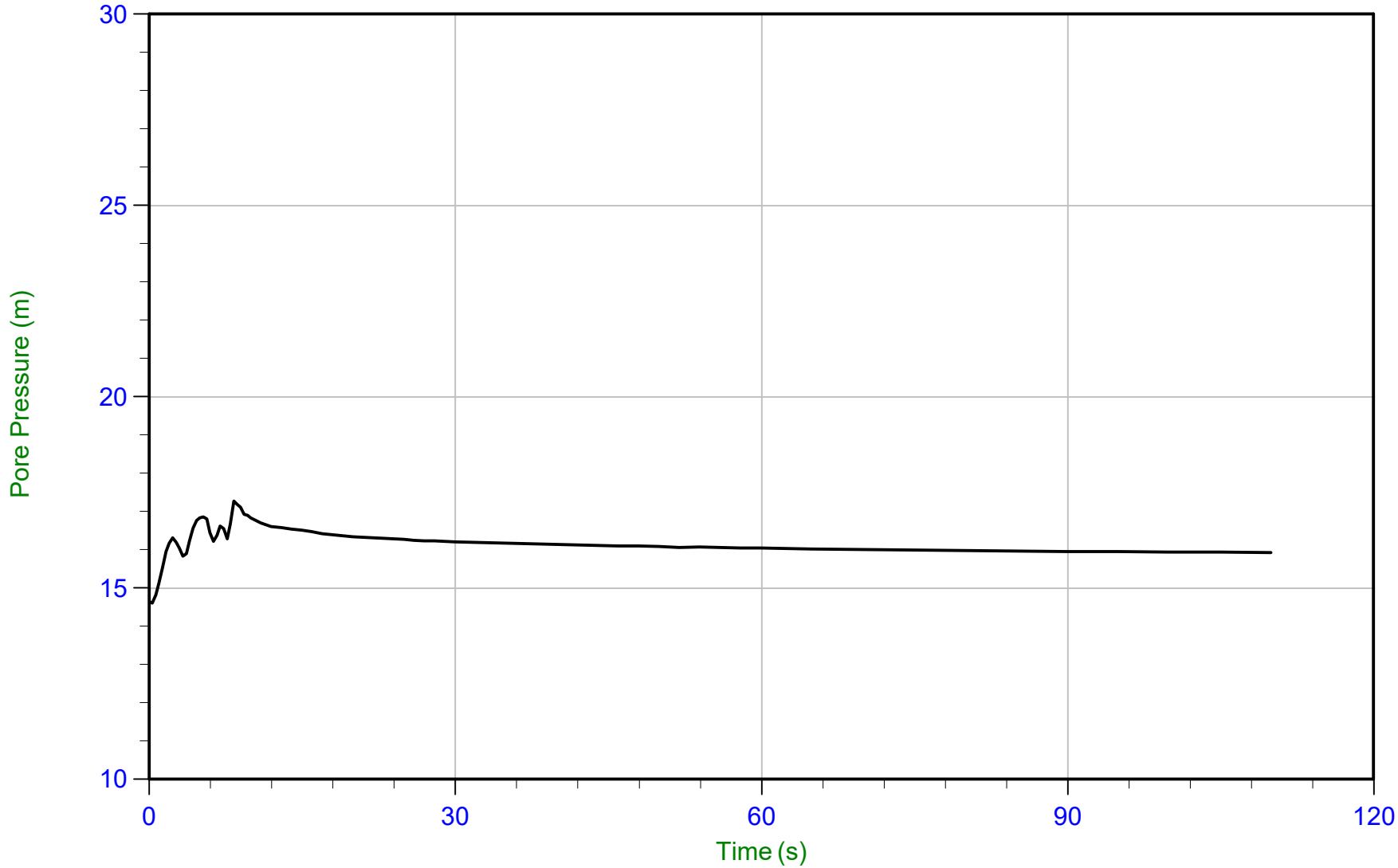
T(50): 8.4 s
Ir: 100
Ch: 83.7 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-01 10:18
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH201
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD201.PPF2
Depth: 23.125 m / 75.868 ft
Duration: 110.0 s

u Min: 14.6 m
u Max: 17.3 m
u Final: 15.9 m

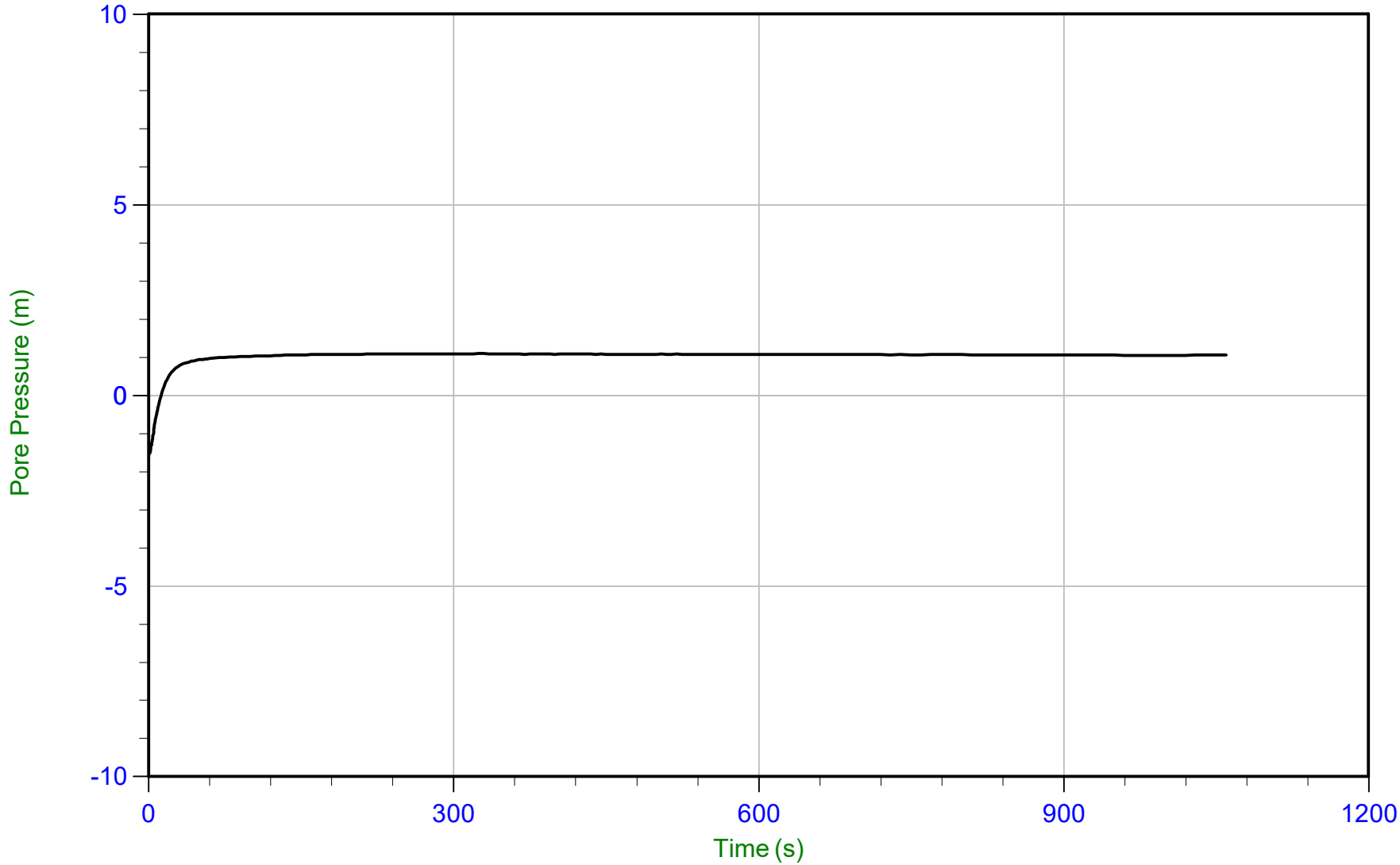
WT: 7.2 m / 23.7 ft
Ueq: 15.9 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD202.PPF2
Depth: 1.000 m / 3.281 ft
Duration: 1060.0 s

u Min: -1.6 m
u Max: 1.1 m
u Final: 1.1 m

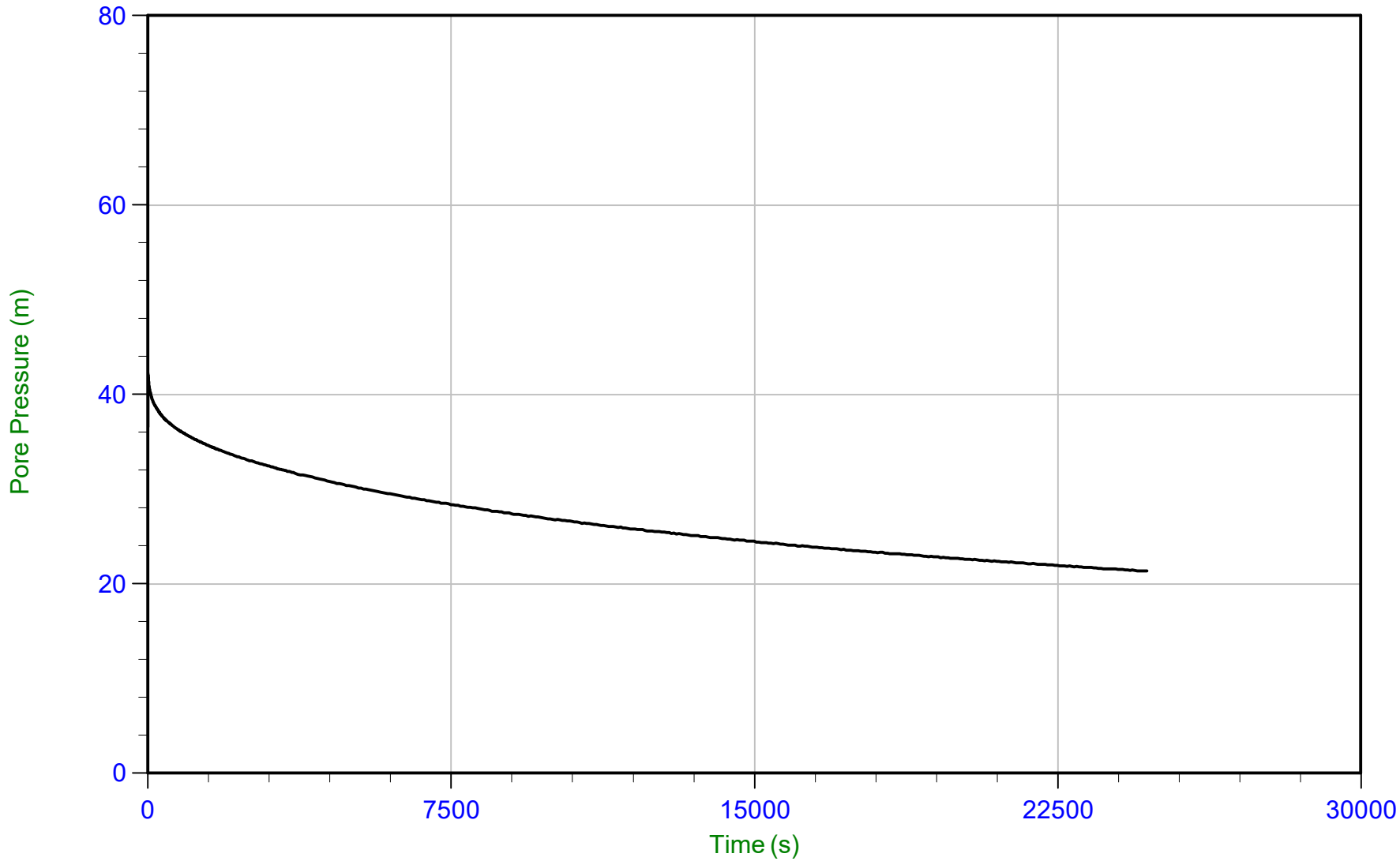
WT: -0.1 m / -0.3 ft
Ueq: 1.1 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD202.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 24720.0 s

u Min: 21.4 m
u Max: 42.2 m
u Final: 21.4 m

WT: -0.1 m / -0.3 ft
Ueq: 7.6 m
U(50): 24.92 m

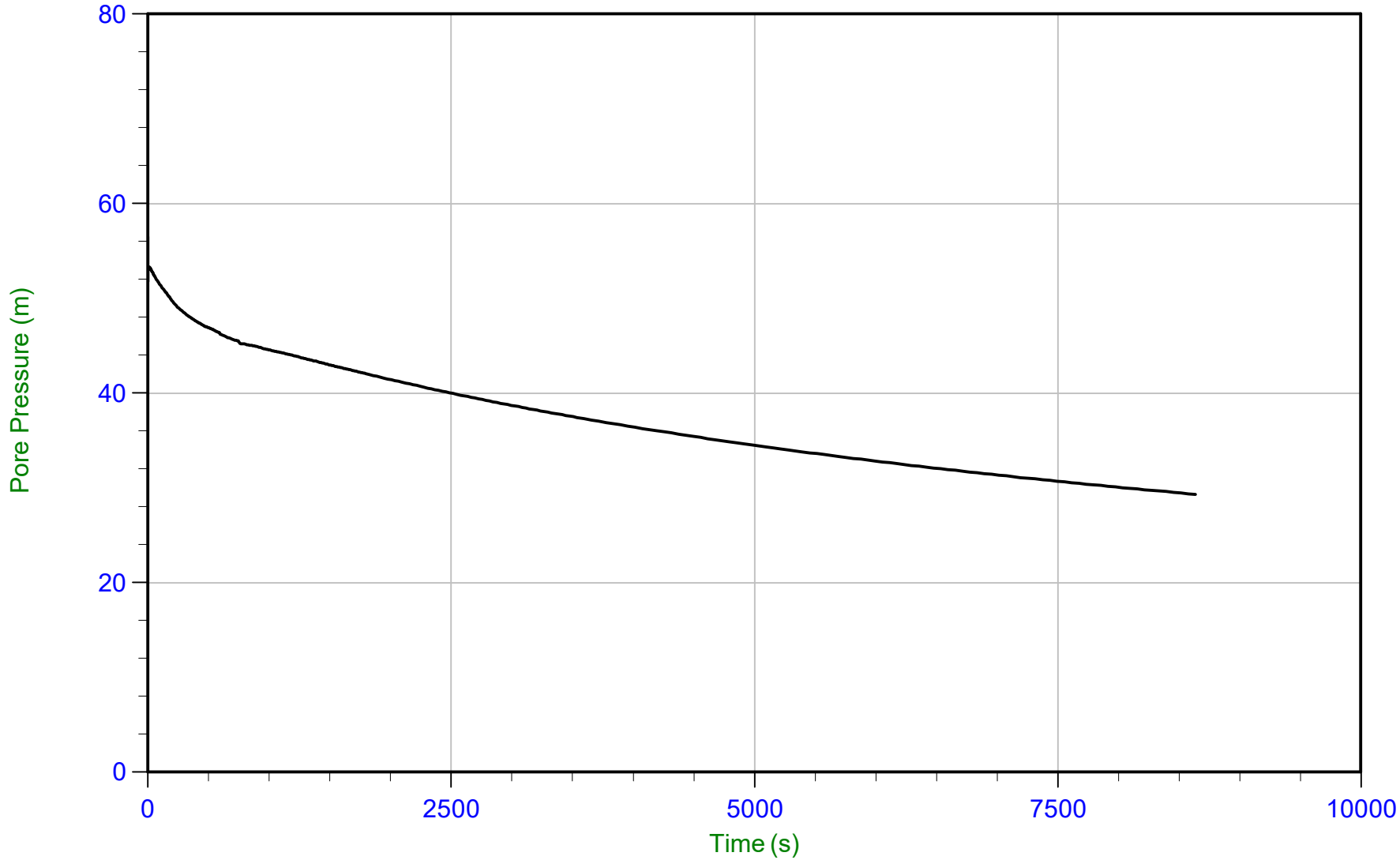
T(50): 13839.4 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD202.PPF2
Depth: 12.500 m / 41.010 ft
Duration: 8640.0 s

u Min: 29.3 m
u Max: 56.5 m
u Final: 29.3 m

WT: -0.1 m / -0.3 ft
Ueq: 12.6 m
U(50): 34.56 m

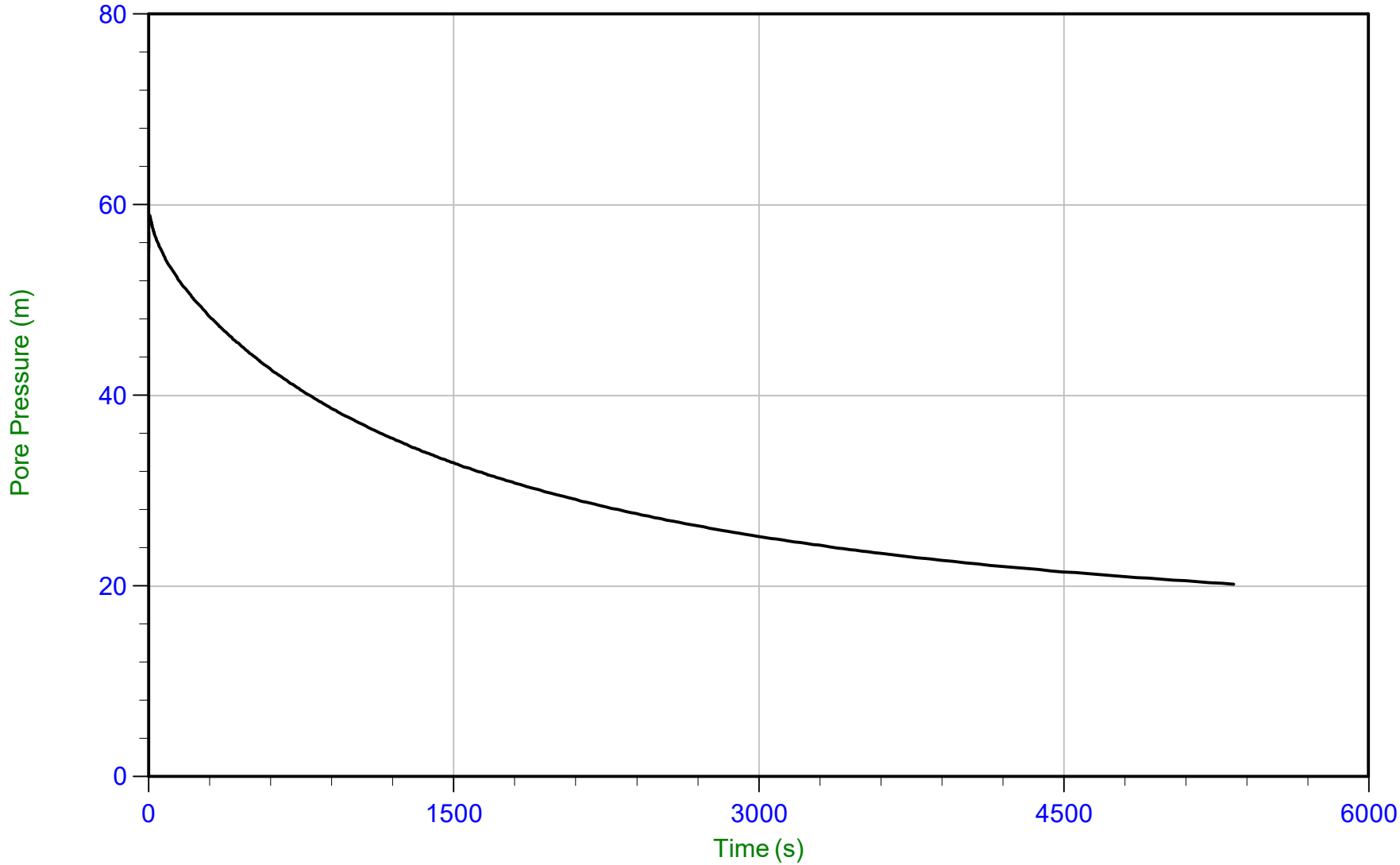
T(50): 4966.6 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD202.PPF2
Depth: 17.500 m / 57.414 ft
Duration: 5340.0 s

u Min: 20.2 m
u Max: 58.9 m
u Final: 20.2 m

WT: -0.1 m / -0.3 ft
Ueq: 17.6 m
U(50): 38.24 m

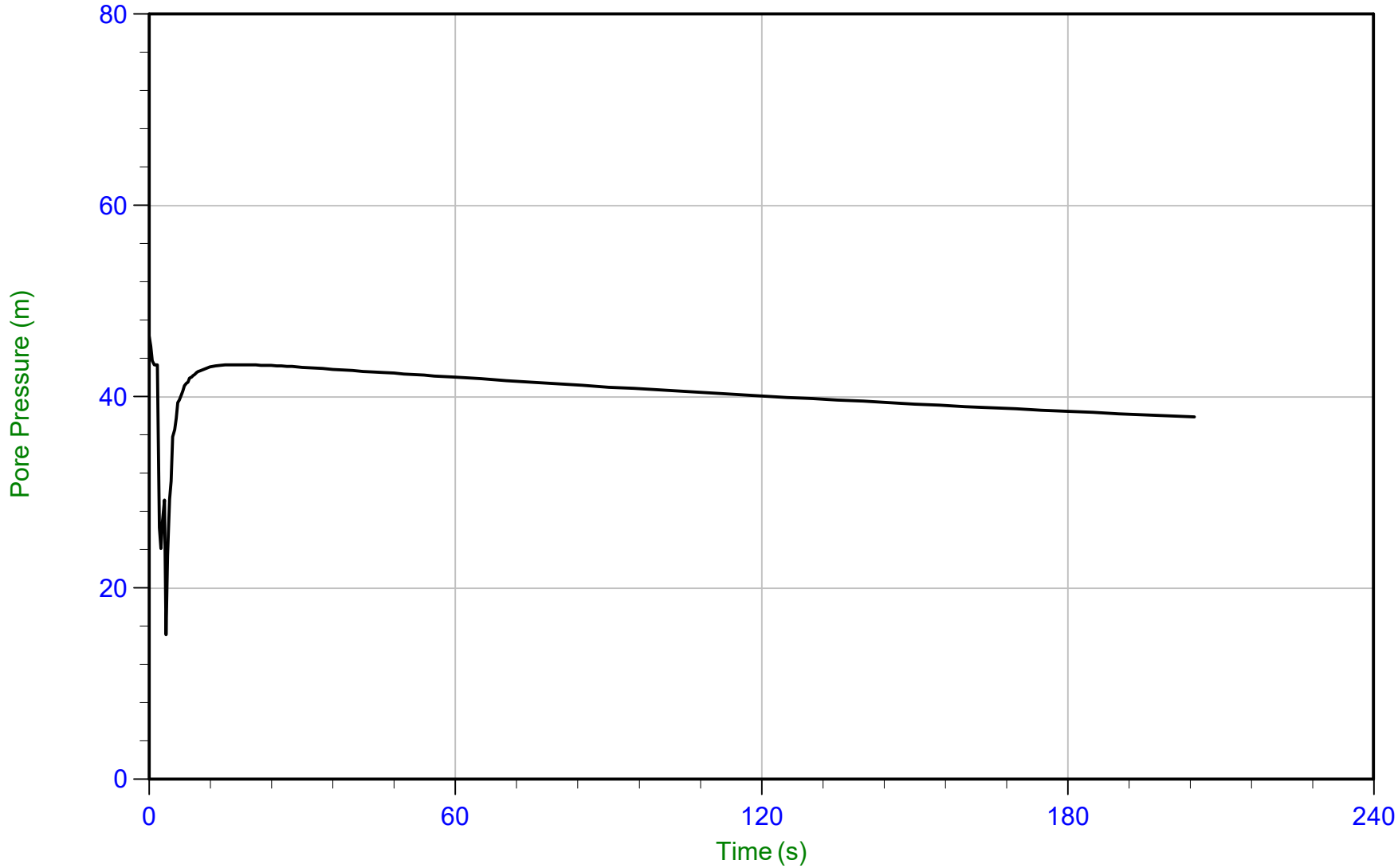
T(50): 929.2 s
Ir: 100
Ch: 0.8 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-04 12:33
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH202
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD202.PPF2
Depth: 18.950 m / 62.171 ft
Duration: 205.0 s

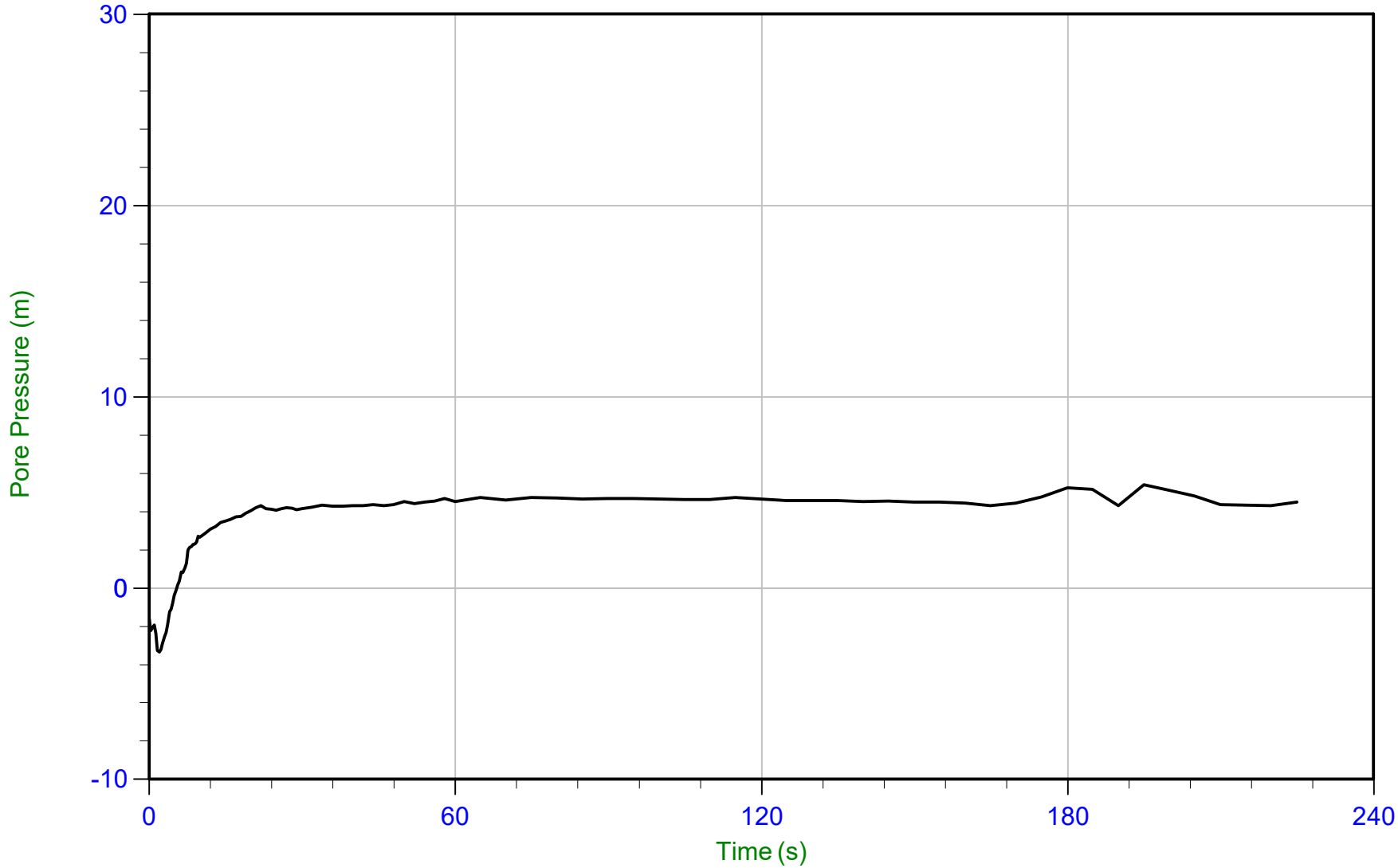
u Min: 15.1 m
u Max: 46.3 m
u Final: 37.9 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD205.PPF2
Depth: 4.000 m / 13.123 ft
Duration: 225.0 s

u Min: -3.3 m
u Max: 5.4 m
u Final: 4.5 m

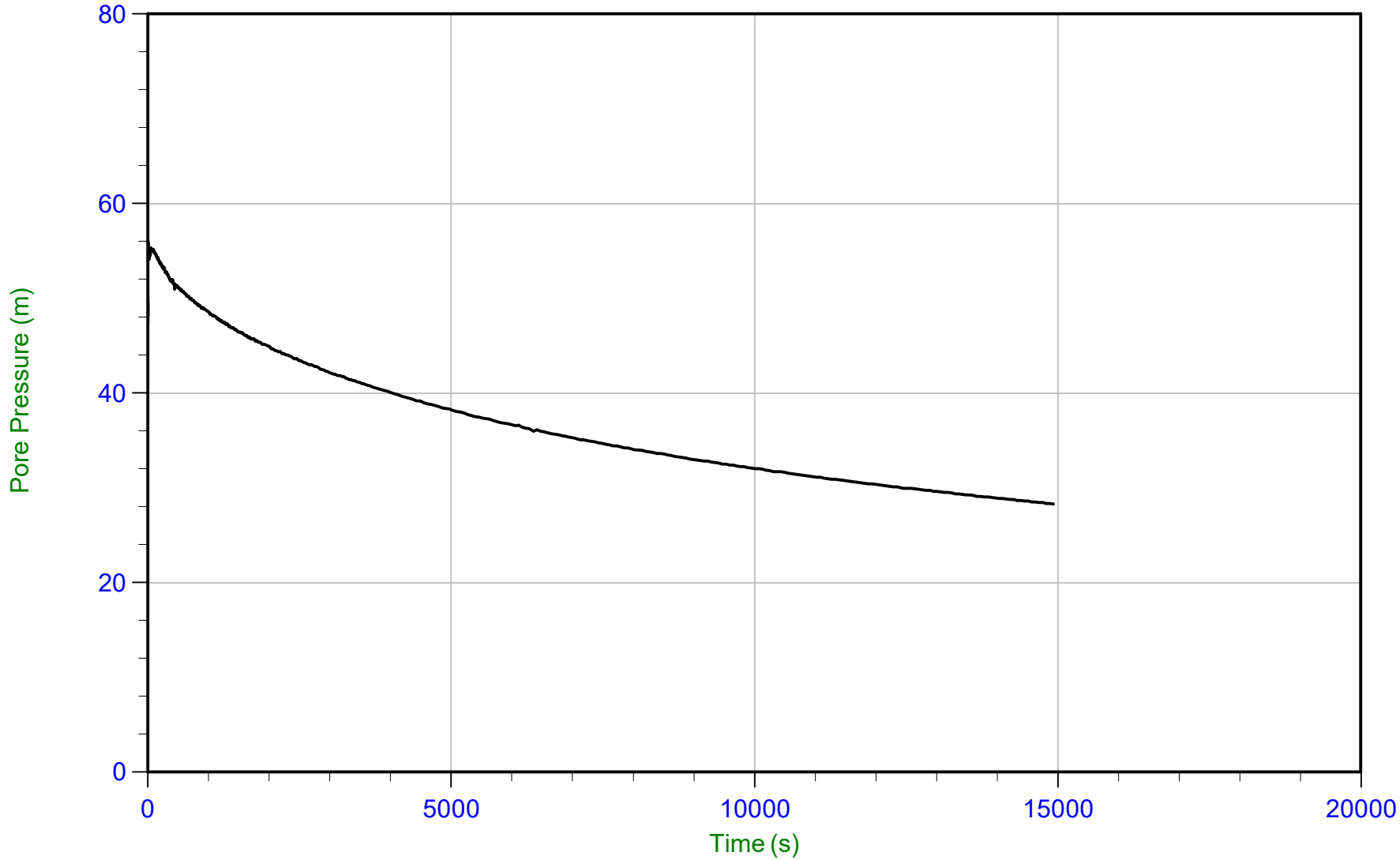
WT: -0.5 m / -1.6 ft
Ueq: 4.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD205.PPF2
Depth: 7.525 m / 24.688 ft
Duration: 14940.0 s

u Min: 28.3 m
u Max: 56.1 m
u Final: 28.3 m

WT: -0.5 m / -1.6 ft
Ueq: 8.0 m
U(50): 32.08 m

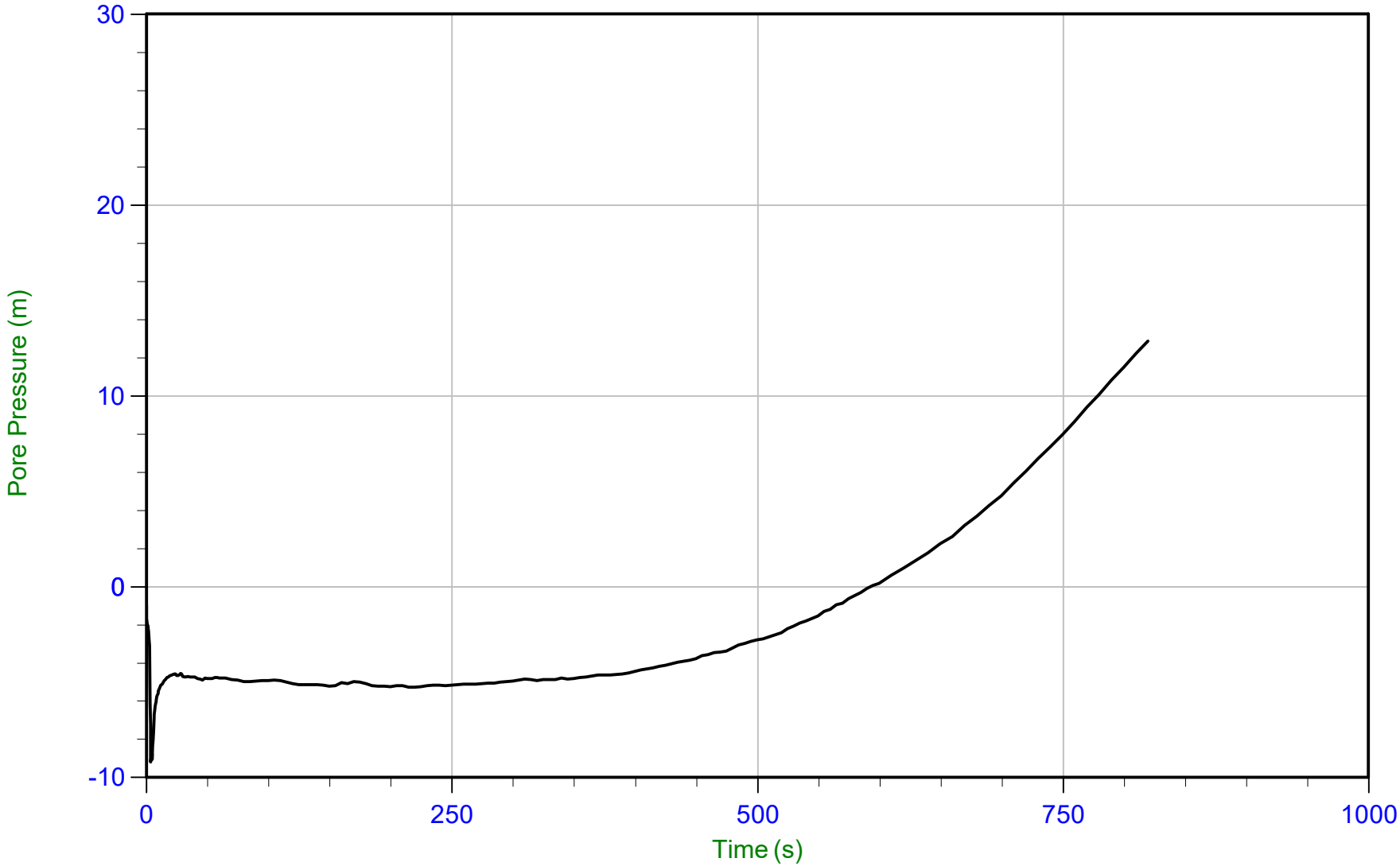
T(50): 9959.5 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 09:04
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD205.PPF2
Depth: 7.725 m / 25.344 ft
Duration: 820.0 s

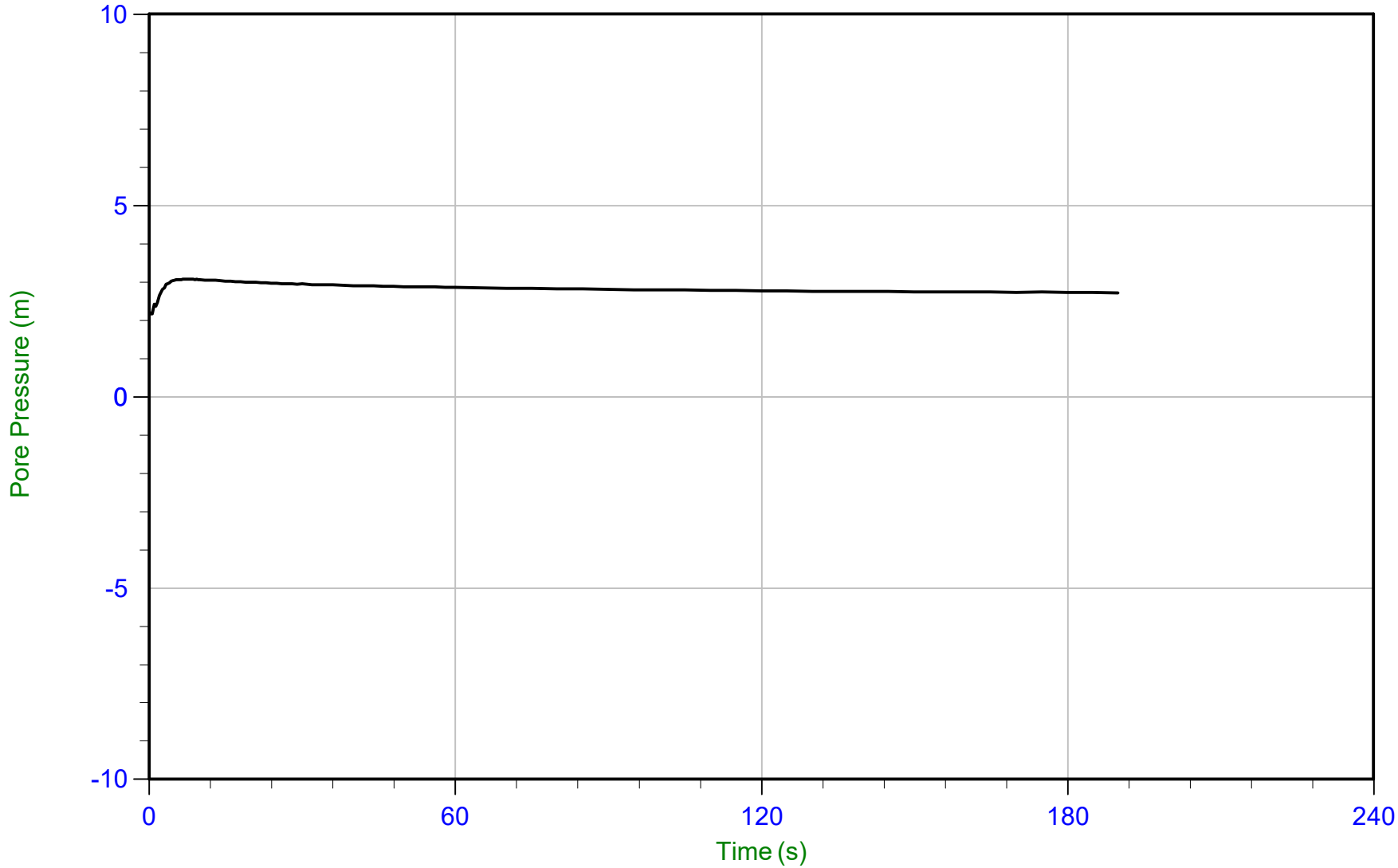
u Min: -9.2 m
u Max: 12.9 m
u Final: 12.9 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD205b.PPF2
Depth: 3.000 m / 9.842 ft
Duration: 190.0 s

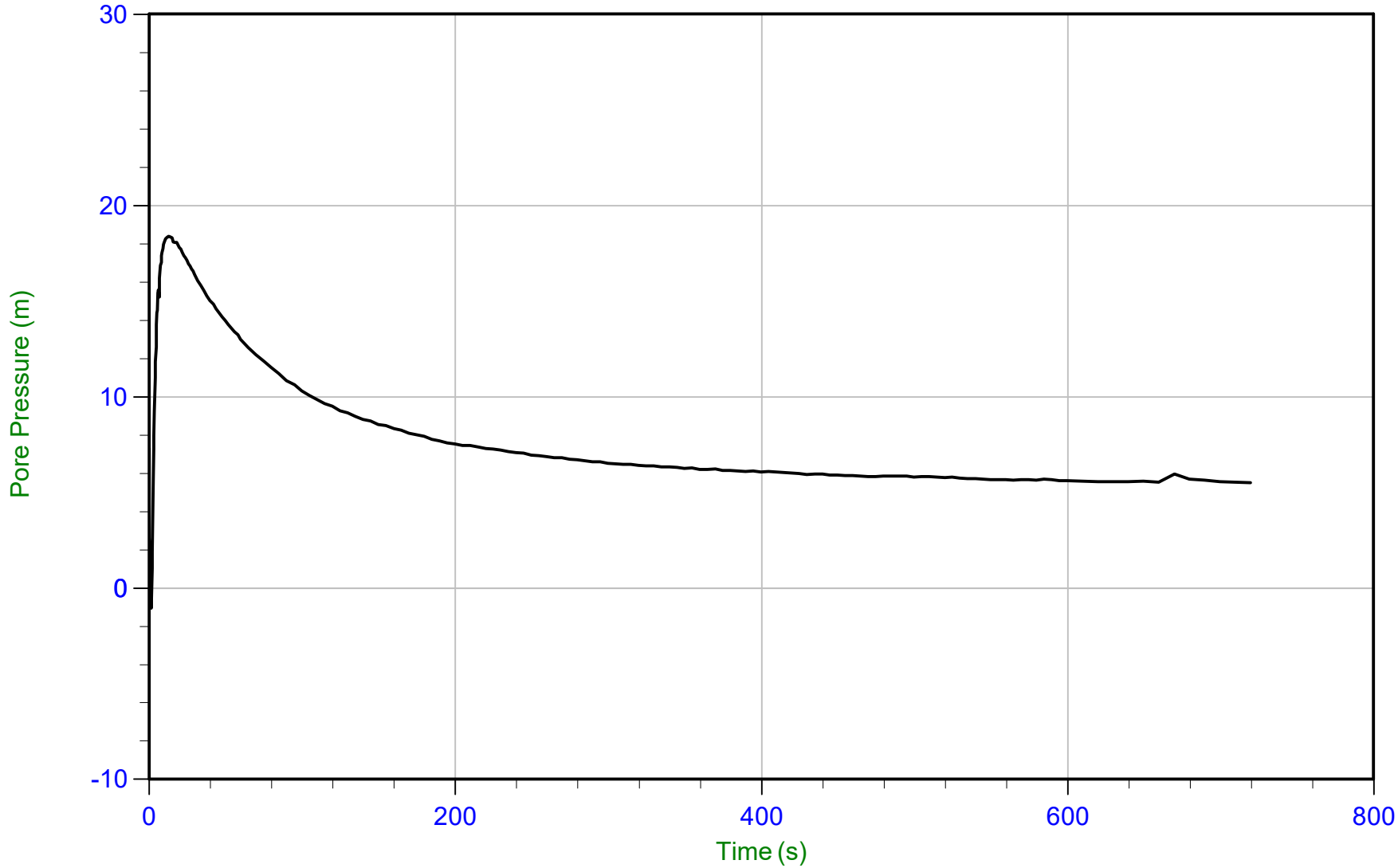
u Min: 2.2 m
u Max: 3.1 m
u Final: 2.7 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD205b.PPF2
Depth: 5.000 m / 16.404 ft
Duration: 720.0 s

u Min: -1.1 m
u Max: 18.4 m
u Final: 5.5 m

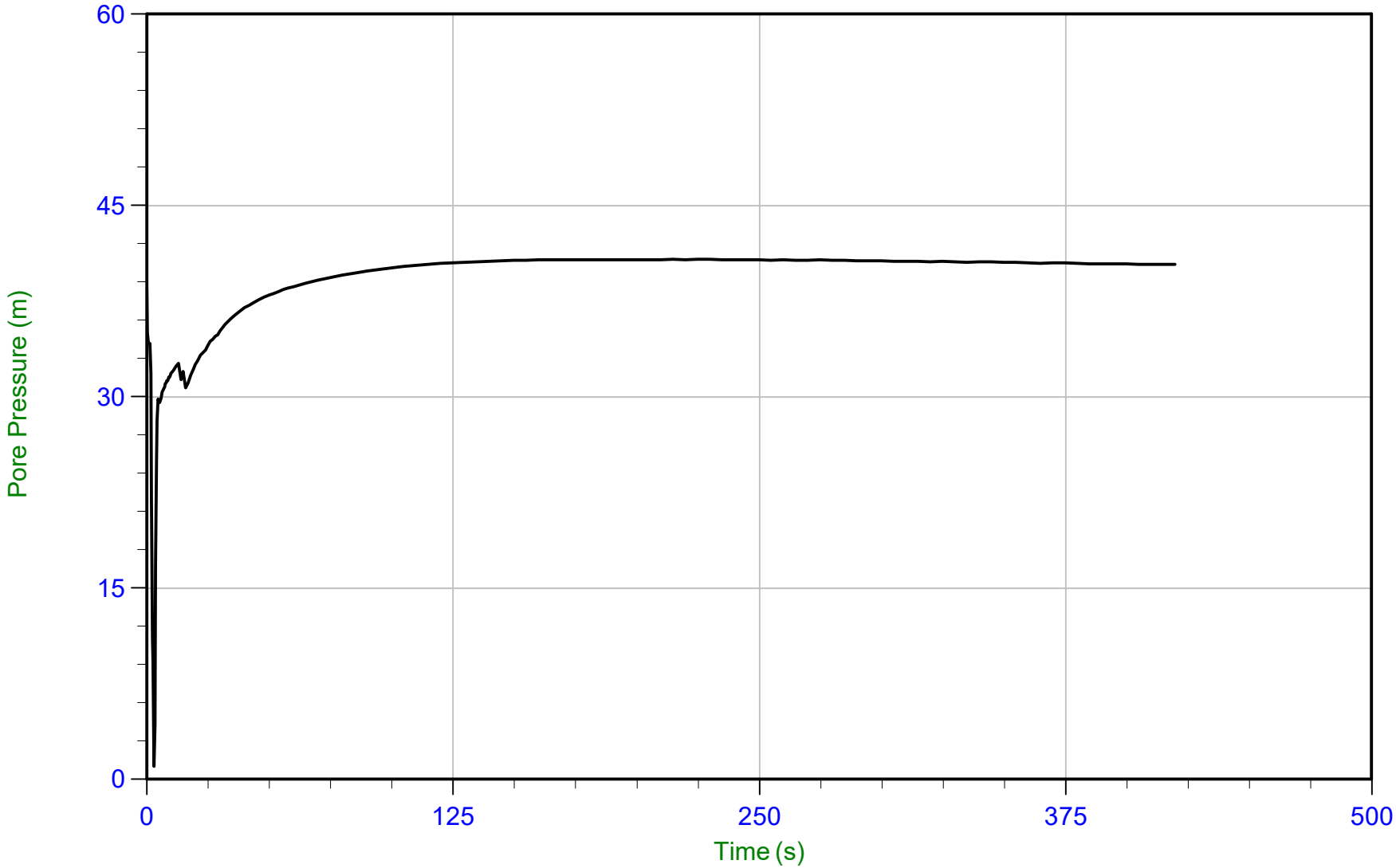
WT: -0.5 m / -1.6 ft
Ueq: 5.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-08 15:11
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH205B
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD205b.PPF2
Depth: 7.650 m / 25.098 ft
Duration: 420.0 s

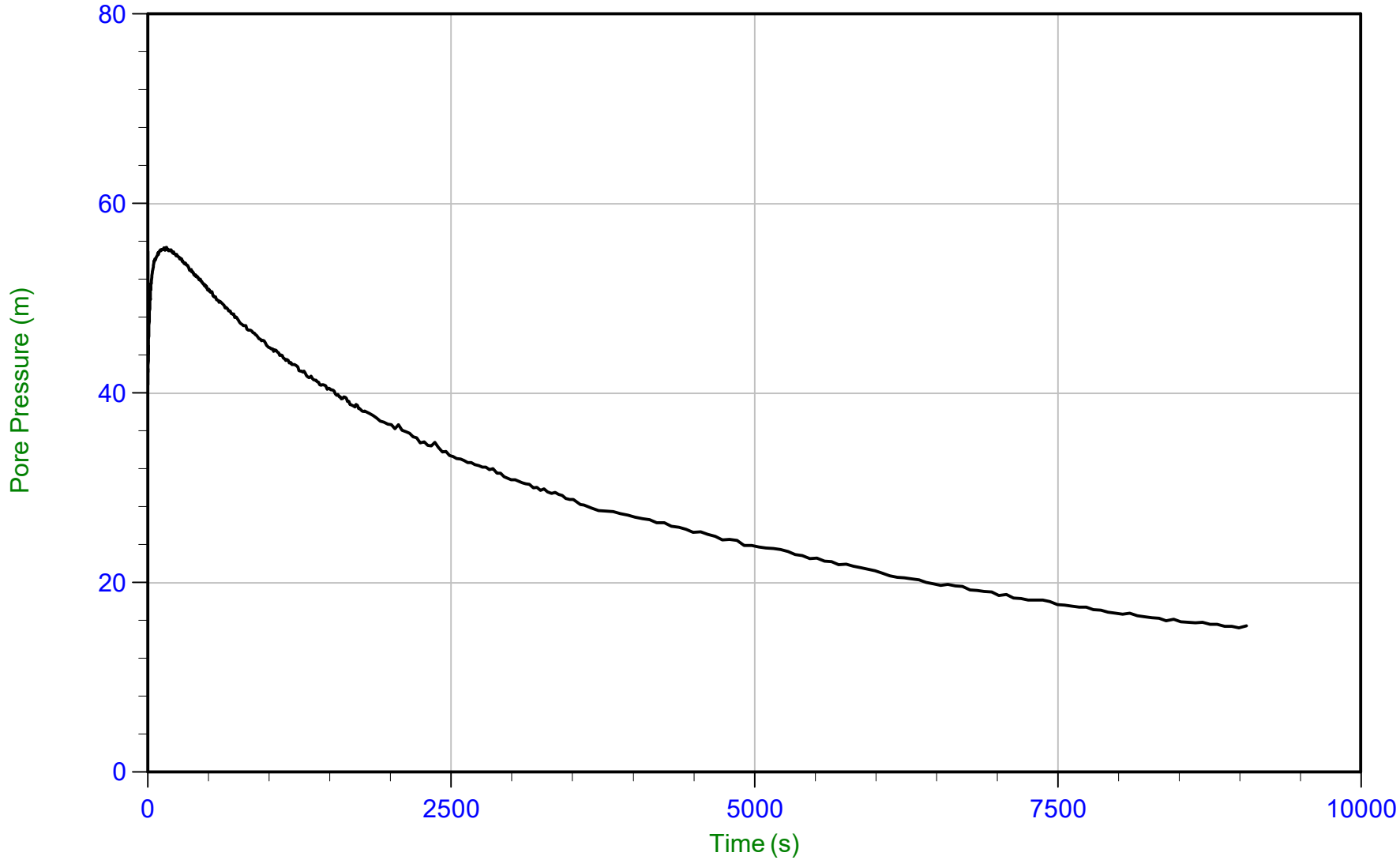
u Min: 1.0 m
u Max: 40.8 m
u Final: 40.4 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-12 09:14
Site: Crawford Mine - SRK

Sounding: CPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_CPWRD207.PPF2
Depth: 5.000 m / 16.404 ft
Duration: 9060.0 s

u Min: 15.2 m
u Max: 55.4 m
u Final: 15.5 m

WT: 0.4 m / 1.3 ft
Ueq: 4.6 m
U(50): 30.00 m

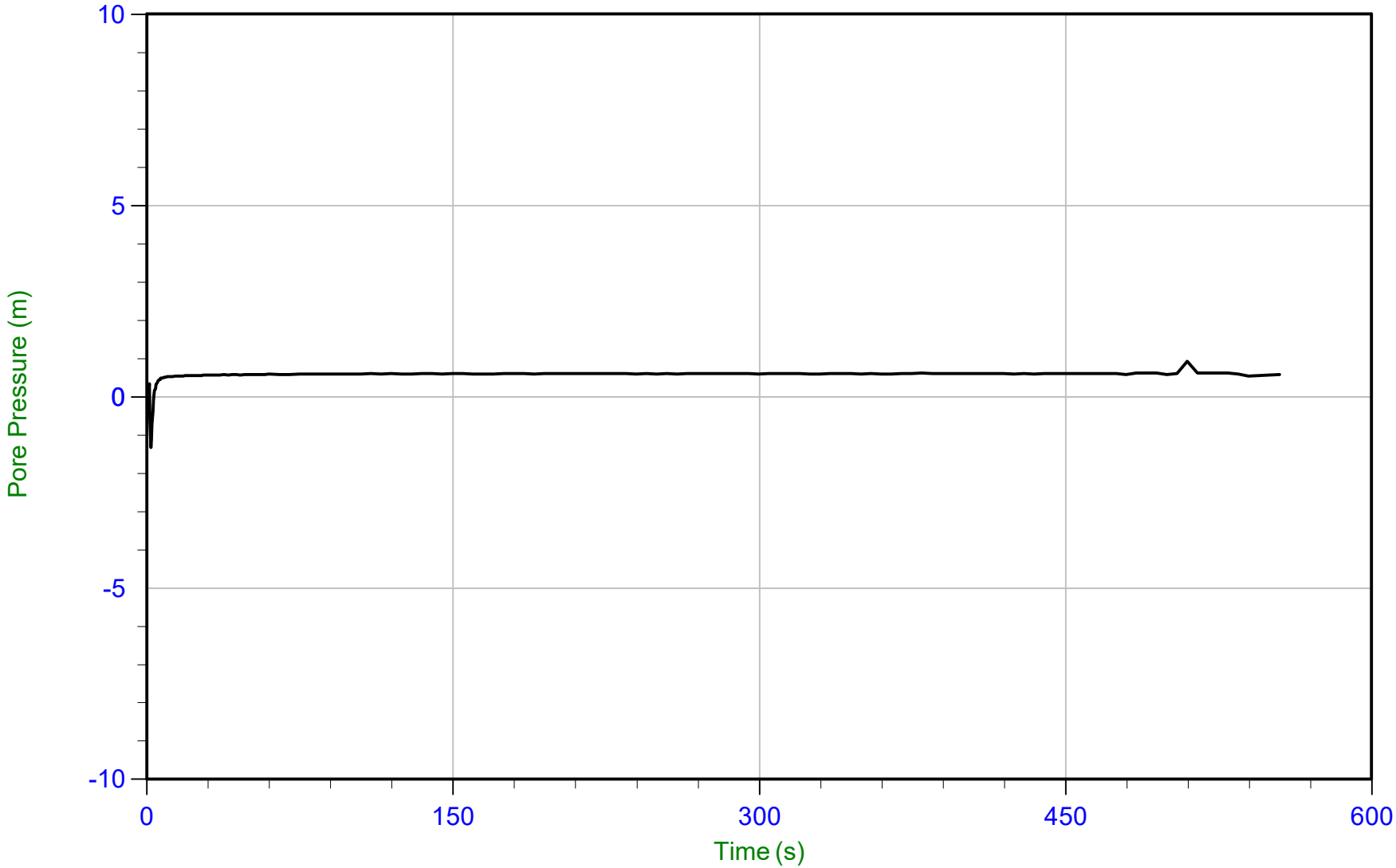
T(50): 3024.3 s
Ir: 100
Ch: 0.2 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD207.PPF2
Depth: 1.000 m / 3.281 ft
Duration: 555.0 s

u Min: -1.3 m
u Max: 0.9 m
u Final: 0.6 m

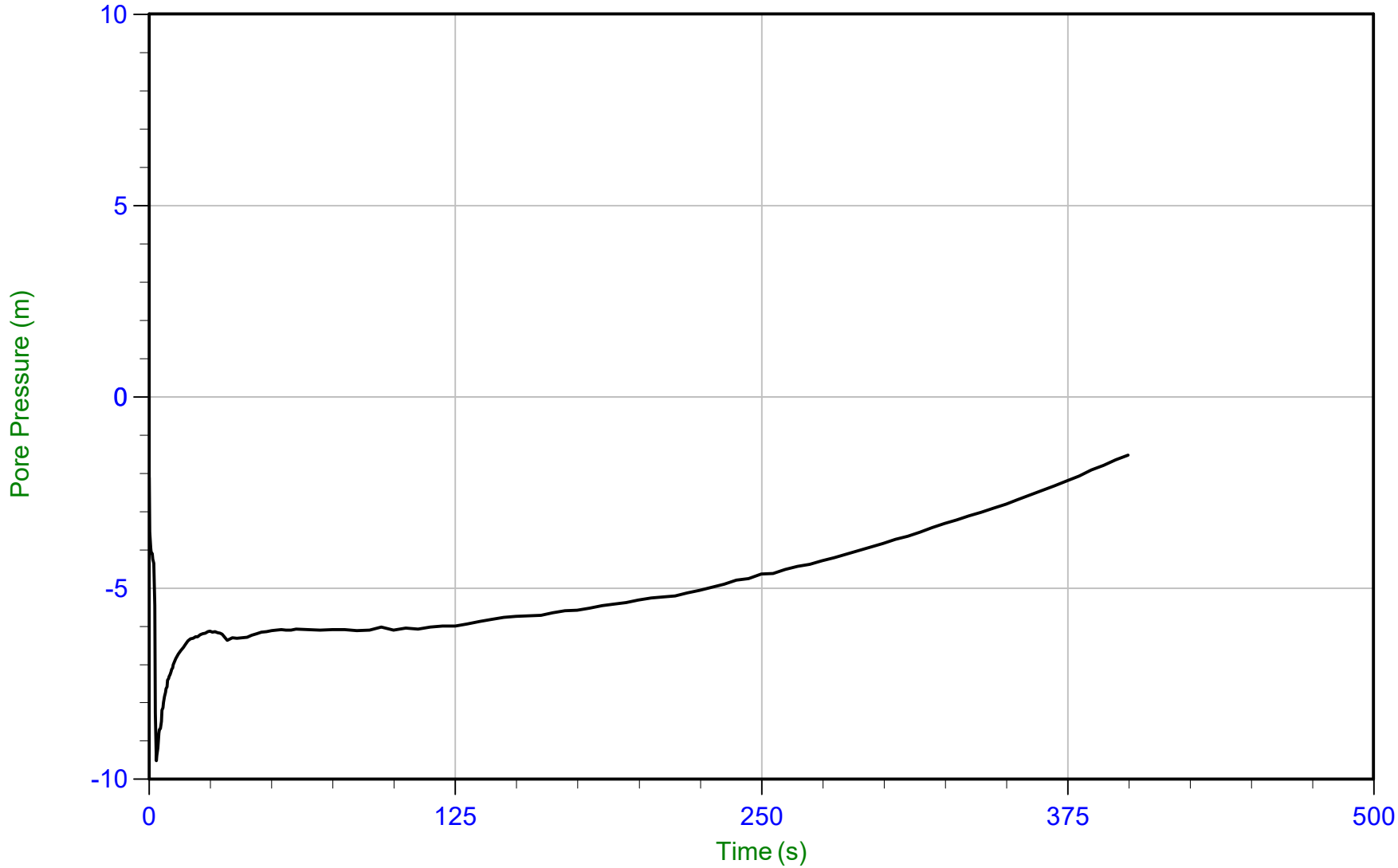
WT: 0.4 m / 1.3 ft
Ueq: 0.6 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-11 14:26
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH207
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD207.PPF2
Depth: 6.250 m / 20.505 ft
Duration: 400.0 s

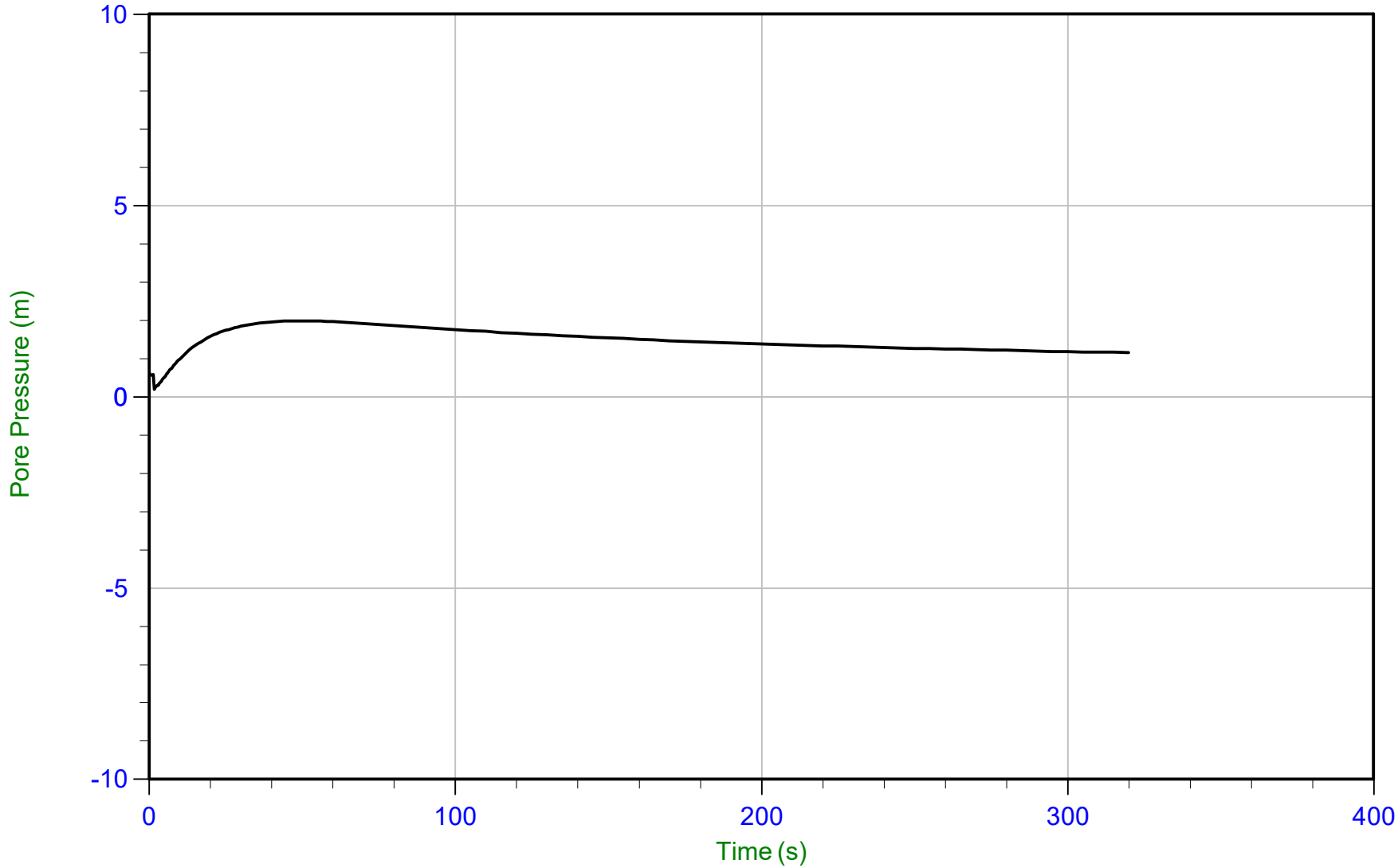
u Min: -9.5 m
u Max: -1.5 m
u Final: -1.5 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD212.PPF2
Depth: 1.000 m / 3.281 ft
Duration: 320.0 s

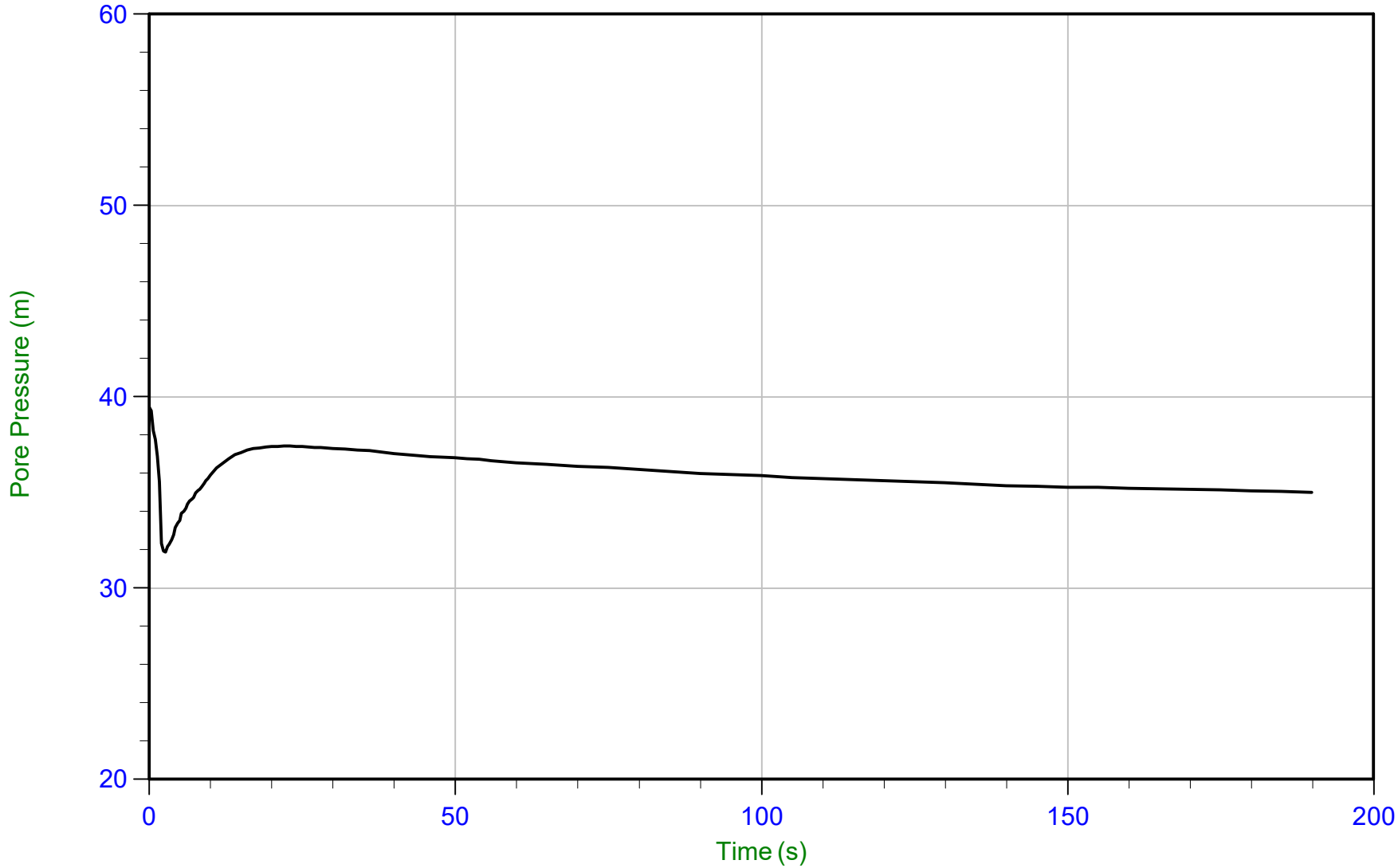
u Min: 0.2 m
u Max: 2.0 m
u Final: 1.2 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD212.PPF2
Depth: 5.000 m / 16.404 ft
Duration: 190.0 s

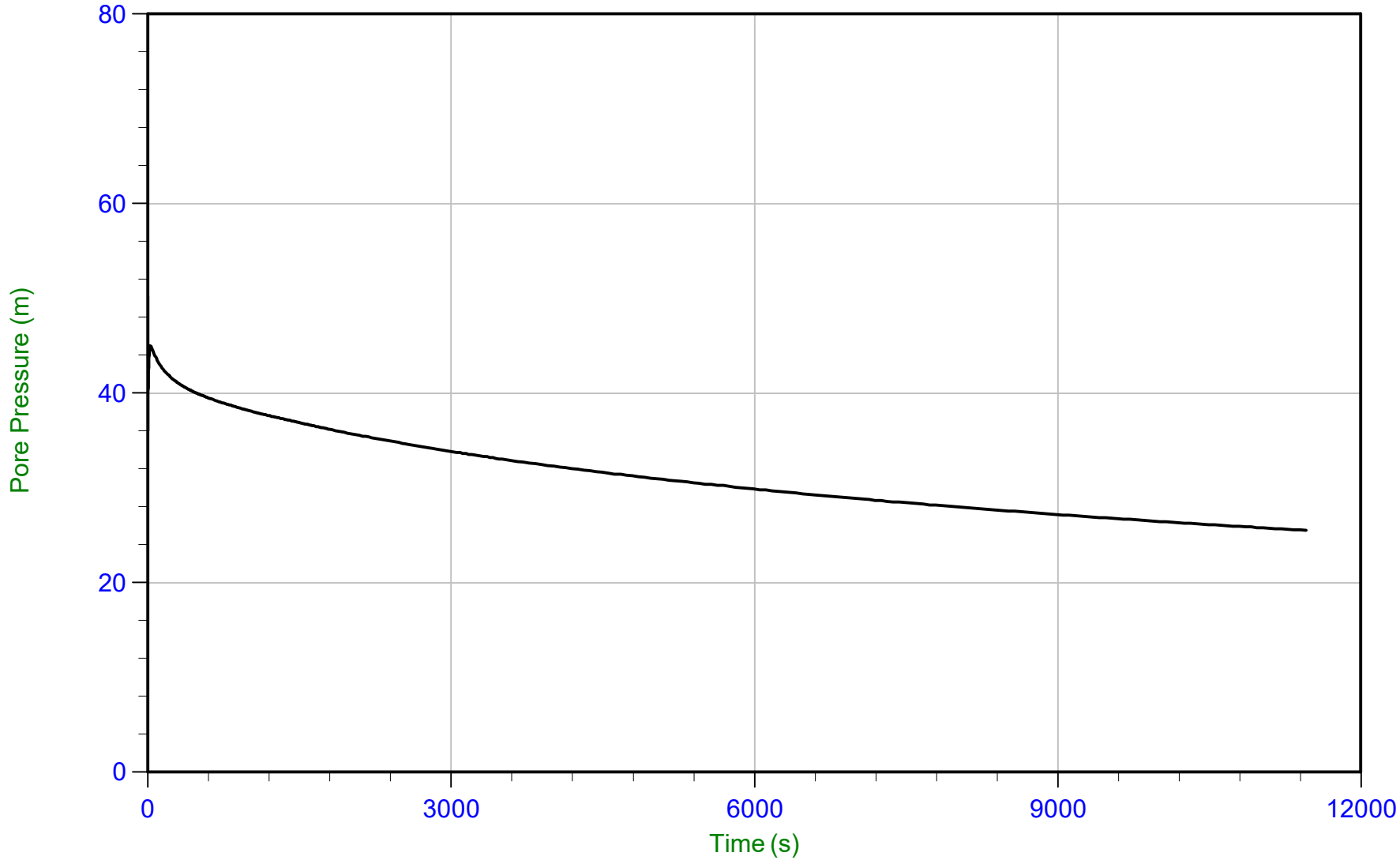
u Min: 31.9 m
u Max: 39.5 m
u Final: 35.0 m

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD212.PPF2
Depth: 7.500 m / 24.606 ft
Duration: 11460.0 s

u Min: 25.5 m
u Max: 50.2 m
u Final: 25.5 m

WT: 2.7 m / 8.9 ft
Ueq: 4.8 m
U(50): 27.51 m

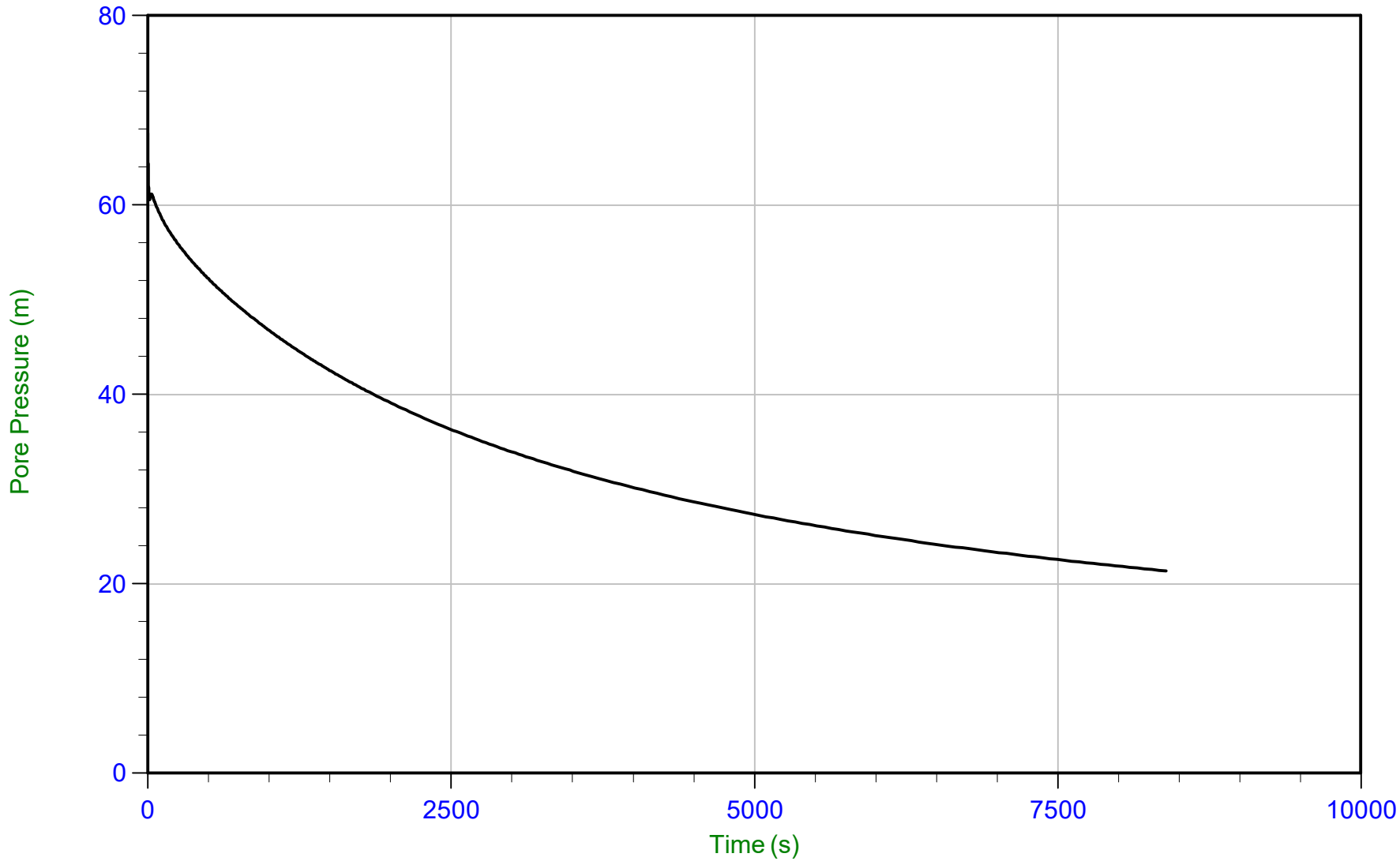
T(50): 8598.4 s
Ir: 100
Ch: 0.1 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD212.PPF2
Depth: 12.575 m / 41.256 ft
Duration: 8400.0 s

u Min: 21.4 m
u Max: 67.6 m
u Final: 21.4 m

WT: 2.7 m / 8.9 ft
Ueq: 9.9 m
U(50): 38.74 m

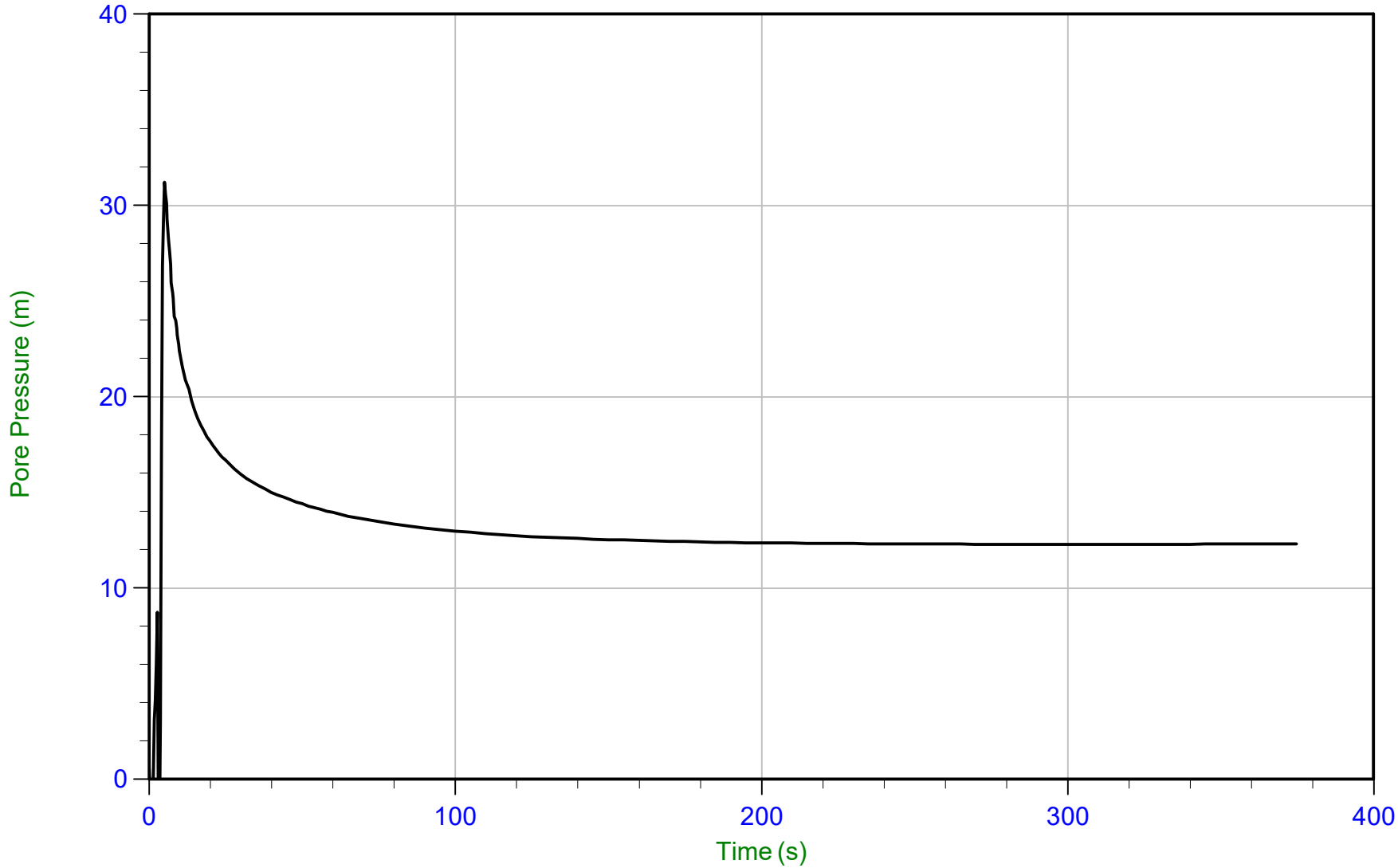
T(50): 2063.6 s
Ir: 100
Ch: 0.3 cm²/min

CONETEC

Canada Nickel Company

Job No: 24-05-27159
Date: 2024-03-03 08:13
Site: Crawford Mine - SRK

Sounding: SCPT24-WRD-BH212
Cone: 958:T1500F15U35 Area=15 cm²



Trace Summary:

Filename: 24-05-27159_SPWRD212.PPF2
Depth: 15.000 m / 49.212 ft
Duration: 375.0 s

u Min: -3.1 m
u Max: 31.2 m
u Final: 12.3 m

WT: 2.7 m / 8.9 ft
Ueq: 12.3 m

Description of Methods for Calculated CPT Geotechnical Parameters

CONETEC

CALCULATED CPT GEOTECHNICAL PARAMETERS

A Detailed Description of the Methods Used in ConeTec's CPT Geotechnical Parameter Calculation and Plotting Software



Revision SZW-Rev 18

Revised February 10, 2023
Prepared by Jim Greig, M.A.Sc, P.Eng (BC, AB, ON)

Limitations

The geotechnical parameter output was prepared specifically for the site and project named in the accompanying report subject to objectives, site conditions and criteria provided to ConeTec by the client. The output may not be relied upon by any other party or for any other site without the express written permission of ConeTec Group (ConeTec) or any of its affiliates. For this project, ConeTec has provided site investigation services, prepared factual data reporting and produced geotechnical parameter calculations consistent with current best practices. No other warranty, expressed or implied, is made.

To understand the calculations that have been performed and to be able to reproduce the calculated parameters the user is directed to the basic descriptions for the methods in this document and the detailed descriptions and their associated limitations and appropriateness in the technical references cited for each parameter.

ConeTec's Calculated CPT Geotechnical Parameters as of February 10, 2023.

ConeTec's CPT parameter calculation and plotting routine provides a tabular output of geotechnical parameters based on current published CPT correlations and is subject to change to reflect the current state of practice. Due to drainage conditions and the basic assumptions and limitations of the correlations, not all geotechnical parameters provided are considered applicable for all soil types. The results are presented only as a guide for geotechnical use and should be carefully examined for consideration in any geotechnical design. Reference to current literature is strongly recommended. ConeTec does not warranty the correctness or the applicability of any of the geotechnical parameters calculated by the program and does not assume liability for any use of the results in any design or review. For verification purposes we recommend that representative hand calculations be done for any parameter that is critical for design purposes. The end user of the parameter output should also be fully aware of the techniques and the limitations of any method used by the program. The purpose of this document is to inform the user as to which methods were used and to direct the end user to the appropriate technical papers and/or publications for further reference.

The geotechnical parameter output was prepared specifically for the site and project named in the accompanying report subject to objectives, site conditions and criteria provided to ConeTec by the client. The output may not be relied upon by any other party or for any other site without the express written permission of ConeTec Group (ConeTec) or any of its affiliates.

The CPT calculations are based on values of tip resistance, sleeve friction and pore pressures considered at each data point or averaged over a user specified layer thickness (e.g., 0.20 m). Note that q_t is the tip resistance corrected for pore pressure effects and q_c is the recorded tip resistance. The corrected tip resistance (corrected using u_2 pore pressure values) is used for all calculations. Since all ConeTec cones have equal end area friction sleeves pore pressure corrections to sleeve friction, f_s, are not performed.

Corrected tip resistance: $q_t = q_c + (1-a) \cdot u_2$ (consistent units are required)

where: q_t is the corrected tip resistance
q_c is the recorded tip resistance
u_2 is the recorded dynamic pore pressure from behind the tip (u_2 position)
a is the Net Area Ratio for the cone (typically 0.80 for ConeTec cones)

The total stress calculations are based on soil unit weight values that have been assigned to the Soil Behavior Type (SBT) zones, from a user defined unit weight profile, by using a single uniform value throughout the profile, through unit weight estimation techniques described in various technical papers or from a combination of these methods. The parameter output files indicate the method(s) used.

Effective vertical overburden stresses are calculated using the total stress and equilibrium pore pressure (u_{eq} or u_o) values derived from an assumed hydrostatic distribution of pore pressures below the water table or from a user defined equilibrium pore pressure profile (typically obtained from CPT dissipation tests) or a combination of the two. For over water projects the stress effects of the column of water above the mudline are taken into account as is the appropriate unit weight of water. How this is done depends on where the instruments are zeroed (i.e. on deck or at the mudline). The parameter output files indicate the method(s) used.

A majority of parameter calculations are derived from or driven by results based on material types as determined by the various soil behavior type charts depicted in Figures 1 through 6. The parameter output files indicate the method(s) used.

The Soil Behavior Type classification chart shown in Figure 1 is the classic non-normalized SBT Chart developed at the University of British Columbia and reported in Robertson, Campanella, Gillespie and Greig (1986). Figure 2 shows the original normalized (linear method) SBTn chart developed by Robertson (1990). The Bq classification charts

shown in Figures 3a and 3b incorporate pore pressures into the SBT classification and are based on the methods described in Robertson (1990). Many of these charts have been summarized in Lunne, Robertson and Powell (1997). The Jefferies and Davies SBT chart shown in Figure 3c is based on the techniques discussed in Jefferies and Davies (1993) which introduced the concept of the Soil Behavior Type Index parameter, I_c. Take note that the I_c parameter developed by Robertson and Fear (1995) and Robertson and Wride (1998) is similar in concept but uses a slightly different calculation method than that defined by Jefferies and Davies (1993) as the latter incorporates pore pressure in their technique through the use of the Bq parameter. The normalized Qtn SBT chart shown in Figure 4 is based on the work by Robertson (2009) utilizing a variable stress ratio exponent, n, for normalization based on a slightly modified redefinition and iterative approach for I_c. The boundary curves drawn on the chart are based on the work described in Robertson (2010).

Figure 5 shows a revised 1986 SBT Chart presented to CPT'10 by Robertson (2010b). It is known as the Updated non-normalized Soil Behavior Chart (also referred to as the Rev SBT Chart (PKR2010) in our output files). This chart was produced to be more in line with all post-1986 Robertson charts having the same 9 soil type zones, a $\log_{10}$ axis for friction ratio, R_f in this case, and a unitless tip resistance axis.

Figure 6 shows a revised behavior based chart by Robertson (2016) depicting contractive-dilative zones. As the zones represent material behavior rather than soil gradation ConeTec has chosen a set of zone colors that are less likely to be confused with material type colors from previous SBT charts. These colors differ from those used by Dr. Robertson. A green palette was selected for the dilative (desirable) side of the chart and a red palette for the contractive side of the chart.

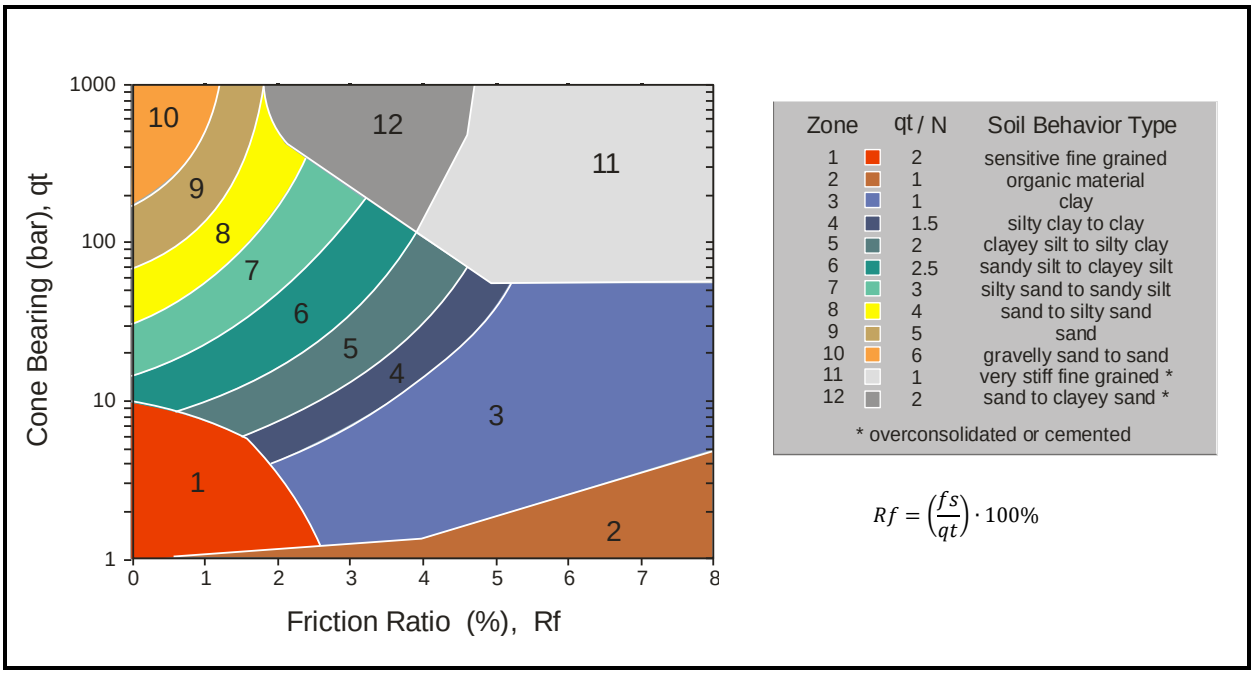


Figure 1. Non-normalized Soil Behavior Type Classification Chart (SBT)

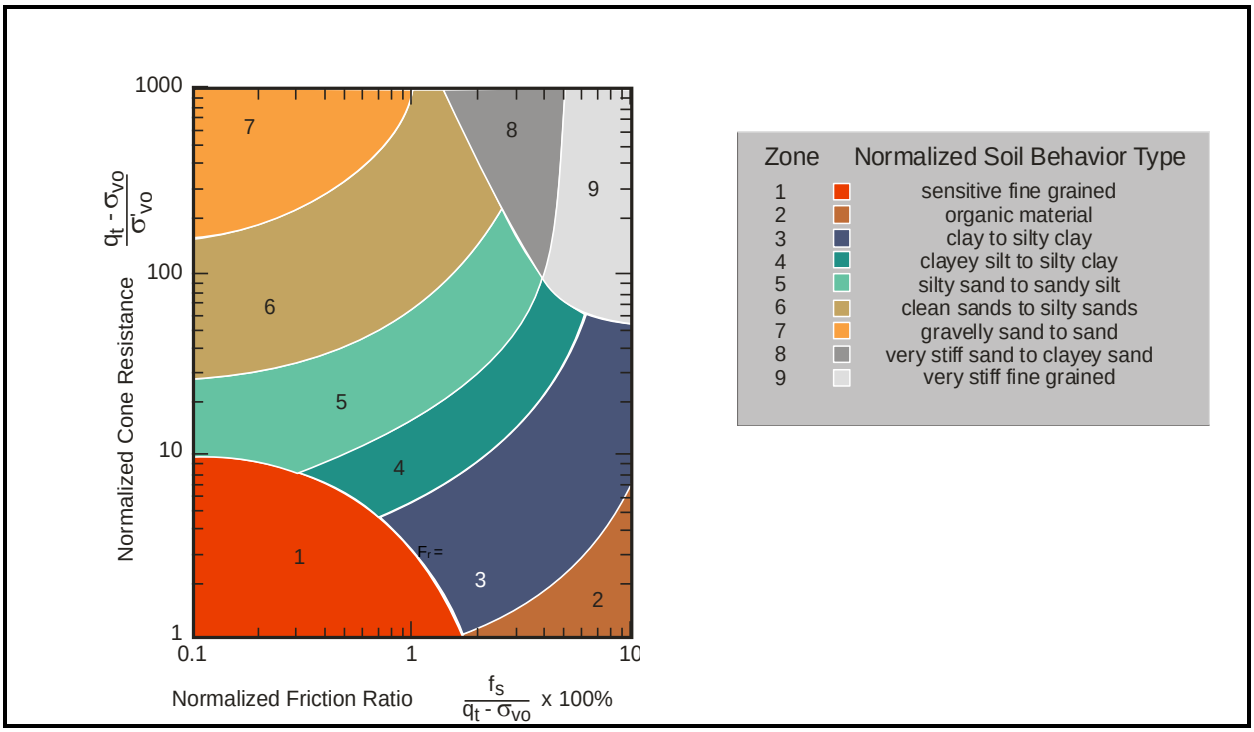


Figure 2. Normalized Soil Behavior Type Classification Chart (SBTn)

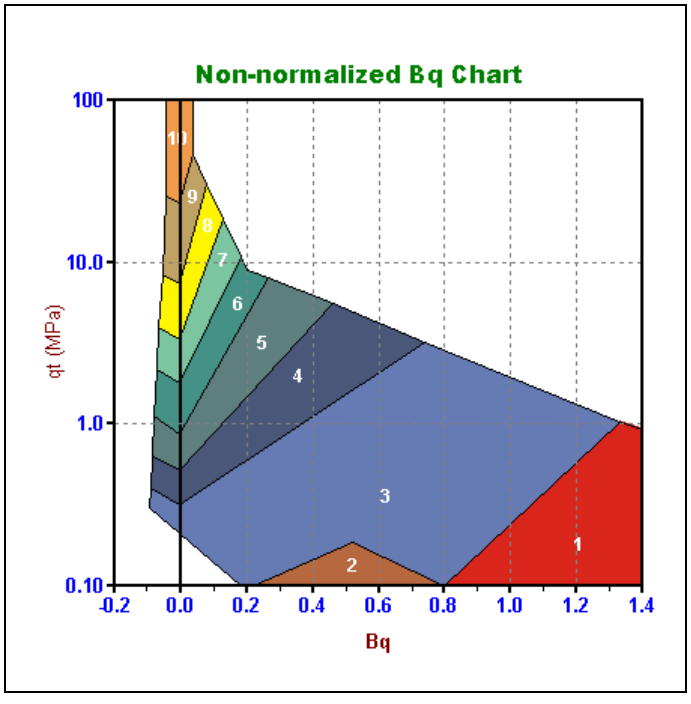


Figure 3a. Alternate Soil Behavior Type Chart (SBT Bq): q_t - B_q

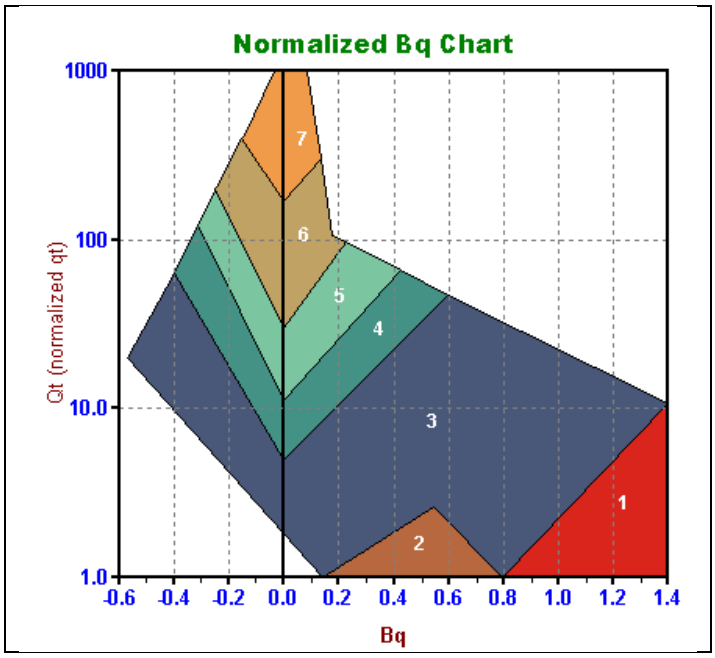


Figure 3b. Alternate Soil Behavior Type Charts (SBT Bqn): Q_t-B_q

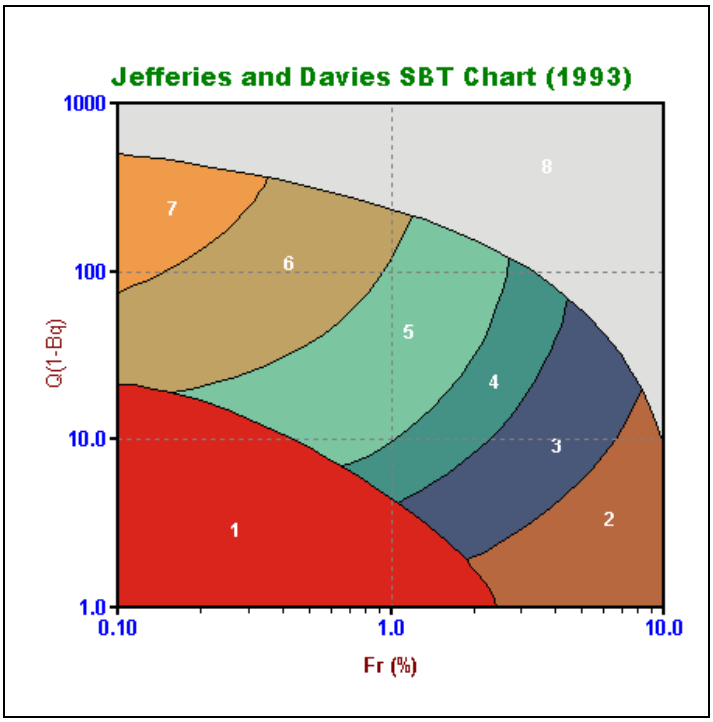


Figure 3c. Alternate Soil Behavior Type Charts: $Q(1-B_q)$ - F_r

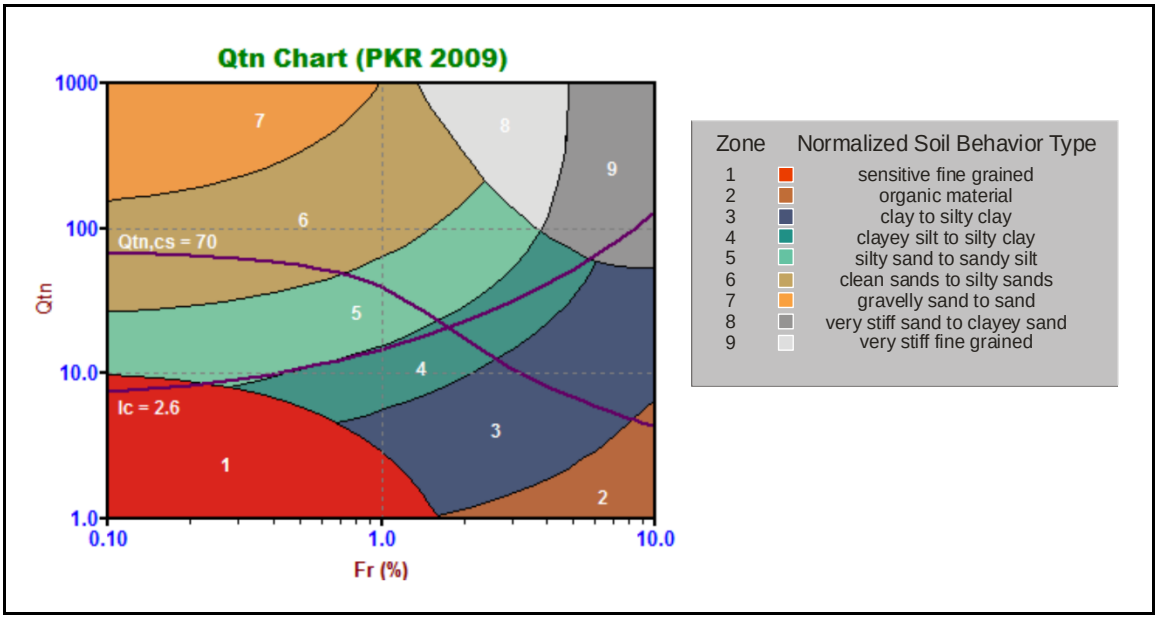


Figure 4. Normalized Soil Behavior Type Chart using Q_{tn} (SBT Qtn)

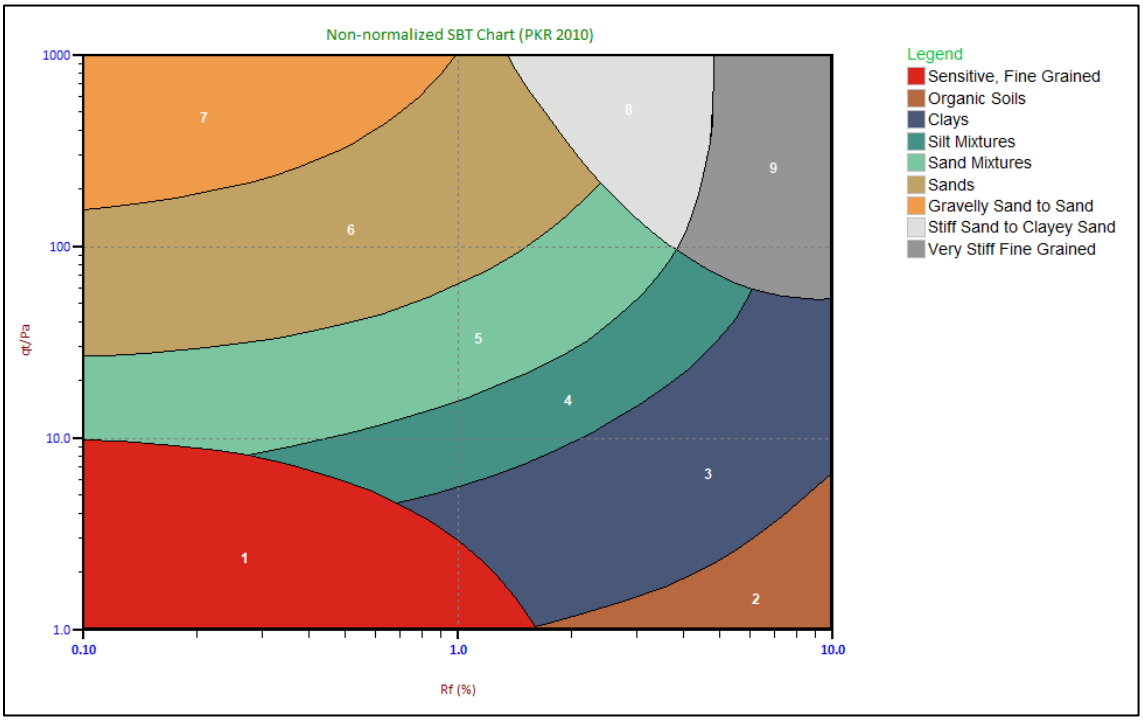


Figure 5. Non-normalized Soil Behavior Type Chart (2010)

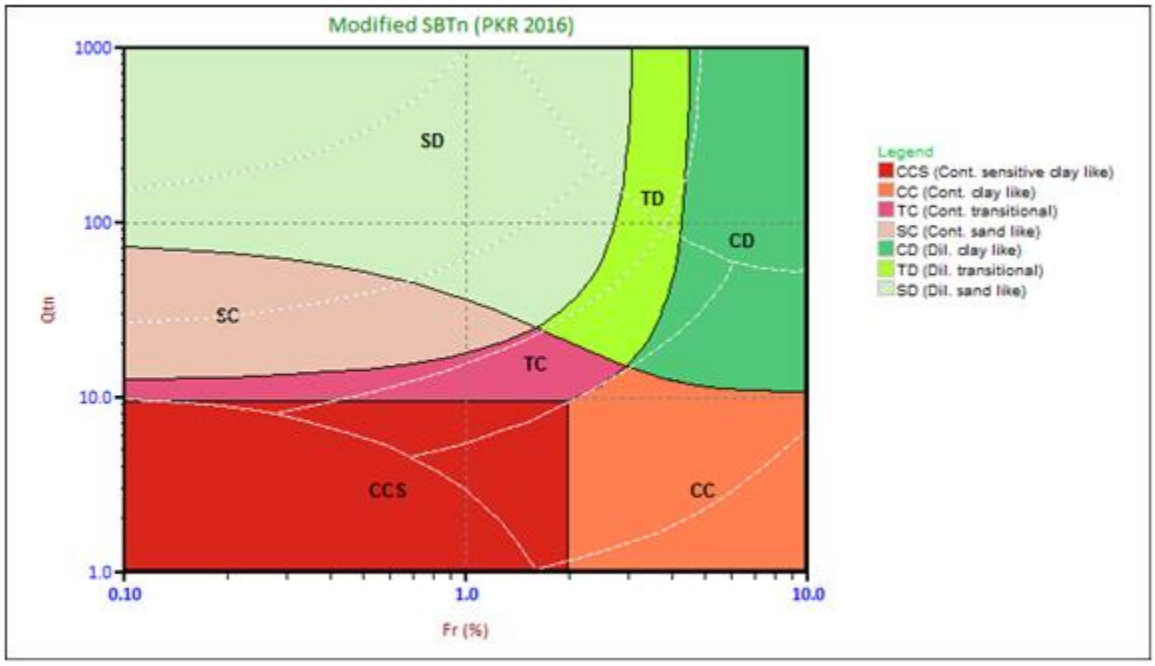


Figure 6. Modified SBTn Behavior Based Chart

Details regarding the geotechnical parameter calculations are provided in Tables 1a and 1b. The appropriate references cited are listed in Table 2. Non-liquefaction specific parameters are detailed in Table 1a and liquefaction specific parameters are detailed in Table 1b.

Where methods are based on charts or techniques that are too complex to describe in this summary, we recommend that the user refer to the cited material. Specific limitations for each method are described in the cited material.

Where the results of a calculation/correlation are deemed *'invalid'* the value will be represented by the text strings "-9999", "-9999.0", the value 0.0 (Zero) or an empty cell. Invalid results will occur because of (and not limited to) one or a combination of:

1. Invalid or undefined CPT data (e.g., drilled out section or data gap).

2. Where the calculation method is inappropriate, for example, drained parameters in a material behaving in an undrained manner (and vice versa).

3. Where input values are beyond the range of the referenced charts or specified limitations of the correlation method.

4. Where pre-requisite or intermediate parameter calculations are invalid.

The parameters selected for output from the program are often specific to a particular project. As such, not all of the calculated parameters listed in Tables 1and 1a may be included in the output files delivered with this report.

The output files are typically provided in Microsoft Excel XLS, XLSX or CSV format. The ConeTec software has several options for output depending on the number or types of calculated parameters desired or those specifically contracted for by the client. Each output file is named using the original file base name (from the .COR file) followed

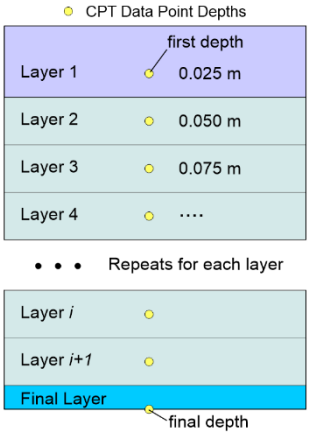
by a three or four character indicator of the output set selected (e.g. BSC, TBL, NLI, NL2, IFI, IFI2, IFI3) and possibly followed by an operator selected suffix identifying the characteristics of the particular calculation run.

Table 1a. CPT Parameter Calculation Methods – Non liquefaction Parameters

Reference Notes: CK* - Common Knowledge, U* - Unpublished

Calculated Parameter	Description	Equation	Ref
Depth	Mid Layer Depth *(where calculations are done at each point then Mid Layer Depth = Recorded Depth)*	*[Depth (Layer Top) + Depth (Layer Bottom)]/ 2.0*	CK*
Elevation	Elevation of Mid Layer is based on the sounding collar elevation supplied by the client or through a site survey In Sweden a variation of elevation is used where the elevation increases with depth. We refer to this as inverse elevation.	Elevation = Collar Elevation – Depth InverseElevation = Collar Elevation + Depth	CK* N/A
Avg qc	Averaged recorded tip value (q_c)	$Avgqc = \frac{1}{n}\sum_{i=1}^{n} q_c$ *n=1 when calculations are done at each point*	CK*
Avg qt	Averaged corrected tip (q_t) where: $q_t = q_c + (1-a)\cdot u_2$ Averaged q_t is not calculated using the average q_c and averaged u values. Averaged q_t is based on the average of the q_t values calculated at each data point.	$Avgqt = \frac{1}{n}\sum_{i=1}^{n} q_t$ *n=1 when calculations are done at each point*	1
Avg fs	Averaged sleeve friction (f_s) No pore pressure corrections are applied to f_s.	$Avgfs = \frac{1}{n}\sum_{i=1}^{n} fs$ *n=1 when calculations are done at each point*	CK*
Avg Rf	Averaged friction ratio (R_f) where friction ratio is defined as: $R_f = 100\% \cdot \frac{fs}{q_t}$	$AvgRf = 100\% \cdot \frac{Avgfs}{Avgqt}$ *not an average of individual R_f values*	CK*
Avg u	Averaged dynamic pore pressure *(u)*	$Avgu = \frac{1}{n}\sum_{i=1}^{n} u_i$ *n=1 when calculations are done at each point*	CK*
Avg Res	Averaged Resistivity (this data is not always available since it is a specialized test requiring an additional module)	$AvgRes = \frac{1}{n}\sum_{i=1}^{n} Resistivity_i$ *n=1 when calculations are done at each point*	CK*
Avg UVIF	Averaged UVIF ultra-violet induced fluorescence (this data is not always available since it is a specialized test requiring an additional module)	$AvgUVIF = \frac{1}{n}\sum_{i=1}^{n} UVIF_i$ *n=1 when calculations are done at each point*	CK*
Avg Temp	Averaged Temperature (this data is not always available)	$AvgTemp = \frac{1}{n}\sum_{i=1}^{n} Temperature_i$ *n=1 when calculations are done at each point*	CK*
Avg Gamma	Averaged Gamma Counts (this data is not always available since it is a specialized test requiring an additional module)	$AvgGamma = \frac{1}{n}\sum_{i=1}^{n} Gamma_i$ *n=1 when calculations are done at each point*	CK*
SBT	Soil Behavior Type as defined by Robertson et al 1986 (often referred to as Robertson and Campanella, 1986)	See Figure 1	1, 5
SBTn	Normalized Soil Behavior Type as defined by Robertson 1990 (linear normalization using Q_t, now referred to as Q_{t1})	See Figure 2	2, 5

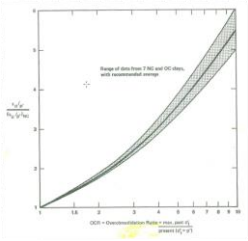
Calculated Parameter	Description	Equation	Ref
SBT-Bq	Non-normalized Soil Behavior type based on non-normalized tip resistance and the B_q parameter	See Figure 3a	1, 2, 5
SBT-Bqn	Normalized Soil Behavior type based on normalized tip resistance (Q_t, now called Q_{t1}) and the B_q parameter	See Figure 3b	2, 5
SBT-JandD	Soil Behavior Type as defined by Jeffries and Davies	See Figure 3c	7
SBT Qtn	Soil Behavior Type as defined by Robertson (2009) using a variable stress ratio exponent for normalization based on $I_{c\ (PKR\ 2009)}$	See Figure 4	15
Modified Non-normalized SBT Chart SBT (PKR2010)	This is a revised version of the simple 1986 non-normalized SBT chart (presented at CPT '10). The revised version has been reduced from 12 zones to 9 zones to be similar to the normalized Robertson charts. Other updates include a dimensionless tip resistance normalized to atmospheric pressure, q_t/P_a, on the vertical axis and a log scale for non-normalized friction ratio, R_f, along the horizontal axis.	See Figure 5	33
Modified SBTn (contractive /dilative)	Modified SBTn chart as defined by Robertson (2016) indicating zones of contractive/dilative behavior. Note that ConeTec displays the chart with colors different from Robertson. ConeTec's colors were chosen to avoid confusion with soil type descriptions.	See Figure 6	30
Unit Wt.	Unit Weight of soil determined from one of the following user selectable options: 1) uniform value 2) value assigned to each SBT zone 3) value assigned to each SBTn zone 4) value assigned to SBTn zone as determined from Robertson and Wride (1998) based on q_{c1n} 5) values assigned to SBT Qtn zones 6) values based on Robertson updated non-normalized Soil Behavior Type Chart (2010b) 6) Mayne f_s (sleeve friction) method 7) Robertson and Cabal 2010 method 8) user supplied unit weight profile The last option may co-exist with any of the other options.	See references	3, 5, 15, 21, 24, 29, 33

Calculated Parameter	Description	Equation	Ref
TStress σ_v	Total vertical overburden stress at Mid Layer Depth *A layer is defined as the averaging interval specified by the user where depths are reported at their respective mid-layer depth.* For data calculated at each point layers are defined using the recorded depth as the mid-point of the layer. Thus, a layer starts half-way between the previous depth and the current depth unless this is the first point in which case the layer start is at zero depth. The layer bottom is half-way from the current depth to the next depth unless it is the last data point. Defining layers affects how stresses are calculated since the unit weight attributed to a data point is used throughout the entire layer. This means that to calculate the stresses the total stress at the top and bottom of a layer are required. The stress at mid layer is determined by adding the incremental stress from the layer top to the mid-layer depth. The stress at the layer bottom becomes the stress at the top of the subsequent layer. Stresses are NOT calculated from mid-point to mid-point. For over-water work the total stress due to the column of water above the mid line is taken into account where appropriate.	$TStress = \sum_{i=1}^{n} \gamma_i h_i$ *where* γ_i is layer unit weight h_i is layer thickness 	CK*
EStress σ_v'	Effective vertical overburden stress at mid-layer depth.	$\sigma_v' = \sigma_v - u_{eq}$	CK*
Equil u u_{eq} or u_0	Equilibrium pore pressures are determined from one of the following user selectable options: 1) hydrostatic below the water table 2) user supplied profile 3) combination of those above When a user supplied profile is used/provided a linear interpolation is performed between equilibrium pore pressures defined at specific depths. If the profile values start below the water table then a linear transition from zero pressure at the water table to the first defined pointed is used. Equilibrium pore pressures may come from dissipation tests, adjacent piezometers or other sources. Occasionally, an extra equilibrium point ("assumed value") will be provided in the profile that does not come from a recorded value to smooth out any abrupt changes or to deal with material interfaces. These "assumed" values will be indicated on our plots and in tabular summaries.	For the hydrostatic option: $u_{eq} = \gamma_w \cdot (D - D_{wt})$ where u_{eq} is equilibrium pore pressure γ_w is the unit weight of water D is the current depth D_{wt} is the depth to the water table	CK*
K_0	Coefficient of earth pressure at rest, K_0.	$K_O = (1 - \sin\Phi') OCR^{\sin\Phi'}$	17
C_n	Overburden stress correction factor used for $(N_1)_{60}$ and older CPT parameters.	$C_n = (P_a/\sigma_v')^{0.5}$ where $0.0 < C_n < 2.0$ *(user adjustable, typically ranging from 1.7 to 2.0)* P_a *is atmospheric pressure (100 kPa)*	4, 12

Calculated Parameter	Description	Equation	Ref
C_q	Overburden stress normalizing factor.	$C_q = 1.8 / [0.8 + (\sigma_v'/P_a)]$ where *$0.0 < C_q < 2.0$ (user adjustable)* *P_a is atmospheric pressure (100 kPa)* *Robertson and Wride define C_q to be the same as C_n. The Olson definition above is used in the program.*	3, 12
N_{60}	SPT N value at 60% energy calculated from q_t/N ratios assigned to each SBT zone. This method has abrupt N value changes at zone boundaries.	*See Figure 1*	5
$(N_1)_{60}$	SPT N_{60} value corrected for overburden pressure.	$(N_1)_{60} = C_n \bullet N_{60}$	4
$N_{60}I_c$	SPT N_{60} values based on the I_c parameter, as defined by Robertson and Wride 1998 (3), or by Robertson 2009 (15).	$(q_t/P_a)/ N_{60} = 8.5 (1 – I_c/4.6)$ $(q_t/P_a)/ N_{60} = 10^{(1.1268 – 0.2817Ic)}$ P_a being atmospheric pressure	3, 5 15, 31
$(N_1)_{60}I_c$	SPT N_{60} value corrected for overburden pressure (using N_{60} I_c). User has 3 options.	*1) $(N_1)_{60}Ic = C_n \bullet (N_{60} I_c)$* 2) $q_{c1n}/ (N_1)_{60}I_c = 8.5 (1 – I_c/4.6)$ 3) $(Q_{tn})/ (N_1)_{60}I_c = 10^{(1.1268 – 0.2817Ic)}$	4 5 15, 31
S_u or S_u (N_{kt})	Undrained shear strength based on q_t S_u factor N_{kt} is user selectable.	$Su = \frac{qt - \sigma_v}{N_{kt}}$	1, 5
S_u or S_u (N_{du}) or S_u ($N_{\Delta u}$)	Undrained shear strength based on pore pressure S_u factor $N_{\Delta u}$ is user selectable.	$Su = \frac{u_2 - u_{eq}}{N_{\Delta u}}$	1, 5
D_r	Relative Density determined from one of the following user selectable options: 1) Ticino Sand 2) Hokksund Sand 3) Schmertmann (1978) 4) Jamiolkowski (1985) - All Sands 5) Jamiolkowski et al (2003) (various compressibilities, K_o)	See reference (methods 1 through 4) Jamiolkowski et al (2003) reference	5 14
PHI ϕ	Friction Angle determined from one of the following user selectable options (methods 1 through 4 are for sands and method 5 is for silts and clays): 1) Campanella and Robertson 2) Durgunoglu and Mitchel 3) Janbu 4) Kulhawy and Mayne 5) NTH method (clays and silts)	See appropriate reference	5 5 5 11 23
Delta U/q_t $\Delta u/q_t$ du/q_t	Differential pore pressure ratio (older parameter used before B_q was established)	$= \frac{\Delta u}{qt}$ *where:* $\Delta u = u - u_{eq}$ *and u = dynamic pore pressure* *u_{eq} = equilibrium pore pressure*	39

Calculated Parameter	Description	Equation	Ref
B_q	Pore pressure parameter	$Bq = \frac{\Delta u}{qt - \sigma_v}$ where: $\Delta u = u - u_{eq}$ *and* u *= dynamic pore pressure* u_{eq} *= equilibrium pore pressure*	1, 2, 5
Net q_t or qtNet	Net tip resistance (used in many subsequent correlations)	$qt - \sigma_v$	36
q_e or qE or q_E	Effective tip resistance (using the dynamic pore pressure u_2 and not equilibrium pore pressure)	$q_t - u_2$	36
qeNorm	Normalized effective tip resistance	$\frac{qt - u_2}{\sigma_v'}$	36
Q_t or Norm: Qt or Q_{t1}	Normalized q_t for Soil Behavior Type classification as defined by Robertson (1990) using a linear stress normalization. Note this is different from Q_{tn}. This parameter was renamed to Q_{t1} in Robertson, 2009. Without normalization limits this parameter calculates to very high unrealistic values at low stresses.	$Qt = \frac{qt - \sigma_v}{\sigma_v'}$	2, 5, 15
F_r or Norm: Fr	Normalized Friction Ratio for Soil Behavior Type classification as defined by Robertson (1990)	$Fr = 100\% \cdot \frac{fs}{qt - \sigma_v}$	2, 5
Q(1-B_q) Q(1-B_q) + 1	Q(1-B_q) grouping as suggested by Jefferies and Davies for their classification chart and the establishment of their I_c parameter. Later papers added the +1 term to the equation.	$Q \cdot (1 - Bq)$ $Q \cdot (1 - Bq) + 1$ *where Bq is defined as above and Q is the same as the normalized tip resistance,* Q_{t1}*, defined above*	6, 7, 34
q_{c1}	Normalized tip resistance, q_{c1}, using a fixed stress ratio exponent, n (this method has stress units)	$q_{c1} = q_t \cdot (Pa/\sigma_v')^{0.5}$ where: P_a = atmospheric pressure	21
q_{c1} (0.5)	Normalized tip resistance, q_{c1}, using a fixed stress ratio exponent, n (this method is unit-less)	$q_{c1}(0.5) = (q_t/P_a) \cdot (Pa/\sigma_v')^{0.5}$ where: P_a = atmospheric pressure	5
q_{c1} (C_n)	Normalized tip resistance, q_{c1}, based on C_n (this method has stress units)	$q_{c1}(Cn) = C_n * q_t$	5, 12
q_{c1} (C_q)	Normalized tip resistance, q_{c1}, based on C_q (this method has stress units)	$q_{c1}(Cq) = C_q * q_t$ (some papers use q_c)	5, 12
q_{c1n}	normalized tip resistance, q_{c1n}, using a variable stress ratio exponent, n (where n=0.0, 0.70, or 1.0) (this method is unit-less)	$q_{c1n} = (q_t / P_a)(P_a/\sigma_v')^n$ where: P_a = atm. Pressure and n varies as described below	3

Calculated Parameter	Description	Equation	Ref
I_c or Ic (RW1998)	Soil Behavior Type Index as defined by Robertson and Wride (1997, 1998) for estimating grain size characteristics and providing smooth gradational changes across the SBTn chart. Ic(RW1998) is different from that of Jefferies and Davies (7) and is different from Ic(PKR2009).	$I_c = [(3.47 - \log_{10}Q)^2 + (\log_{10} Fr + 1.22)^2]^{0.5}$ *Where:* $Q = \left(\frac{qt - \sigma_v}{P_a}\right)\left(\frac{P_a}{\sigma_v'}\right)^n$ *Or* $Q = q_{c1n} = \left(\frac{qt}{P_a}\right)\left(\frac{P_a}{\sigma_v'}\right)^n$ *depending on the iteration in determining I_c* *And Fr is in percent* *P_a = atmospheric pressure* *n has the following distinct values:* *0.5, 0.75 and 1.0* *and is determined in an iterative manner based on the resulting I_c in each iteration* *Note that NCEER replaced 0.75 with 0.70*	3, 4, 5 10
I_c (PKR 2009)	Soil Behavior Type Index, I_c (PKR 2009) is based on a variable stress ratio exponent n, which itself is based on I_c (PKR 2009). An iterative calculation is required to determine I_c (PKR 2009) and its corresponding n (PKR 2009).	*I_c (PKR 2009) =* *$[(3.47 - \log_{10}Q_{tn})^2 + (1.22 + \log_{10}F_r)^2]^{0.5}$*	15
n (PKR 2009)	Stress ratio exponent n, based on I_c (PKR 2009). An iterative calculation is required to determine n (PKR 2009) and its corresponding I_c (PKR 2009).	*n (PKR 2009) = 0.381 (I_c) + 0.05 (σ_v'/P_a) – 0.15*	15
Q_{tn} (PKR 2009)	Normalized tip resistance using a variable stress ratio exponent based on I_c (PKR 2009) and n (PKR 2009). An iterative calculation is required to determine Q_{tn} (PKR 2009).	*$Q_{tn} = [(qt - \sigma_v)/P_a](P_a/\sigma_v')^n$* *where P_a = atmospheric pressure (100 kPa)* *n = stress ratio exponent described above*	15
FC	Apparent fines content (%)	*FC=1.75($Ic^{3.25}$) - 3.7* *FC=100 for $I_c > 3.5$* *FC=0 for $I_c < 1.26$* *FC = 5% if 1.64 < I_c < 2.6 AND F_r<0.5*	3
I_c Zone	This parameter is the Soil Behavior Type zone based on the I_c parameter (valid for zones 2 through 7 on SBTn or SBT Qtn charts)	I_c < 1.31 Zone = 7 1.31 < I_c < 2.05 Zone = 6 2.05 < I_c < 2.60 Zone = 5 2.60 < I_c < 2.95 Zone = 4 2.95 < I_c < 3.60 Zone = 3 I_c > 3.60 Zone = 2	3
CD	The contractive / dilative boundary on Robertson's Modified SBTn (contractive/dilative) Chart shown in Figure 6 above. The boundary is marked as CD = 70 on the chart in the relevant paper. Similar to the $Q_{tn,cs}$ = 70 line in Figure 4.	CD = 70 = $(Q_{tn} - 11)(1 + 0.06F_r)^{17}$ lower bound of CD = 60: CD = 60 = $(Q_{tn} - 9.5)(1 + 0.06F_r)^{17}$	30

Calculated Parameter	Description	Equation	Ref
I_B	Hyberbolic fit defining the boundary between SBT soil types proposed by Schneider as a better fit than the I_c circles. I_B = 32 represents the boundary for most sand like soils. I_B = 22 represents the upper boundary for most clay like soils. The region between I_B=22 and I_B=32 is the "transitional soil" zone.	$I_B = 100\ (Q_{tn} + 10) / (70 + Q_{tn} F_r)$	30
State Param or State Parameter or ψ	The state parameter index, ψ, is defined as the difference between the current void ratio, e, and the critical void ratio, e_c. Positive ψ - contractive soil Negative ψ - dilative soil This is based on the work by Been and Jefferies (1985) and Plewes, Davies and Jefferies (1992) This method uses mean normal stresses based on a uniform value of K_0 or a calculated K_0 using methods described elsewhere in this document	See reference	6, 8
Yield Stress σ_p'	Yield stress is calculated using the following methods 1) General method 2) 1st order approximation using q_tNet (clays) 3) 1st order approximation using Δu_2 (clays) 4) 1st order approximation using q_e (clays) 5) Based on Vs	All stresses in kPa 1) $\sigma_p' = 0.33 \cdot (q_t - \sigma_v)^{m'} (\sigma_{atm}/100)^{1-m'}$ where $m' = 1 - \frac{0.28}{1 + (I_c / 2.65)^{25}}$ 2) $\sigma_p' = 0.33 \cdot (q_t - \sigma_v)$ 3) $\sigma_p' = 0.54 \cdot (\Delta u_2)$ $\Delta u_2 = u_2 - u_0$ 4) $\sigma_p' = 0.60 \cdot (q_t - u_2)$ 5) $\sigma_p' = (Vs/4.59)^{1.47}$	19 20 20 20 18
OCR OCR(JS1978) YSR(Mayne2014) YSR (qtNet) YSR (deltaU) YSR (qe) YSR (Vs) OCR (PKR2015)	Over Consolidation Ratio based on 1) Schmertmann (1978) method involving a plot plot of S_u/σ_v' /($S_u/\sigma_v')_{NC}$ and OCR  2) based on Yield stresses described above 3) approximate version based on qtNet 4) approximate version based on Δu 5) approximate version based on effective tip, q_e 6) approximate version based on shear wave velocity, V_s and σ_v' 7) based on Qt	1) requires a user defined value for NC Su/P_c' ratio 2 through 5) *based on yield stresses* 6) YSR (Vs) = $\sigma_p'(Vs) / \sigma_v'$ 7) OCR = $0.25 \cdot (Qt)^{1.25}$	9 19 20 20 20 18 32
Es/qt	Intermediate parameter for calculating Young's Modulus, E, in sands. It is the Y axis of the reference chart. Note that Figured 5.59 from reference 5, Lunne, Robertson and Powell, (LRP) has an error. The X axis values are too high by a factor of 10. The plot is based on Baldi's (not Bellotti as cited in	Based on Figure 5.59 in the reference	5, 37

Calculated Parameter	Description	Equation	Ref
	LRP) original Figure 3 where the X axis is: $\frac{q_c}{\sqrt{\sigma'_v}}$ (both in kPa) with a range of 200 to 3000. Figure 5.59 from LRP shows a dimensionless form of the equation, q_{c1}, displaying the same range of values. Figure 5.59's X axis uses $q_{c1} = \left(\frac{q_c}{P_a}\right)\left(\frac{P_a}{\sigma'_v}\right)^{0.5}$ The two expressions are not the same: they differ by a factor of $\frac{\sqrt{P_a}}{P_a}$. With P_a taken to be 100 kPa the factor is 1/10. Substituting typical values of 200 bar (20000 kPa) for q_c and 225 kPa for σ_v' one gets: 20000 / 15 = 1333.33 for Bellotti's axis and $(200/1)(100/225)^{0.5}$ = 200 * (10/15) = 133.3 for LRP's axis (noting that P_a = 1 bar) showing a factor of 10 difference.		
Es or E_s Young's Modulus E	Young's Modulus based on the work done in Italy. There are three types of sands considered in this technique. The user selects the appropriate type for the site from: a) OC Sands b) Aged NC Sands c) Recent NC Sands Each sand type has a family of curves that depend on mean normal stress. The program calculates mean normal stress and linearly interpolates between the two extremes provided in the E_s/q_t chart. E_s is evaluated for an axial strain of 0.1%.	Mean normal stress is evaluated from: $\sigma'_m = \frac{1}{3}(\sigma'_v + \sigma'_h + \sigma'_h)$ where σ_v'= vertical effective stress σ_h'= horizontal effective stress *and* $\sigma_h = K_o \cdot \sigma_v'$ with K_o assumed to be 0.5	5
Delta U/TStress $\Delta u / \sigma_v$	Differential pore pressure ratio with respect to total stress	$= \frac{\Delta u}{\sigma_v}$ *where:* $\Delta u = u - u_{eq}$	39
Delta U/EStress, P Value, Excess Pore Pressure Ratio $\Delta u/\sigma_v'$	Differential pore pressure ratio with respect to effective stress. Key parameter (P, Normalized Pore Pressure Parameter, Excess Pore Pressure Ratio) in the Winckler et. al. static liquefaction method.	$= \frac{\Delta u}{\sigma'_v}$ *where:* $\Delta u = u - u_{eq}$	25, 25a
Su/EStress S_u/σ_v'	Undrained shear strength ratio with respect to vertical effective overburden stress using the S_u (N_{kt}) method	= *Su* (N_{kt}) / σ_v'	9, 23
Vs or V_s	Recorded shear wave velocities (not estimated). The shear wave velocities are typically collected over 1 m depth intervals. Each data point over the relevant depth range is assigned the same V_s value.	recorded data	27
Vp or V_p	Recorded compression wave (or P wave) velocities (not estimated). The P wave velocities are typically collected over 1 m depth intervals. Each data point over the relevant depth range is assigned the same V_p value.	recorded data	27

Calculated Parameter	Description	Equation	Ref
V_{s30} V_{s100}	The average shear wave velocity of the near surface materials to a depth of 30 m (100 ft). It is based on the sum of all travel times through all layers in the top 30m (100 ft). V_{s100} is the same calculation as V_{s30} except down to a depth of 100 feet.	$V_{s30} = \frac{total\ thickness\ of\ all\ layers\ to\ 30\ m}{\Sigma\left(\frac{layer\ thickness}{layer\ shear\ wave\ velocity}\right)}$ $V_{s30} = \frac{total\ thickness\ of\ all\ layers\ to\ 30\ m}{\Sigma\ (layer\ travel\ times)}$	38
G_{max}	G_{max} determined from SCPT shear wave velocities (not estimated values). Note that seismic data (V_s) is collected over set depth intervals (typically 1 meter). Each data point over the test segment is assigned the same V_s value. Since soil density changes with depth, slightly different G_{max} values may be calculated over the test depth interval.	$G_{max} = \rho V_s^2$ where ρ is the mass density of the soil determined from the estimated unit weights at each test depth	27
qtNet/G_{max}	Net tip resistance ratio with respect to the small strain modulus G_{max} determined from SCPT shear wave velocities (not estimated values)	$= (qt - \sigma_v) / G_{max}$ where $G_{max} = \rho V_s^2$ and ρ is the mass density of the soil determined from the estimated unit weights at each test depth	15, 28, 30
qUlt	A site specific and client specific parameter for estimating the limiting stress for "crane walk" accessibility	$q_{ult} = CraneWalkFactor \cdot S_u$ Where: *CraneWalkFactor* is client provided	U*
Estimated G_o	Estimated value for small strain shear modulus	$G_o = 0.0188[10^{(0.55Ic + 1,68)}](q_t - \sigma_v)$	15
Estimated E_{25}	Estimated value for Young's Modulus, E, at a 25% working load	$E_{25} = \alpha_E$ (qtNet) where $\alpha_E = 0.015[10^{(0.55Ic + 1,68)}]$	15
k_{SBT}	Estimated soil permeability derived from Soil Behavior Type (SBT) Chart I_c values.	For $1.0 < I_c \leq 3.27$: $k = 10^{(0.952 - 3.04Ic)}$ in m/s For $3.27 < Ic < 4.0$: $k = 10^{(-4.52 - 1.37Ic)}$ in m/s	35
M or D' Constrained Modulus	Constrained Modulus based on 1) Robertson, M 2) Mayne, D'	1) Robertson $M = \alpha_M (q_t - \sigma_v)$ $I_c > 2.2$ (fine grained) $\alpha_M = Qt$ when $Qt < 14$ $\alpha_M = 14$ when $Qt > 14$ $Ic < 2.2$ (coarse grained) $\alpha_M = 0.0188\ [10^{(0.55Ic + 1.68)}]$ $D' = \alpha_D (qt - \sigma_v)$ where $\alpha_D = 5$	32 23

Table 1b. CPT Parameter Calculation Methods – Liquefaction Parameters

Calculated Parameter	Description	Equation	Ref
K_{SPT} or K_s	Equivalent clean sand factor for $(N_1)60$	$K_{SPT} = 1 + ((0.75/30) \bullet (FC - 5))$	10
K_{CPT} or K_c (RW1998)	Equivalent clean sand correction for q_{c1N}	$K_{cpt} = 1.0$ for $I_c \leq 1.64$ $K_{cpt} = f(I_c)$ for $I_c > 1.64$ (see reference) $K_c = -0.403\ I_c^4 + 5.581\ I_c^3 - 21.63 I_c^2 + 33.75\ I_c - 17.88$	3, 10
K_c (PKR 2010)	Clean sand equivalent factor to be applied to Q_{tn}	$K_c = 1.0$ for $I_c \leq 1.64$ $K_c = -0.403\ I_c^4 + 5.581\ I_c^3 - 21.63 I_c^2 + 33.75\ I_c - 17.88$ for $I_c > 1.64$	16
$(N_1)_{60cs}I_C$	Clean sand equivalent SPT $(N_1)_{60}I_c$. User has 3 options.	1) $(N_1)_{60cs}Ic = \alpha + \beta((N_1)_{60}I_c)$ 2) $(N_1)_{60cs}Ic = K_{SPT} * ((N_1)_{60}I_c)$ 3) $(q_{c1ncs})/(N_1)_{60cs}I_c = 8.5\ (1 - I_c/4.6)$ FC ≤ 5%: $\alpha = 0,\ \beta = 1.0$ FC ≥ 35% $\alpha = 5.0,\ \beta = 1.2$ 5% < FC < 35% $\alpha = exp[1.76 - (190/FC^2)]$ $\beta = [0.99 + (FC^{1.5}/1000)]$	10 10 5
q_{c1ncs}	Clean sand equivalent q_{c1n}	$q_{c1ncs} = q_{c1n} \bullet K_{cpt}$	3
$Q_{tn,cs}$ (PKR 2010)	Clean sand equivalent for Q_{tn} described above - Q_{tn} being the normalized tip resistance based on a variable stress exponent as defined by Robertson (2009)	$Q_{tn,cs} = Q_{tn} \cdot K_c$ (PKR 2016)	16
Su(Liq)/ESv or $S_u(Liq)/\sigma_v'$	Liquefied shear strength ratio as defined by Olson and Stark	$\frac{S_u(Liq)}{\sigma_v'} = 0.03 + 0.0143(q_{c1})$ Note: σ_v' and s_v' are synonymous	13
Su(Liq)/ESv or $S_u(Liq)/\sigma_v'$ (PKR 2010)	Liquefied shear strength ratio as defined by Robertson (2010)	$\frac{S_u(Liq)}{\sigma_v'}$ Based on a function involving $Q_{tn,cs}$	16
S_u (Liq) (PKR 2010)	Liquefied shear strength derived from the liquefied shear strength ratio and effective overburden stress	$S_u(Liq) = \sigma_v' \cdot \left(\frac{S_u(Liq)}{\sigma_v'}\right)$	16
Cont/Dilat Tip	Contractive / Dilative q_{c1} Boundary based on $(N_1)_{60}$	$(\sigma_v')_{boundary} = 9.58 \times 10^{-4}\ [(N_1)_{60}]^{4.79}$ q_{c1} is calculated from specified q_t(MPa)/N ratio	13
CRR	Cyclic Resistance Ratio (for Magnitude 7.5)	$q_{c1ncs} < 50$: $CRR_{7.5} = 0.833\ [q_{c1ncs}/1000] + 0.05$ $50 \leq q_{c1ncs} < 160$: $CRR_{7.5} = 93\ [q_{c1ncs}/1000]^3 + 0.08$	10
Kg or K_g	Small strain Stiffness Ratio Factor, K_g	$[G_{max}/q_t]/[q_{c1n}{}^{-m}]$ m = empirical exponent, typically 0.75	26

Calculated Parameter	Description	Equation	Ref
K_g*	Revised K_g factor extended to fine grained soils (Robertson).	$K_g^* = (G_o / q_n)(Q_{tn})^{0.75}$ where q_n is the net tip resistance = $q_t - \sigma_v$	30
SP Distance	State Parameter Distance, Winckler static liquefaction method	Perpendicular distance on Q_{tn} chart from plotted point to state parameter Ψ = -0.05 curve	25
URS NP Fr	Normalized friction ratio point on Ψ = -0.05 curve used in SP distance calculation		25
URS NP Q_{tn}	Normalized tip resistance (Q_{tn}) point on Ψ = -0.05 curve used in SP Distance calculation		25

Table 2. References

No.	Reference
1	Robertson, P.K., Campanella, R.G., Gillespie, D. and Greig, J., 1986, "Use of Piezometer Cone Data", Proceedings of InSitu 86, ASCE Specialty Conference, Blacksburg, Virginia.
2	Robertson, P.K., 1990, "Soil Classification Using the Cone Penetration Test", Canadian Geotechnical Journal, Volume 27. This includes the discussions and replies.
3	Robertson, P.K. and Wride (Fear), C.E., 1998, "Evaluating cyclic liquefaction potential using the cone penetration test", Canadian Geotechnical Journal, 35: 442-459.
4	Robertson, P.K. and Wride, C.E., 1997, "Cyclic Liquefaction and its Evaluation Based on SPT and CPT", NCEER Workshop Paper, January 22, 1997.
5	Lunne, T., Robertson, P.K. and Powell, J. J. M., 1997, " Cone Penetration Testing in Geotechnical Practice," Blackie Academic and Professional.
6	Plewes, H.D., Davies, M.P. and Jefferies, M.G., 1992, "CPT Based Screening Procedure for Evaluating Liquefaction Susceptibility", 45th Canadian Geotechnical Conference, Toronto, Ontario, October 1992.
7	Jefferies, M.G. and Davies, M.P., 1993, "Use of CPTu to Estimate equivalent N_{60}", Geotechnical Testing Journal, 16(4): 458-467.
8	Been, K. and Jefferies, M.P., 1985, "A state parameter for sands", Geotechnique, 35(2), 99-112.
9	Schmertmann, 1978, "Guidelines for Cone Penetration Test Performance and Design", Federal Highway Administration Report FHWA-TS-78-209, U.S. Department of Transportation.
10	Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils, Salt Lake City, 1996, chaired by Leslie Youd.
11	Kulhawy, F.H. and Mayne, P.W., 1990, "Manual on Estimating Soil Properties for Foundation Design, Report No. EL-6800", Electric Power Research Institute, Palo Alto, CA, August 1990, 306 p.
12	Olson, S.M. and Stark, T.D., 2002, "Liquefied strength ratio from liquefied flow failure case histories", Canadian Geotechnical Journal, 39: 951-966.
13	Olson, Scott M. and Stark, Timothy D., 2003, "Yield Strength Ratio and Liquefaction Analysis of Slopes and Embankments", Journal of Geotechnical and Geoenvironmental Engineering, ASCE, August 2003.
14	Jamiolkowski, M.B., Lo Presti, D.C.F. and Manassero, M., 2003, "Evaluation of Relative Density and Shear Strength of Sands from CPT and DMT", Soil Behaviour and Soft Ground Construction, ASCE, GSP N0. 119, 201-238.
15	Robertson, P.K., 2009, "Interpretation of cone penetration tests – a unified approach", Canadian Geotechnical Journal, 46: 1337-1355.
16	Robertson, P.K., 2010a, "Evaluation of Flow Liquefaction and Liquefied Strength Using the Cone Penetration Test", Journal of Geotechnical and Geoenvironmental Engineering, ASCE, June 2010.
17	Mayne, P.W. and Kulhawy, F.H., 1982, "Ko-OCR Relationships in Soil", Journal of the Geotechnical Engineering Division, ASCE, Vol. 108, GT6, pp. 851-872.
18	Mayne, P.W., Robertson P.K. and Lunne T., 1998, "Clay stress history evaluated from seismic piezocone tests", Proceedings of the First International Conference on Site Characterization – ISC '98, Atlanta Georgia, Volume 2, 1113-1118.

No.	Reference
19	Mayne, P.W., 2014, "Generalized CPT Method for Evaluating Yield Stress in Soils", Geocharacterization for Modeling and Sustainability (GSP 235: Proc. GeoCongress 2014, Atlanta, GA), ASCE, Reston, Virginia: 1336-1346.
20	Mayne, P.W., 2015, "Geocharacterization by In-Situ Testing", Continuing Education Course, Vancouver, BC, January 6-8, 2015.
21	Robertson, P.K. and Fear, C.E., 1995, "Liquefaction of sands and its evaluation", Proceedings of the First International Conference on Earthquake Engineering, Keynote Lecture IS Tokyo '95, Tokyo Japan, 1995.
22	Mayne, P.W., Peuchen, J. and Boumeester, D., 2010, "Soil unit weight estimation from CPTs", Proceeding of the 2nd International Symposium on Cone Penetration Testing (CPT '10), Vol 2, Huntington Beach, California; Omnipress: 169-176.
23	Mayne, P.W., 2007, "NCHRP Synthesis 368 on Cone Penetration Test", Transportation Research Board, National Academies Press, Washington, D.C., 118 pages.
24	Mayne, P.W., 2014, "Interpretation of geotechnical parameters from seismic piezocone tests.", Key note address #2, proceedings, 3rd International Symposium on Cone Penetration Testing (CPT'14, Las Vegas), ISSMGE Technical Committee TC102.
25	Winckler, Christina, Davidson, Richard, Yenne, Lisa, Pilz, Jorgen, 2014, "CPTu-Based State Characterization of Tailings Liquefaction Susceptibility", Tailings and Mine Waste, 2014.
25a	Winckler, Christina, Davidson, Richard, Yenne, Lisa, Pilz, Jorgen, 2014, "CPTu-Based State Characterization of Tailings Liquefaction Susceptibility", Powerpoint presentation, Tailings and Mine Waste, 2014.
26	Schneider, J.A. and Moss, R.E.S., 2011, "Linking cyclic stress and cyclic strain based methods for assessment of cyclic liquefaction triggering in sands", Geotechnique Letters 1, 31-36.
27	Rice, A., 1984, "The Seismic Cone Penetrometer", M.A.Sc. thesis submitted to the University of British Columbia, Dept. of Civil Engineering, Vancouver, BC, Canada.
28	Gillespie, D.G., 1990, "Evaluating Shear Wave Velocity and Pore Pressure Data from the Seismic Cone Penetration Test", Ph.D. thesis submitted to the University of British Columbia, Dept. of Civil Engineering, Vancouver, BC, Canada.
29	Robertson, P.K and Cabal, K.L., 2010, "Estimating soil unit weight from CPT", Proceedings of the 2nd International Symposium on Cone Penetration Testing (CPT '10), Huntington Beach, California.
30	Robertson, P.K., 2016, "Cone penetration test (CPT)-based soil behaviour type (SBT) classification system – an update", Canadian Geotechnical Journal, July 2016.
31	Robertson, P.K., 2012, "Interpretation of in-situ tests – some insights", Mitchell Lecture, ISC'4, Recife, Brazil.
32	Robertson, P.K., Cabal, K.L. 2015, "Guide to Cone Penetration Testing for Geotechnical Engineering", 6th Edition.
33	Robertson, P.K., 2010b, "Soil behaviour type from CPT: an update", Proceedings of the 2nd International Symposium on Cone Penetration Testing (CPT '10), Huntington Beach, California.
34	Been, K., Romero, S., Obermeyer, J. and Hebeler, G., 2012, "Determining in situ state of sand and silt tailings from the CPT", Tailings and Mine Waster 2012, 325-333.
35	Robertson, P.K., 2010, "Estimating in-situ soil permeability from CPT & CPTu", Proceedings of the 2nd International Symposium on Cone Penetration Testing (CPT '10), Huntington Beach, California.
36	Mayne, P.W., Cargill, E. and Greig, J., 2023, "The Cone Penetration Test: A CPT Design Parameter Manual", ConeTec Group
37	Baldi, G., Bellotti, R., Ghionna,V., Jamiolkowski, M. and Lo Presti, D. 1989. Modulus of sands from CPTs and DMTs. *Proc. Intl. Conf. on Soil Mechanics & Foundation Engineering*, Vol. 1 (ICSMFE, Rio de Janeiro), Balkema, Rotterdam: 165–170. www.issmge.org
38	Crow, H.L, Hunter, J.A. and Bobrowsky, P.T., 2012, "National shear wave measurement guidelines for Canadian seismic site assessment", Proceedings of GeoManitoba 2012, the 65th Canadian Geotechnical Conference.
39	Campanella, R.G., Robertson, P.K., Gillespie, D., 1982, "Cone penetration testing in deltaic soils", Canadian Geotechnical Journal, 20: 23-35.

Electric Field Vane Shear Test Profile Summary, Results and Timing

CONETEC

Job Number:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford SCPTu - SRK
Start Date:	2024-02-15
End Date:	2024-03-21

ELECTRIC FIELD VANE SHEAR TEST SUMMARY

Sounding ID	File Name	Adjacent CPT Sounding ID	Rig	Date From	Date To	Northing[1] (m)	Easting[1] (m)	Refer to Notation Number
VST24-LGE-BH04	24-05-27159_VST04	N/A	Portable	2024-02-26	2024-02-26	5407273	476519	
VST24-LGE-BH05	24-05-27159_VST05	N/A	Portable	2024-02-15	2024-02-15	5408925	475900	
VST24-LGE-BH201	24-05-27159_VST201	SCPT24-LGE-BH201	Portable	2024-02-21	2024-02-22	5407385	474826	
VST24-LGE-BH202	24-05-27159_VST202	SCPT24-LGE-BH202	Portable	2024-02-20	2024-02-20	5408589	475370	
VST24-LGE-BH203	24-05-27159_VST203	SCPT24-LGE-BH203	Portable	2024-02-19	2024-02-19	5409185	476444	
VST24-LGE-BH204	24-05-27159_VST204	SCPT24-LGE-BH204	Portable	2024-02-23	2024-02-23	5407349	475668	
VST24-TMF-MW08AB	24-05-27159_VSTTMF08AB	SCPT24-TMF-MW08AB	Portable	2024-03-13	2024-03-15	5401996	476471	
VST24-TMF-BH202	24-05-27159_VSTTMF202	SCPT24-TMF-BH202	Portable	2024-03-18	2024-03-19	5404211	476824	
VST24-TMF-BH207	24-05-27159_VSTTMF207	SCPT24-TMF-BH207	Portable	2024-03-16	2024-03-17	5402798	476815	
VST24-WRD-BH201	24-05-27159_VSTWRD201	SCPT24-WRD-BH201	Portable	2024-03-05	2024-03-06	5411098	473341	
VST24-WRD-BH202	24-05-27159_VSTWRD202	SCPT24-WRD-BH202	Portable	2024-03-20	2024-03-21	5412173	474133	
VST24-WRD-BH205	24-05-27159_VSTWRD205	SCPT24-WRD-BH205	Portable	2024-03-16	2024-03-16	5413522	474142	
VST24-WRD-BH207	24-05-27159_VSTWRD207	SCPT24-WRD-BH207	Portable	2024-03-15	2024-03-15	5414551	474232	
VST24-WRD-BH212	24-05-27159_VSTWRD212	SCPT24-WRD-BH212	Portable	2024-03-09	2024-03-10	5411065	474214	
VST24-WRD-BH218	24-05-27159_VSTWRD218	N/A	Portable	2024-03-14	2024-03-14	5414720	473205	

1. Coordinates were collected with a consumer grade GPS device in Datum WGS84/ Zone 17N.

Job Number:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford SCPTu - SRK
Start Date:	2024-02-15
End Date:	2024-03-21

ELECTRIC FIELD VANE SHEAR TEST RESULTS

Sounding ID	File Name	Date	Load Cell Serial Number	Load Cell Location	Casing/Drillout Depth (m)	Test Depth[1] (m)	Vane Diameter D (mm)	Vane Height H (mm)	Top Taper Angle i_T (deg)	Bottom Taper Angle i_B (deg)	Vane Factor (kPa/Nm)	Peak Torque (Nm)	Remolded Torque (Nm)	Peak Stress (kPa)	Remolded Stress (kPa)	Peak Frictional Stress (kPa)	Remolded Frictional Stress (kPa)	Su Peak (kPa)	Su Remolded (kPa)	Sensitivity	Refer to Notation Number
VST24-LGE-BH04	24-05-27159_VST04	2024-02-26	AVLC040	Surface	7.01	8.23	75	150	45	45	0.6106	74.11	28.14	45.3	17.2	2.6	2.6	42.7	14.6	2.9	
VST24-LGE-BH04	24-05-27159_VST04	2024-02-26	AVLC040	Surface	10.36	11.89	75	150	45	45	0.6106	65.00	16.18	39.7	9.9	1.8	2.2	37.9	7.7	4.9	
VST24-LGE-BH04	24-05-27159_VST04	2024-02-27	AVLC040	Surface	13.41	14.94	75	150	45	45	0.6106	66.17	21.05	40.4	12.9	1.7	2.3	38.7	10.6	3.7	
VST24-LGE-BH04	24-05-27159_VST04	2024-02-27	AVLC040	Surface	16.46	17.68	75	150	45	45	0.6106	61.61	22.79	37.6	13.9	1.2	1.2	36.4	12.7	2.9	
VST24-LGE-BH05	24-05-27159_VST05	2024-02-15	AVLC039	Surface	9.14	10.67	75	150	45	45	0.6106	>110.73									2
VST24-LGE-BH05	24-05-27159_VST05	2024-02-15	AVLC039	Surface	12.80	13.11	75	150	45	45	0.6106	90.07	32.09	55.0	19.6	1.2	2.1	53.8	17.5	3.1	
VST24-LGE-BH201	24-05-27159_VST201	2024-02-22	AVLC040	Surface	3.05	4.27															9
VST24-LGE-BH201	24-05-27159_VST201	2024-02-22	AVLC040	Surface	3.05	4.57	75	150	45	45	0.6106		37.41		22.8		2.4		20.5		4
VST24-LGE-BH202	24-05-27159_VST202	2024-02-20	AVLC039	Surface	3.96	4.57	75	150	45	45	0.6106	63.05	7.63	38.5	4.7	1.6	0.4	36.9	4.3	8.6	
VST24-LGE-BH203	24-05-27159_VST203	2024-02-19	AVLC039	Surface	6.10	6.71	75	150	45	45	0.6106	14.94	16.38		10.0	1.4	1.3		8.7		5
VST24-LGE-BH203	24-05-27159_VST203	2024-02-19	AVLC039	Surface	13.11	14.33	75	150	45	45	0.6106	77.95	22.30	47.6	13.6	1.7	1.7	45.9	11.9	3.8	
VST24-LGE-BH203	24-05-27159_VST203	2024-02-19	AVLC039	Surface	19.20	19.81	75	150	45	45	0.6106	41.46	9.91	25.3	6.0	1.1	0.9	24.2	5.1	4.7	
VST24-LGE-BH203	24-05-27159_VST203	2024-02-19	AVLC039	Surface	22.25	23.17	75	150	45	45	0.6106	79.20	23.81	48.4	14.5	2.8	3.4	45.5	11.1	4.1	
VST24-LGE-BH204	24-05-27159_VST204	2024-02-23	AVLC039	Surface	7.01	7.62	75	150	45	45	0.6106	28.89	20.55	17.6	12.5	1.7	1.4	15.9	11.1	1.4	
VST24-LGE-BH204	24-05-27159_VST204	2024-02-24	AVLC039	Surface	12.19	13.41	75	150	45	45	0.6106	83.55	21.49	51.0	13.1	7.4	3.8	43.6	9.3	4.7	
VST24-LGE-BH204	24-05-27159_VST204	2024-02-24	AVLC039	Surface		18.29															6
VST24-TMF-MW08AB	24-05-27159_VSTTMF08AB	2024-03-13	AVLC040	Surface	7.01	8.54	60	120	45	45	1.1926	8.75	3.90	10.4	4.6	1.0	1.0	9.5	3.7	2.6	
VST24-TMF-MW08AB	24-05-27159_VSTTMF08AB	2024-03-14	AVLC040	Surface	13.72	14.33	60	120	45	45	1.1926	41.32	15.57	49.3	18.6	3.4	3.4	45.9	15.1	3.0	3
VST24-TMF-MW08AB	24-05-27159_VSTTMF08AB	2024-03-15	AVLC040	Surface	19.20	20.27	60	120	45	45	1.1926	57.23	20.06	68.3	23.9	3.6	2.6	64.7	21.4	3.0	
VST24-TMF-MW08AB	24-05-27159_VSTTMF08AB	2024-03-15	AVLC040	Surface	27.43	28.96	60	120	45	45	1.1926	70.47	32.63	84.0	38.9	7.4	4.1	76.6	34.8	2.2	
VST24-TMF-BH202	24-05-27159_VSTTMF202	2024-03-18	AVLC040	Surface	3.96	4.57	60	120	45	45	1.1926	17.79	7.89	21.2	9.4	0.9	2.4	20.3	7.0	2.9	
VST24-TMF-BH202	24-05-27159_VSTTMF202	2024-03-18	AVLC040	Surface	7.01	7.32															8
VST24-TMF-BH202	24-05-27159_VSTTMF202	2024-03-19	AVLC038	Surface	11.58	13.41	60	120	45	45	1.1926	41.89	15.81	50.0	18.9	5.1	3.6	44.8	15.3	2.9	
VST24-TMF-BH202	24-05-27159_VSTTMF202	2024-03-19	AVLC038	Surface	14.63	16.16	60	120	45	45	1.1926	34.12	7.35	40.7	8.8	2.1	2.1	38.5	6.6	5.8	7
VST24-TMF-BH202	24-05-27159_VSTTMF202	2024-03-19	AVLC038	Surface	17.68	19.42	60	120	45	45	1.1926	53.24	25.95	63.5	30.9	5.2	5.1	58.3	25.9	2.3	
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-16	AVLC040	Surface		3.96															9
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-16	AVLC040	Surface		4.27															9
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-16	AVLC040	Surface	3.96	4.57	60	120	45	45	1.1926	16.13		19.2		0.7		18.5			
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-16	AVLC040	Surface	3.96	4.88	60	120	45	45	1.1926	19.61	9.12	23.4	10.9	1.9	0.5	21.5	10.4	2.1	
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-17	AVLC040	Surface	12.19	12.50	60	120	45	45	1.1926	36.24	10.73	43.2	12.8	2.0	4.0	41.3	8.8	4.7	
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-17	AVLC040	Surface	17.68	18.59	60	120	45	45	1.1926	31.20	3.57	37.2	4.3	2.3	0.4	34.9	3.9	9.0	
VST24-TMF-BH207	24-05-27159_VSTTMF207	2024-03-17	AVLC040	Surface	20.73	21.34	60	120	45	45	1.1926	37.80	6.60	45.1	7.9	5.3	2.7	39.8	5.2	7.7	
VST24-WRD-BH201	24-05-27159_VSTWRD201	2024-03-05	AVLC040	Surface	5.49	6.10	75	150	45	45	0.6106	41.59		25.4		1.4		24.0			
VST24-WRD-BH201	24-05-27159_VSTWRD201	2024-03-05	AVLC040	Surface	5.49	6.40	75	150	45	45	0.6106	73.56	41.33	44.9	25.2	2.4	1.7	42.5	23.5	1.8	11
VST24-WRD-BH201	24-05-27159_VSTWRD201	2024-03-05	AVLC040	Surface	10.97	11.58	75	150	45	45	0.6106	68.55	22.35	41.9	13.6	1.8	1.8	40.1	11.8	3.4	
VST24-WRD-BH201	24-05-27159_VSTWRD201	2024-03-06	AVLC040	Surface	16.16	17.37	75	150	45	45	0.6106	91.22	35.18	55.7	21.5	3.5	3.5	52.2	18.0	2.9	
VST24-WRD-BH201	24-05-27159_VSTWRD201	2024-03-06	AVLC040	Surface	19.51	21.34	75	150	45	45	0.6106	88.71				3.3					12
VST24-WRD-BH201	24-05-27159_VSTWRD201	2024-03-06	AVLC040	Surface		21.64															8
VST24-WRD-BH202	24-05-27159_VSTWRD202	2024-03-20	AVLC066	Surface	4.57	5.80	40	80	45	45	4.0249	11.07	6.17	44.5	24.9	7.9	13.7	36.7	11.2	3.3	
VST24-WRD-BH202	24-05-27159_VSTWRD202	2024-03-20	AVLC066	Surface	7.62	8.84															10
VST24-WRD-BH202	24-05-27159_VSTWRD202	2024-03-20	AVLC066	Surface	7.62	9.23	60	120	45	45	1.1926	72.77	36.53	86.8	43.6	16.4	10.0	70.4	33.6	2.1	
VST24-WRD-BH202	24-05-27159_VSTWRD202	2024-03-20	AVLC066	Surface	7.62	9.55	60	120	45	45	1.1926	68.51	51.46	81.7	61.4	9.3	15.8	72.4	45.6	1.6	
VST24-WRD-BH202	24-05-27159_VSTWRD202	2024-03-20	AVLC066	Surface	10.67	11.89	60	120	45	45	1.1926	39.60	10.02	47.2	11.9	5.1	3.5	42.1	8.4	5.0	
VST24-WRD-BH202	24-05-27159_VSTWRD202	2024-03-21	AVLC066	Surface	14.63	16.15	60	120	45	45	1.1926	42.53	9.92	50.7	11.8	4.5	3.1	46.3	8.8	5.3	
VST24-WRD-BH205	24-05-27159_VSTWRD205	2024-03-16	AVLC066	Surface	4.57	5.80	40	80	45	45	4.0249	11.31	4.58	45.5	18.4	9.4	8.6	36.1	9.8	3.7	
VST24-WRD-BH205	24-05-27159_VSTWRD205	2024-03-16	AVLC066	Surface	4.57	6.15	60	120	45	45	1.1926	33.20	20.81	39.6	24.8	4.9	2.8	34.7	22.0	1.6	
VST24-WRD-BH205	24-05-27159_VSTWRD205	2024-03-16	AVLC066	Surface	6.10	7.30	60	120	45	45	1.1926	>108.43	59.17		70.6	3.6	2.4		68.1		2
VST24-WRD-BH207	24-05-27159_VSTWRD207	2024-03-15	AVLC066	Surface	3.95	5.15	60	120	45	45	1.1926	>104.49				12.9					2
VST24-WRD-BH207	24-05-27159_VSTWRD207	2024-03-15	AVLC066	Surface	3.95	5.50	40	80	45	45	4.0249	44.19	25.98	177.9	104.6	43.4	45.0	134.4	59.6	2.3	
VST24-WRD-BH212	24-05-27159_VSTWRD212	2024-03-09	AVLC066	Surface	2.44	3.66	75	150	45	45	0.6106	49.11	18.83	30.0	11.5	1.7	1.2	28.3	10.3	2.7	
VST24-WRD-BH212	24-05-27159_VSTWRD212	2024-03-09	AVLC066	Surface	7.01	8.54	75	150	45	45	0.6106	42.57	12.35	26.0	7.5	1.2	1.5	24.8	6.0	4.1	

Job Number:	24-05-27159
Client:	Canada Nickel Company
Project:	Crawford SCPTu - SRK
Start Date:	2024-02-15
End Date:	2024-03-21

ELECTRIC FIELD VANE SHEAR TEST RESULTS

Sounding ID	File Name	Date	Load Cell Serial Number	Load Cell Location	Casing/Drillout Depth (m)	Test Depth[1] (m)	Vane Diameter D (mm)	Vane Height H (mm)	Top Taper Angle i_T (deg)	Bottom Taper Angle i_B (deg)	Vane Factor (kPa/Nm)	Peak Torque (Nm)	Remolded Torque (Nm)	Peak Stress (kPa)	Remolded Stress (kPa)	Peak Frictional Stress (kPa)	Remolded Frictional Stress (kPa)	Su Peak (kPa)	Su Remolded (kPa)	Sensitivity	Refer to Notation Number
VST24-WRD-BH212	24-05-27159_VSTWRD212	2024-03-10	AVLC066	Surface	12.80	13.41	75	150	45	45	0.6106	83.47	20.22	51.0	12.3	2.1	2.1	48.8	10.2	4.8	
VST24-WRD-BH215	24-05-27159_VSTWRD215	2024-03-11	AVLC066	Surface		3.66															6
VST24-WRD-BH218	24-05-27159_VSTWRD218	2024-03-14	AVLC066	Surface		3.66															6
VST24-WRD-BH218	24-05-27159_VSTWRD218	2024-03-14	AVLC066	Surface	3.95	5.15	60	120	45	45	1.1926	43.06	25.93	51.3	30.9	3.2	1.1	48.1	29.9	1.6	

1. Test depths are referenced to the middle of the vane.
2. Vane load cell was maxed out.
3. Slip coupler effect not observed in the remold test. The peak frictional stress value was assumed as the remolded frictional stress.
4. Unsuccessful peak test. Remolded test data is provided.
5. Unsucessful peak test. Peak test data provided for reference
6. Test attempt was unsuccessful due ground conditions resulting in damage to the vane blade.
7. Slip coupler effect not observed in the peak test. The remolded frictional stress value was assumed as the peak frictional stress.
8. Test attempt was unsuccessful due to an equipment issue.
9. Test attempt was unsuccesful. The test was re-done at 4.57 m.
10. Test unsuccessful due to chuck slippage during the test. The test was re-done at 9.23m.
11. Chuck slippage observed during the peak test.
12. No clear peak stress captured. Attempted re-test at 21.64 m was unsuccesful

CONETEC

Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Start Date: 2024-02-15
End Date: 2024-03-21

ELECTRIC FIELD VANE SHEAR TEST TIMING

Sounding ID	Date	Test Depth[1] (m)	Vane Insertion Time (HH:mm)	Peak Test Start Time (HH:mm)	Insertion to Start Interval (min)	Start to Failure Interval (sec)	Peak Test Avg Rate (deg/sec)	Remolding Completion Time (HH:mm)	Remold Test Start Time (HH:mm)	Remolding to Start Interval (min)	Remold Test Avg Rate (deg/sec)	Refer to Notation Number
VST24-LGE-BH04	2024-02-26	8.23	16:12	16:13	1	407	0.11	16:51	16:51	1	0.10	
VST24-LGE-BH04	2024-02-26	11.89	22:24	22:24	0	776	0.11	22:54	22:54	1	0.10	
VST24-LGE-BH04	2024-02-27	14.94	01:10	01:10	1	435	0.10	01:34	01:34	0	0.10	
VST24-LGE-BH04	2024-02-27	17.68	04:07	04:08	1	404	0.10	04:41	04:41	1	0.09	
VST24-LGE-BH05	2024-02-15	10.67	15:15	15:16	2	661	0.09					
VST24-LGE-BH05	2024-02-15	13.11	17:18	17:20	2	491	0.10	18:04	18:05	1	0.10	
VST24-LGE-BH201	2024-02-22	4.57						00:59	00:59	0	0.10	
VST24-LGE-BH202	2024-02-20	4.57	16:19	16:23	4	521	0.10	17:07	17:07	0	0.10	
VST24-LGE-BH203	2024-02-19	6.71	23:35	23:39	5	193	0.10	00:11	00:12	1	0.06	
VST24-LGE-BH203	2024-02-19	14.33	03:13	03:15	3	985	0.05	03:43	03:43	1	0.10	
VST24-LGE-BH203	2024-02-19	19.81	11:44	11:45	1	471	0.10	12:21	12:21	0	0.11	
VST24-LGE-BH203	2024-02-19	23.17	14:21	14:21	0	598	0.10	14:54	14:54	0	0.11	
VST24-LGE-BH204	2024-02-23	7.62	17:37	17:41	4	432	0.11	18:22	18:22	0	0.11	
VST24-LGE-BH204	2024-02-24	13.41	01:48	01:48	1	2203	0.05	02:41	02:41	1	0.10	
VST24-TMF-MW08AB	2024-03-13	8.54	16:05	16:06	1	596	0.05	16:50	16:50	0	0.06	
VST24-TMF-MW08AB	2024-03-14	14.33	02:11	02:16	5	228	0.10	02:51	02:50	0	0.10	
VST24-TMF-MW08AB	2024-03-15	20.27	23:59	00:02	1	257	0.10	23:59	00:37	1	0.11	
VST24-TMF-MW08AB	2024-03-15	28.96	04:14	04:14	1	366	0.10	04:44	04:44	1	0.10	
VST24-TMF-BH202	2024-03-18	4.57	21:56	22:00	4	234	0.10	22:33	22:33	0	0.10	
VST24-TMF-BH202	2024-03-19	13.41	03:38	03:40	2	270	0.11	04:12	04:12	0	0.11	
VST24-TMF-BH202	2024-03-19	16.16	11:02	11:02	1	102	0.09	11:35	11:35	1	0.08	
VST24-TMF-BH202	2024-03-19	19.42	13:56	13:56	1	426	0.09	14:27	14:27	1	0.08	
VST24-TMF-BH207	2024-03-16	4.57	23:21	23:23	3	361	0.10					
VST24-TMF-BH207	2024-03-16	4.88	23:36	23:40	5	258	0.00	00:24	00:25	1	0.10	
VST24-TMF-BH207	2024-03-17	12.50	02:49	02:51	2	301	0.10	03:20	03:21	1	0.11	
VST24-TMF-BH207	2024-03-17	18.59	10:20	10:21	1	212	0.09	10:59	10:59	1	0.09	
VST24-TMF-BH207	2024-03-17	21.34	12:16	12:17	1	422	0.08	13:03	13:03	1	0.09	
VST24-WRD-BH201	2024-03-05	6.10	14:58	15:02	5	561	0.10					
VST24-WRD-BH201	2024-03-05	6.40	15:34	15:34	0	702	0.11	16:25	16:25	1	0.10	

Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Start Date: 2024-02-15
End Date: 2024-03-21

ELECTRIC FIELD VANE SHEAR TEST TIMING

Sounding ID	Date	Test Depth[1] (m)	Vane Insertion Time (HH:mm)	Peak Test Start Time (HH:mm)	Insertion to Start Interval (min)	Start to Failure Interval (sec)	Peak Test Avg Rate (deg/sec)	Remolding Completion Time (HH:mm)	Remold Test Start Time (HH:mm)	Remolding to Start Interval (min)	Remold Test Avg Rate (deg/sec)	Refer to Notation Number
VST24-WRD-BH201	2024-03-05	11.58	21:55	21:56	1	382	0.10	22:22	22:22	0	0.10	
VST24-WRD-BH201	2024-03-06	17.37	03:19	03:19	1	457	0.09	03:43	03:43	0	0.10	
VST24-WRD-BH201	2024-03-06	21.34	12:42	12:46	5	1744	0.10					
VST24-WRD-BH202	2024-03-20	5.80	12:45	12:46	2	1035	0.09	13:08	13:08	0	0.11	
VST24-WRD-BH202	2024-03-20	9.23	15:39	15:39	1	1081	0.10	16:16	16:16	0	0.11	
VST24-WRD-BH202	2024-03-20	9.55	16:34	16:34	0	380	0.10	16:54	16:54	0	0.10	
VST24-WRD-BH202	2024-03-20	11.89	23:45	23:49	4	262	0.00	00:20	00:19	0	0.11	
VST24-WRD-BH202	2024-03-21	16.15	03:40	03:42	3	612	0.10	04:15	04:14	0	0.10	
VST24-WRD-BH205	2024-03-16	5.80	11:22	11:23	1	250	0.10	11:44	11:44	1	0.10	
VST24-WRD-BH205	2024-03-16	6.15	12:14	12:14	1	339	0.10	12:34	12:34	1	0.10	
VST24-WRD-BH205	2024-03-16	7.30	14:26	14:27	1	1355	0.10	14:59	14:59	1	0.09	
VST24-WRD-BH207	2024-03-15	5.15	14:45	14:48	4	461	0.10					
VST24-WRD-BH207	2024-03-15	5.50	15:26	15:28	3	767	0.10	15:55	15:54	0	0.10	
VST24-WRD-BH212	2024-03-09	3.66	13:39	13:42	4	300	0.10	14:21	14:21	1	0.10	
VST24-WRD-BH212	2024-03-09	8.54	17:36	17:36	0	809	0.11	21:42	21:42	1	0.09	
VST24-WRD-BH212	2024-03-10	13.41	01:50	01:51	1	4130	0.02	03:15	03:15	1	0.10	
VST24-WRD-BH218	2024-03-14	5.15	12:33	12:34	1	315	0.09	13:14	13:15	1	0.09	

1. Test depths are referenced to the middle of the vane.

Electric Field Vane Shear Test Plots

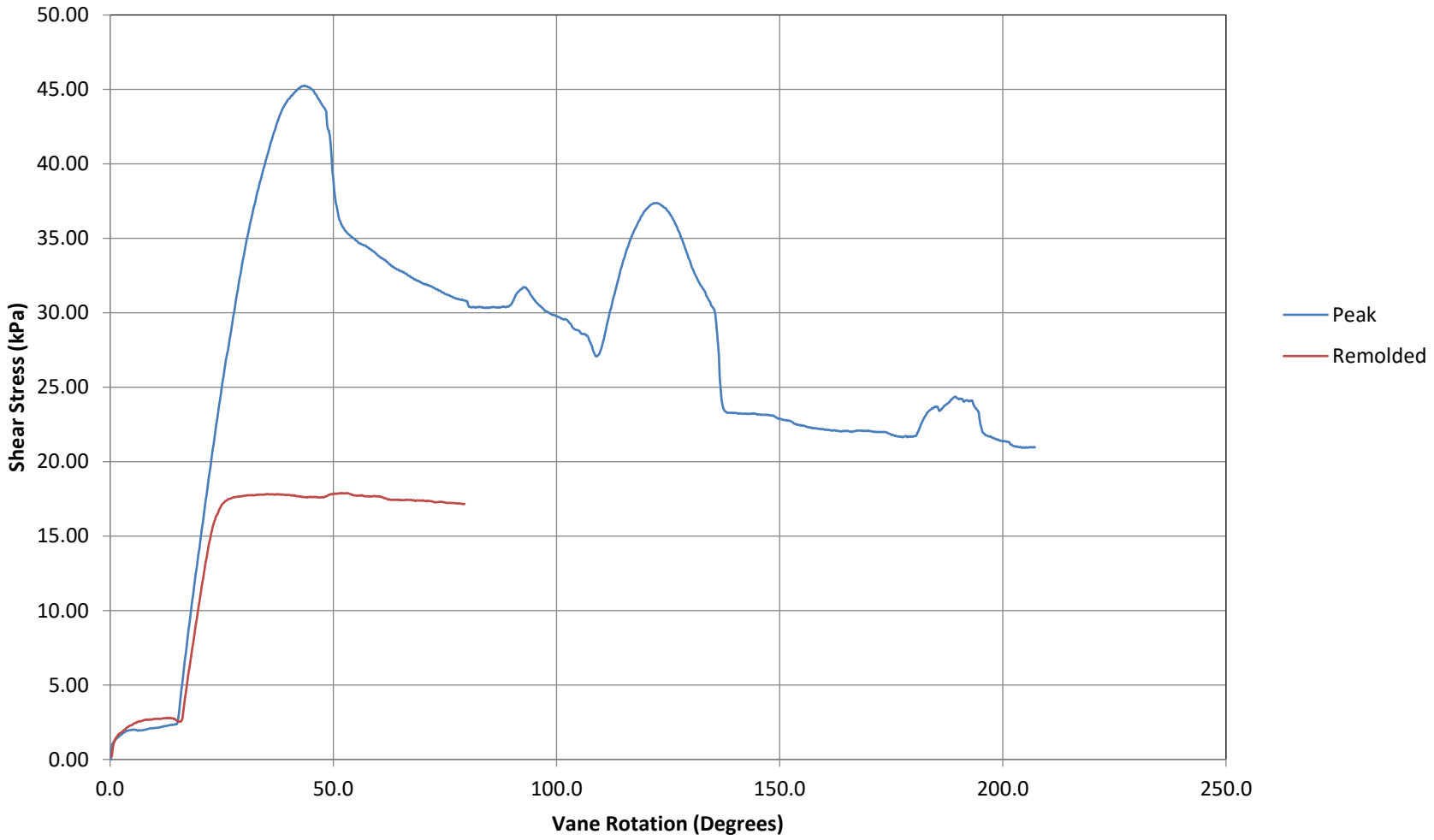
CONETEC

Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH04

Test Date: 26-Feb-2024 16:13
Test Depth (m): 8.23
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407273
Easting (m): 476519

Vane Shear Test

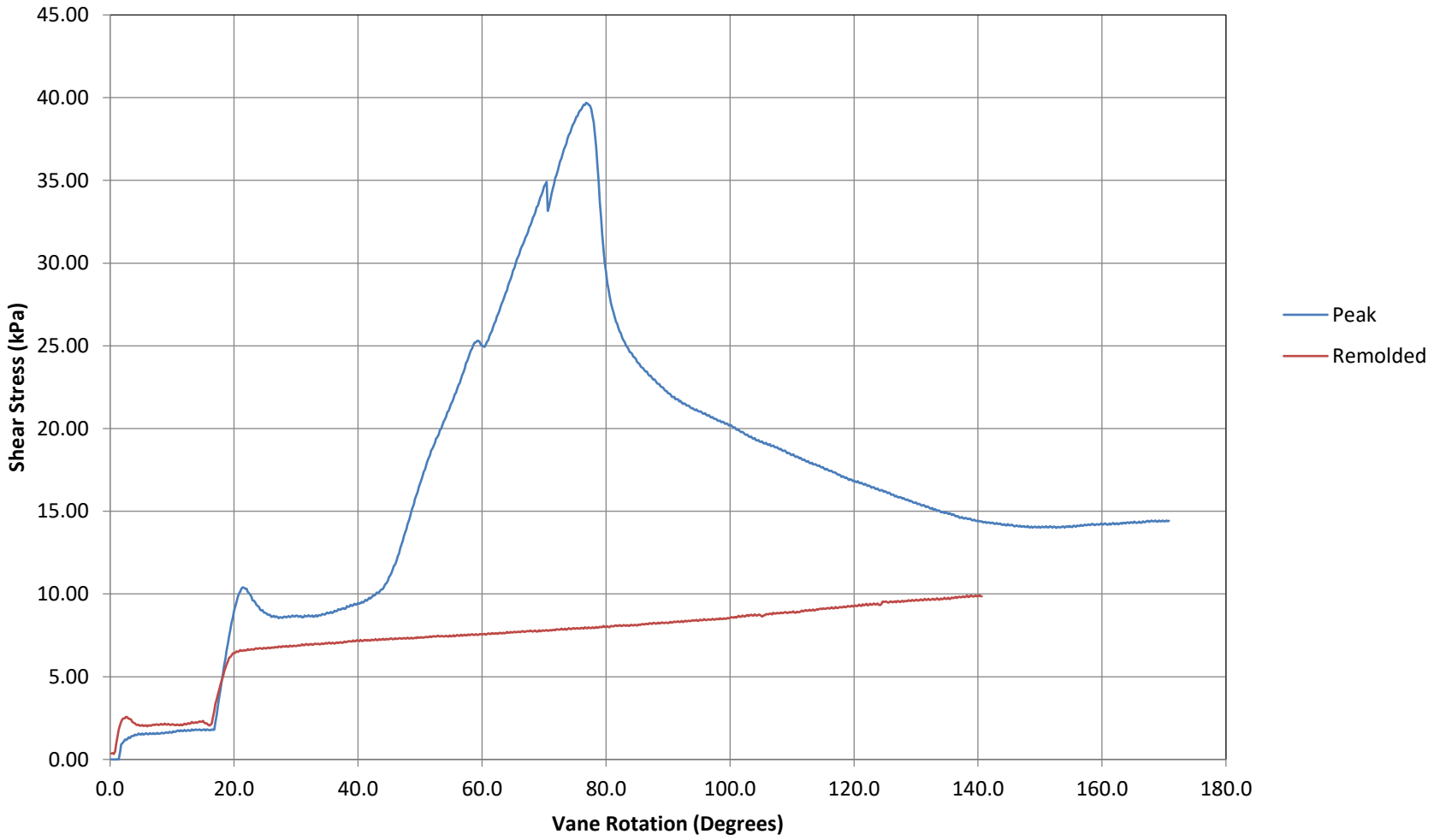


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH04

Test Date: 26-Feb-2024 22:24
Test Depth (m): 11.89
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407273
Easting (m): 476519

Vane Shear Test

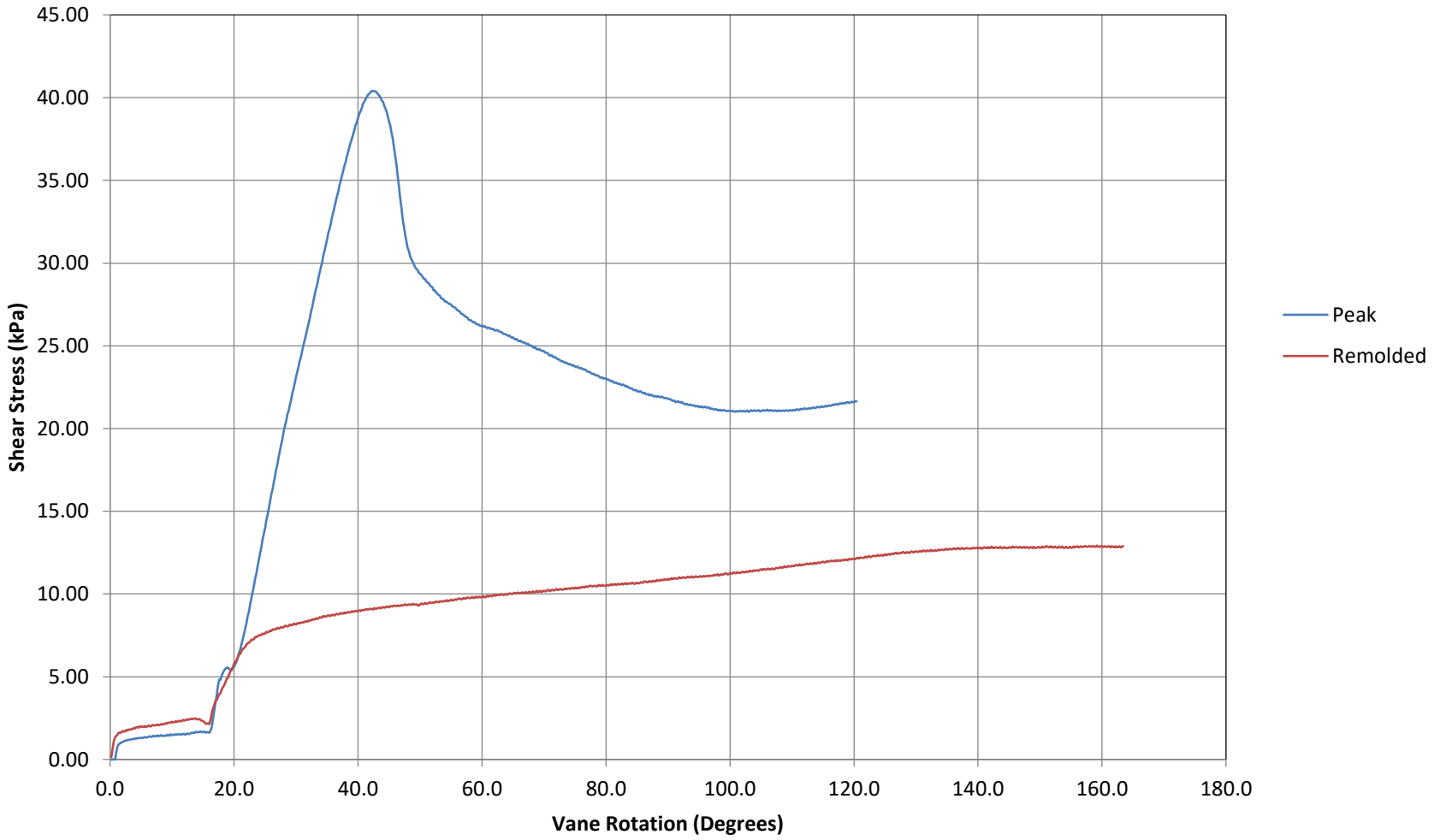


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH04

Test Date: 27-Feb-2024 01:10
Test Depth (m): 14.94
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407273
Easting (m): 476519

Vane Shear Test

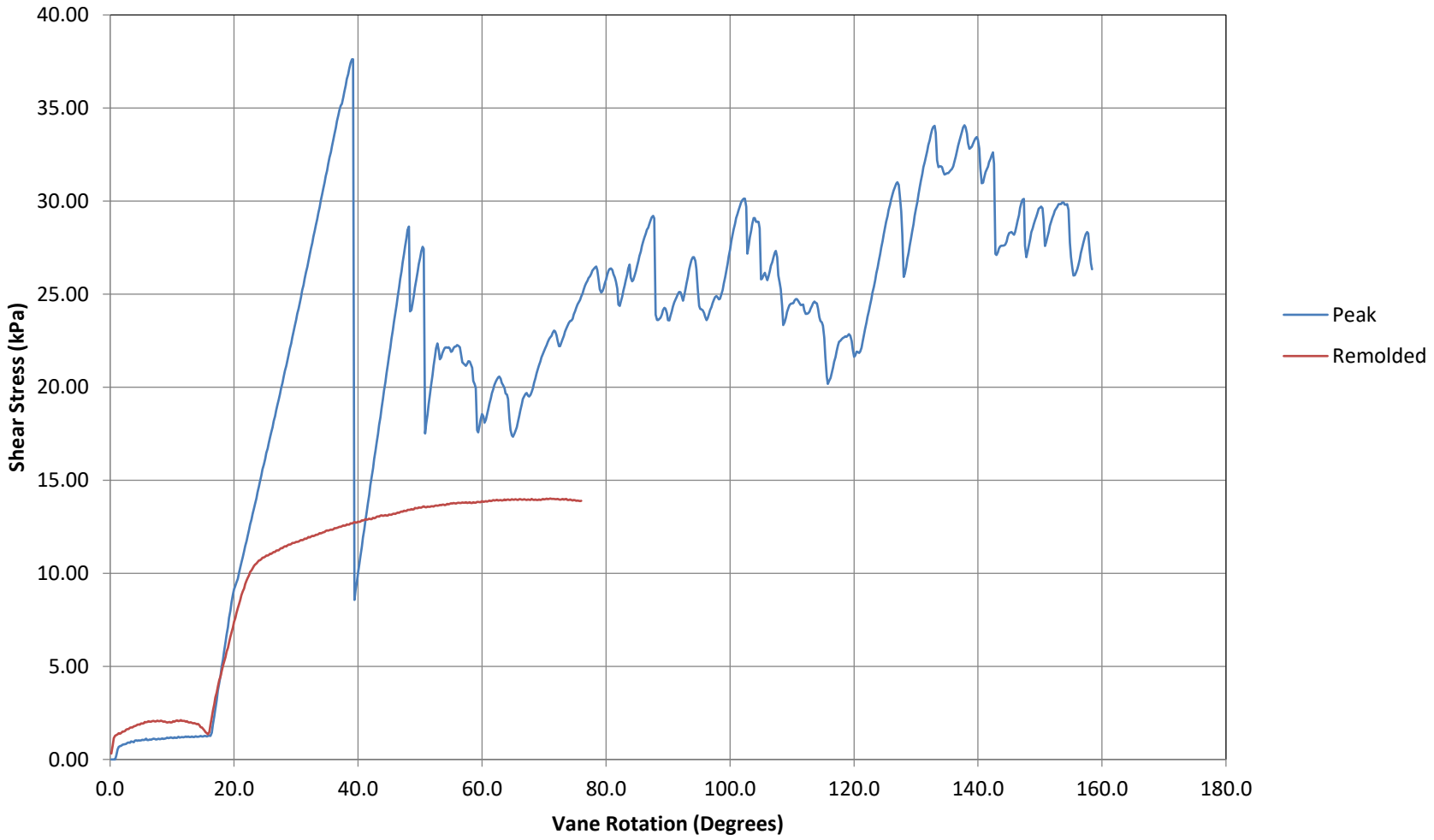


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH04

Test Date: 27-Feb-2024 04:08
Test Depth (m): 17.68
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407273
Easting (m): 476519

Vane Shear Test

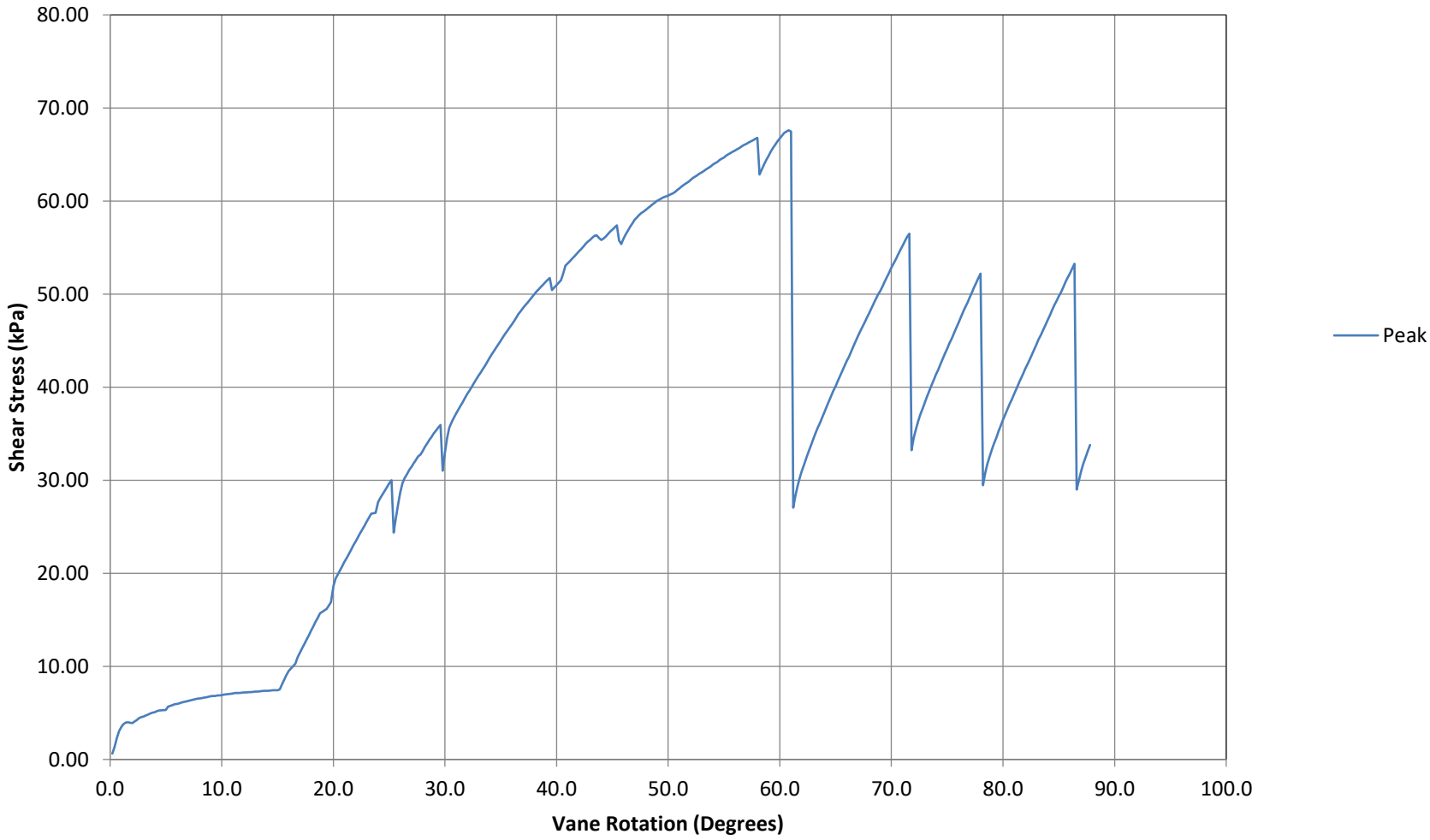


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH05

Test Date: 15-Feb-2024 15:16
Test Depth (m): 10.67
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5408925
Easting (m): 475900

Vane Shear Test

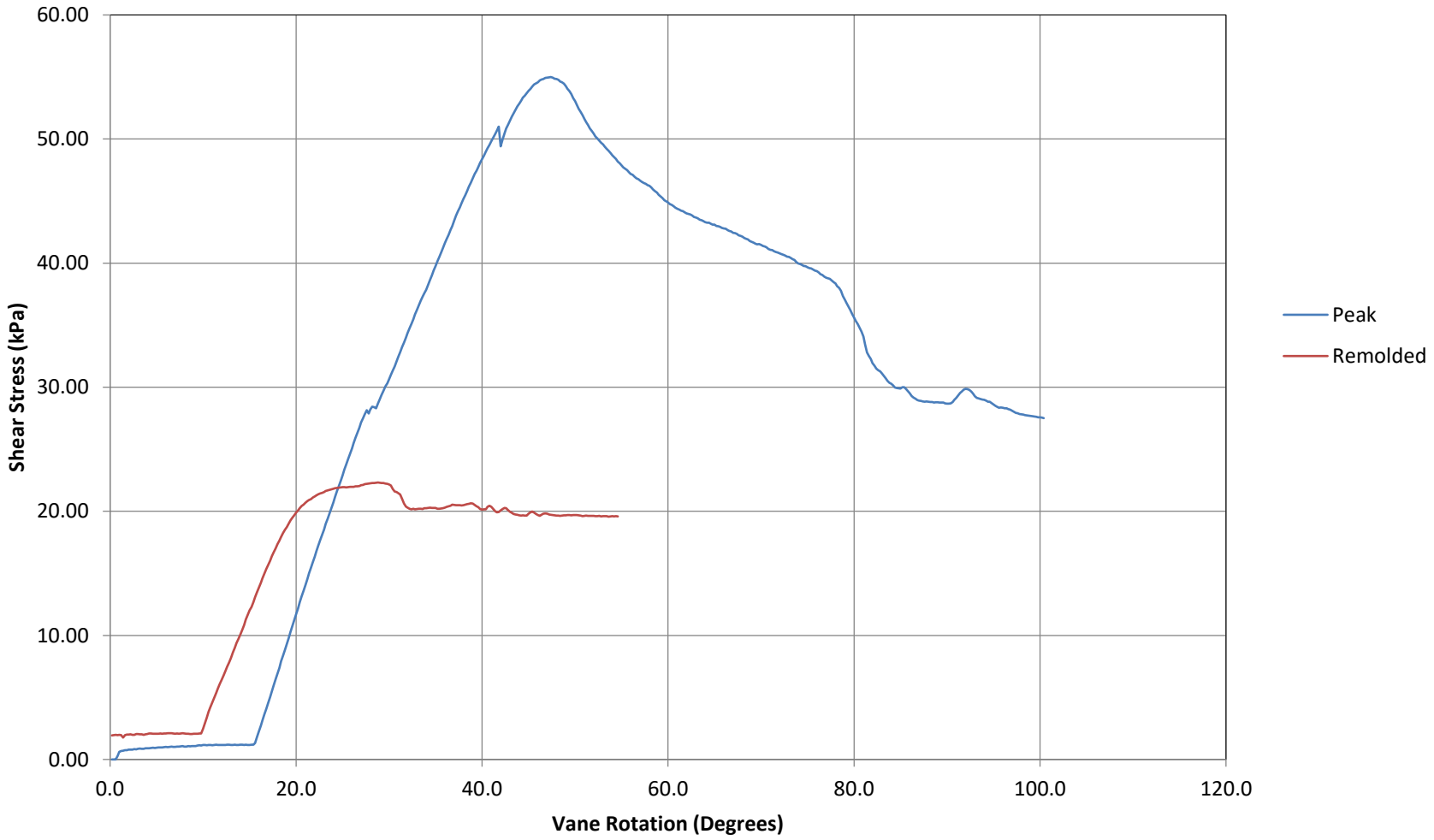


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH05

Test Date: 15-Feb-2024 17:20
Test Depth (m): 13.11
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5408925
Easting (m): 475900

Vane Shear Test

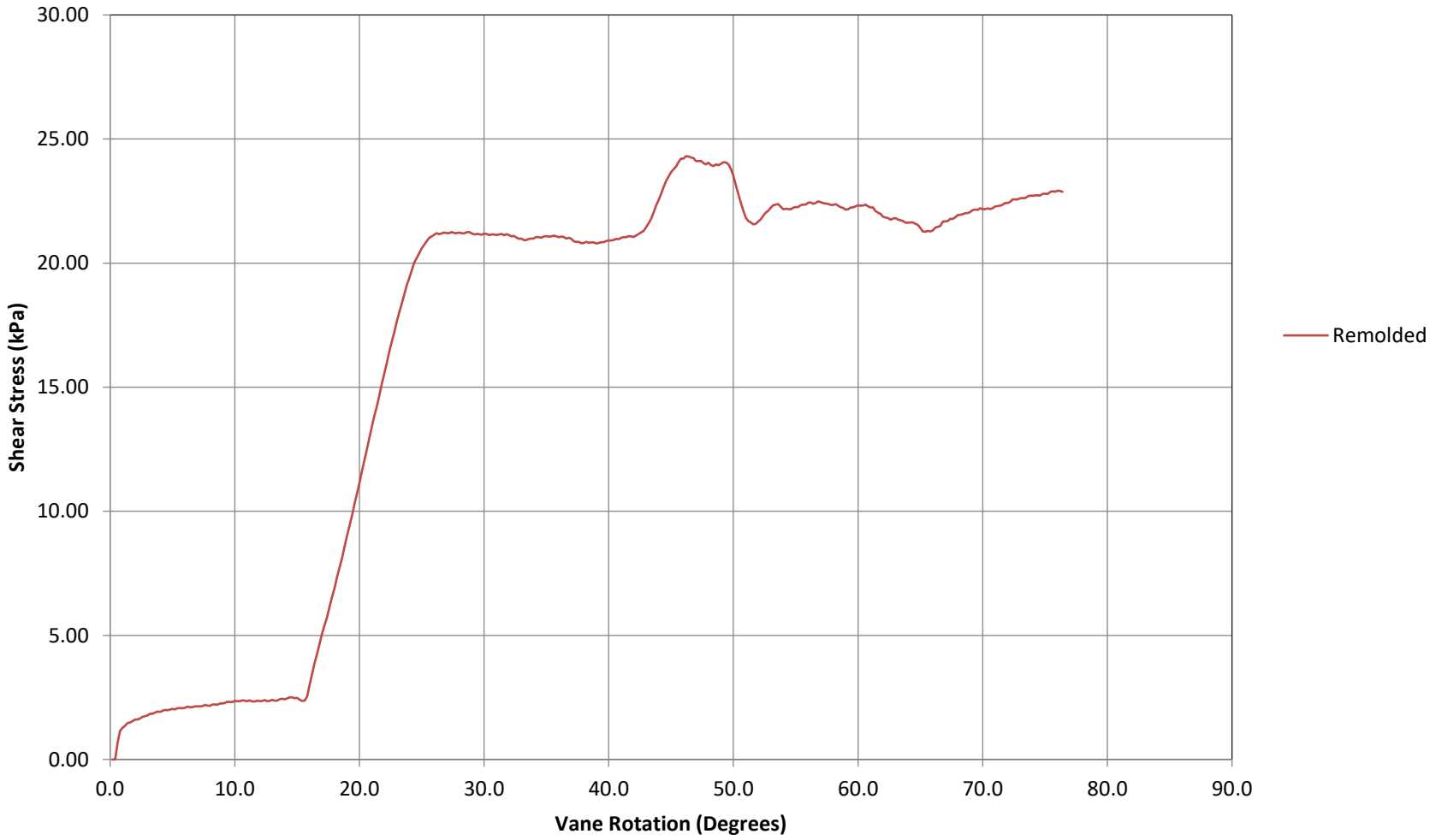


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH201

Test Date: 22-Feb-2024 00:59
Test Depth (m): 4.57
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407385
Easting (m): 474826

Vane Shear Test

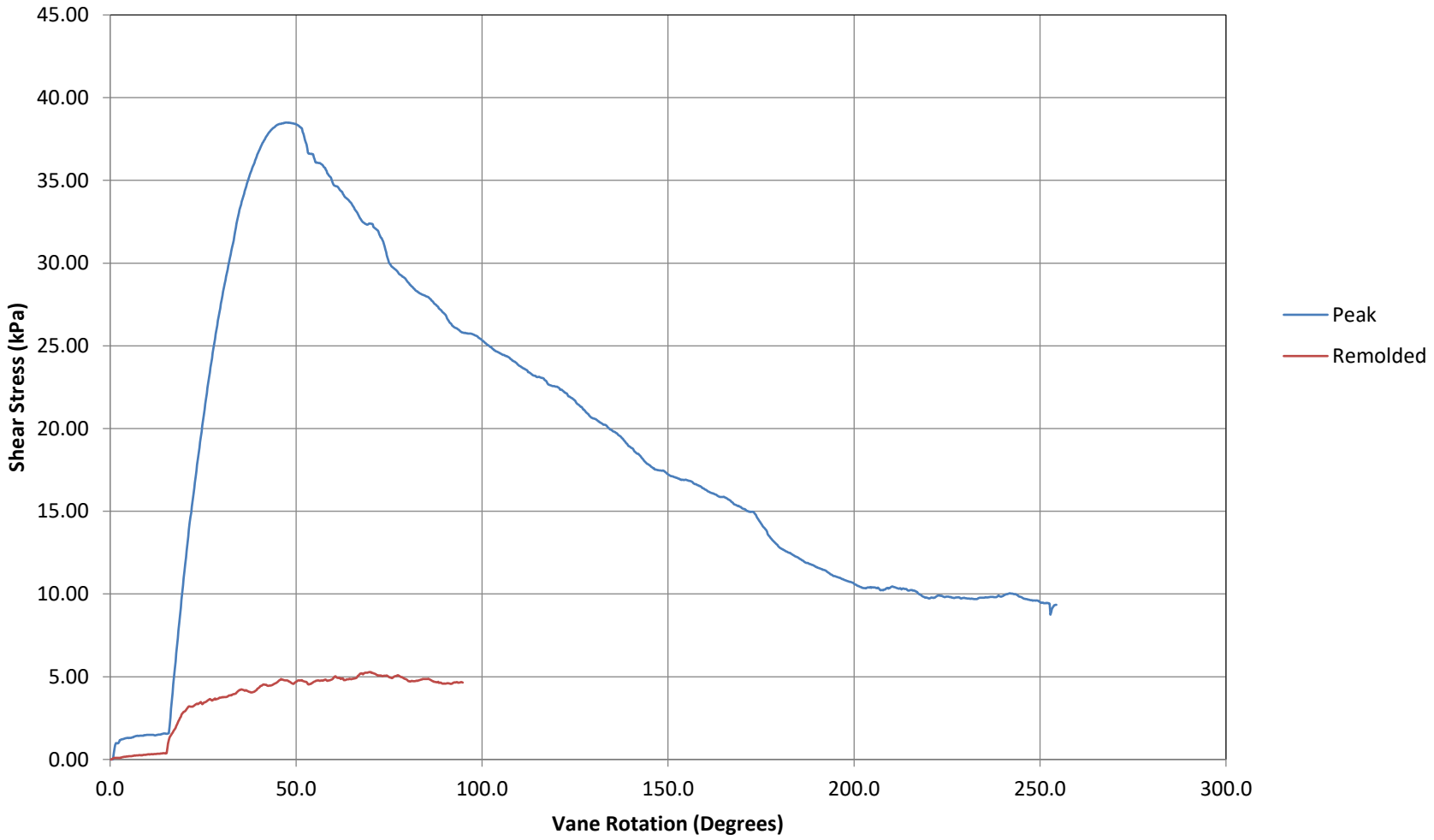


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH202

Test Date: 20-Feb-2024 16:23
Test Depth (m): 4.57
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5408589
Easting (m): 475370

Vane Shear Test

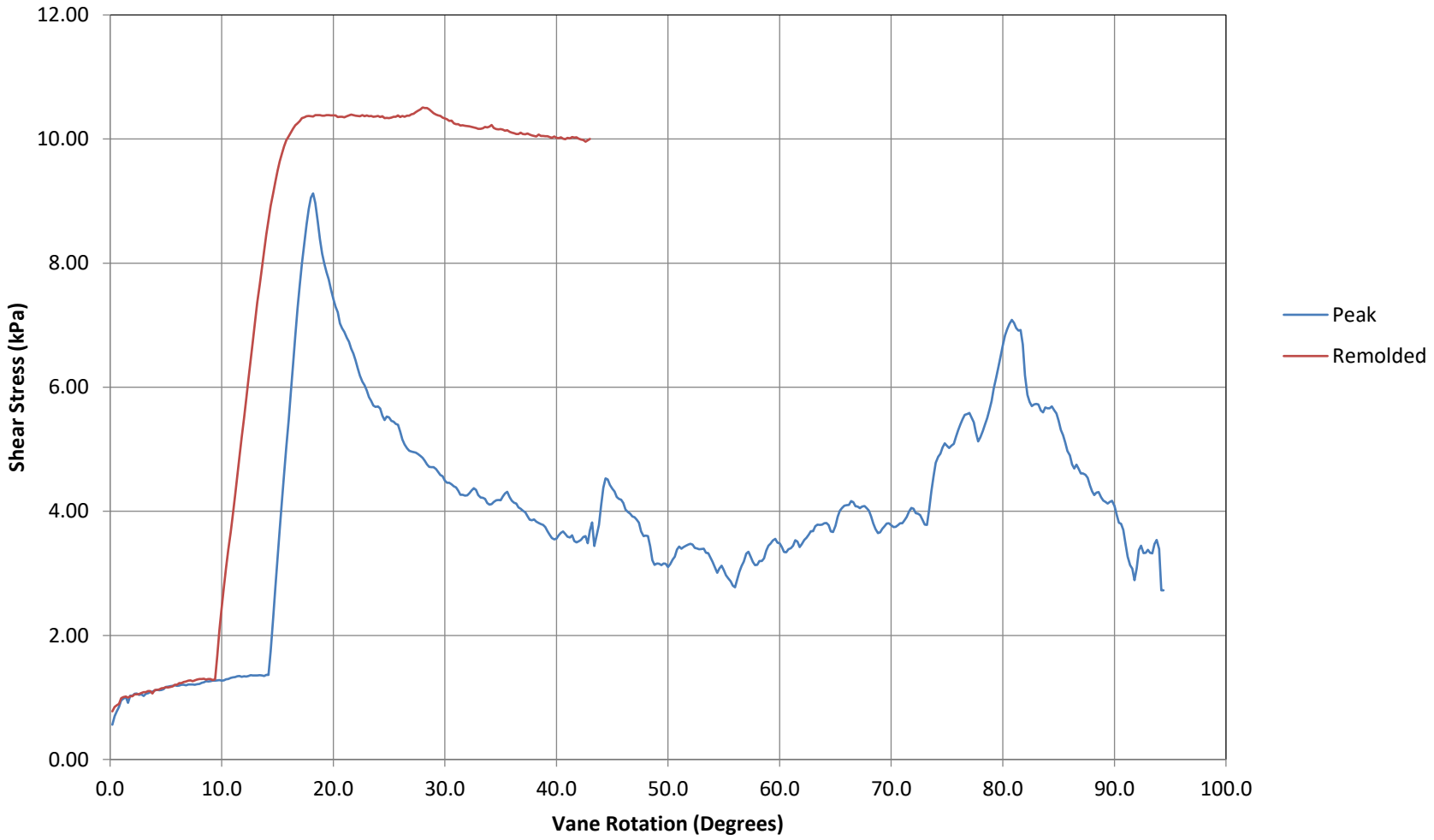


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH203

Test Date: 19-Feb-2024 23:39
Test Depth (m): 6.71
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5409185
Easting (m): 476444

Vane Shear Test

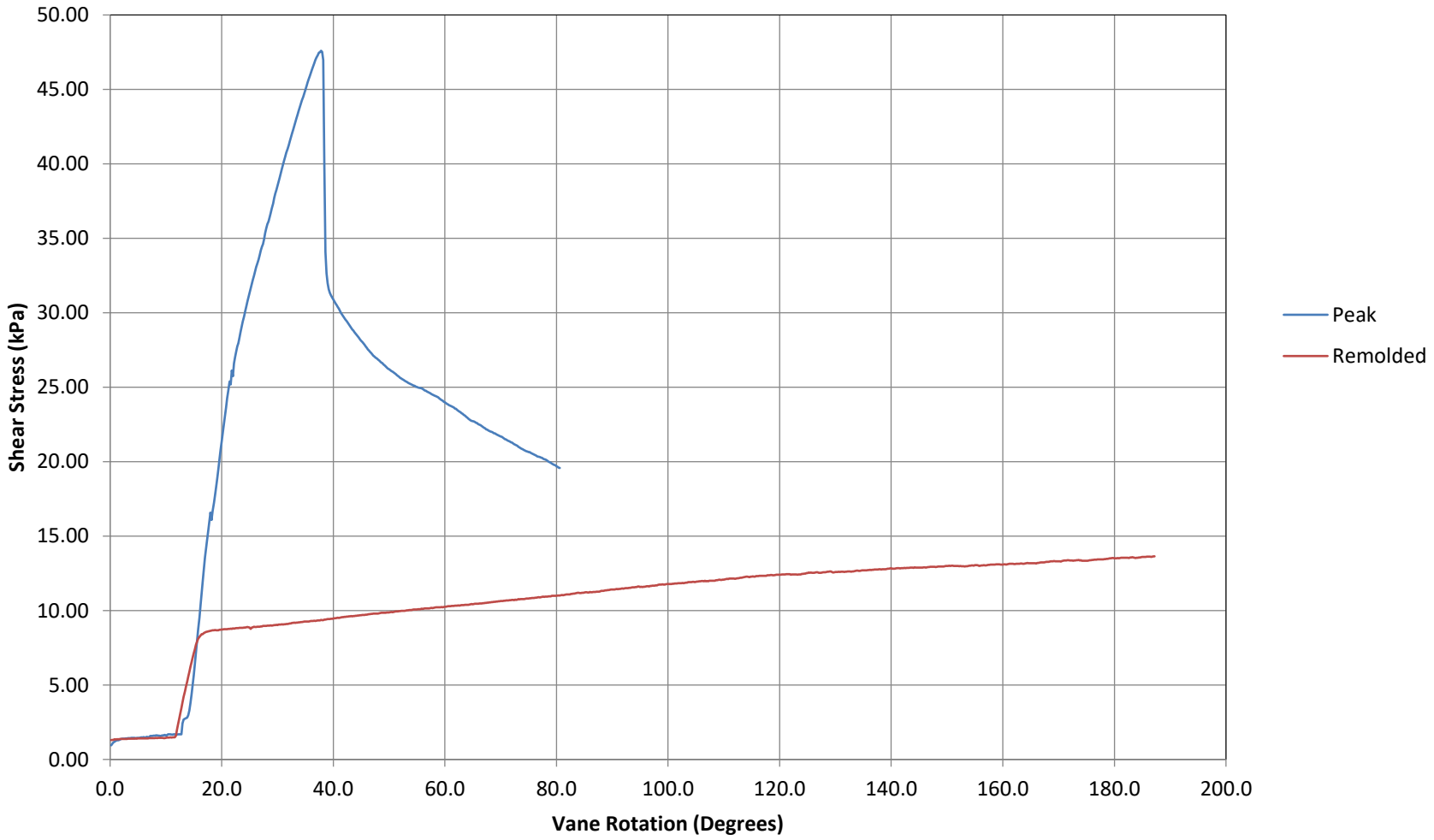


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH203

Test Date: 19-Feb-2024 03:15
Test Depth (m): 14.33
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5409185
Easting (m): 476444

Vane Shear Test

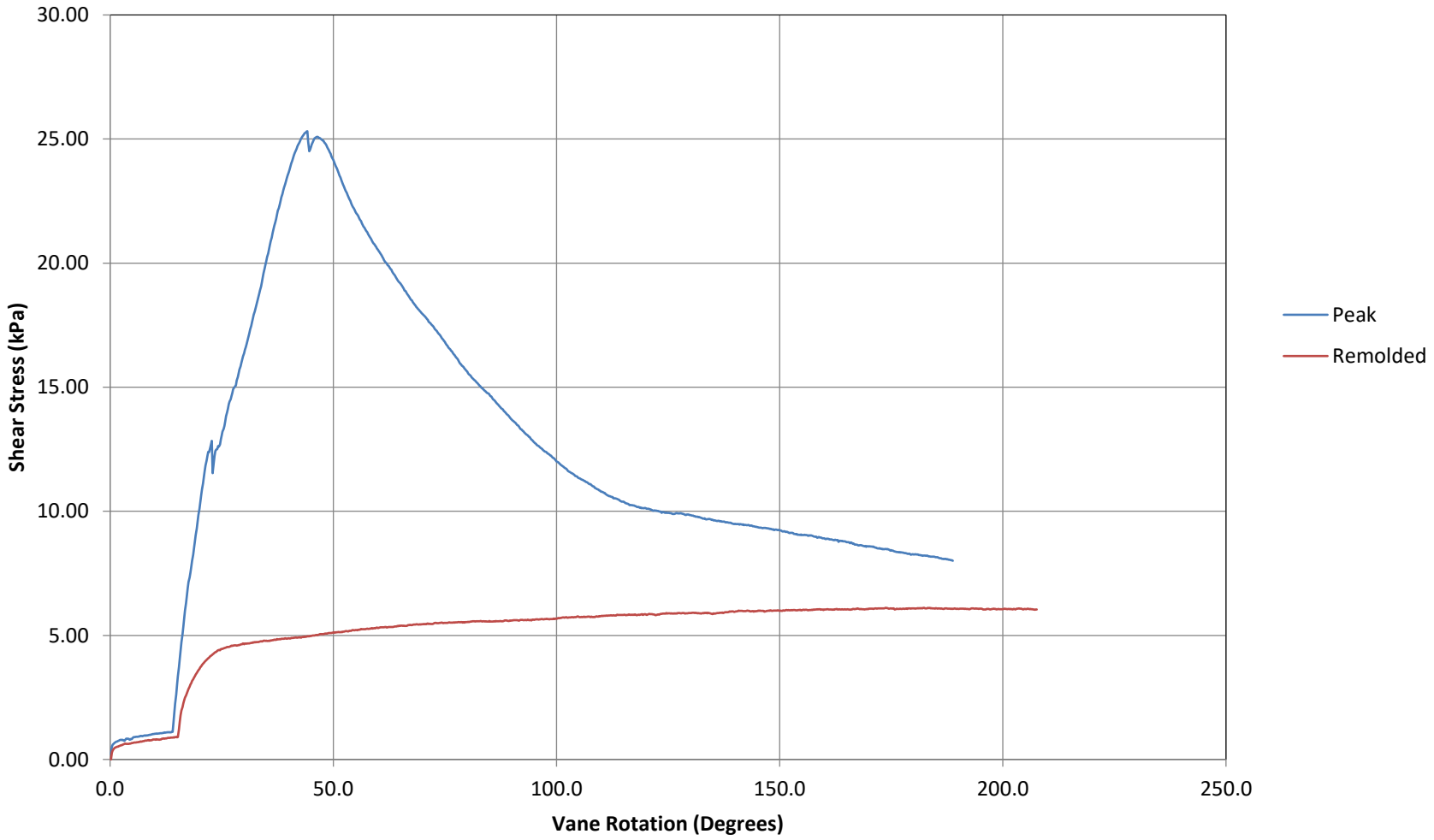


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH203

Test Date: 19-Feb-2024 11:45
Test Depth (m): 19.81
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5409185
Easting (m): 476444

Vane Shear Test

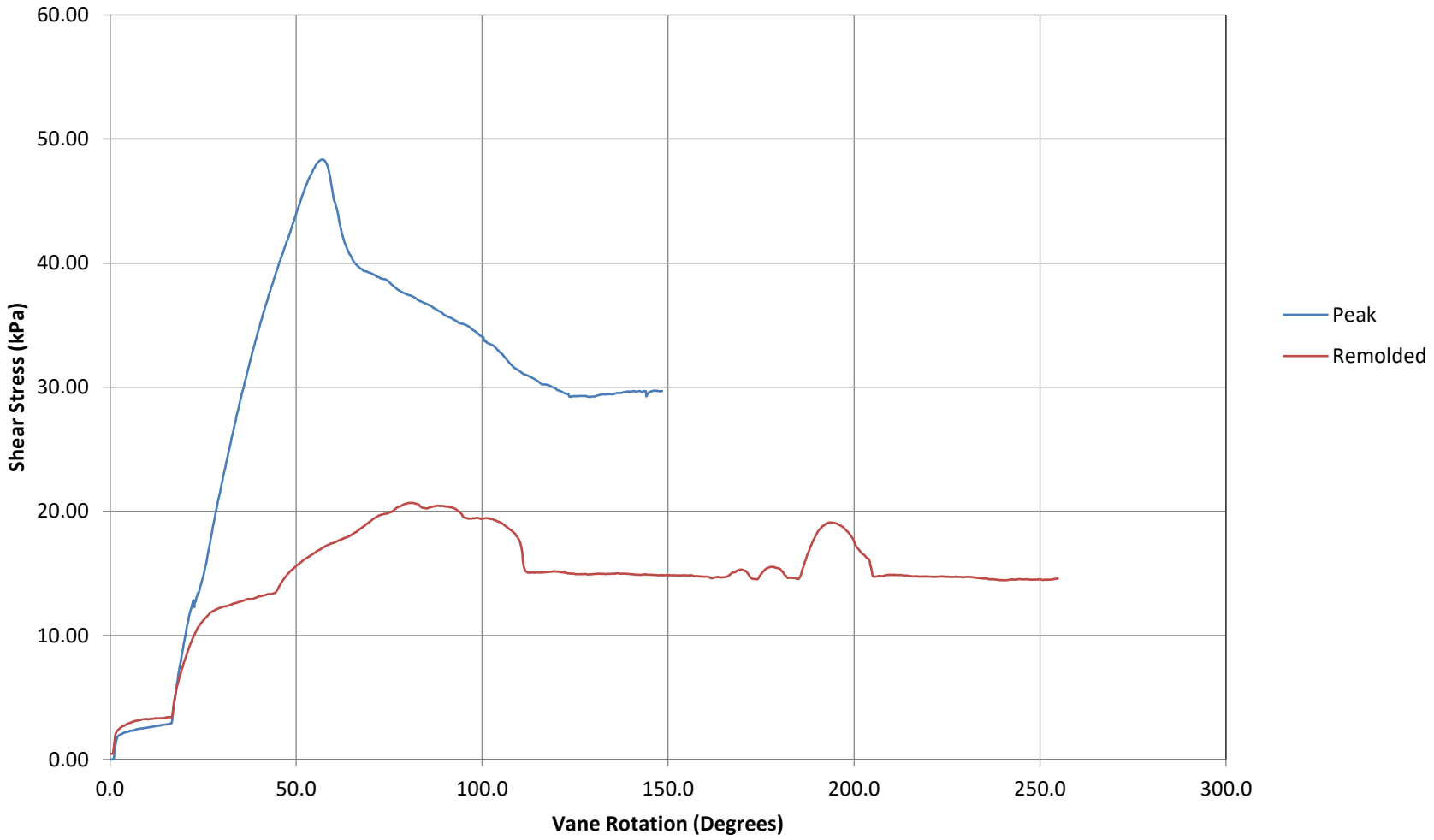


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH203

Test Date: 19-Feb-2024 14:21
Test Depth (m): 23.17
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5409185
Easting (m): 476444

Vane Shear Test

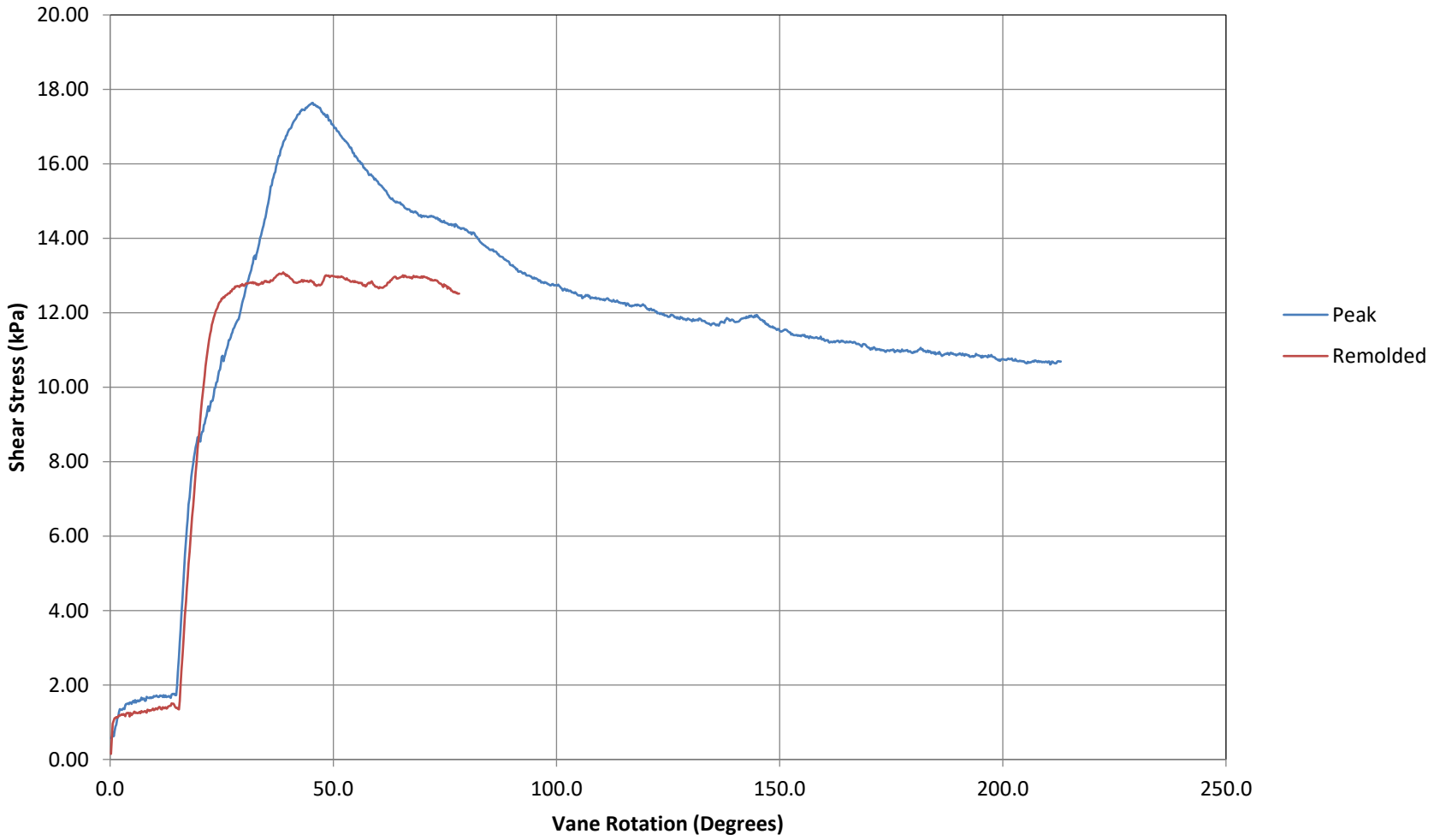


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH204

Test Date: 23-Feb-2024 17:41
Test Depth (m): 7.62
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407349
Easting (m): 475668

Vane Shear Test

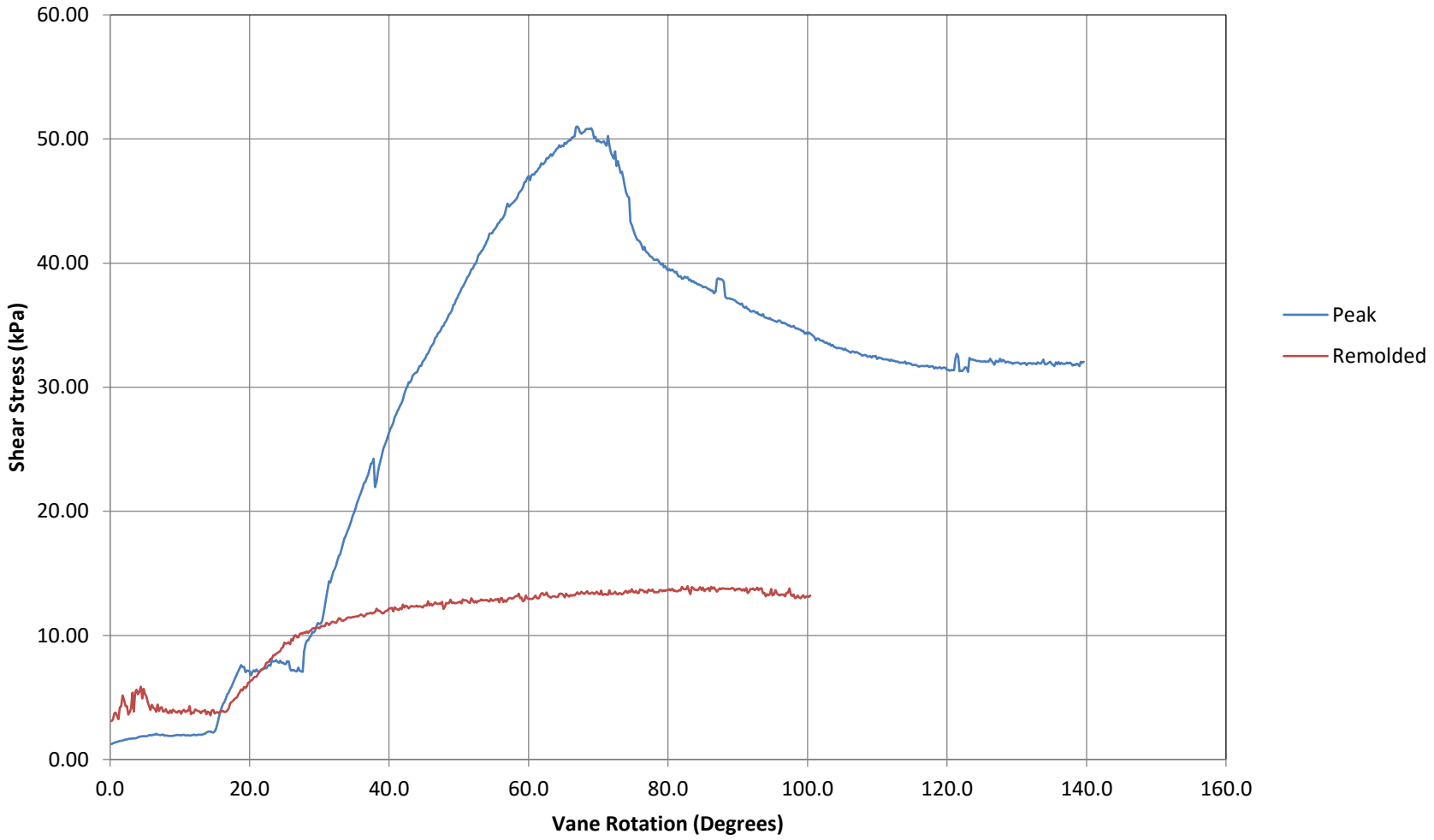


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-LGE-BH204

Test Date: 24-Feb-2024 01:48
Test Depth (m): 13.41
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5407349
Easting (m): 475668

Vane Shear Test

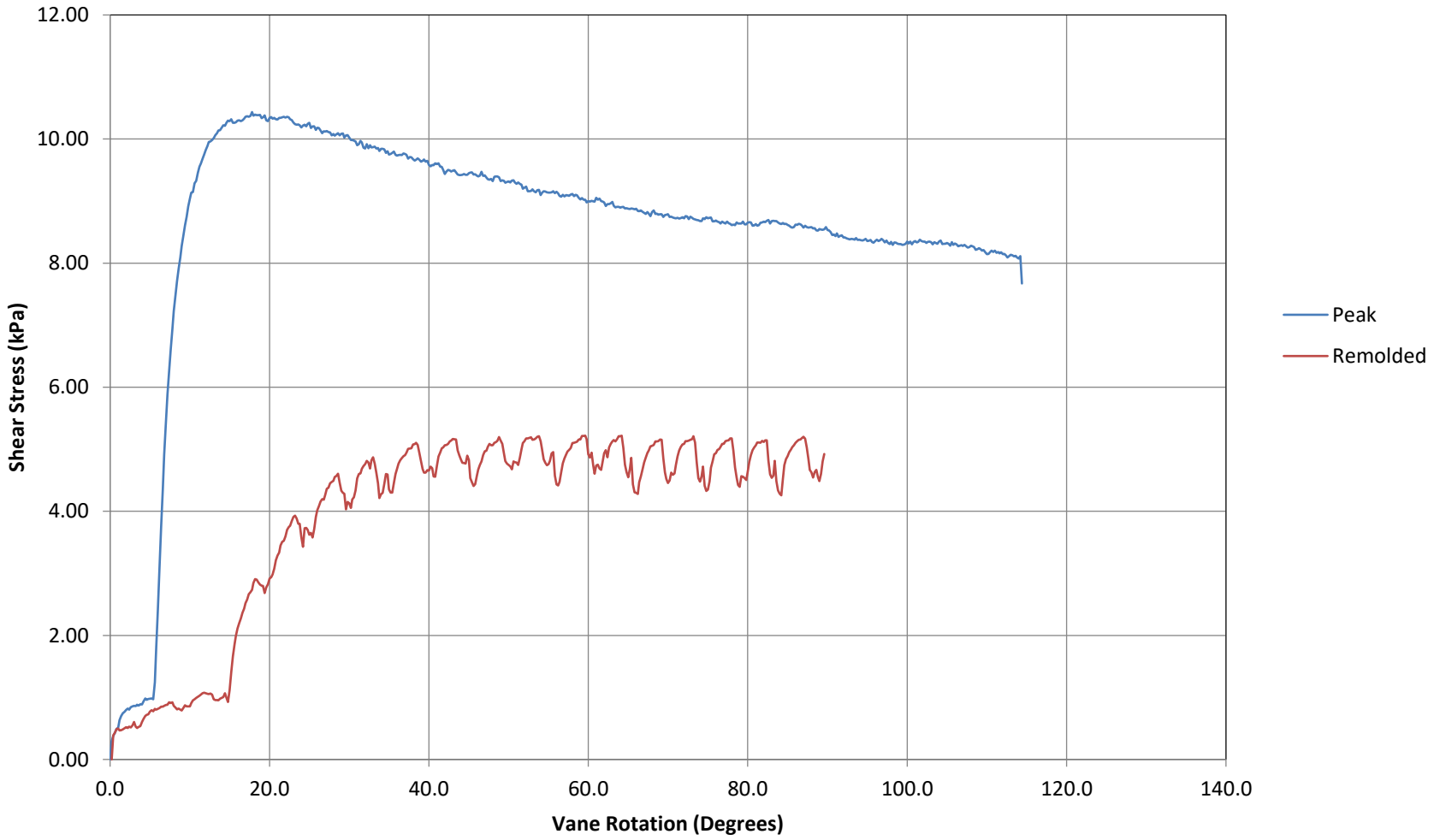


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-MW08AB

Test Date: 13-Mar-2024 16:06
Test Depth (m): 8.54
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5401996
Easting (m): 476471

Vane Shear Test

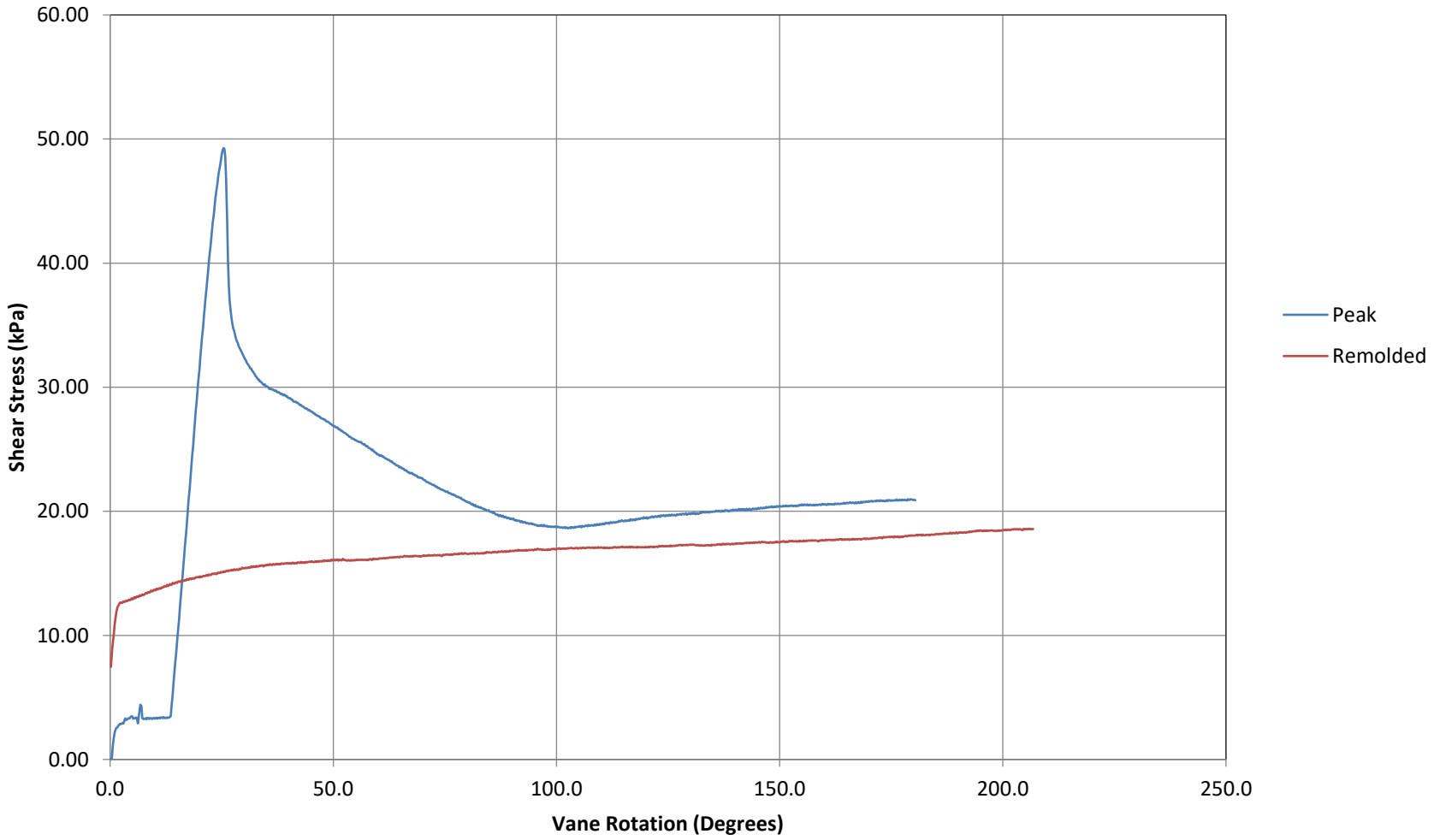


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-MW08AB

Test Date: 14-Mar-2024 02:16
Test Depth (m): 14.33
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5401996
Easting (m): 476471

Vane Shear Test

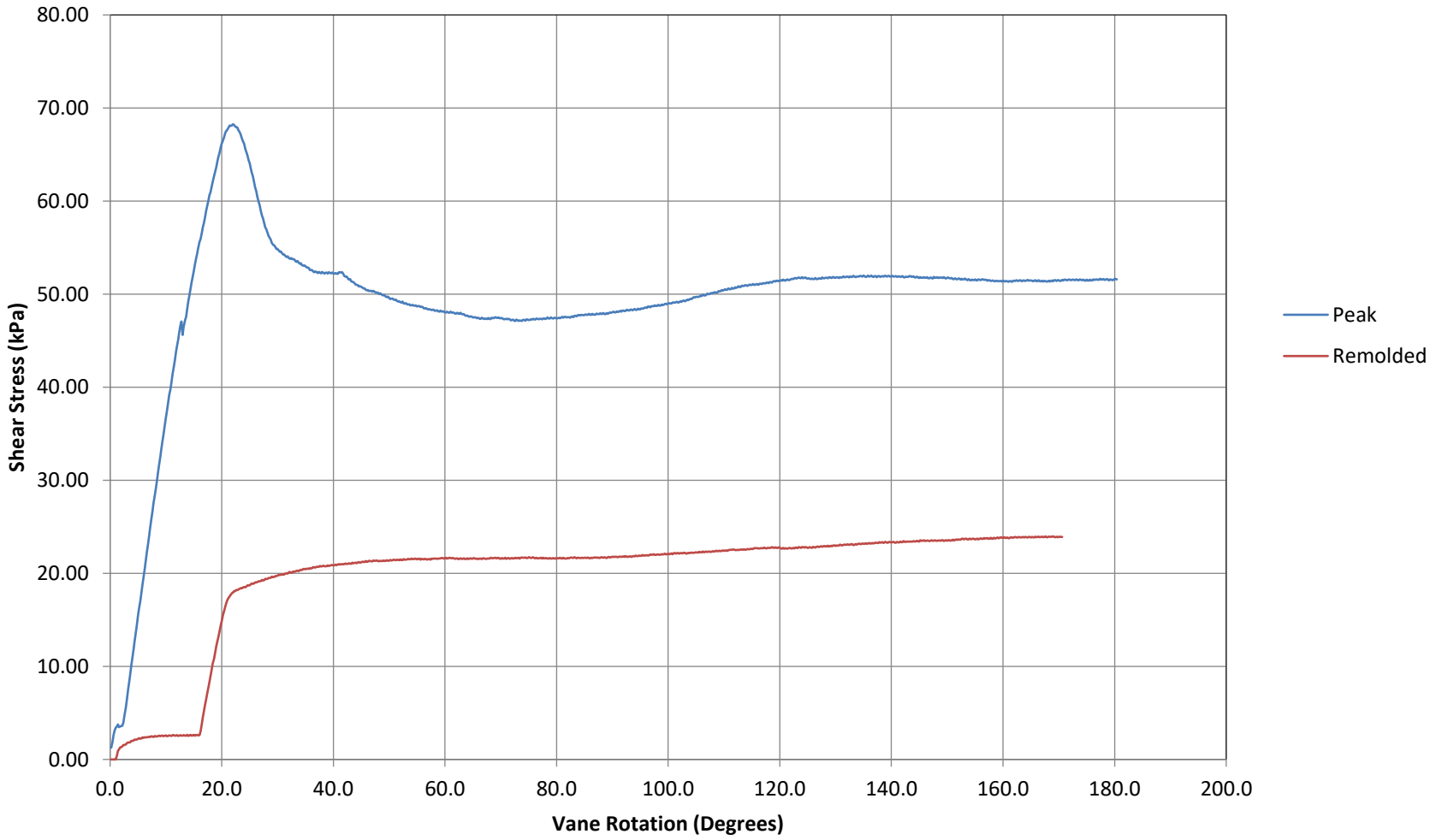


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-MW08AB

Test Date: 15-Mar-2024 00:02
Test Depth (m): 20.27
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5401996
Easting (m): 476471

Vane Shear Test

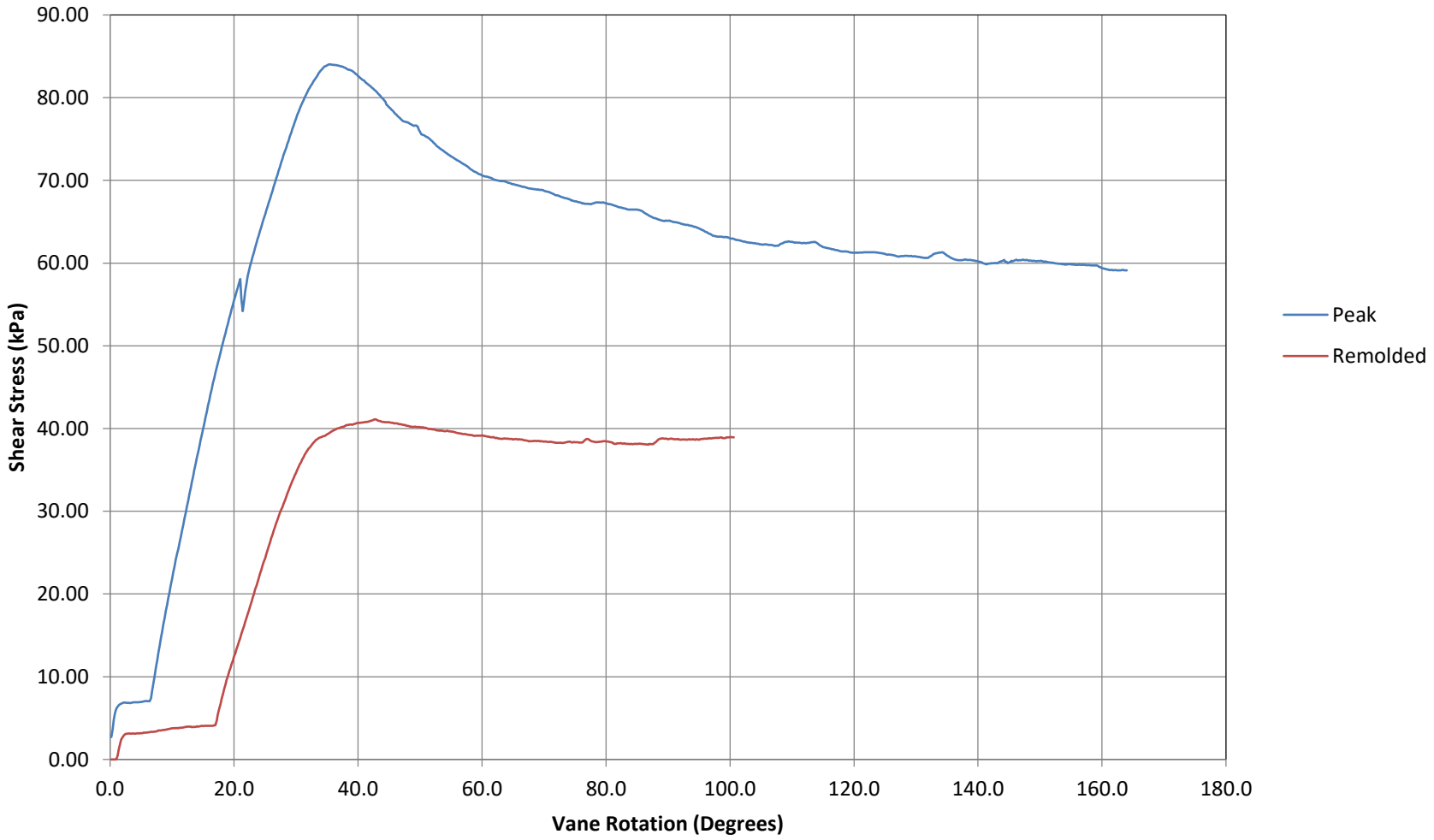


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-MW08AB

Test Date: 15-Mar-2024 04:14
Test Depth (m): 28.96
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5401996
Easting (m): 476471

Vane Shear Test

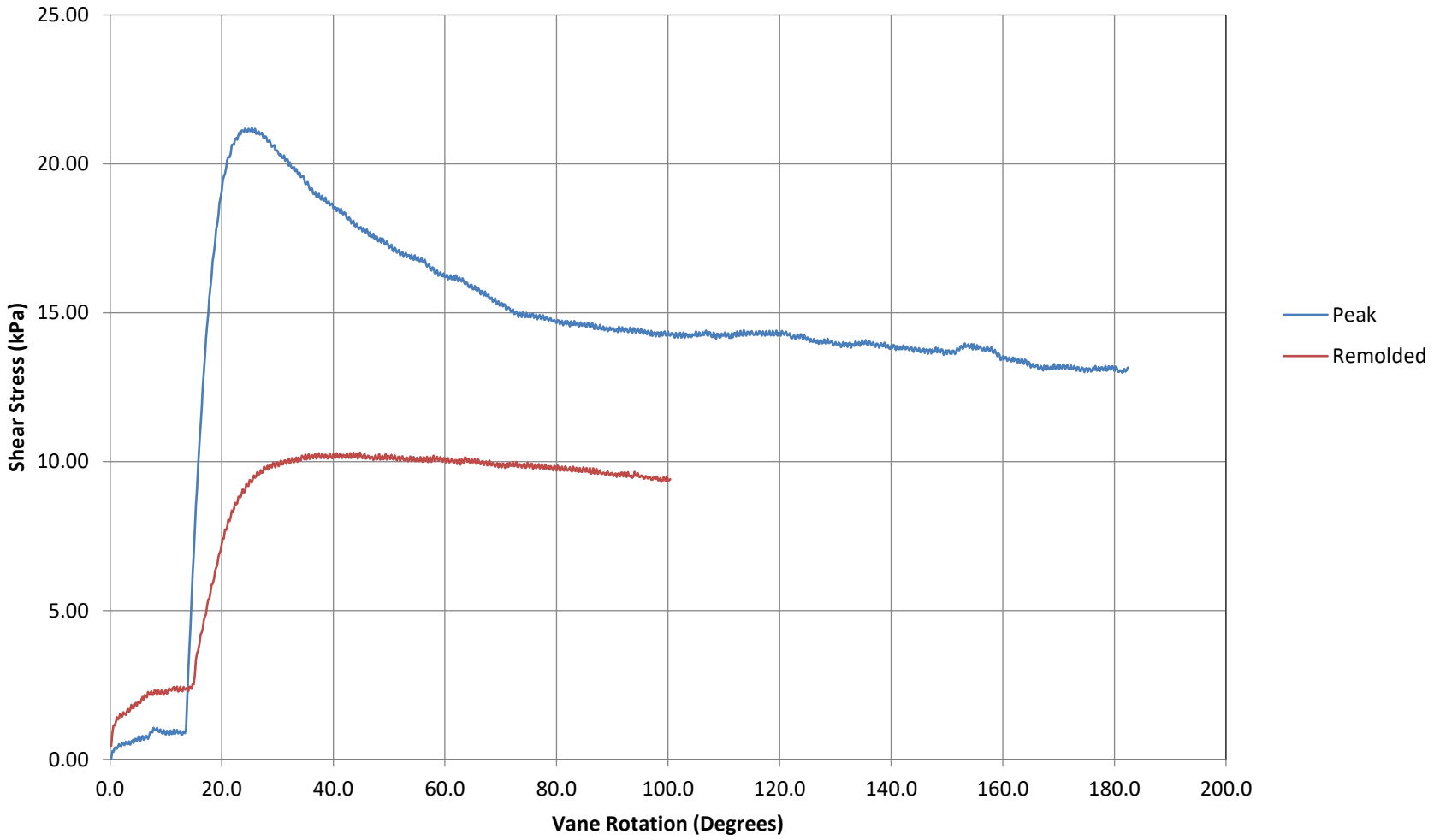


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH202

Test Date: 18-Mar-2024 22:00
Test Depth (m): 4.57
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5404211
Easting (m): 476824

Vane Shear Test

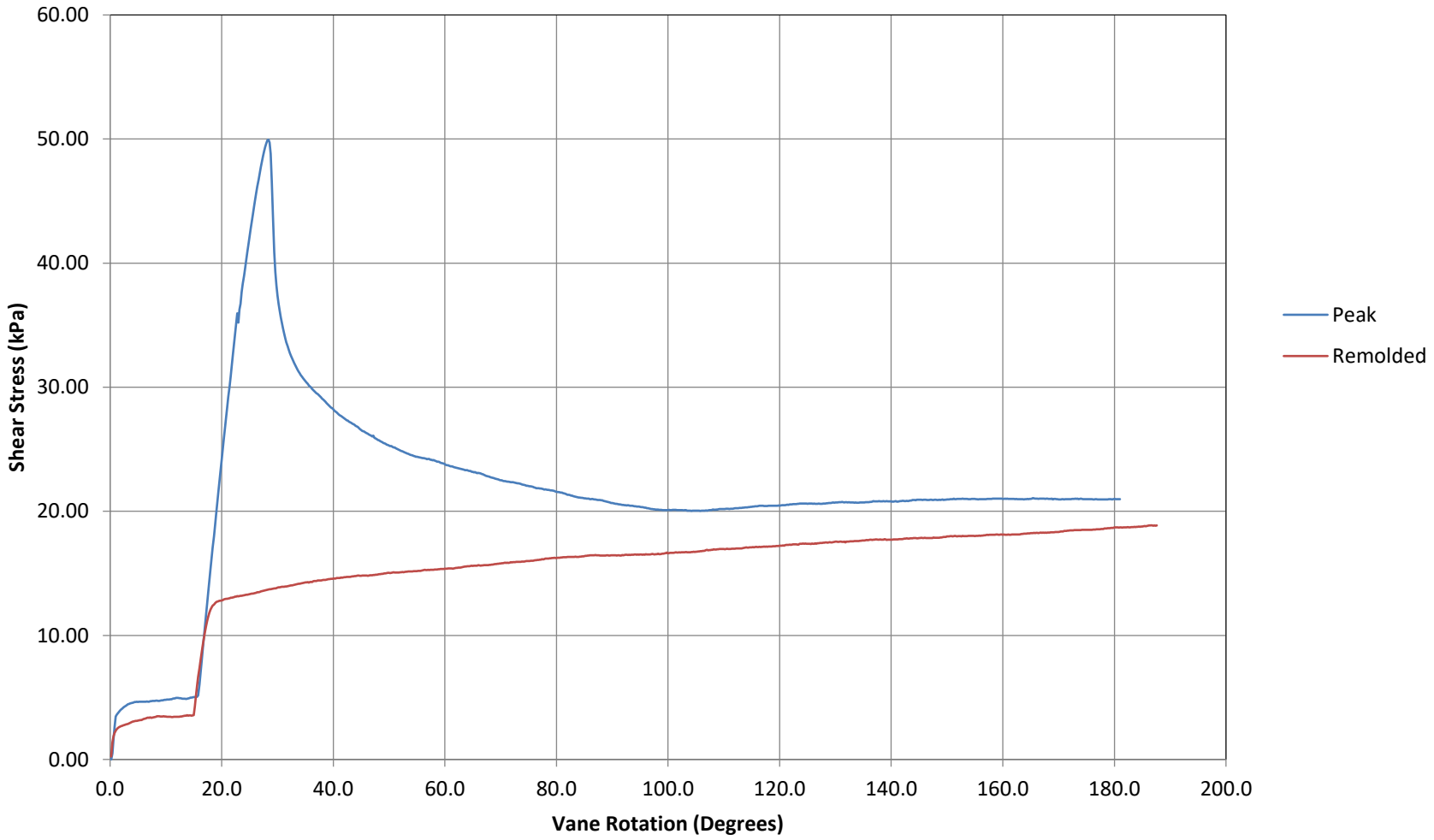


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH202

Test Date: 19-Mar-2024 03:40
Test Depth (m): 13.41
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5404211
Easting (m): 476824

Vane Shear Test

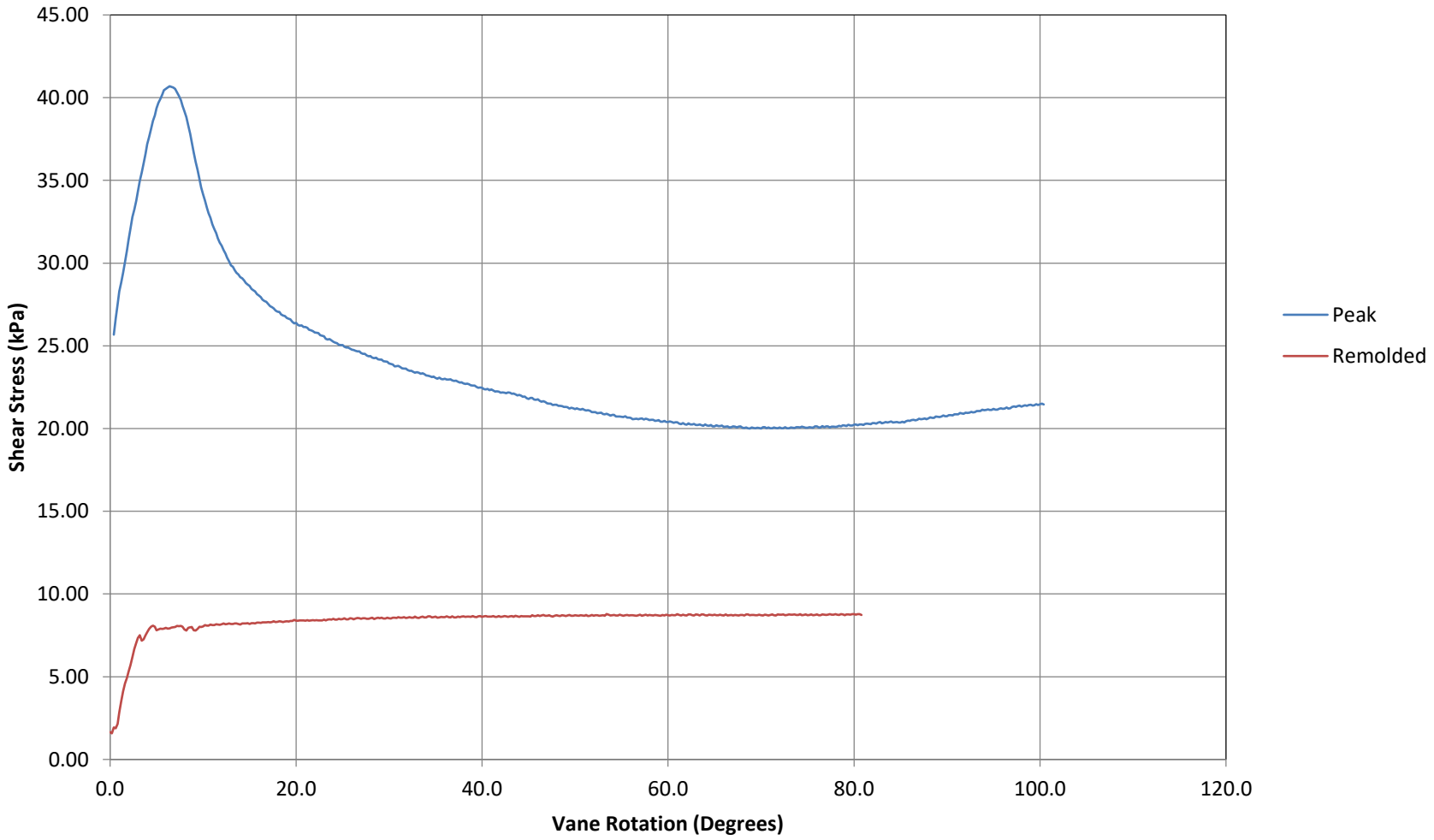


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH202

Test Date: 19-Mar-2024 11:02
Test Depth (m): 16.16
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5404211
Easting (m): 476824

Vane Shear Test

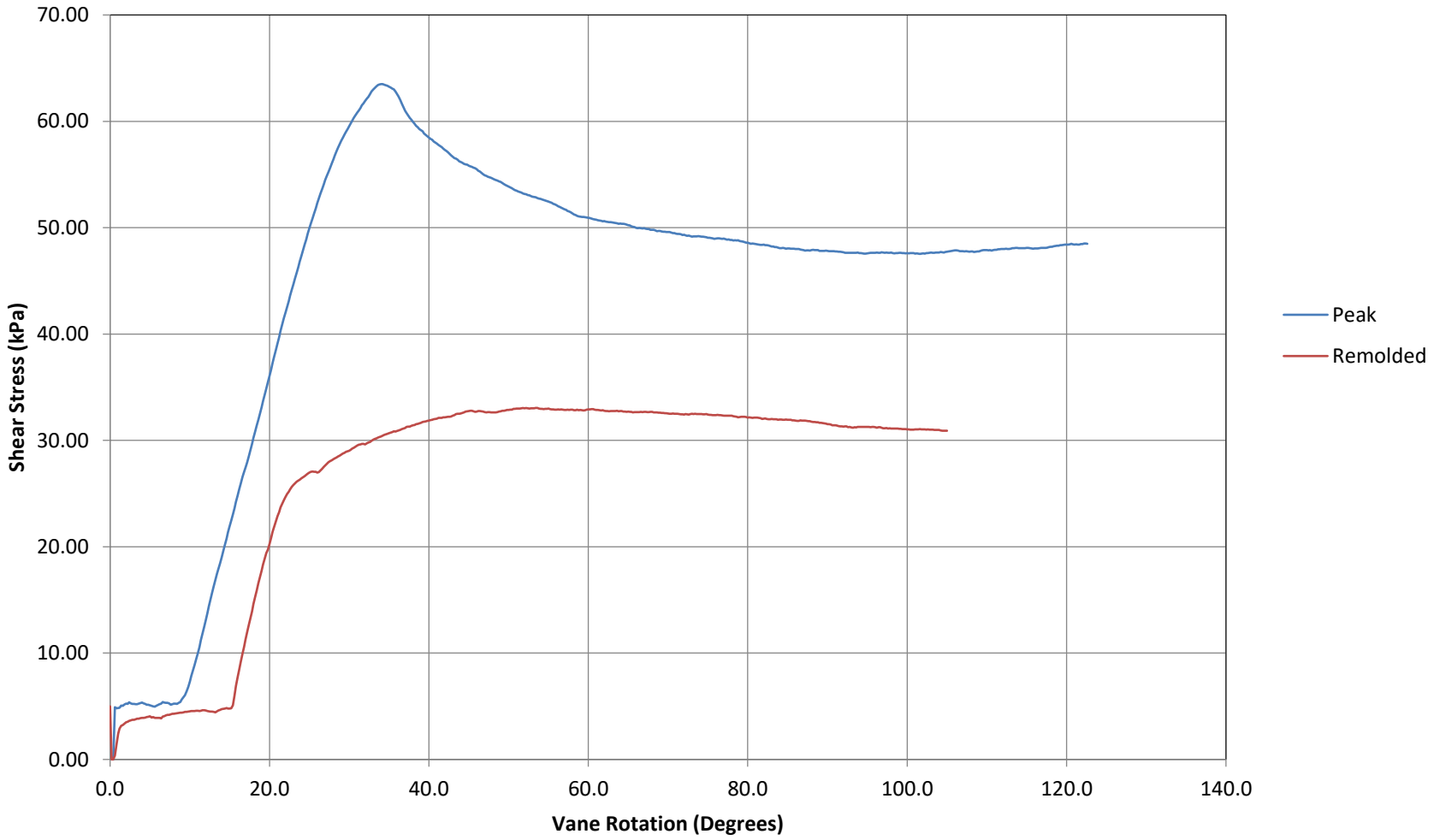


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH202

Test Date: 19-Mar-2024 13:56
Test Depth (m): 19.42
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5404211
Easting (m): 476824

Vane Shear Test

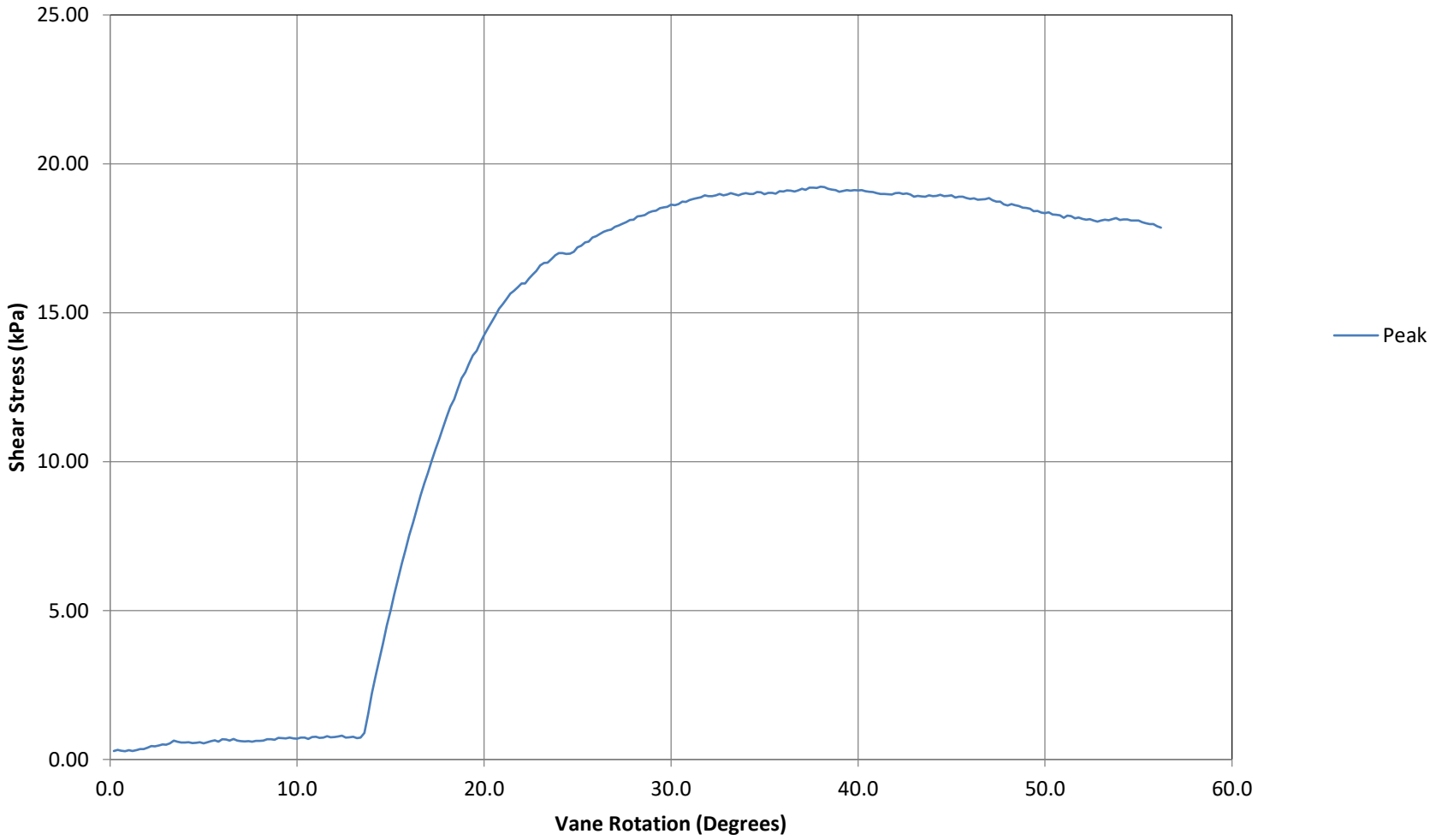


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH207

Test Date: 16-Mar-2024 23:23
Test Depth (m): 4.57
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5402798
Easting (m): 476815

Vane Shear Test

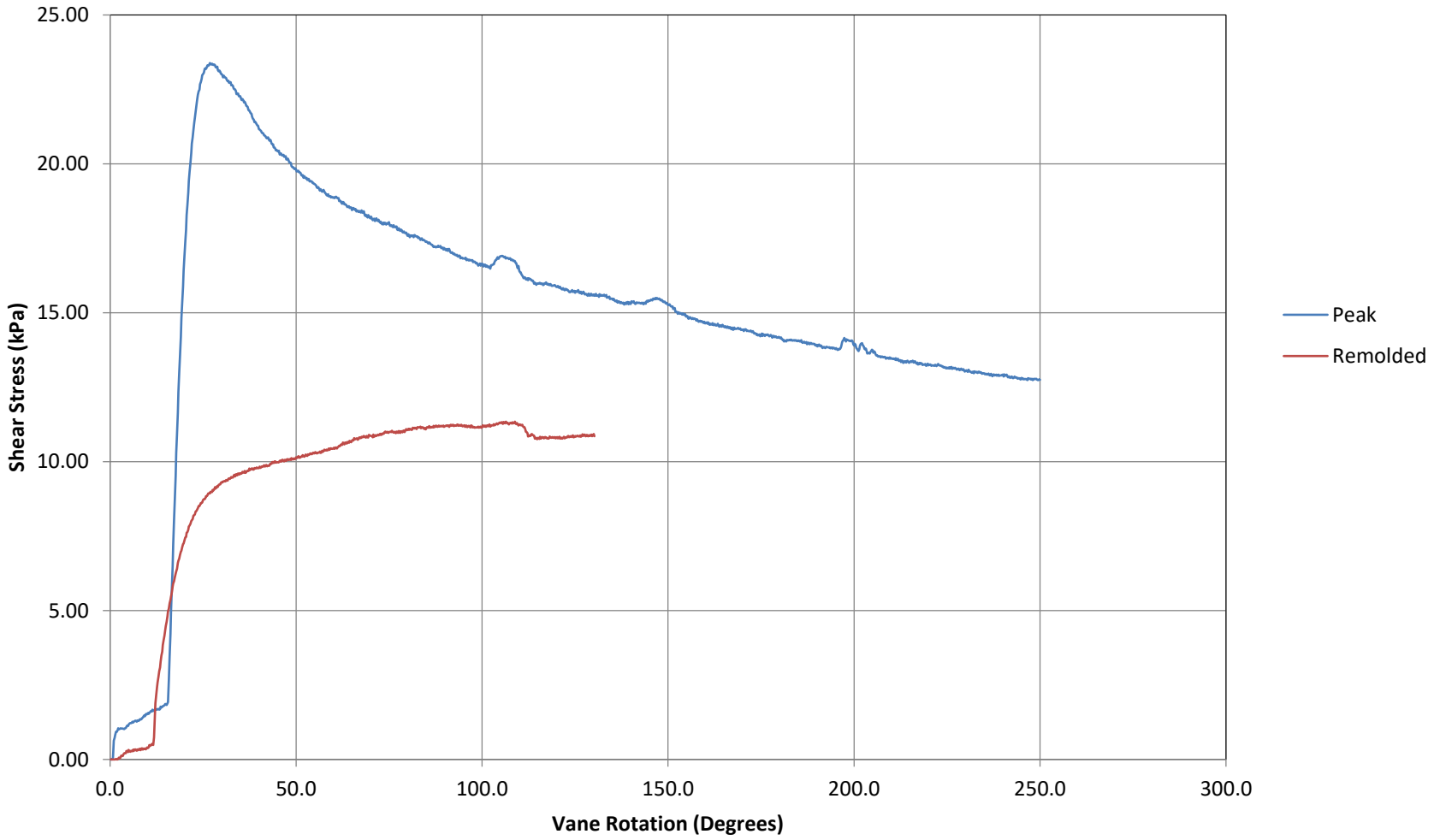


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH207

Test Date: 16-Mar-2024 23:40
Test Depth (m): 4.88
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5402798
Easting (m): 476815

Vane Shear Test

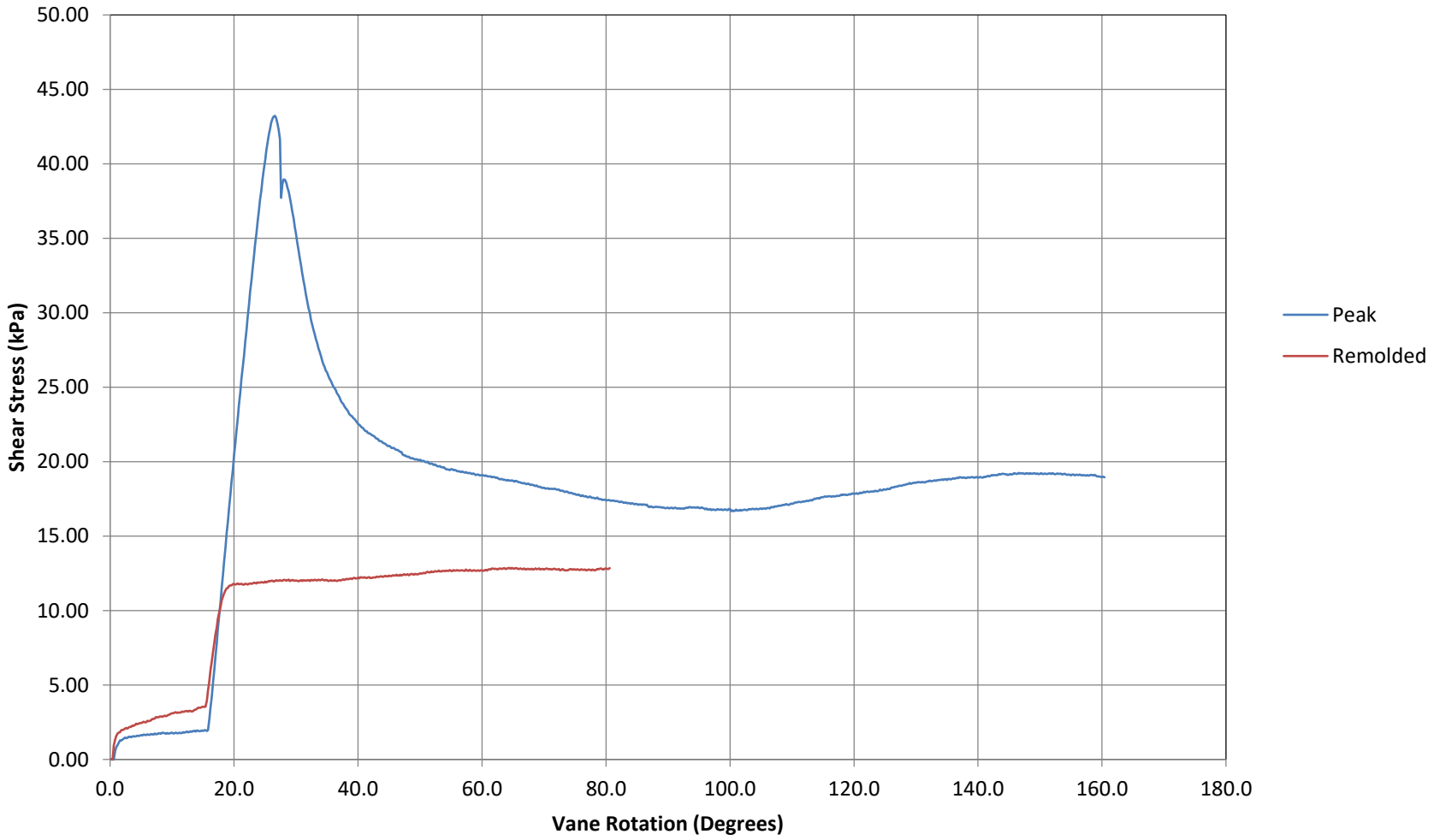


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH207

Test Date: 17-Mar-2024 02:51
Test Depth (m): 12.50
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5402798
Easting (m): 476815

Vane Shear Test

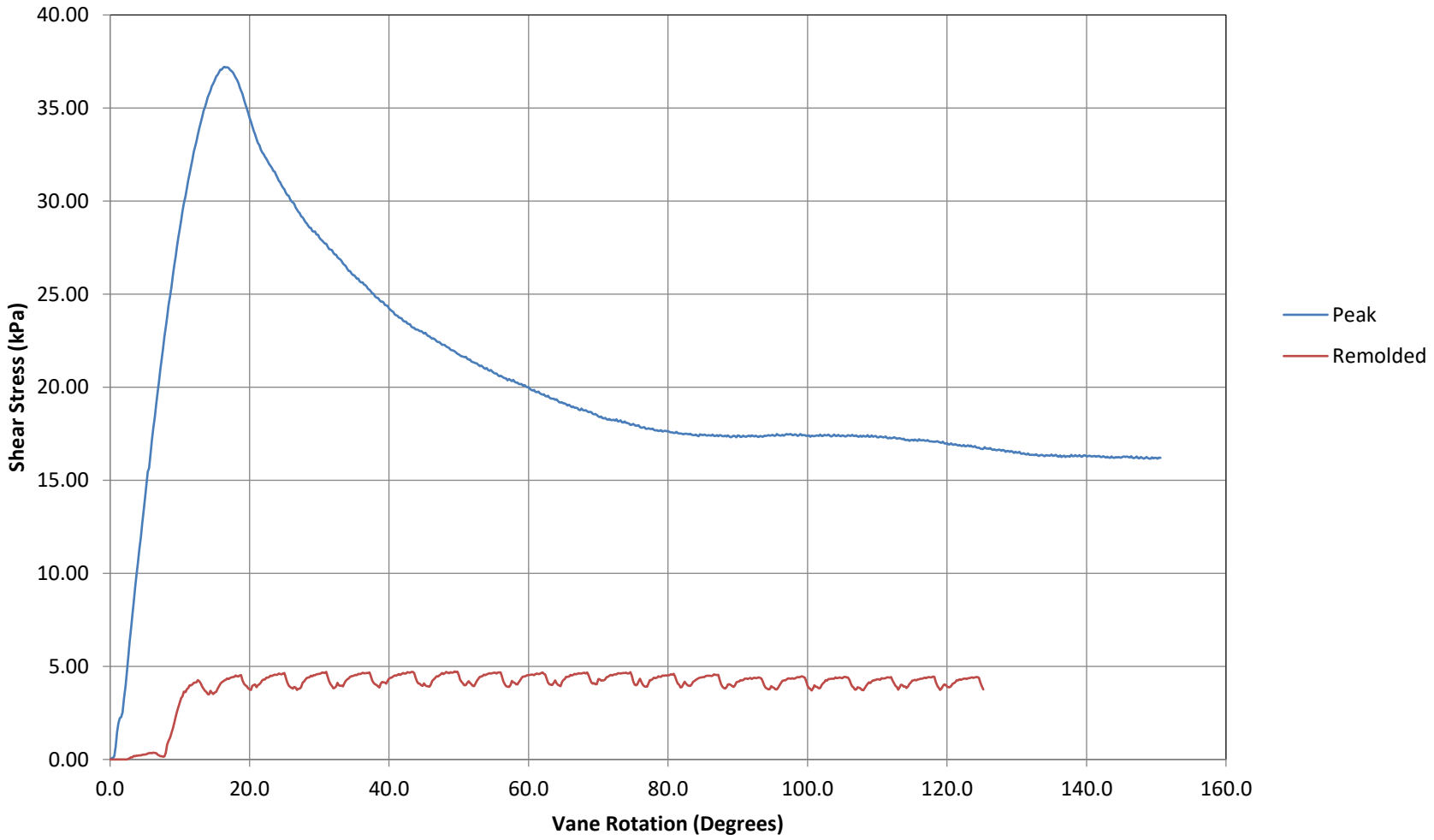


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH207

Test Date: 17-Mar-2024 10:21
Test Depth (m): 18.59
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5402798
Easting (m): 476815

Vane Shear Test

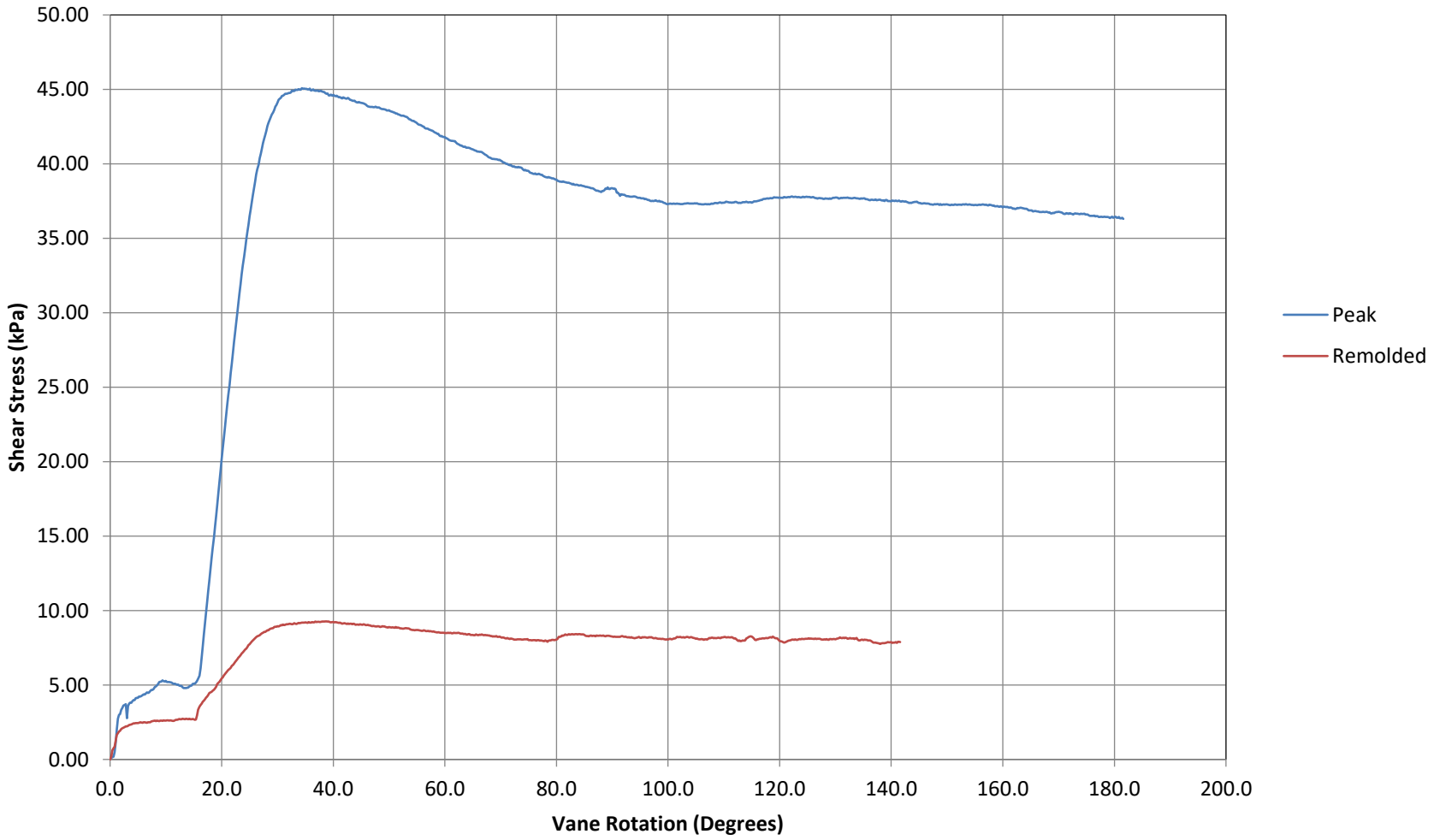


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-TMF-BH207

Test Date: 17-Mar-2024 12:17
Test Depth (m): 21.34
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5402798
Easting (m): 476815

Vane Shear Test

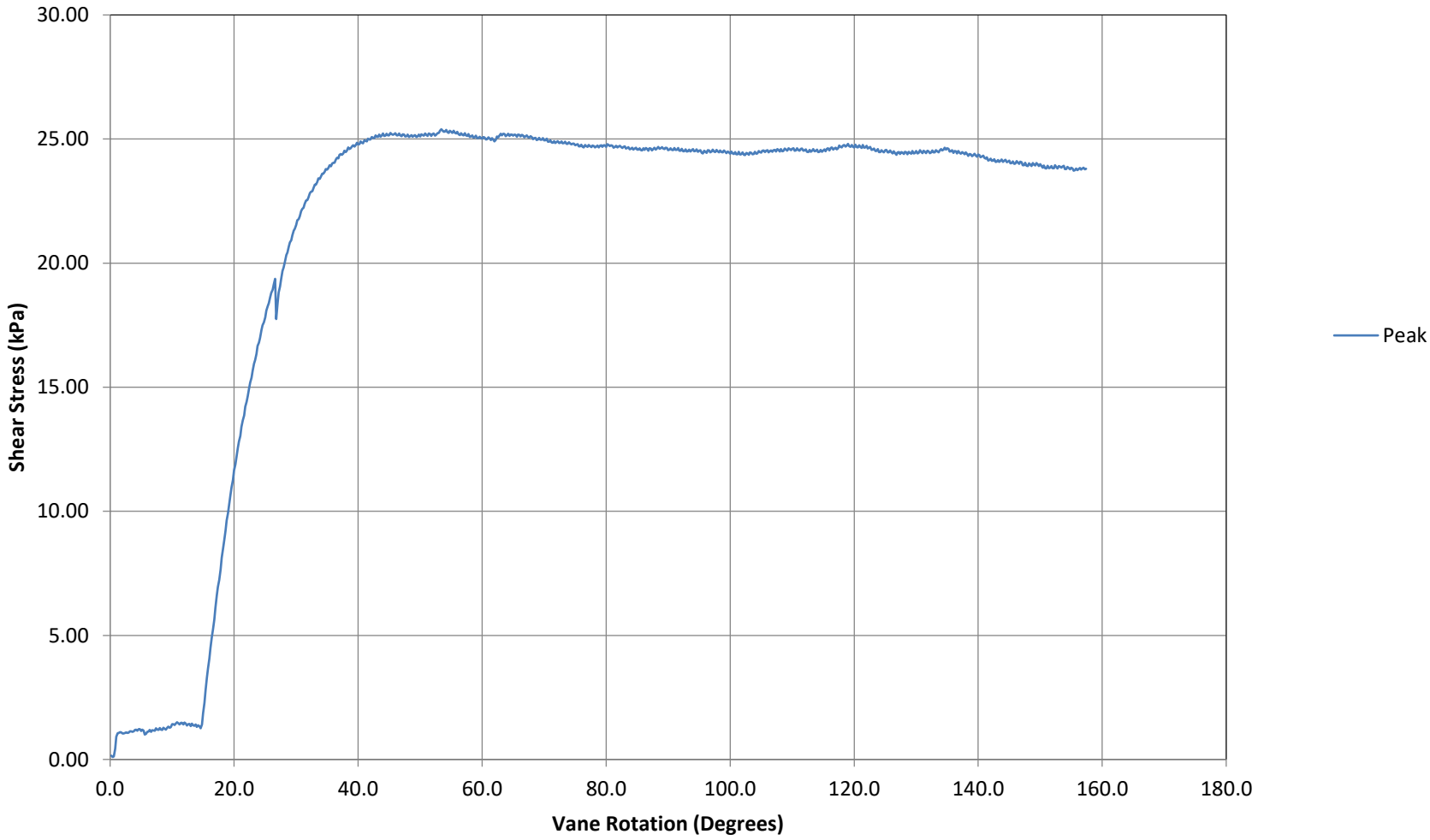


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH201

Test Date: 05-Mar-2024 15:02
Test Depth (m): 6.10
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411098
Easting (m): 473341

Vane Shear Test

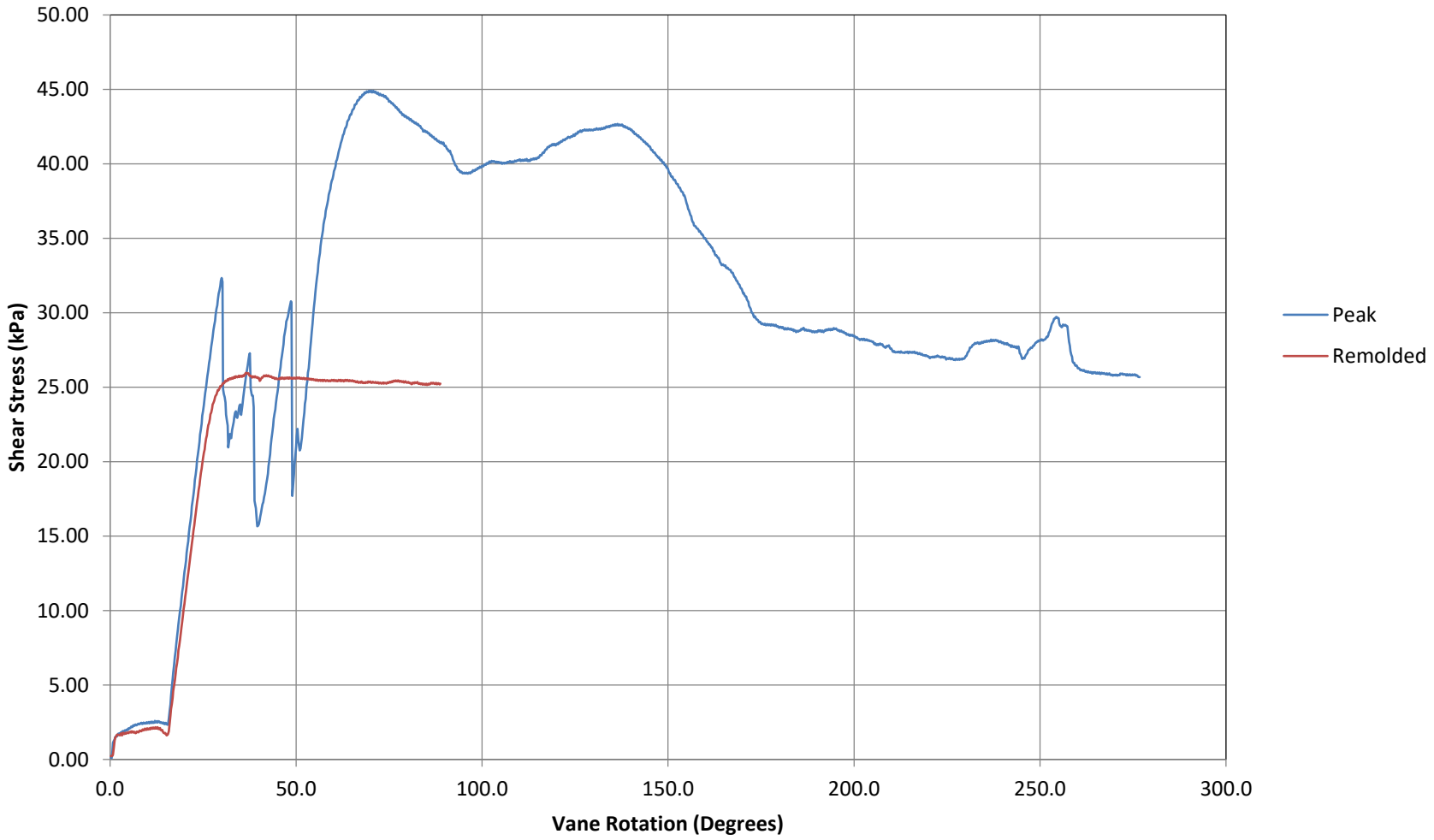


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH201

Test Date: 05-Mar-2024 15:34
Test Depth (m): 6.40
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411098
Easting (m): 473341

Vane Shear Test

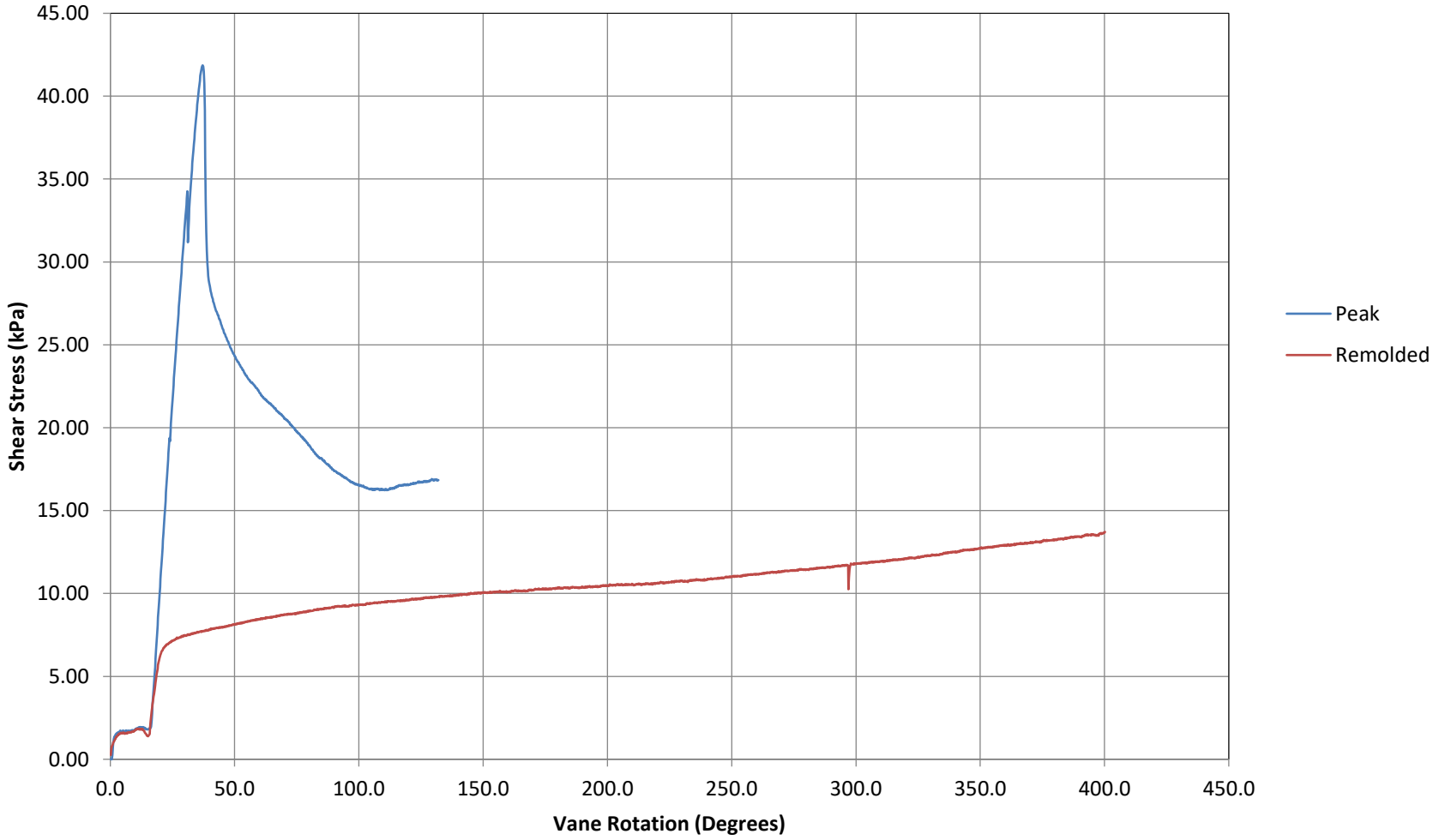


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH201

Test Date: 05-Mar-2024 21:56
Test Depth (m): 11.58
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411098
Easting (m): 473341

Vane Shear Test

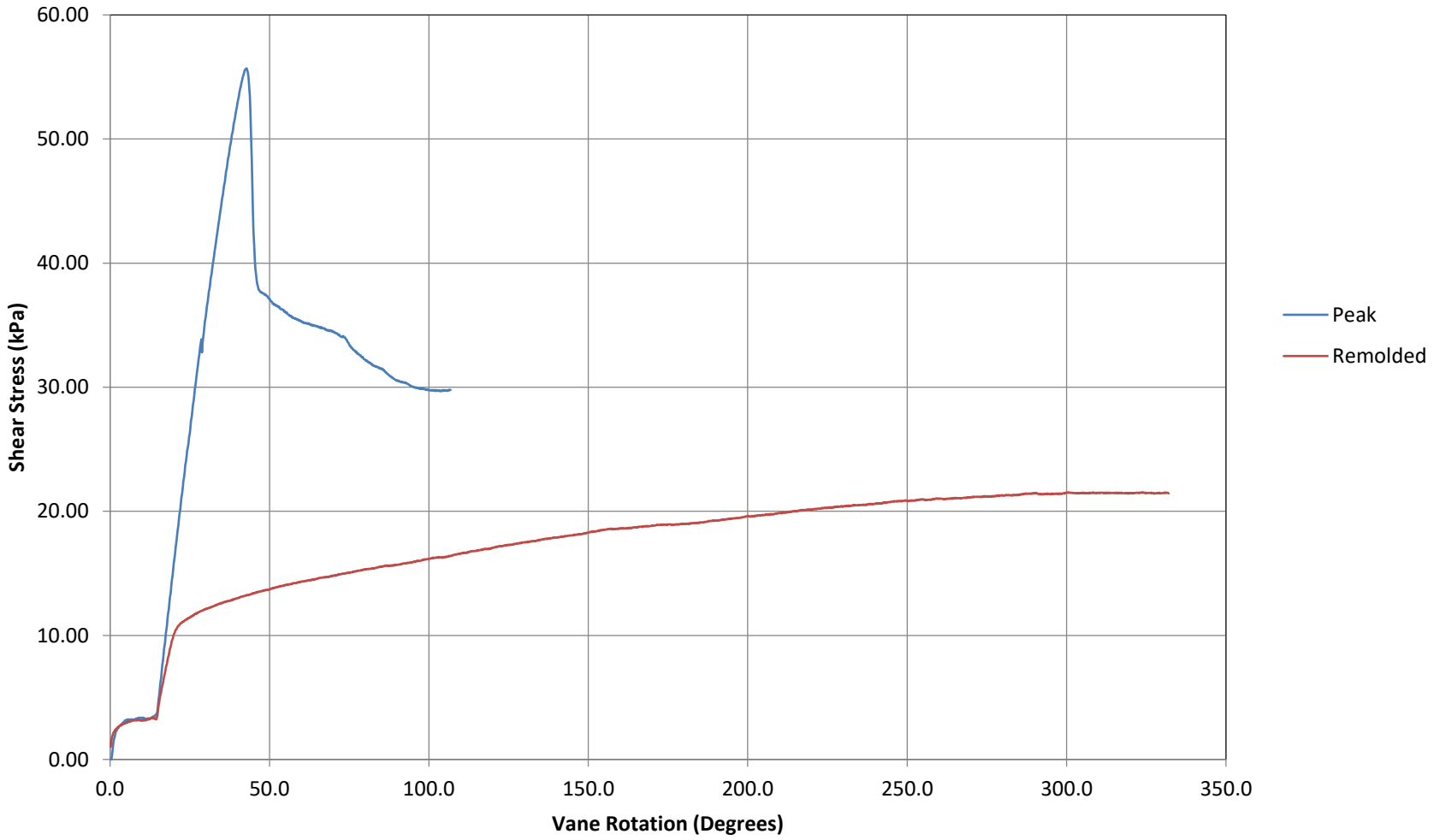


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH201

Test Date: 06-Mar-2024 03:19
Test Depth (m): 17.37
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411098
Easting (m): 473341

Vane Shear Test

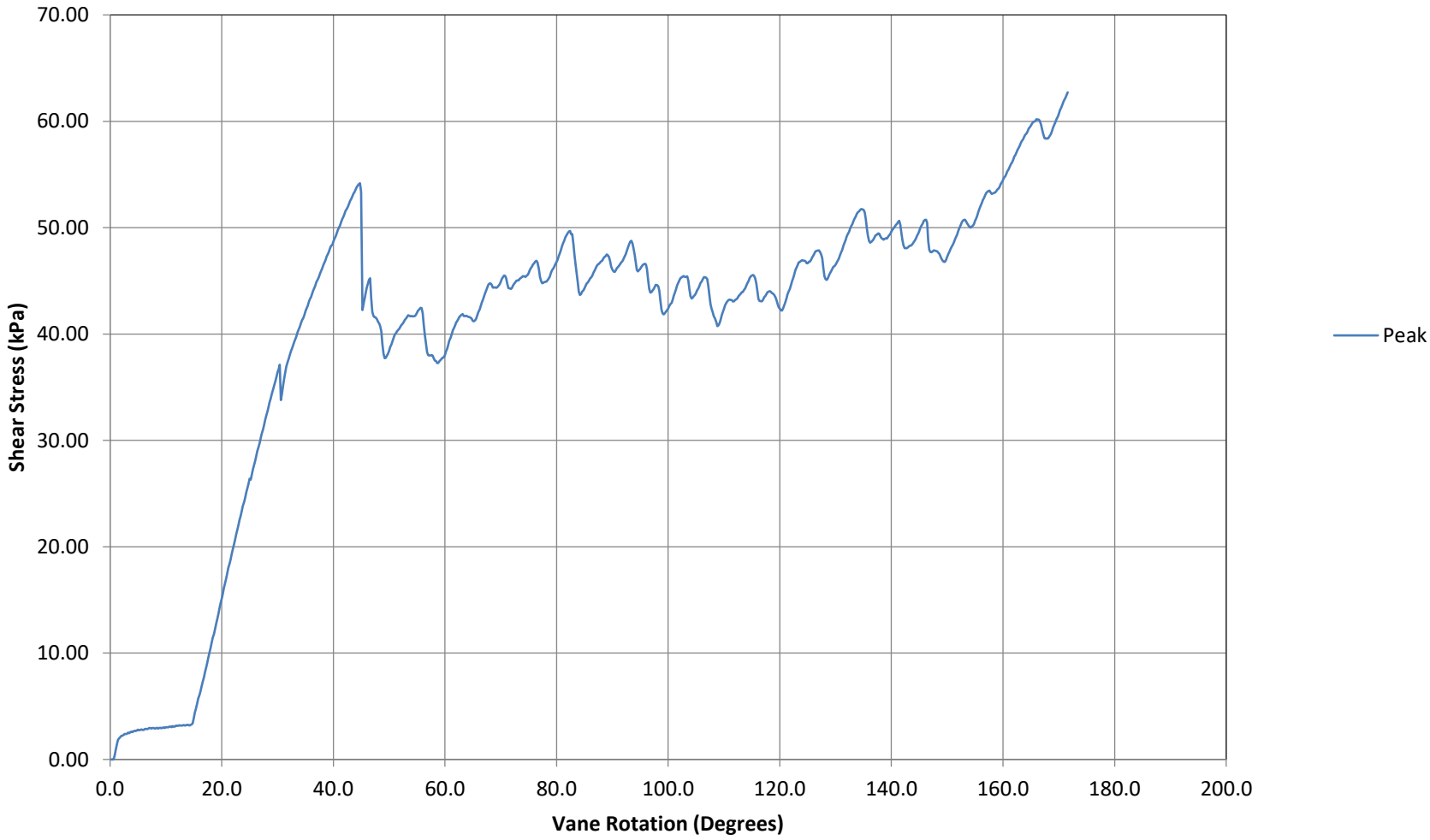


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH201

Test Date: 06-Mar-2024 12:46
Test Depth (m): 21.34
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411098
Easting (m): 473341

Vane Shear Test

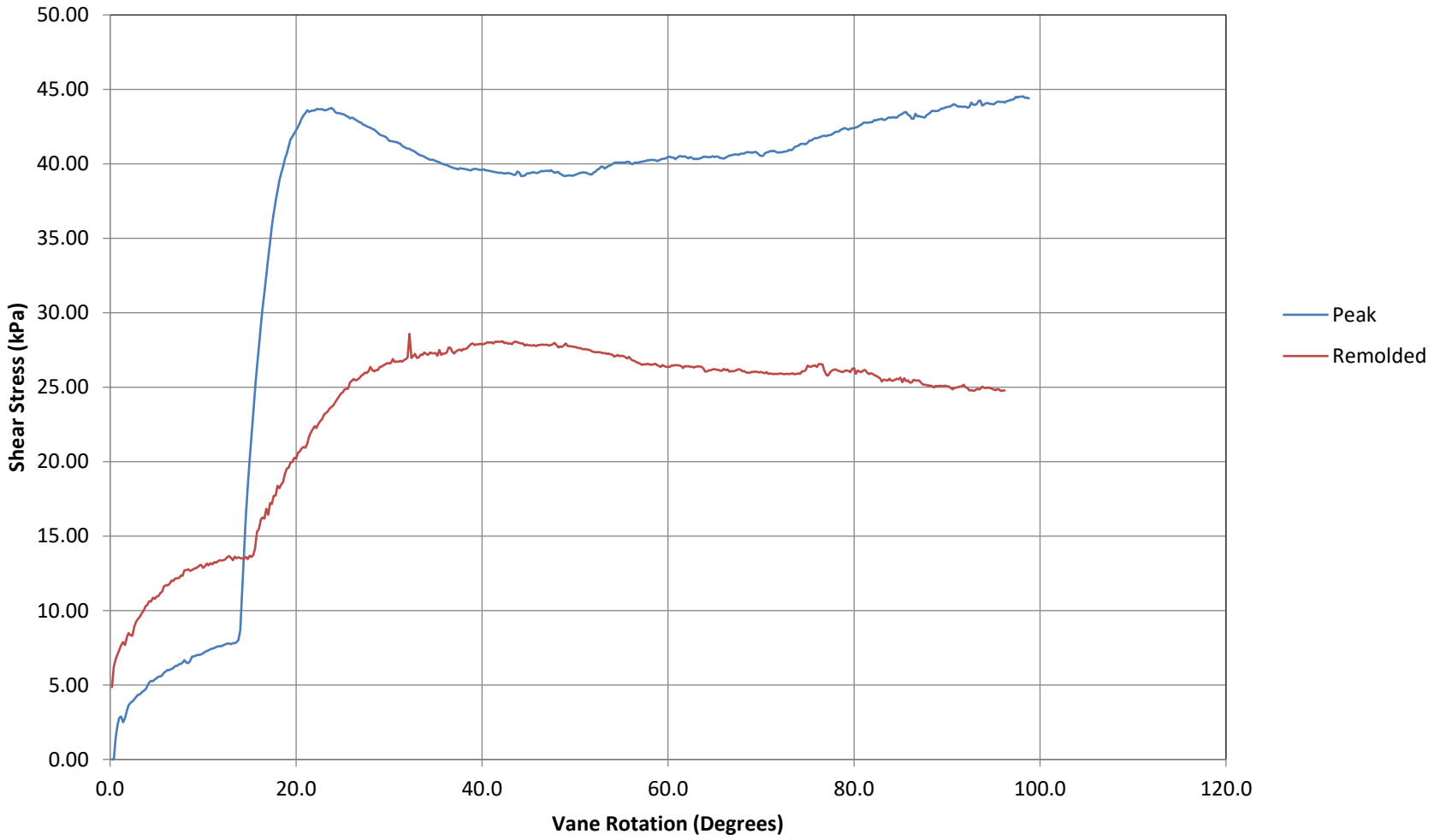


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH202

Test Date: 20-Mar-2024 12:46
Test Depth (m): 5.80
Vane Type: Adara solid double tapered 40 x 80 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5412173
Easting (m): 474133

Vane Shear Test

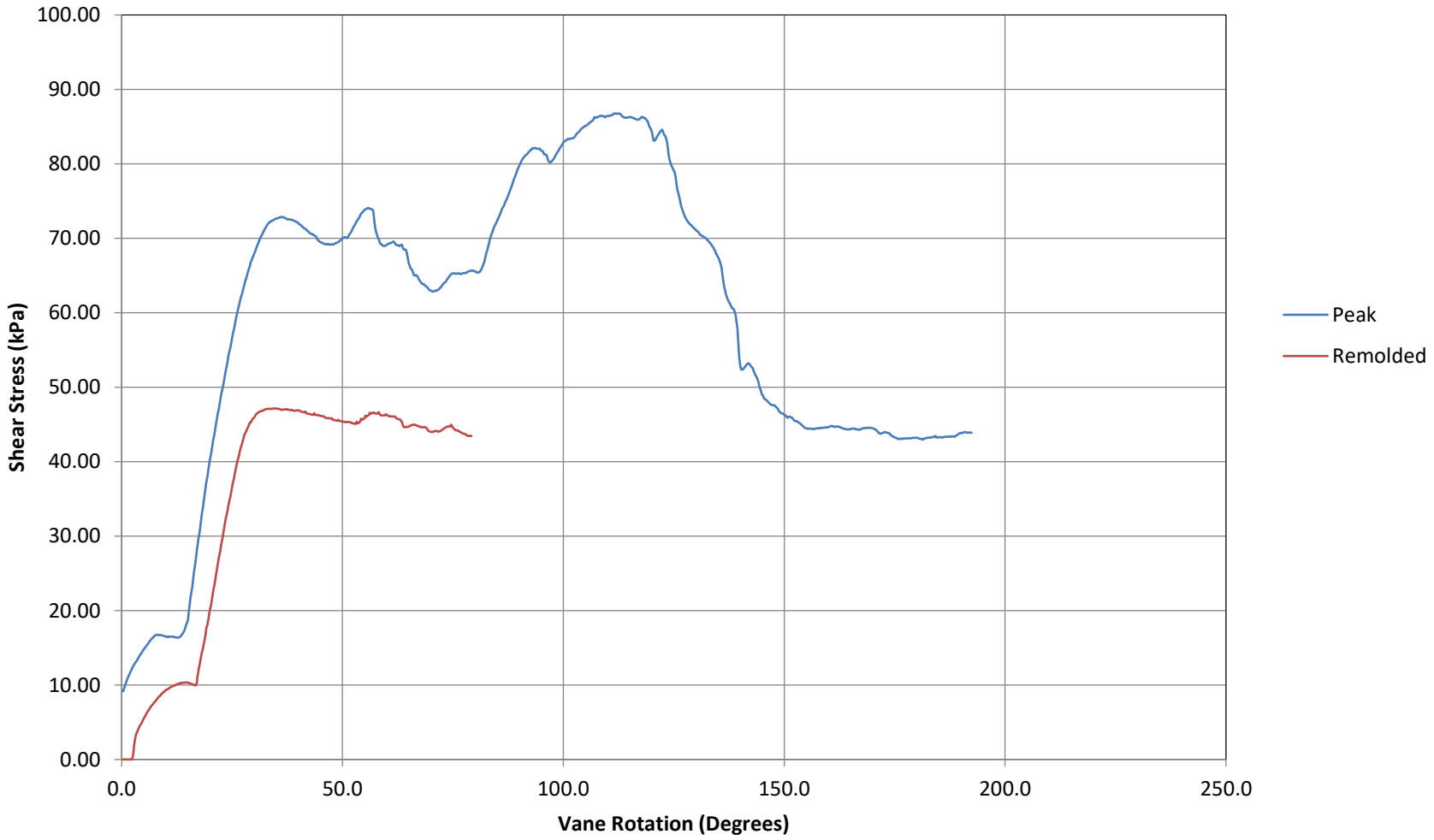


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH202

Test Date: 20-Mar-2024 15:39
Test Depth (m): 9.23
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5412173
Easting (m): 474133

Vane Shear Test

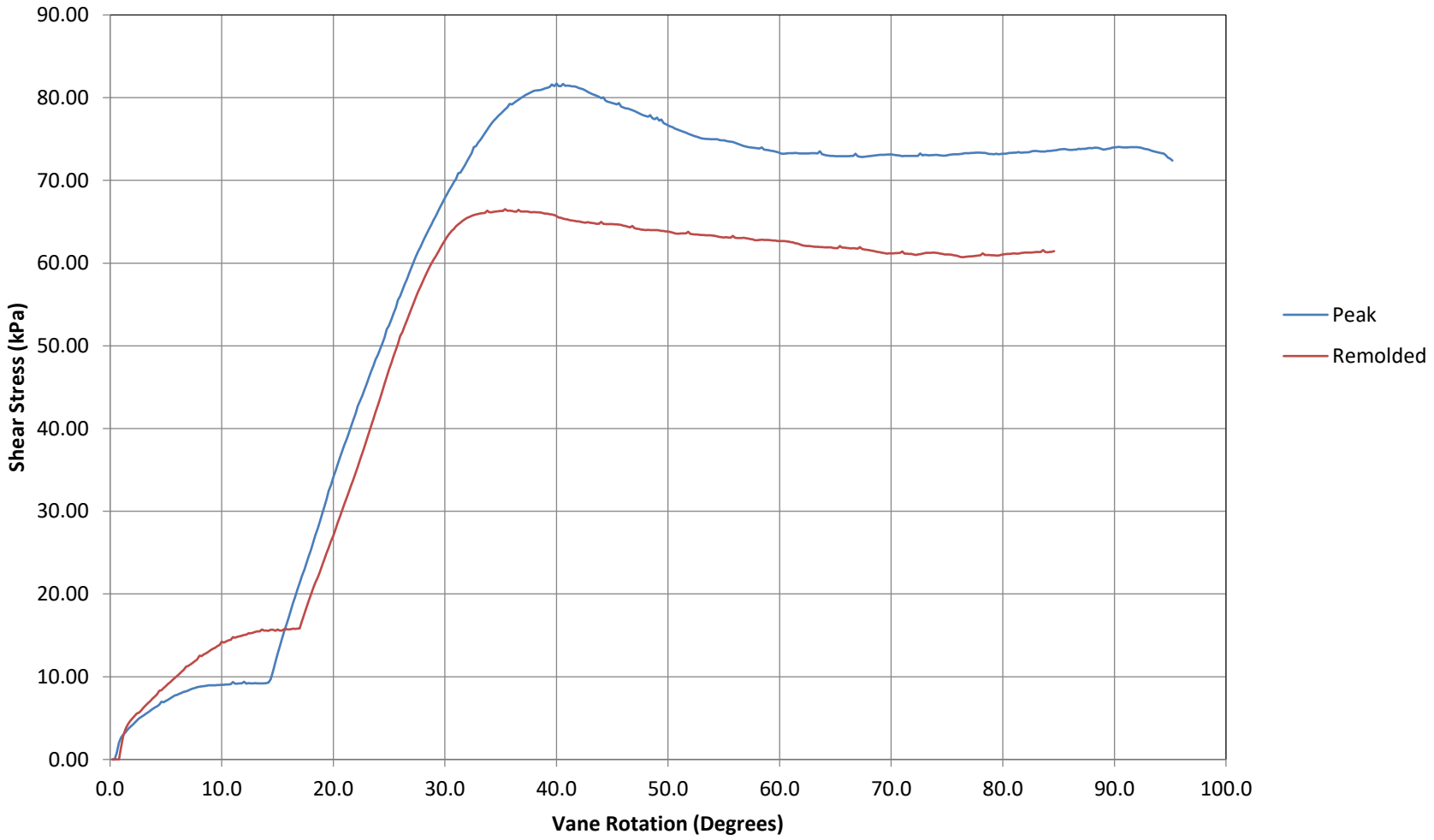


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH202

Test Date: 20-Mar-2024 16:34
Test Depth (m): 9.55
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5412173
Easting (m): 474133

Vane Shear Test

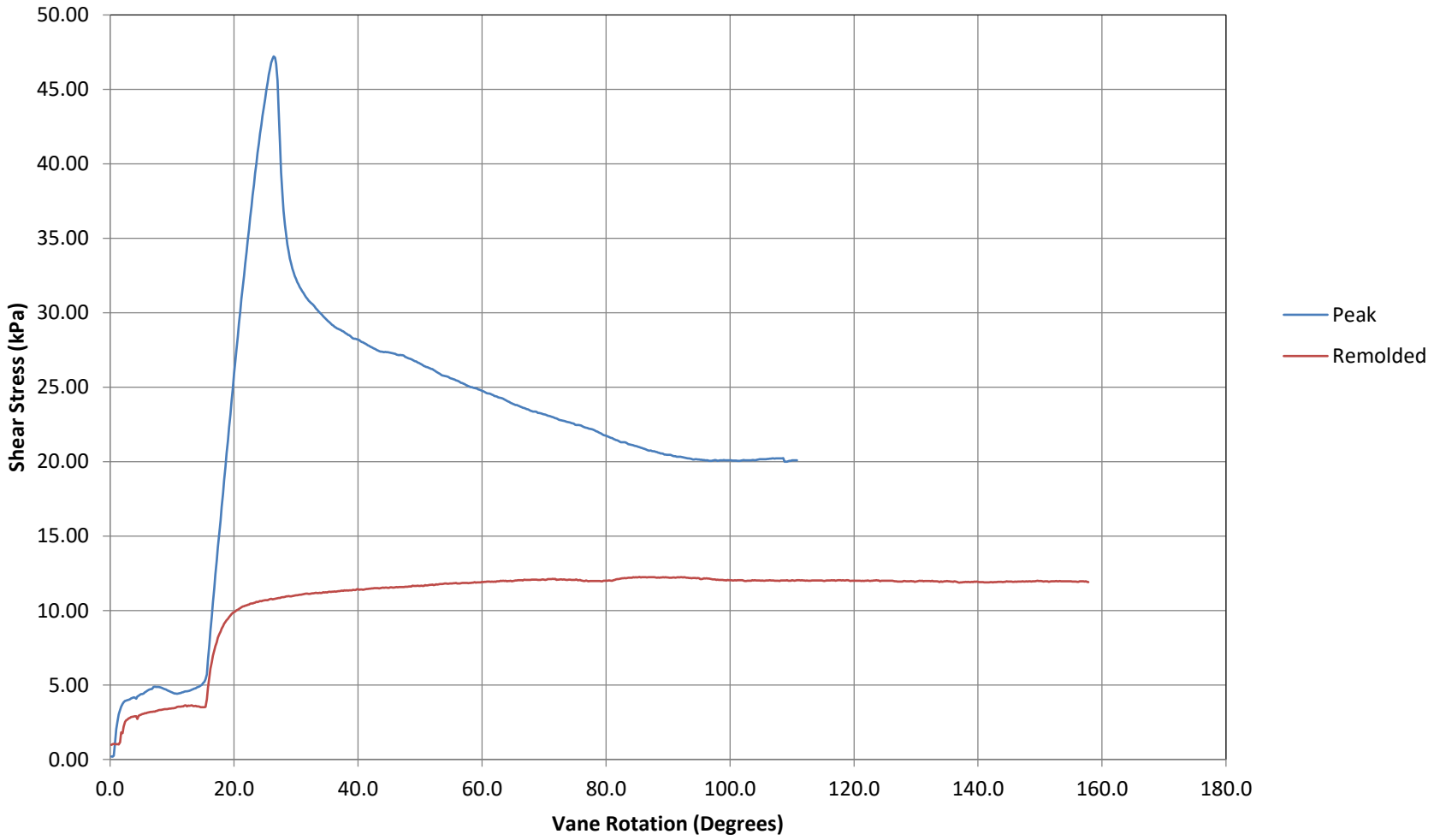


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH202

Test Date: 20-Mar-2024 23:49
Test Depth (m): 11.89
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5412173
Easting (m): 474133

Vane Shear Test

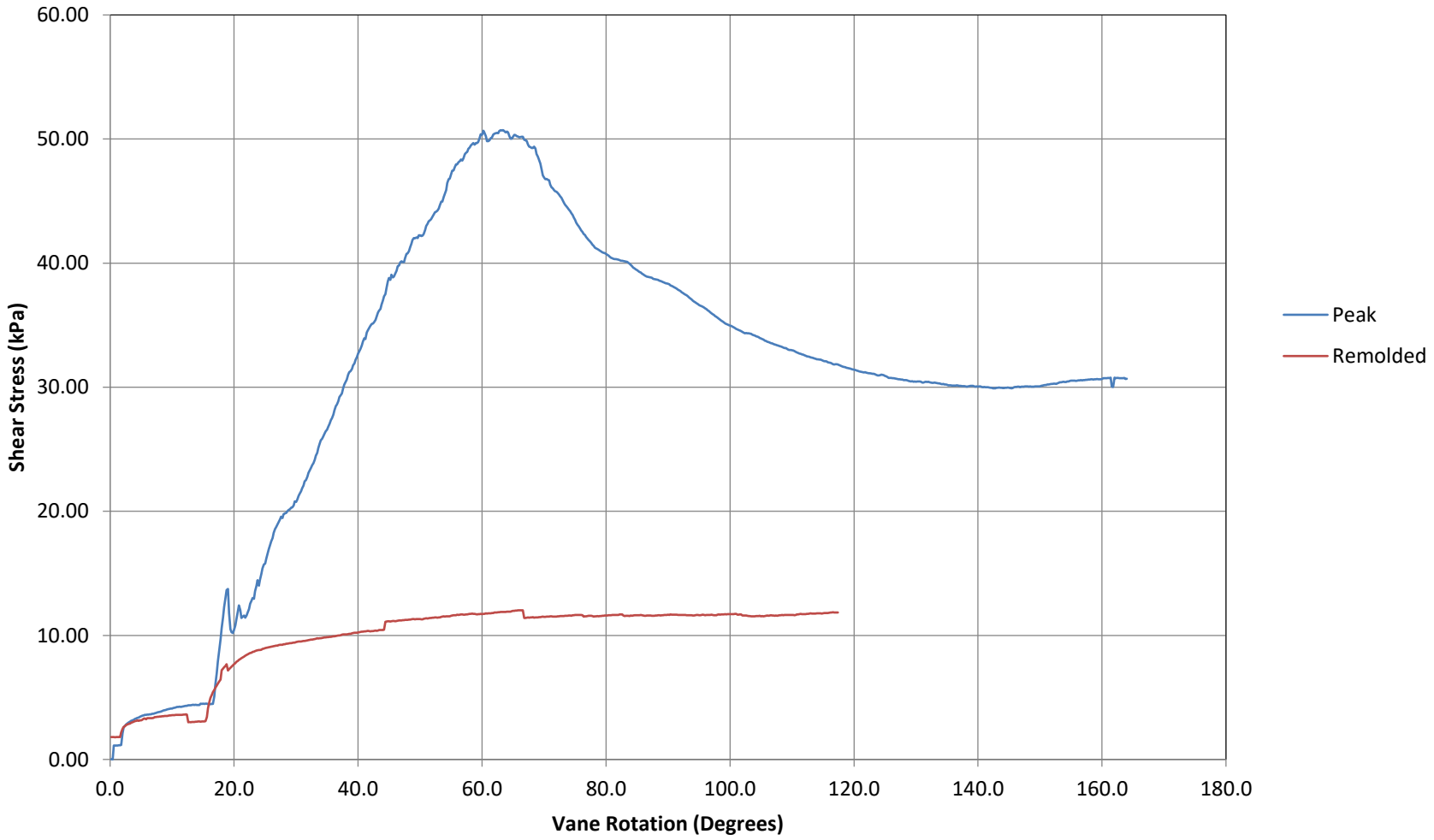


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH202

Test Date: 21-Mar-2024 03:42
Test Depth (m): 16.15
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5412173
Easting (m): 474133

Vane Shear Test

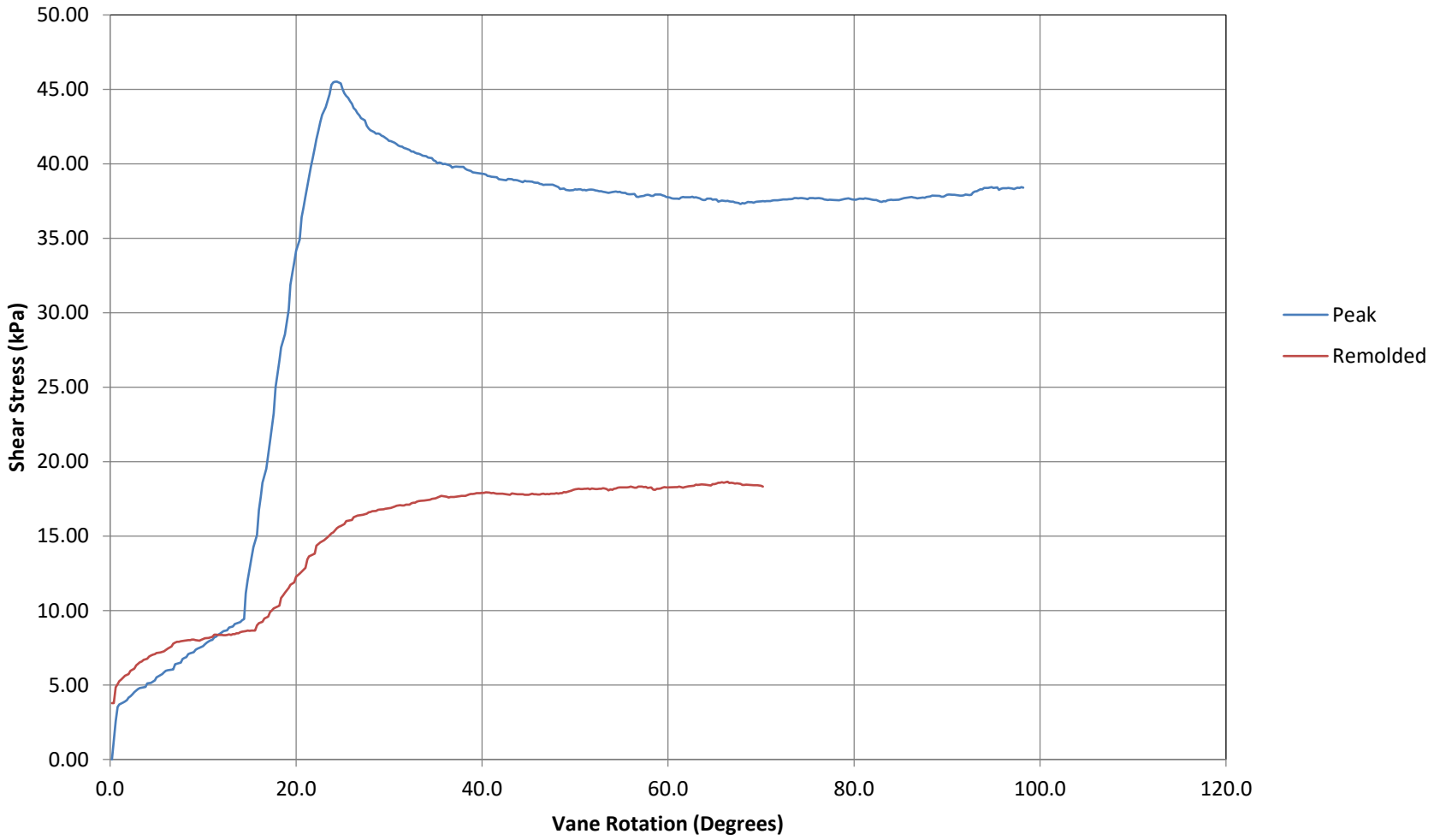


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH205

Test Date: 16-Mar-2024 11:23
Test Depth (m): 5.80
Vane Type: Adara solid double tapered 40 x 80 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5413522
Easting (m): 474142

Vane Shear Test

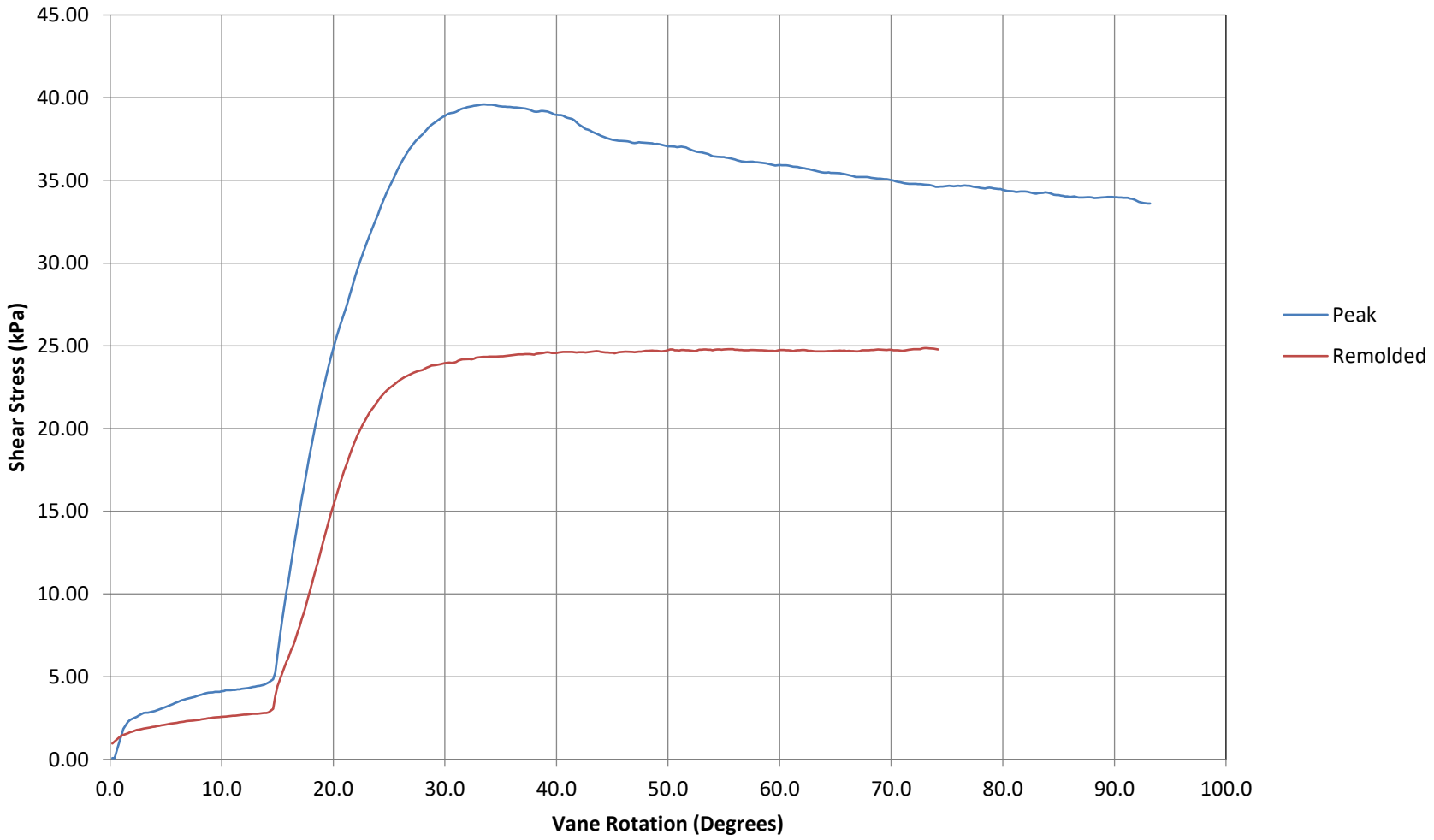


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH205

Test Date: 16-Mar-2024 12:14
Test Depth (m): 6.15
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5413522
Easting (m): 474142

Vane Shear Test

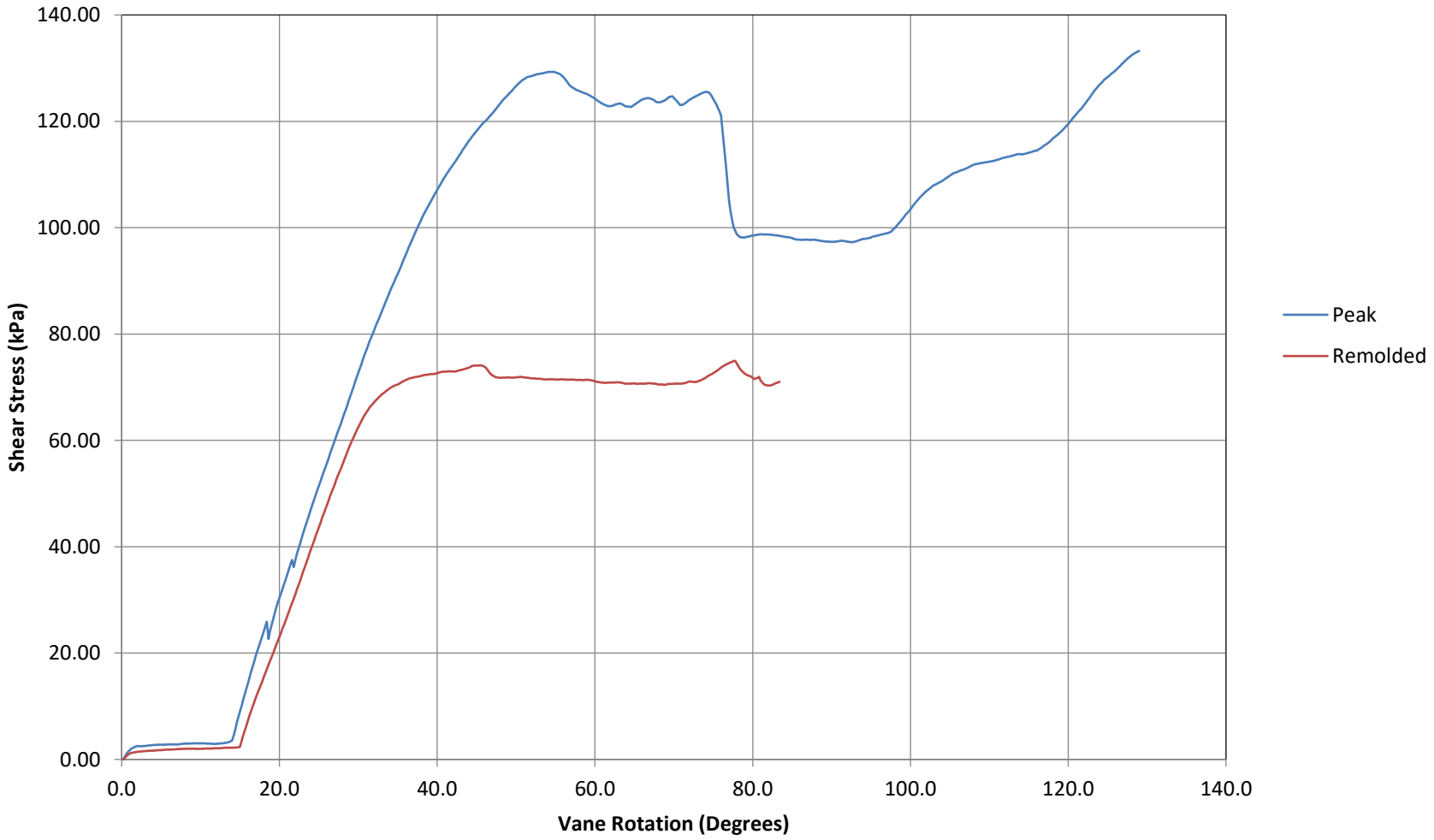


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH205

Test Date: 16-Mar-2024 14:27
Test Depth (m): 7.30
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5413522
Easting (m): 474142

Vane Shear Test

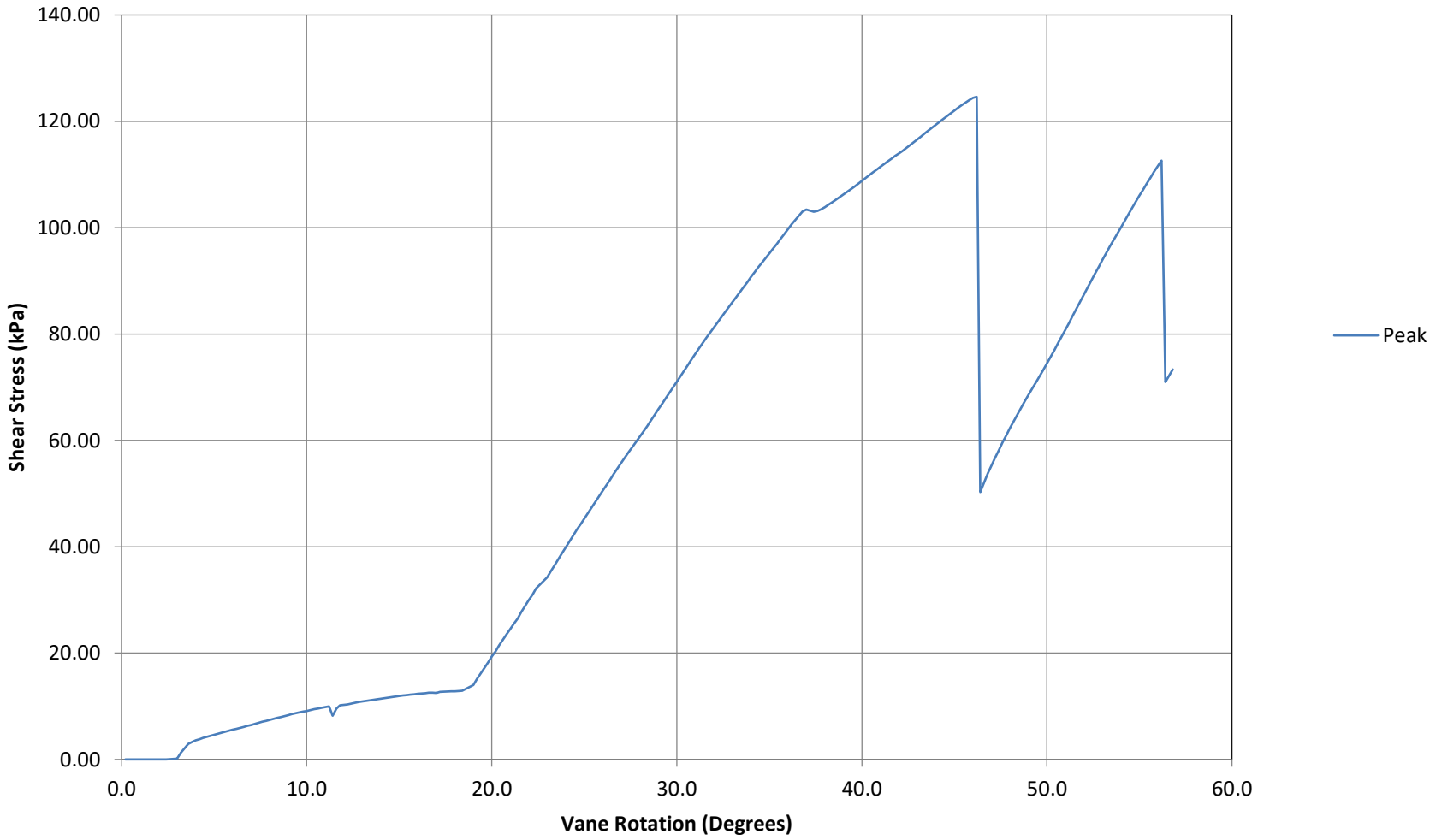


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH207

Test Date: 15-Mar-2024 14:48
Test Depth (m): 5.15
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5414551
Easting (m): 474232

Vane Shear Test

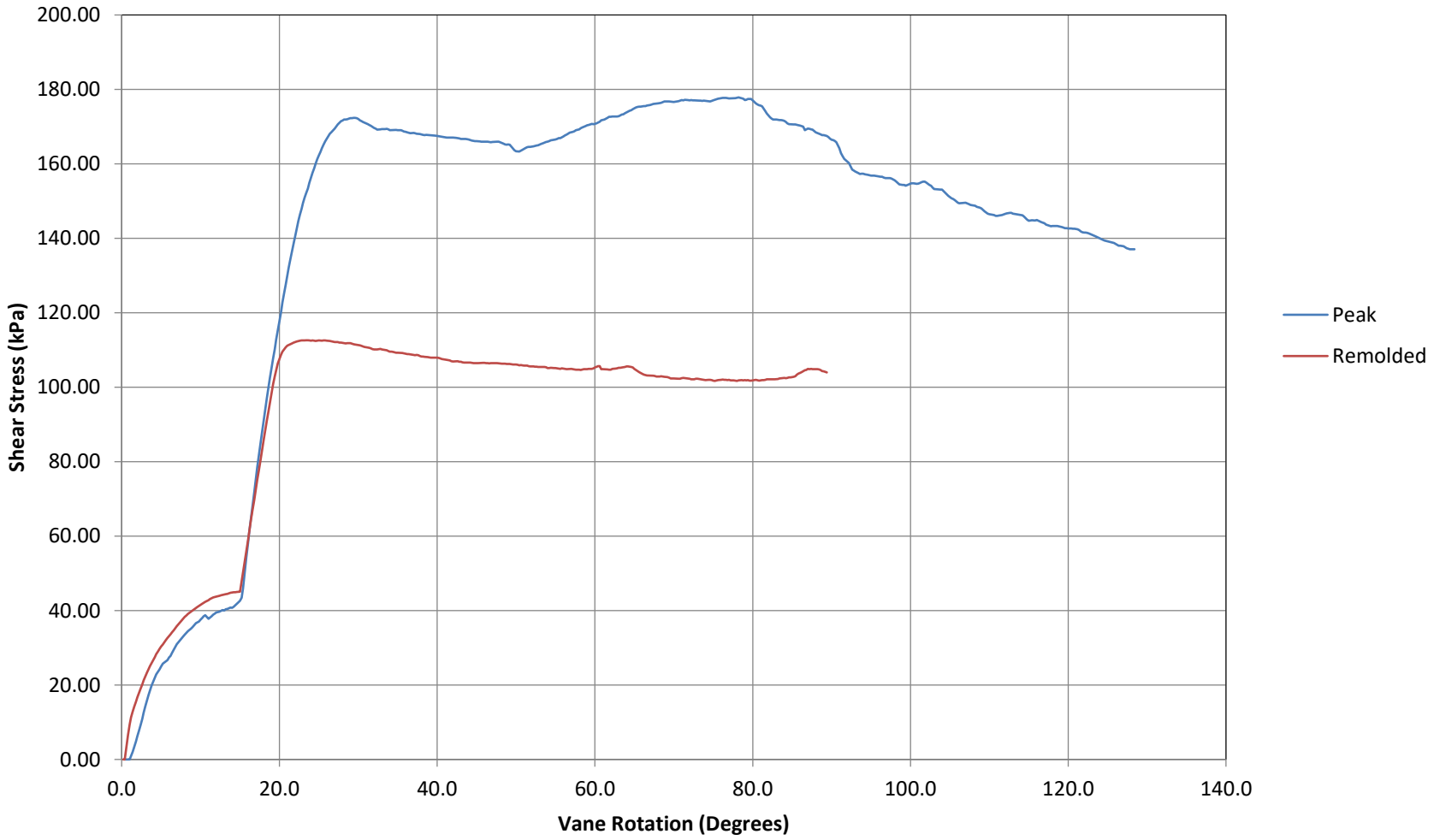


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH207

Test Date: 15-Mar-2024 15:28
Test Depth (m): 5.50
Vane Type: Adara solid double tapered 40 x 80 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5414551
Easting (m): 474232

Vane Shear Test

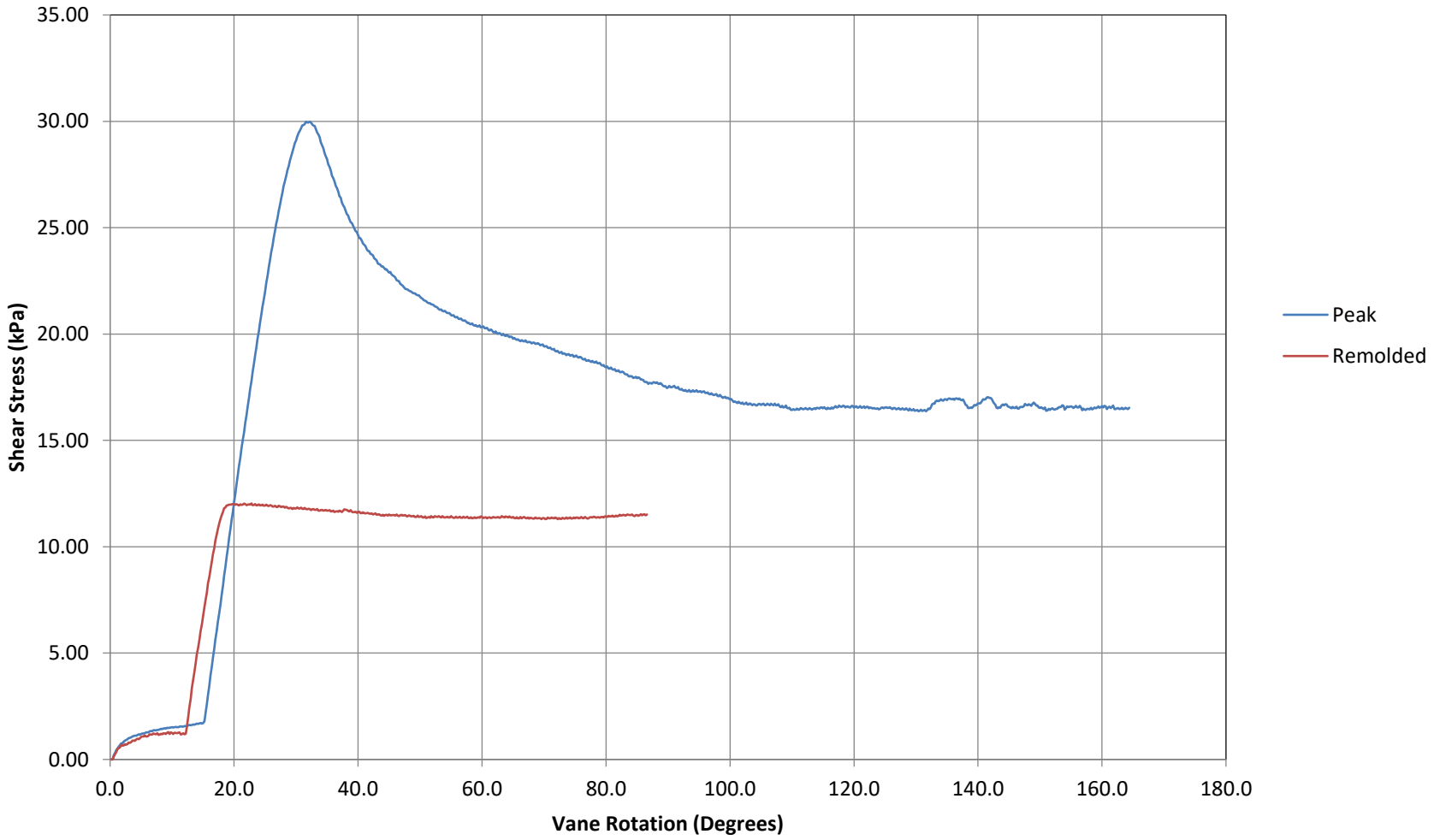


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH212

Test Date: 09-Mar-2024 13:42
Test Depth (m): 3.66
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411065
Easting (m): 474214

Vane Shear Test

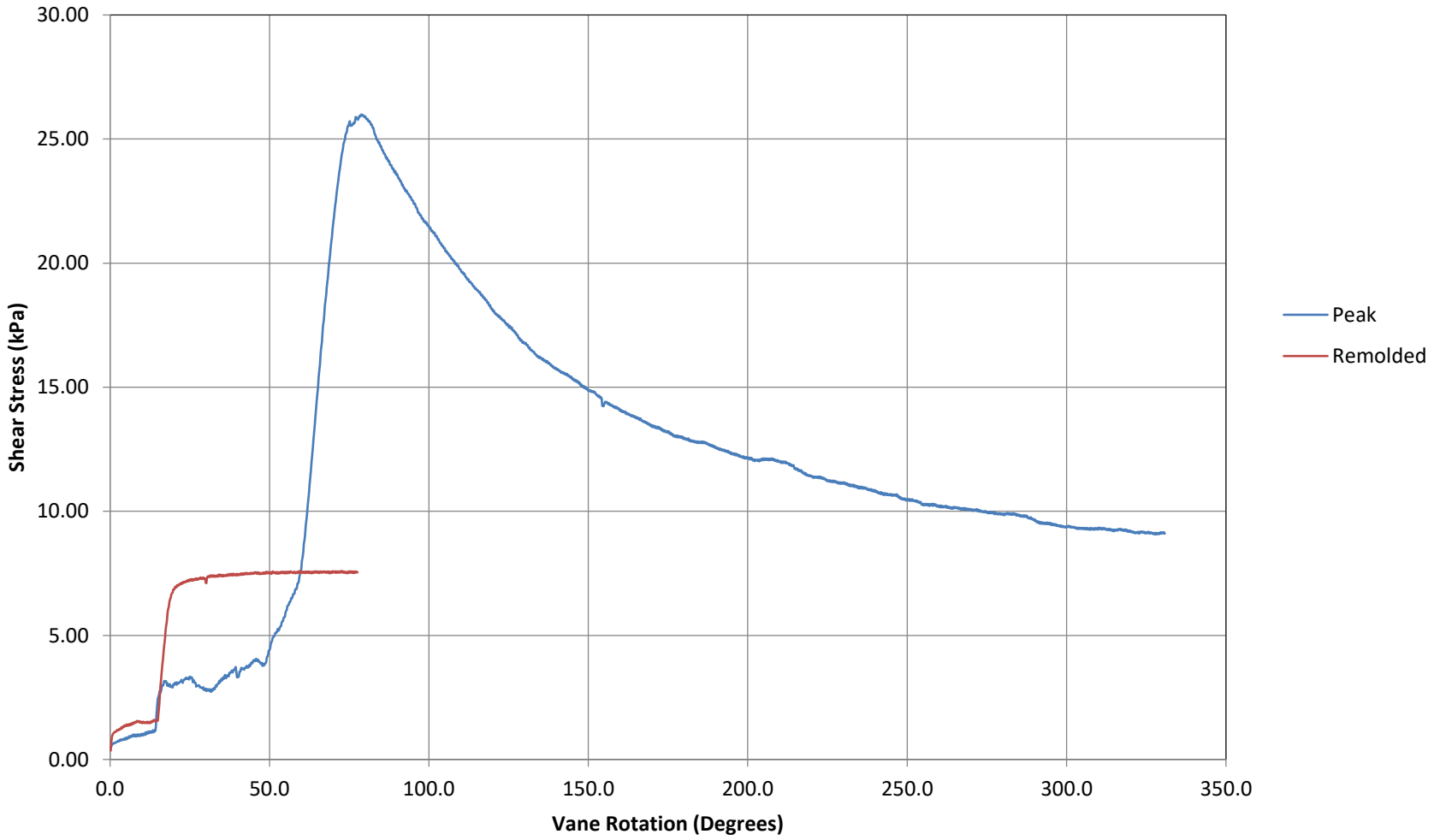


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH212

Test Date: 09-Mar-2024 17:36
Test Depth (m): 8.54
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411065
Easting (m): 474214

Vane Shear Test

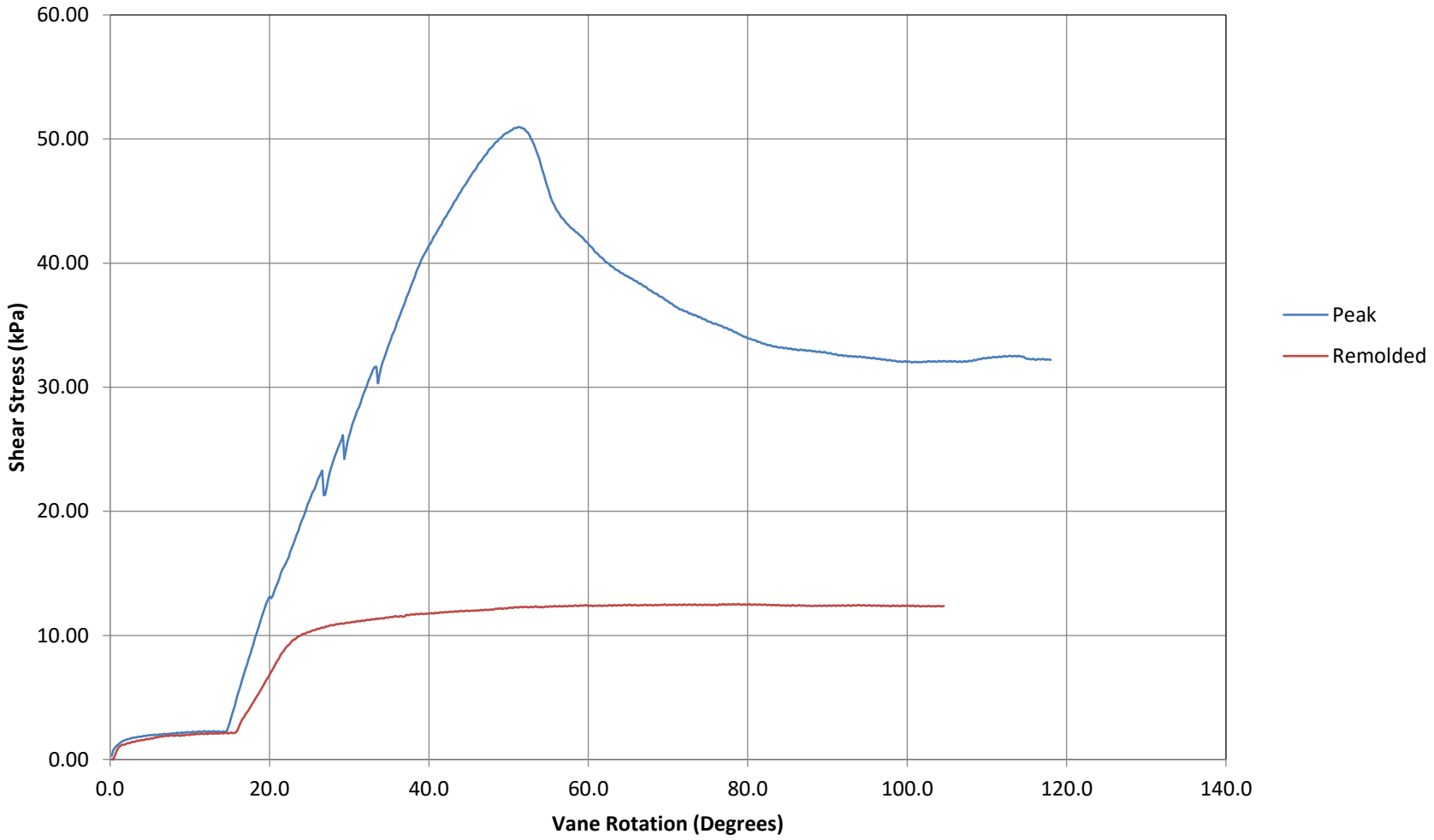


Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH212

Test Date: 10-Mar-2024 01:51
Test Depth (m): 13.41
Vane Type: Adara solid double tapered 75 x 150 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5411065
Easting (m): 474214

Vane Shear Test



Job Number: 24-05-27159
Client: Canada Nickel Company
Project: Crawford SCPTu - SRK
Sounding: VST24-WRD-BH218

Test Date: 14-Mar-2024 12:34
Test Depth (m): 5.15
Vane Type: Adara solid double tapered 60 x 120 mm (45°, 45°)

Coordinate System: WGS 84 / UTM zone 17N
Northing (m): 5414720
Easting (m): 473205

Vane Shear Test

